



Supplementary Information

Quantification Approaches of Fatigue Crack Resistance of Thermoplastic Tape Layered Composites with Multiple Delaminations

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Calculations of the transverse and shear moduli

The transverse and shear moduli were estimated according to Reuss model using Equation S1 and Equation S2.

$$E_2 = \frac{E_{2f}E_m}{E_m f_v + E_{2f}(1 - f_v)}$$
(S1)

$$G_{12} = \frac{G_{12f}G_m}{G_m f_v + G_{12f}(1 - f_v)}$$

$$G_m = \frac{E_m}{2(1 + \vartheta_m)}$$
(S2)

The following values of Young's modulus and Poisson's ratio of PPS, transverse, and shear moduli of the carbon fiber were used: $E_m = 3.45$ GPa [1], $\vartheta_m = 0.38$ [2], $E_{2f} = 13$ GPa [3], $G_{12f} = 11.3$ GPa [3].

Table 1. The transverse and shear moduli calculated for the laminates.

Laminate	E ₂ , GPa	<i>G</i> ₁₂ , GPa
c-5-330	6.01	2.58
c-10-350	5.69	2.39
f-5-330	5.56	2.31
f-10-350	6.20	2.70

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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (http://creativecommons.org/licenses/by/4.0/). The fiber volume fraction f_v was found according to Equation S3 [4].

$$f_{v} = \frac{\frac{w_{f}}{\rho_{f}}}{\frac{w_{f}}{\rho_{f}} + \frac{1 - w_{f}}{\rho_{m}}}$$
(S3)

where ρ_f , ρ_m are the densities of the fiber and matrix, respectively, and w_f is the fiber weight fraction determined using thermogravimetric analysis (TGA).

TGA was performed using the thermogravimetric analyzer TGA/DSC1 Star System (Mettler Toledo, USA). The CF-PPS samples were cut out of the laminates at three equally spaced positions (start, middle, and end of lamination) and had a mass of about 20 mg. Firstly, the specimens were heated from 30 °C to 600 °C at 5 K/min under nitrogen atmosphere in order to perform pyrolysis of the PPS matrix. After that, the samples were cooled down to 200 °C at –20 K/min under the nitrogen atmosphere, and then heated up to 800 °C at 5 K/min under oxygen atmosphere to fully combust the carbon fibers.

The results of w_f values are summarized in Table S2. The corresponding fiber volume fractions f_v were calculated using Equation 11 with fiber density ρ_f of 1.8 g/cm³ and PPS density ρ_m of 1.35 g/cm³ [5].

Table 2. Fiber weight and volume fractions of the laminates obtained using thermogravimetric analysis (TGA).

Laminate	<i>m,</i> mg	<i>w_f</i> , %	f _v , %
c-5-330	20.8±0.1	64.7±2.0	57.9±0.2
c-10-350	20.0±0.6	60.6±1.7	53.6±1.7
f-5-330	20.3±0.6	58.7±0.9	51.6±1.0
f-10-350	20.0±0.4	67.1±0.8	60.4±0.9

Table 3. Δ calculated at the first and last 2.5 mm of the crack length (Δ_{start} and Δ_{end}) and at the entire range of the crack length a_{calc} ($\Delta_{all points}$) for clamping- and flipping-specimens tested under fatigue mode I DCB loading.

Clamping							
5-330				10-350			
Δ_{start}	Δ_{end} ,	$\Delta_{all \ points}$,	Specime	Δ_{start} ,	Δ_{end} ,	$\Delta_{all \ points}$	
mm	mm	mm	n	mm	mm	mm	
2.95 **	3.47 **	3.19 **	01	-9.95	-11.17	-10.66	
-26.48	-30.24	-28.41	02*	-14.16	-16.39	-15.26	
-18.47	-22.22	-20.32	03	0.34 **	0.87 **	0.57 **	
		Flipp	oing				
5-330			10-350				
Δ_{start} ,	Δ_{end} ,	$\Delta_{all \ points}$,	Specime	Δ_{start} ,	Δ_{end} ,	$\Delta_{all \ points}$	
mm	mm	mm	n	mm	mm	mm	
-7.26	-8.00	-7.62	01 *	-6.02	-7.05	-6.55	
-11.47	-13.74	-12.56	02	6.27 **	7.27 **	6.72 **	
-14.01	-16.67	-15.28	03	5.37 **	6.25 **	5.82 **	
	5- Δ _{start} , mm 2.95 ** -26.48 -18.47 5- Δ _{start} , mm -7.26 -11.47 -14.01	5-330 Δ_{start} Δ_{end} mm mm 2.95 ** 3.47 ** -26.48 -30.24 -18.47 -22.22 5-330 Δ_{start} Δ_{end} mm mm -7.26 -8.00 -11.47 -13.74 -14.01 -16.67	Clamy Clamy $5-330$ $\Delta_{all points'}$ $\Delta_{start'}$ $\Delta_{end'}$ $\Delta_{all points'}$ mm mm mm 2.95 ** 3.47 ** 3.19 ** -26.48 -30.24 -28.41 -18.47 -22.22 -20.32 Flipp 5-330 T $\Delta_{start'}$ $\Delta_{end'}$ $\Delta_{all points'}$ mm mm mm -7.26 -8.00 -7.62 -11.47 -13.74 -12.56 -14.01 -16.67 -15.28	Clamping Clamping 5-30 Call points, Specime Δ_{start} , Δ_{end} , $\Delta_{all points}$, Specime mm mm n n 2.95 ** 3.47 ** 3.19 ** 01 -26.48 -30.24 -28.41 02* -18.47 -22.22 -20.32 03 Flipping 5-330 Δ_{start} , Δ_{end} , $\Delta_{all points}$, Specime mm mm n n -7.26 -8.00 -7.62 01* -71.47 -13.74 -12.56 02 -14.01 -16.67 -15.28 03	Clamping Clamping 5-30 $\Delta_{all points}$ Specime Δ_{start} Δ_{start} Δ_{end} $\Delta_{all points}$ Specime Δ_{start} mm mm mm n mm 2.95 ** 3.47 ** 3.19 ** 01 -9.95 -26.48 -30.24 -28.41 02* -14.16 -18.47 -22.22 -20.32 03 0.34 ** Flipping m Mail points, Specime Δ_{start} Δ_{start} Δ_{end} $\Delta_{all points}$ Specime Δ_{start} Δ_{start} Δ_{end} $\Delta_{all points}$ Specime Δ_{start} -7.26 -8.00 -7.62 01^* -6.02 -11.47 -13.74 -12.56 02 6.27^{**} -14.01 -16.67 -15.28 03 5.37^{**}	Clamping IOI IO-350 Δ_{start} Δ_{end} $\Delta_{all points}$ Specime Δ_{start} Δ_{end} Δ_{start} Δ_{end} mm n Δ_{end} 2.95 ** 3.47 ** 3.19 ** 01 -9.95 -11.17 -26.48 -30.24 -28.41 02^{*} -14.16 -16.39 -18.47 -22.22 -20.32 03 0.34 ** 0.87 ** Flipting -22.22 -20.32 03 0.34 ** 0.87 ** -52.22 -20.32 03 0.34 ** 0.87 ** -52.22 -20.32 03 0.34 ** 0.87 ** -52.22 -20.32 03 0.34 ** 0.87 ** -52.22 -20.32 03 0.34 ** 0.87 ** -52.22 -20.32 03 0.34 ** 0.87 ** -18.47 Δ_{end} Δ_{start} Δ_{end} Δ_{end} Δ	

* A single mid-plane delamination was observed visually on the specimen surface during testing of these specimens.

** Positive Δ , further Δ =0 was used for the calculations of E_1 .

Clamping							
5-330				10-350			
Specimen	χ^2_{start}	χ^2_{end}	$\chi^2_{all \ points}$	Specimen	χ^2_{start}	χ^2_{end}	$\chi^2_{all points}$
01	0 **	0 **	0 **	01	39.5	49.8	45.4
02 *	244.1	318.291	280.9	02 *	83.2	111.5	96.6
03	118.4	171.344	143.3	03	0 **	0 **	0 **
Flipping							
5-330			10-350				
Specimen	χ^2_{start}	χ^2_{end}	$\chi^2_{all \ points}$	Specimen	χ^2_{start}	χ^2_{end}	$\chi^2_{all points}$
01	26.0	31.5	28.6	01 *	13.3	18.3	15.8
02 *	59.7	85.6	71.5	02	0 **	0 **	0 **
03	87.2	123.5	103.8	03	0 **	0 **	0 **

Table 4. χ^2 calculated using Δ_{start} , Δ_{end} , and $\Delta_{all \ points}$ for clamping- and flipping-specimens tested under fatigue mode I DCB loading.

* A single mid-plane delamination was observed visually on the specimen surface during testing of these specimens.

** Since a zero value was used instead of positive Δ , χ^2 that is $(\Delta/h)^2$ was equivalent to zero.

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