

Article

RETRACTED: Non-Destructive Testing Mechanism for Pre-Stressed Steel Wire Using Acoustic Emission Monitoring

Jothi Saravanan Thiyagarajan 

School of Infrastructure, Indian Institute of Technology Bhubaneswar, Argul-Jatni Rd, Kansapada, Odisha 752050, India; tjs@iitbbs.ac.in

Received: 6 October 2020; Accepted: 5 November 2020; Published: 7 November 2020;
Retracted: 16 June 2025



Abstract: In this paper, the guided ultrasonic wave propagation characteristics in the axisymmetric pre-stressed viscoelastic waveguide for acoustic emission (AE) monitoring, using the semi-analytical finite element (SAFE) method, is studied broadly. For the numerical investigation, a single high-strength steel wire is considered. A comprehensive and in-depth study on the AE signal's propagation characteristics is carried out based on the SAFE method. Both undamped and damped waveguides are considered for attaining SAFE solutions and presented in a detailed manner. The SAFE method for an axisymmetric cross-section in cylindrical coordinates analyzes the two main influencing factors of steel wire in a practical scenario: Material damping and initial tension. For the effect of initial stress, the calculation shows that the initial tensile stress can increase and decrease the energy velocity and attenuation factor of most modal waves above the cut-off frequency, and the effect is linear. Some longitudinal wave modes in the high-frequency region show their potential for AE monitoring as these modes have a low attenuation factor and small external surface vibration. By considering various states of initial stress in a damped waveguide, the effect of pre-stress on the dispersion characteristics is understood in a better manner. A non-destructive testing (NDT) mechanism for pre-stressed steel wire using AE monitoring is proposed for the health monitoring of structures.

Keywords: ultrasonic guided wave propagation; damped waveguide; semi-analytical finite element method; acoustic emission; steel wire; pre-stress load

1. Introduction

The guided ultrasonic wave propagation technique has significantly attracted worldwide attention, as it provides researchers, engineers, and infrastructure owners a more reliable way to monitor structural conditions for preventing failure. It always offers the best solution for non-destructive testing (NDT) and structural health monitoring as it can propagate over very long distances through the waveguide medium and detect the discontinuity in the medium [1–4]. Wave propagation in elastic rods and derivation of the Pochhammer frequency equation have been comprehensively studied by many researchers in the past [5–7]. Theoretical studies on evaluating dispersion curves are reviewed well. For modeling ultrasonic guided wave propagation, many finite element methods have been used for attaining an exact solution based on the superposition of bulk waves, which includes matrix methods [8]. The limitations include that the precise solution of an arbitrary cross-section does not exist, and the solution cannot be attained for all possible roots. Mainly, the theoretical description method for the propagation characteristics of the acoustic emission (AE) signal in the bridge cable or transmission line conductors is still in the development stage. Therefore, this paper mainly studies the

AE signal's propagation characteristics in the damped cylindrical waveguide, namely, high-strength steel wire.

An effective numerical method for analyzing waveguide media properties is the semi-analytical finite element (SAFE) method. The basic idea is to discretize the waveguide medium's cross-section into a finite element (FE) form while preserving wave propagation's theoretical formula in the axial direction [9–12]. In this way, the eigenvalue system for a modal solution is established, and the original frequency equation is converted into eigenvalues to solve the problem. The method is simple and can adapt to more complex waveguide structures. Compared with the 3D-FE method, the advantage is that it can obtain the exclusive wave phenomenon's characteristics and essence more clearly. The method can be implemented to any arbitrary cross-section and axisymmetric structures, as it includes solid rod [11–15], plate structures [16–19], hollow cylinders [20,21], different geometric sections (such as rails) [12–15,22–24], and composite laminate sections [9,14,20], etc. Compared with the wave equation method's solution, the advantage is that its calculation theory and method are simple and can effectively solve the complex wavenumber domain solution and adapt to more complex waveguide structures. Compared with the 3D FEM, the SAFEM is advantageous. It can obtain the characteristics and nature of the fluctuation phenomenon more clearly, and pertinently, high-cost finite element calculations are avoided.

Many researchers have studied the axial loading on the undamped and damped waveguide medium. In this aspect, Chen and Wilcox [25] used a particular finite element calculation strategy to study the circular cross-section and rail section. In contrast, Loveday [24] used a general SAFE method to examine them. However, the two only consider the material to be ideal elasticity and do not consider the material damping factor. A similar study by Mazzotti et al. [21] calculated the non-uniform stress field distribution on the cross-section of rail and circular pipes and considered the material damping factor. The basic acoustoelastic formulation to standardize an ultrasonic guided wave propagation for observing various stress levels in the seven-wire steel strand is carried out in Chaki and Bourse [26]. Treysède [27,28] has made the most outstanding contributions to the research area of multiple wire waveguides using the SAFE method.

For waveguide media with axisymmetric cross-sections, such as a cylindrical waveguide, the general semi-analytic method's calculation efficiency and accuracy are not high [29]. The reason is that the general semi-analytic method uses a two-dimensional (2D) difference function $N(x, y)$ to describe the deformation of each point in the unit. However, for an axisymmetric section, the displacement field, which satisfies the Pochhammer-Chree frequency equation, must be a radial function, $U(r)$. For the specific problem, directly introducing the trigonometric function $\cos(n\theta)$ (or $\sin(n\theta)$) into the interpolation function will further improve the calculation accuracy and efficiency. Moreover, different displacement fields can be used to analyze the longitudinal, bending, and torsion wave modes ignored by the general method. Henceforth, it is convenient to use a cylindrical coordinate system for axisymmetric sections.

In the present work, to study the guided ultrasonic wave characteristics, including the effect of initial stress and structural damping, the axisymmetric SAFE method is utilized. This paper discusses the SAFE method of the axisymmetric cross-section for an undamped and damped condition and comprehensively considers the AE signal's propagation characteristics in a single steel wire. The damped waveguide's dispersion characteristics, namely, the wavenumber-frequency curve, energy velocity curve, and attenuation factor curve, are studied to influence the varying initial tensile stresses. Finally, a mode suitable for AE monitoring is carefully chosen. This study can help select an appropriate mode with low attenuation characteristics that may be useful for monitoring AE and NDT events.

2. A SAFE Method for Undamped Waveguide

The mathematical framework for an infinitely long, axisymmetric waveguide immersed in a vacuum is represented using the semi-analytical method. The technique follows a cylindrical coordinate

system with the cross-section in the r - z plane, as shown in Figure 1. The SAFE model represents fluctuation along the wave propagation axis z with wavenumber (k), and frequency (ω). As the trigonometric function component is introduced in the interpolation function, the displacement interpolation is performed only in its radial direction. In this case, the element form is reduced from 2D to 1D, and the quadratic element has three nodes, as shown in Figure 1.

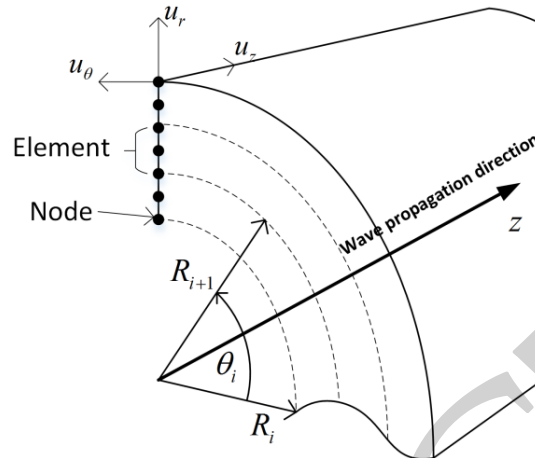


Figure 1. Representation of the semi-analytical finite element (SAFE) model and its nodal degree of freedom.

For bending wave mode, the displacement field vector is given as:

$$\mathbf{u} = \begin{bmatrix} u_r & u_\theta & u_z \end{bmatrix}^T \quad (1)$$

where r, θ, z represent the radial, circumferential, and axial directions of the axisymmetric cross-section, respectively. The strain and stress vectors are expressed as:

$$\begin{aligned} \boldsymbol{\varepsilon} &= \begin{bmatrix} \varepsilon_r & \varepsilon_\theta & \varepsilon_z & \gamma_{r\theta} & \gamma_{\theta z} & \gamma_{zr} \end{bmatrix}^T \\ \boldsymbol{\sigma} &= \begin{bmatrix} \sigma_r & \sigma_\theta & \sigma_z & \tau_{r\theta} & \tau_{\theta z} & \tau_{zr} \end{bmatrix}^T \end{aligned} \quad (2)$$

According to the geometric relationship in the cylindrical coordinate system, the strain-displacement relationship is expressed as:

$$\boldsymbol{\varepsilon} = \mathbf{L}\mathbf{u}; \quad \mathbf{L} = \begin{bmatrix} \frac{\partial}{\partial r} & \frac{1}{r} & 0 & \frac{1}{r} \frac{\partial}{\partial \theta} & 0 & \frac{\partial}{\partial z} \\ 0 & \frac{1}{r} \frac{\partial}{\partial \theta} & 0 & \frac{\partial}{\partial r} - \frac{1}{r} & \frac{\partial}{\partial z} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} & 0 & \frac{1}{r} \frac{\partial}{\partial \theta} & \frac{\partial}{\partial r} \end{bmatrix}^T \quad (3)$$

where $\mathbf{L}$ is the differential operator. Since the cylindrical coordinate system is still an orthogonal coordinate system, the material stiffness matrix $\mathbf{D}$ is the same as in the rectangular Cartesian coordinate system [14]. For further understanding of the element stiffness and mass matrices, Appendix A is derived for fundamental wave modes.

Wavenumber-Frequency Curve Analysis for Undamped Waveguide

The solution of transcendental equations and the general semi-analytic method is used to obtain the wavenumber-frequency (k - ω) curve in the positive wavenumber domain. Solving the equation requires substituting different circumferential orders n to get the k - ω curves of different modes in a specific frequency range. When the general semi-analytical method is used, the first several orders of frequencies at a given wavenumber can be obtained entirely, whether bending, torsion, or longitudinal

waves. The accuracy of these frequency values will obey the principle of the meshing criterion [17]. The method uses the calculation principle $\omega = \omega(k)$. Its limitation is that it only considers the case of the positive real wavenumber domain. The complete wavenumber domain exists on the complex number plane.

In this paper, a high-strength steel wire with a 5 mm diameter is considered for numerical investigations, and the material characteristics are tabulated in Table 1. Using the $k = k(\omega)$ calculation method, several standard modes of AE signals, namely, flexural— $F(1,m)$, $F(2,m)$, $F(3,m)$, longitudinal— $L(0,m)$, and torsional— $T(0,m)$ modes are calculated. Their corresponding complex k - ω curves are shown in Figure 2, respectively. The x and y axes represent the real part ($Re(k)$) and imaginary part ($Im(k)$) of the wavenumber, and the z -axis represents the frequency. Figure 2 shows that the red, green, and blue lines represent the pure real, pure imaginary, and complex wavenumbers. The plot is obtained by slicing the wavenumber plane along the frequency axis.

Table 1. Material characteristics of high-strength steel wire.

Young's Modulus, E (MPa)	Density, ρ (kg/m ³)	Poisson's Ratio, ν	Diameter, d (mm)	Longitudinal Wave Velocity, C_L (m/s)	Shear Wave Velocity, C_S (m/s)
2×10^5	7850	0.3	5	5856.4	3130.4

On the whole, the complex k - ω curve is symmetric about the x and y axes. It can be observed from Figure 2 that for any k - ω curve, when the frequency is higher than its cut-off frequency, there is no attenuation wave, and the wavenumber is a real value, which is consistent with the curve obtained using the $\omega = \omega(k)$ calculation mode. Below the cut-off frequency, the propagative and evanescent modes appear corresponding to pure imaginary and complex wavenumbers, respectively. Due to their attenuation properties, the waves disappear after a certain distance of propagation. For the bending $k - \omega$ curves in Figure 2a–c, the $Im(k)$ curve starts at the cut-off frequency of the $f = 0$ plane or starts from the $Re(k)$ curve, and the $Im(k)$ curve ends at a higher-order $Re(k)$ curve. For the complex k curve, it starts either at the $f = 0$ plane or the maximum of the $Im(k)$ curve and ends at the minimum of the $Im(k)$ curve or the $Re(k)$ curve. It is worth noting that from the theory of wave propagation mechanics, the cut-off frequency is the minimum frequency point on each real $k - \omega$ curve. This point is not necessarily located at $k = 0$ and may also exist at a smaller wavenumber value as the frequency shows a downward trend before this value. However, the frequency value $k = 0$ is still called a cut-off frequency. For complex k or $Im(k)$ curves, there is no intersection with each other as observed for $Re(k)$ curves.

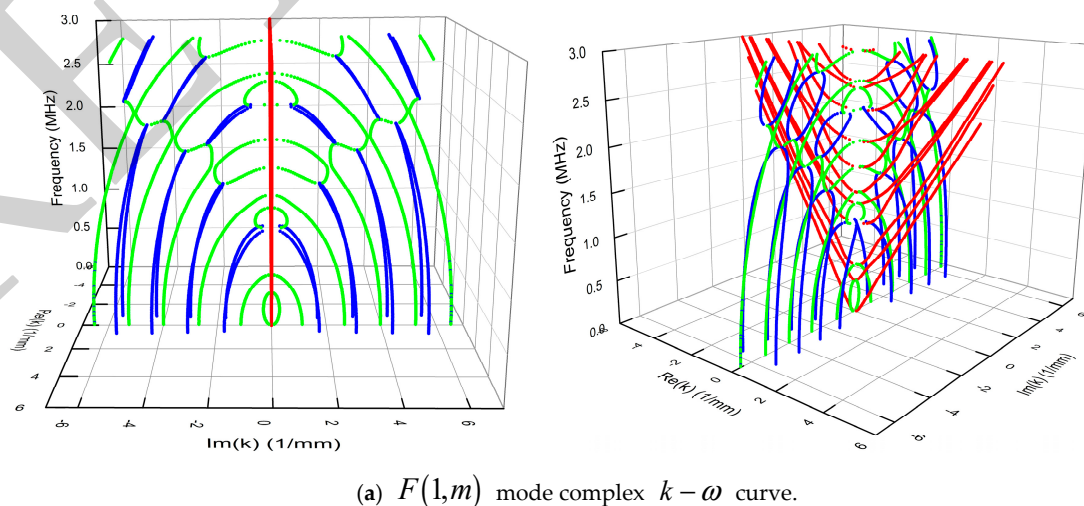


Figure 2. Cont.

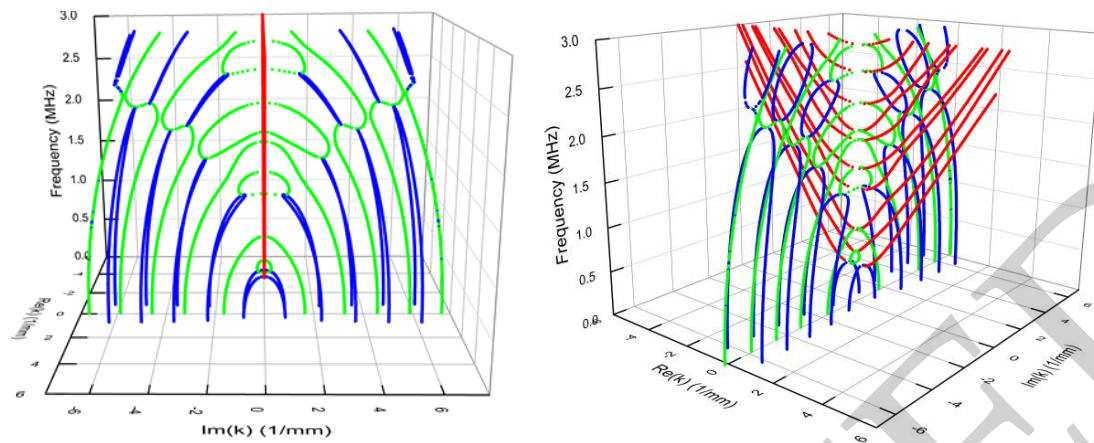
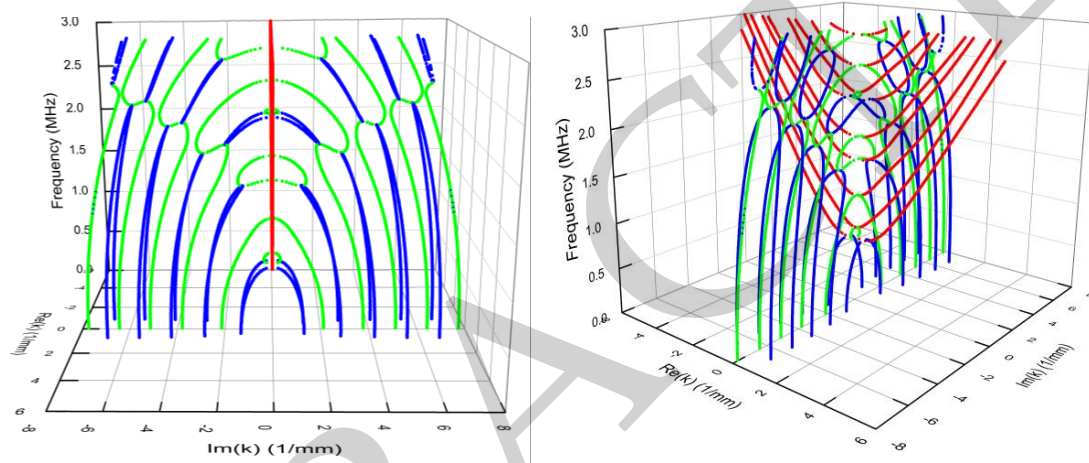
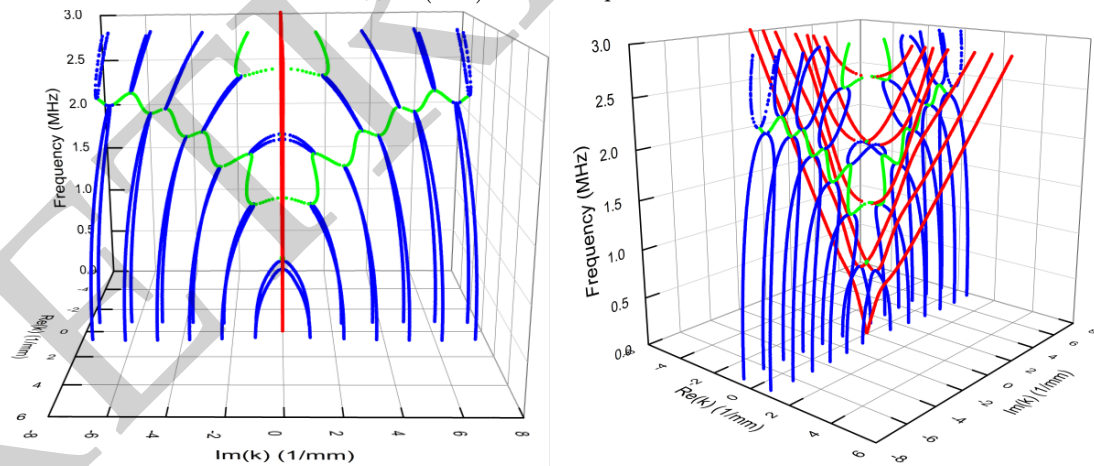
(b) $F(2,m)$ mode complex $k-\omega$ curve.(c) $F(3,m)$ mode complex $k-\omega$ curve.(d) $L(0,m)$ mode complex $k-\omega$ curve.

Figure 2. Cont.

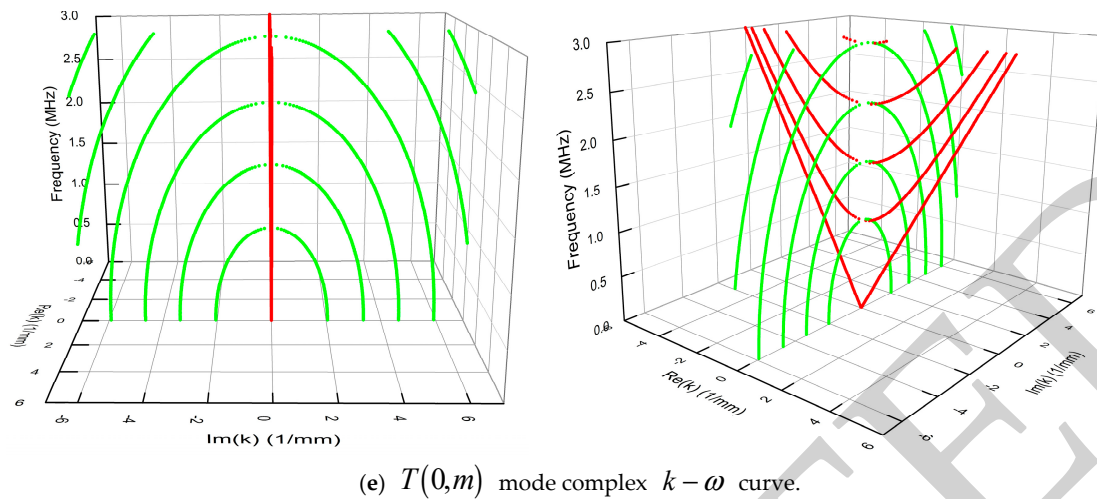


Figure 2. Complex $k - \omega$ curves for the undamped waveguide: (a) $F(1,m)$ mode complex $k - \omega$ curve; (b) $F(2,m)$ mode complex $k - \omega$ curve; (c) $F(3,m)$ mode complex $k - \omega$ curve; (d) $L(0,m)$ mode complex $k - \omega$ curve; (e) $T(0,m)$ mode complex $k - \omega$ curve.

For the longitudinal $k - \omega$ curve in Figure 2d, there is no $Im(k)$ curve starting from the $f = 0$ plane. It begins at the cut-off frequency of a $Re(k)$ curve and terminates at a cut-off frequency of a higher-order $Re(k)$ curve or extends to the high-frequency direction of the positive and negative axis of the imaginary axis, and there is no intersection point with the $Re(k)$ curve. Figure 2d shows a pair of extended $Im(k)$ curves. From the characteristics of the disconnected $k - \omega$ curve, it can be seen that as the frequency increases, the curve will appear more, which is close to the $Re(k)$ curve. For the complex k curve, its characteristics are similar to those of the bending wave. Intuitively, many complex k curves connect the $f = 0$ plane and the $Im(k)$ curve, or between the two $Im(k)$ curves. There are also cases where the maximum value starts from the $Im(k)$ curve, or the $f = 0$ plane ends at the minimum value of the $Re(k)$ curve.

For the torsional $k - \omega$ curve in Figure 2e, only $Im(k)$ curve parts start at the $f = 0$ plane and end at the cut-off frequency of the $Re(k)$ curve. In general, by introducing frequency curves, including complex k and $Im(k)$, each $k - \omega$ curve becomes continuous over the entire frequency domain. The waveform from high frequency to cut-off frequency is non-attenuating, and, from the cut-off frequency, all waves appear to be attenuating up to the $f = 0$ plane.

3. A SAFE Method for Damped Waveguide

3.1. Guided Wave Characteristics

For time-harmonic wave $e^{-i\omega t}$, a linear viscoelastic material model can be simulated by including the imaginary component in the material stiffness matrix [14]:

$$D = D' - iD'' \quad (4)$$

where D' contains the energy storage modulus and D'' consists of the energy dissipation modulus. The coefficients of the viscosity tensor are usually measured at characterization frequency f_{ref} . Two linear viscoelastic models widely used in NDT and AE research are the Kelvin-Voigt and the hysteresis models. For the Kelvin-Voigt model, the complex stiffness is proportional to the frequency f , $D'' \propto f$, then the material stiffness matrix at any frequency f :

$$D_f = D_e - i \frac{f}{f_{ref}} D_v \quad (5)$$

where D_e is the elastic stiffness tensor and D_v is the viscous tensor. At frequency $f = f_{ref}$, the imaginary part of the matrix is the viscous tensor element measured at the characteristic frequency. In the hysteresis model, the imaginary part of the stiffness matrix is independent of frequency:

$$D_f = D_e - iD_v \quad (6)$$

Therefore, for the hysteresis model, the material stiffness matrix only needs to be determined once in the initial calculation; for the Kelvin-Voigt model, it needs to be continuously updated when calculating different frequency situations [14]. For the high-strength steel strands, the hysteresis model is usually used for simulation analysis. In Equation (6), the material stiffness matrix has 21 independent variables as a general form, simulating non-isotropic materials. However, for isotropic viscoelastic materials, the number of independent variables will be reduced to two complex Lamé constants $\tilde{\mu} = \rho\tilde{C}_T^2$ and $\tilde{\lambda} = \rho(\tilde{C}_L^2 - \tilde{C}_T^2)$, where the complex longitudinal wave velocity, $\tilde{C}_L$ and the complex shear wave velocity, $\tilde{C}_T$ are calculated by:

$$\tilde{C}_L = C_L(1 + i\frac{\kappa_L}{2\pi})^{-1}; \quad \tilde{C}_T = C_T(1 + i\frac{\kappa_T}{2\pi})^{-1} \quad (7)$$

where C_L and C_T are the bulk longitudinal wave and shear wave velocity of the material, respectively. For isotropic viscoelastic materials, the properties are determined by measuring the attenuation during the propagation of body longitudinal and transverse waves. Moreover, κ_L and κ_T are the attenuations of longitudinal body wave and transverse body wave, respectively, and their unit is Np/λ . For the high-strength steel strand, the attenuation values are considered as $\kappa_L = 0.003Np/\lambda$ and $\kappa_T = 0.008Np/\lambda$ [29].

For viscoelastic materials, the only $k = k(\omega)$ mode can calculate the k value at a given frequency ω . It yields a $2M$ complex wavenumber value, $k^m = k_{Re}^m + ik_{Im}^m$ ($m = 1 - 2M$, where M is the number of degrees of freedom of the system), and the corresponding complex eigenvalue vector is $U^m = U_{Re}^m + iU_{Im}^m$. For the m th mode, the energy velocity at a certain point on the cross-section of the waveguide medium is given as:

$$c_e^m = \langle P^m \rangle / \langle E^m \rangle \quad (8)$$

where $\langle () \rangle$ represents the time averaging operator for the content in brackets [28]:

$$\langle () \rangle = \frac{1}{T} \int_0^T () dt \quad (9)$$

In Equation (8), P^m represents the Poynting vector at a point on the cross-section; E^m is the total energy at that point. $T = 2\pi/\omega$, $\langle P^m \rangle$ and $\langle E^m \rangle$ are real values [29].

$\langle P^m \rangle$ is expressed as:

$$\langle P^m \rangle = \begin{bmatrix} P_{r/x}^m & P_{\theta/y}^m & P_z^m \end{bmatrix}^T = -\text{Re}(\bar{\sigma}^m v^m) / 2 \quad (10)$$

The unit is $J/(m^2s)$, $\bar{\sigma}^m$ is the classic 3×3 stress tensor. The Poynting vector reflects the direction and magnitude of energy flow at various points in the waveguide medium. For guided waves in ideal elastic materials, the Poynting vector component is only in the z -axis [30].

$\langle E^m \rangle$ is expressed as:

$$\langle E^m \rangle = \langle S^m \rangle + \langle K^m \rangle = \text{Re}((\sigma^m)^T \varepsilon^{m*}) / 4 + \text{Re}(\rho(v^m)^T v^m) / 4 \quad (11)$$

The unit is J/m^3 , where $\langle S^m \rangle$ represents strain energy and $\langle K^m \rangle$ represents kinetic energy. The velocity field, v^m , the strain field, ε^m , and the stress field, σ^m can be obtained by derivation and interpolation of the node displacement vector, q^m of each element, which is derived from the eigenvector,

U^m . However, for guided waves propagating across the entire cross-section, the research object should be aimed at the interface's energy flow. Therefore, integrating the energy velocity component at the above points in the z -direction in the cross-sectional domain can obtain the waveguide's overall energy velocity in the waveguide [20]:

$$C_e^m = \int_{\Omega} \langle P_z^m \rangle / \langle E^m \rangle d\Omega \quad (12)$$

3.2. Wavenumber-Frequency Curve Analysis for Damped Waveguide

Due to the consideration of material damping, there are only complex numbers in the wavenumber. The index reflecting the ratio of the real part and the imaginary part of the wavenumber is introduced to distinguish the degree of damping [31], namely:

$$R = \text{Re}(k^m) / \text{Im}(k^m) \quad (13)$$

When $R > 100$ it represents low damping, $100^{-1} < R < 100$ is medium damping and $R < 100^{-1}$ is high damping. Figure 3a,b shows the complete $k - \omega$ curves of $L_d(0, m)$ and $F_d(1, m)$ in a specific frequency range, respectively. The study is limited to damped waveguides of longitudinal and flexural modes only. The x and y axes represent the real part ($\text{Re}(k)$) and imaginary part ($\text{Im}(k)$) of the wavenumber, the z -axis represents the frequency. Likewise, the red line represents the low damping curve, the green line represents the high damping curve, and the blue line represents the medium damping curve. By comparing with curves in Figure 2, the $k - \omega$ curve for damped waveguide loses its symmetry about the x, y axis, and the curve is only symmetrical about the origin of the coordinate. In ideal elastic materials, the points where several wave-frequency curves intersect (such as the cut-off frequency) are now separated and belong to different curves (Figure 3). For example, for the $L_d(0, 3)$ curve, the frequency is lower than the nominal cut-off frequency (corresponding to the cut-off frequency in an ideal elastic material).

The low-damping curve passes through the middle curve as a semicircle and turns into a negative real wavenumber region to become a middle damping curve. This curve is connected to the lowest point of the negative real wavenumber part of the $L(0, 2)$ curve in an ideal elastic material and finally reaches the $f = 0$ plane. The wavenumber value corresponding to each point on each curve in this example has an imaginary part with the same sign. Therefore, for viscoelastic materials, each $k - \omega$ curve will be single-valued and continuous in the entire frequency domain. The curves do not intersect with each other, which appear in pairs on the complex wavenumber plane of the origin. When the damping of the material approaches infinitely small, the viscoelastic material degenerates into an ideal elastic material. For the viscoelastic material, the points closer to each curve will overlap, and the shape of the curve becomes symmetrical about the x, y axis. The energy velocity and attenuation factor are more reasonable indicators of a damped waveguide medium's wave characteristics. The energy velocity is defined as the group velocity counterpart in a purely elastic material and represents the energy propagation velocity in the waveguide medium. The attenuation factor represents the attenuation of each modal wave with the propagation distance. The energy velocity and attenuation characteristics are obtained by further extracting the data in the $k - \omega$ curve for analysis.

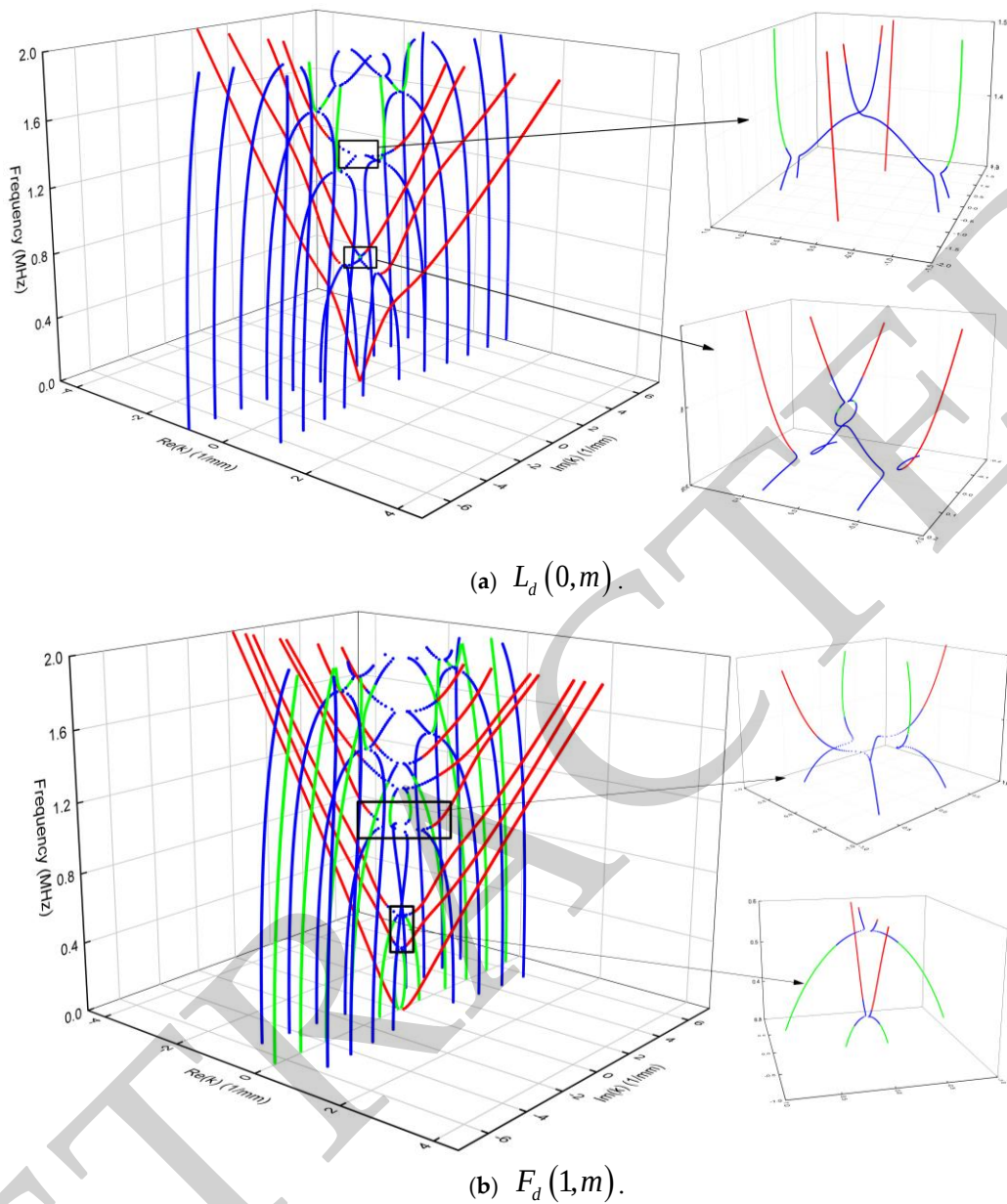


Figure 3. The complex $k - \omega$ curve for the damped waveguide: (a) $L_d(0, m)$; (b) $F_d(1, m)$.

3.3. Attenuation Factor

Figures 4 and 5 show the attenuations of high and low magnitude regions of $L_d(0, m)$ and $F_d(1, m)$ in a specific frequency range. It shows only the positive attenuation, and the negative part is symmetrical to the frequency axis, which is not shown. For the higher value area's attenuation, the amplitude of the fluctuation will be attenuated within the range of several wire diameters d . For example, when $att = 5000$ Np/m, the amplitude of the wave is reduced to 1.4×10^{-11} of the original signal amplitude after attenuation of $1d$. Likewise when $att = 1000$ Np/m, the amplitude of the wave will decay to 1.4×10^{-11} of the initial amplitude after $5d$ attenuation. Therefore, for a sensor at a certain distance from the AE source, this part of the signal will not be extracted, and they correspond to the medium and high damping curves in the wave frequency curve.

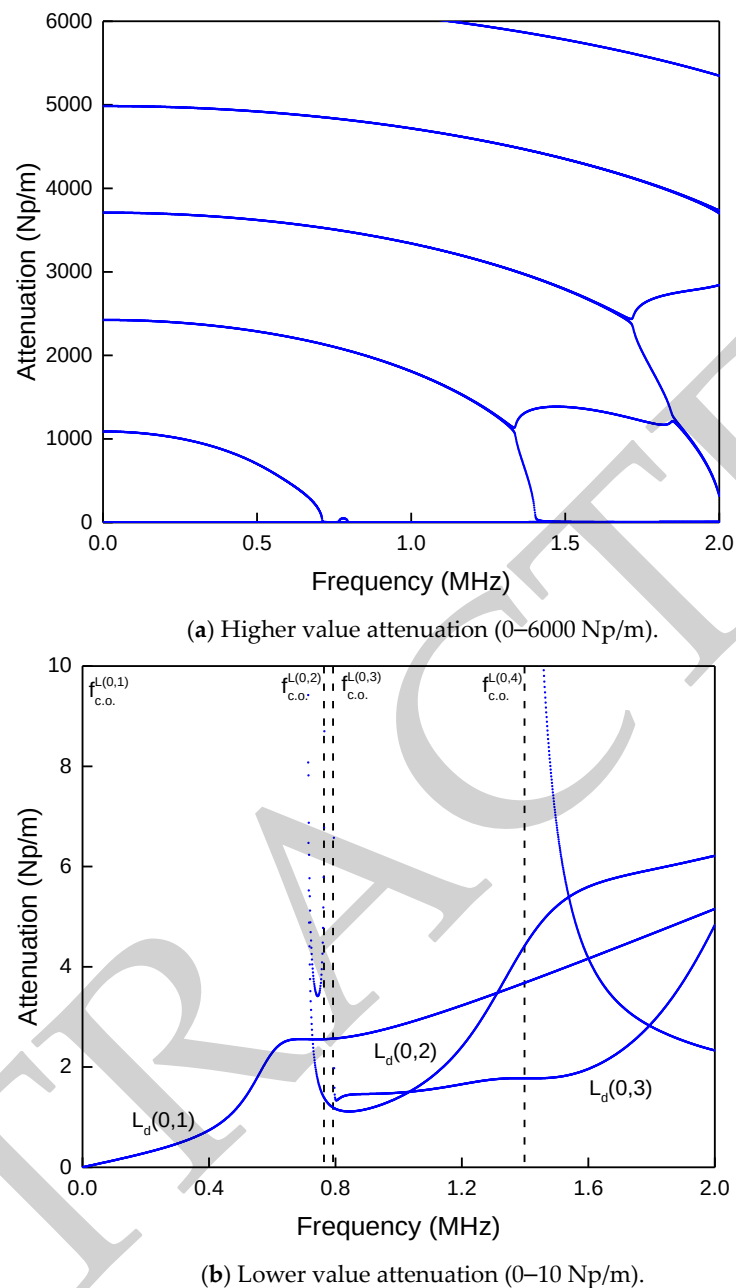
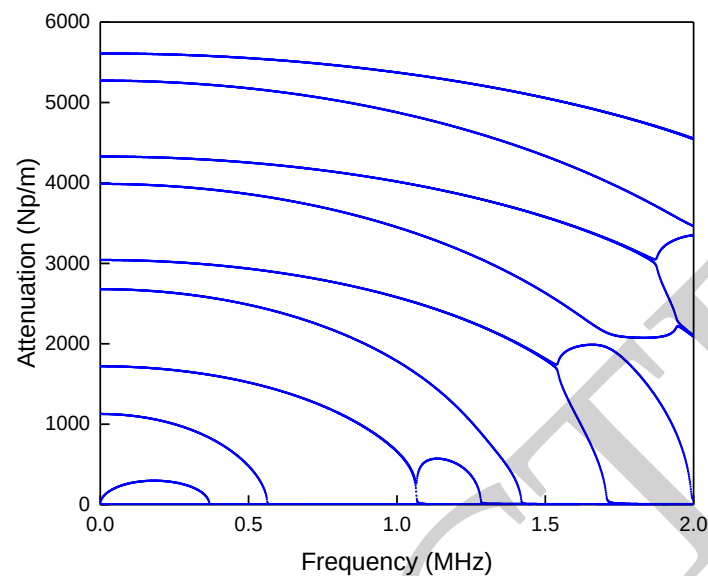


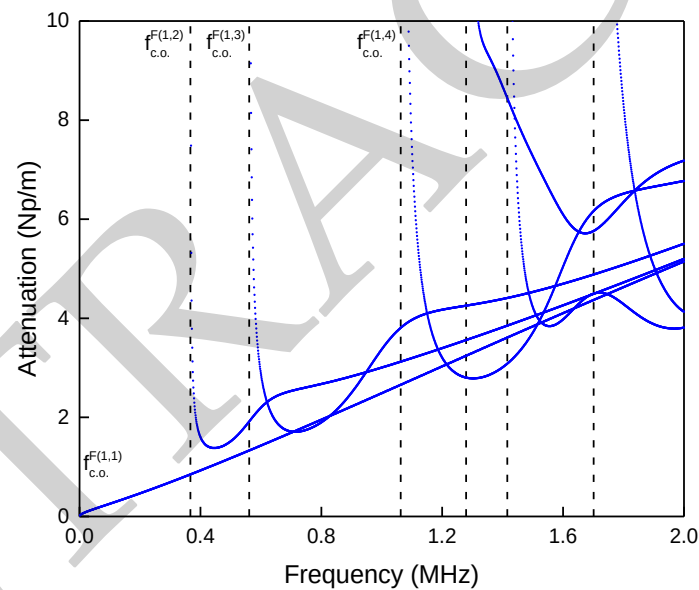
Figure 4. Attenuation curve: (a) Higher value attenuation (0–6000 Np/m); (b) lower value attenuation (0–10 Np/m).

For attenuations in areas of low magnitude, the AE signal can be transmitted to the farther part. For example, for a wave with attenuation $att = 2$ Np/m, the wave will pass 2 m, i.e. $400d$, or when $att = 4$ Np/m, the wave after passing 1 m, the amplitude will be attenuated to about 2% of the original amplitude. Figures 4b and 5b illustrate the cut-off frequency (blue dotted line) of the ideal elastic material's propagation without the attenuation wave, such as $f_{c.o.}^{L(0,m)}$ the superscript represents the corresponding mode and $c.o.$ is the cut-off frequency. It can be seen that the attenuations of $L(0,1)$ and $F(1,1)$ except the lower order modes increase monotonically with frequency from 0. The attenuations of the other modal waves all get the minimum value at a particular frequency higher than the cut-off frequency. Later, it increases with increasing frequency. Subsequently, a small amplitude oscillation in the area near the cut-off frequency, the curve gradually approaches the attenuation curves of the two low-order modes $L(0,1)$ and $F(1,1)$ which extends steadily toward the high-damping region.

Currently, the high-frequency mode of the same circumferential order mode will have a slightly higher attenuation.



(a) Higher value attenuation (0–6000 Np/m).



(b) Lower value attenuation (0–10 Np/m).

Figure 5. Attenuation curve: (a) Higher value attenuation (0–6000 Np/m); (b) lower value attenuation (0–10 Np/m).

The 3D-attenuation curves of flexural modes, namely, $F(n,1)$, $F(n,2)$, $F(n,3)$, and $F(n,4)$ are summarized in Figure 6. It can be seen that, similar to the group velocity dispersion curve, each mode attenuation curve with the same frequency order also has an equal change trend with frequency, but each group of curves is not the same. In the higher frequency region, the high-order mode always has a higher attenuation. It can also be seen that in the high-frequency region, the attenuation is linearly related to the frequency as the modal group velocity is close to the shear wave or Rayleigh wave velocity. The attenuation of the shear wave in the solid medium is $\kappa_T = 0.008Np/\lambda$, that is, $att = 0.008f/C_T$ Np/m. From this formula, the linear relationship between the attenuation and frequency can be qualitatively analyzed.

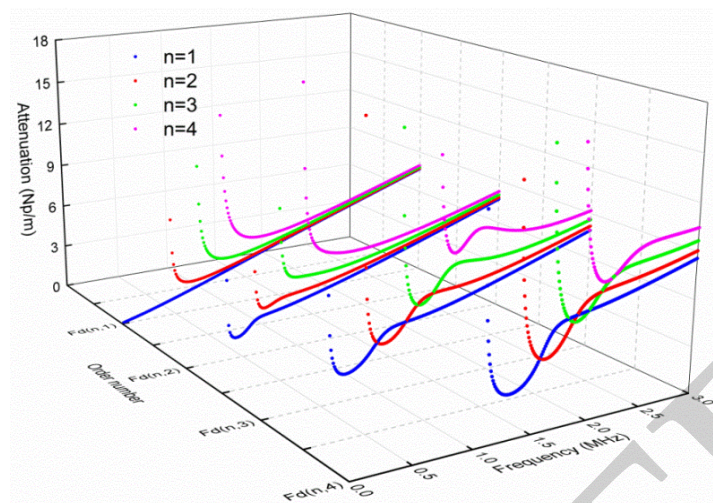


Figure 6. Three dimensional (3D)-attenuation curves for flexural modes.

For viscoelastic materials in a vacuum, the energy will flow in the direction of wave propagation and flow inside the cross-section, which will then be used as energy dissipation in the material. If the waveguide medium is wrapped in fluid or a highly damped material in the circumferential direction, energy will flow outside of the waveguide medium. Figures 7–10 show the Poynting vector on the cross-section of the steel wire in each damped mode, namely, $L_d(0,1)$, $F_d(1,1)$, $F_d(2,1)$, and $F_d(3,1)$ respectively, at a particular frequency. To ensure the comparability between the frequencies $\int_{\Omega} \langle P_z^m \rangle d\Omega$ is used for unitization [20]. It can be seen that the intensity of the Poynting vector flowing in the cross-section is significant, and the attenuation factor is greater at the higher frequency value of that particular mode.

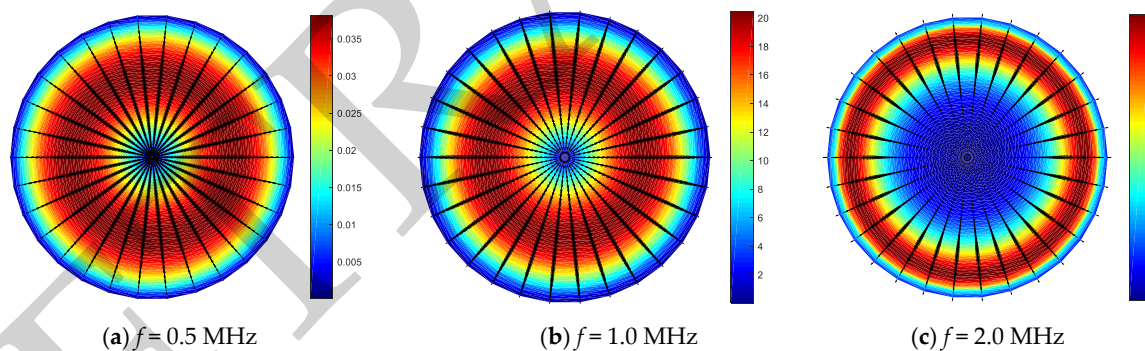


Figure 7. $L_d(0,1)$ Poynting vector at each frequency.

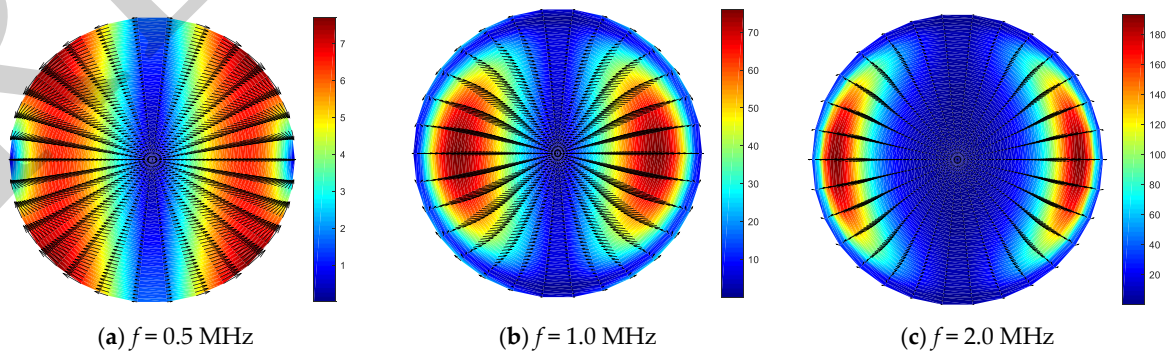


Figure 8. $F_d(1,1)$ Poynting vector at each frequency.

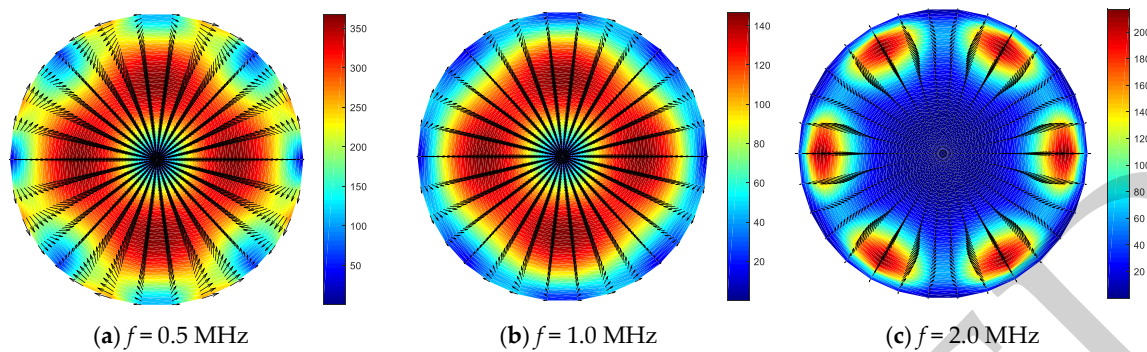


Figure 9. $F_d(2,1)$ Poynting vector at each frequency.

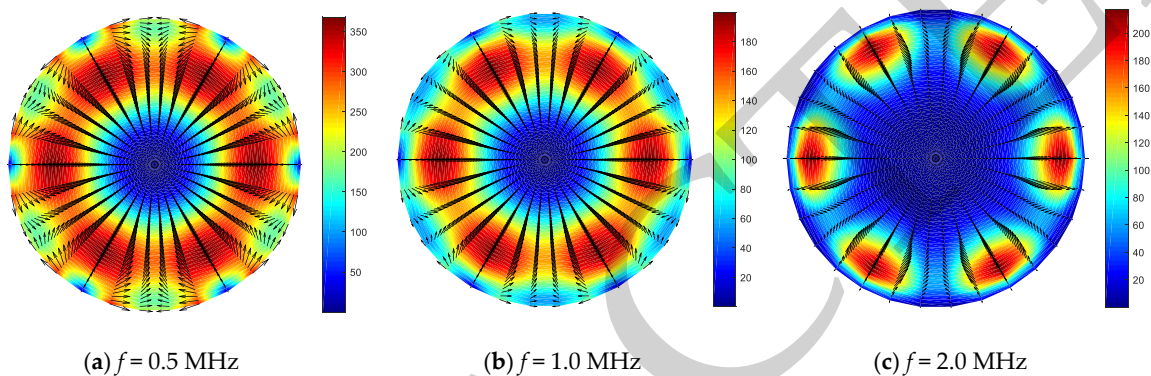
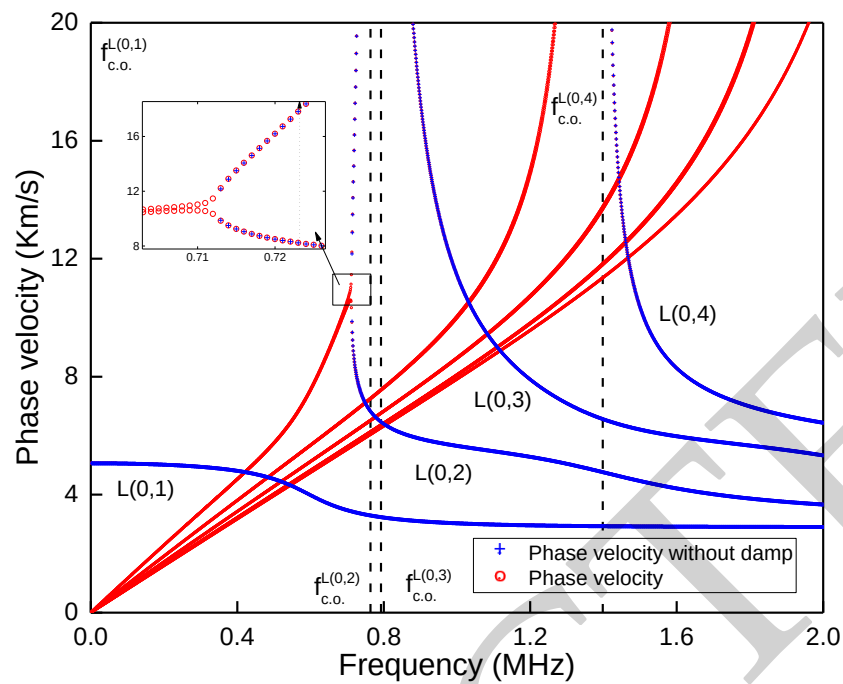


Figure 10. $F_d(3,1)$ Poynting vector at each frequency.

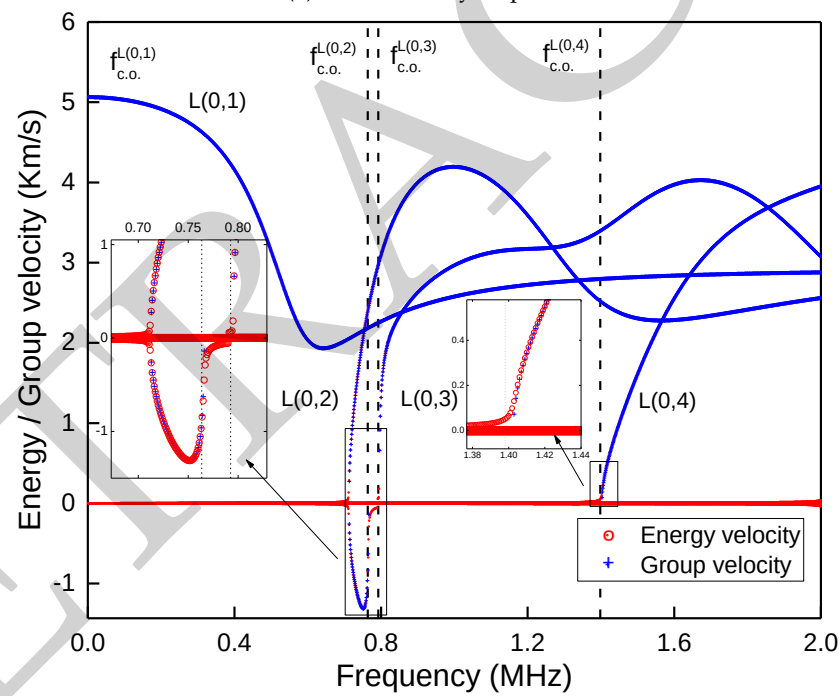
3.4. Phase Velocity and Energy Velocity (Group Velocity)

The phase velocity and energy velocity (group velocity) dispersion curves calculated using the viscoelastic model and the ideal elastic model are compared and analyzed to discuss the effects of material damping on these two wave propagation characteristics. Figures 11 and 12 show the phase velocity and energy velocity (group velocity) of the low-order longitudinal wave mode and bending wave mode. The cut-off frequency of each order mode in an ideal elastic material is also indicated correspondingly. It is worth mentioning that only the positive part is shown in the phase velocity diagram. The negative part is symmetrical with the frequency axis (and is not included here). It can be seen from Figures 11a and 12a that the phase velocity dispersion curves of the two models (damped and undamped) agree well with the range above the cut-off frequency. Still, the phase velocity of the viscoelastic material is slightly lower. However, in the range below the cut-off frequency, the phase velocity curve enters the high and medium damping regions, and there is an absolute difference in the curve.

The phase velocity curve reaches a maximum value with the frequency decrease and then decreases to point $f = 0$, as shown in the partially enlarged view in Figure 11a. Moreover, the phase velocity curve will have an infinite discontinuity near the cut-off frequency, and in its left area, it will decrease to 0 as the frequency decreases. Figure 11b shows that the remaining group velocity curves agree for the energy velocity curve in the range above the cut-off frequency. In contrast, in the range below the cut-off frequency, the energy velocity is close to 0. Extending to point $f = 0$, it shows that the energy propagation speed of the wave in the high and medium damping regions is much lower than that in the small damping region.



(a) Phase velocity dispersion curve.



(b) Energy/group velocity dispersion curve.

Figure 11. Low-order longitudinal wave mode: (a) Phase velocity dispersion curve; (b) Energy/group velocity dispersion curve.

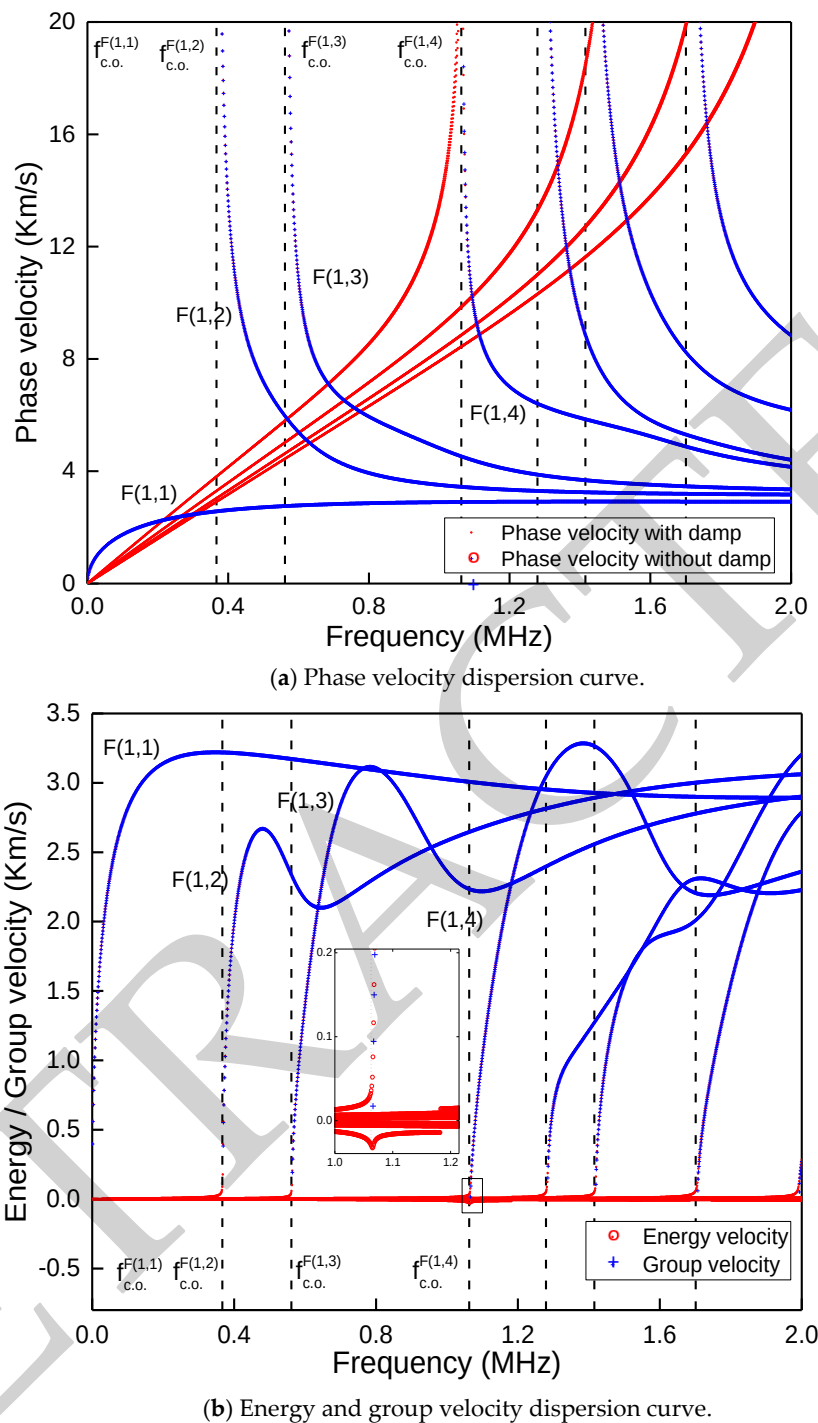
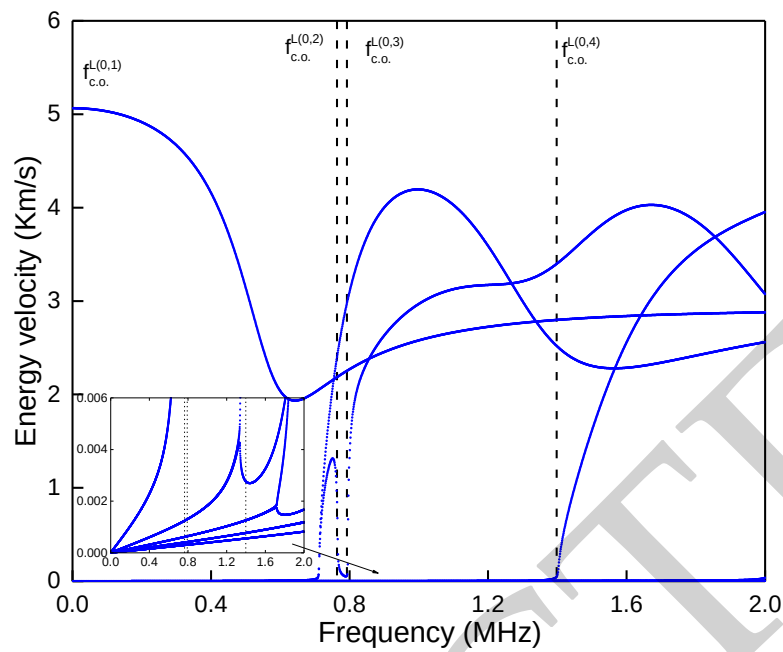
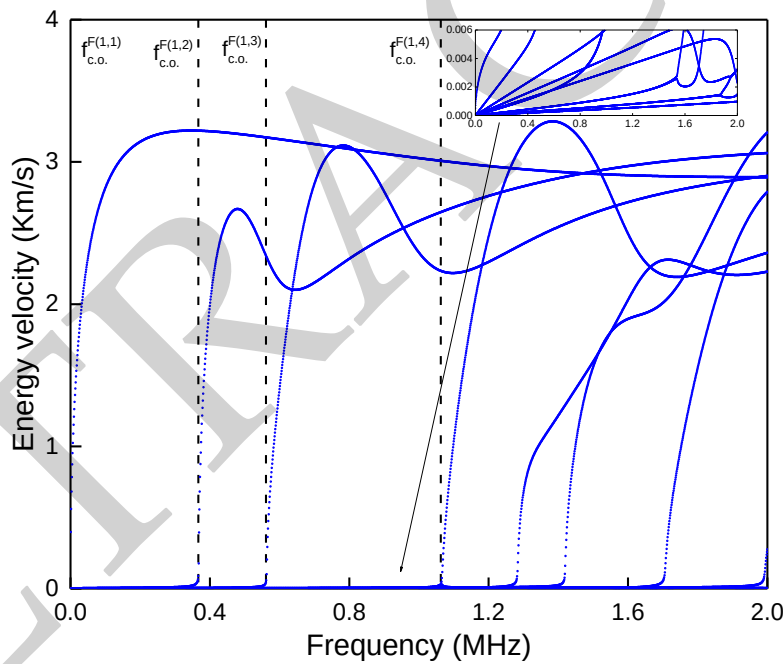


Figure 12. Low-order bending wave mode: (a) Phase velocity dispersion curve; (b) Energy/group velocity dispersion curve.

It can be seen in the partially enlarged part of Figure 12b that the energy velocity curve has a discontinuity near the cut-off frequency. It belongs to two different wavenumber-frequency curves, and the wavenumbers at each point of the two curves have different imaginary parts. If the energy velocity determined according to the same wavenumber-frequency curve points as plotted in the same sub-plot, the energy velocity curve would be continuous everywhere in the frequency domain, as shown in Figure 13. In this case, the wavenumber's imaginary part corresponding to each wave frequency curve's point is greater than 0. As only modes with a positive $Im(k)$ will attenuate as they propagate forward in the z -axis, their energy velocity must be positive.

(a) $L_d(0, m)$ mode.(b) $F_d(1, m)$ mode.**Figure 13.** Energy velocity dispersion curve: (a) $L_d(0, m)$ mode; (b) $F_d(1, m)$ mode.

4. Effect of Initial Tensile Stress on Wave Propagation Characteristics

The high-strength steel wire model analyzed in the previous section ignores the factors caused by pre-stress loading. In actual engineering, the bridge cable cannot be in a stress-free state. The friction between the steel wires and the secondary stress caused by temperature and other factors have a strong practical significance to study the influence of stress on the wave propagation characteristics. In this section, a single 5 mm diameter high-strength steel wire is still used as the research object to analyze the importance of its wave propagation characteristics at a specific stress level.

The virtual work equations need to be established under two equilibrium states to consider the initial stress effect caused due to fluctuations in the elastic body. The first equilibrium state is that a single wire is subjected to axial tension to achieve static balance, and the corresponding static virtual work equation is:

$$\int_V \delta \varepsilon_1^T \sigma_0 dV = \int_V \delta u_1^T P dV \quad (14)$$

where σ_0 represents the initial stress field, which is caused by the axial tensile force, P represents the applied load field, precisely the axial force in this case study. Moreover, $\delta \varepsilon_1$ and δu_1 represent the virtual displacement and virtual strain, respectively, and they should satisfy the boundary conditions of displacement. The second equilibrium state is the dynamic balance of the guided wave as it propagates through the wire. At this time, the virtual work equation considers the inertial force factor and the initial stress field's contribution. The virtual work equation is as follows:

$$\int_V \delta E_2^T (\sigma + \sigma_0) dV + \int_V \delta u_2^T (\rho \ddot{u}) dV = \int_V \delta u_2^T P dV \quad (15)$$

where σ represents the stress field generated by guided wave propagation; δE_2 and δu_2 represents the virtual strain and virtual displacement, respectively, where δE_2 is the complete form of virtual strain, which is $\delta(\varepsilon_2 + e_2)$. It is worth noting that since the two equilibrium states are still in a small deformation state, the virtual work equation has the above simple form and conforms to the linear superposition principle. Figure 14 shows the two equilibrium states for establishing the virtual work equation.



Figure 14. The equilibrium state of the virtual work.

On further substitution and simplification of Equation (15), only work done by $\int_V \delta e_2^T \sigma_0^z dV$ will be retained, as only axial forces are considered here:

$$\int_V \delta e_2^T \sigma_0^z dV = \int_V \delta \left(\frac{1}{2} \left[\left(\frac{\partial u_r}{\partial z} \right)^2 + \left(\frac{\partial u_\theta}{\partial z} \right)^2 + \left(\frac{\partial u_z}{\partial x} \right)^2 \right] \right) \sigma_0^z dV \quad (16)$$

In the finite element format, the interpolation function is used to approximate the element displacement field for the j element as:

$$\int_{V_j} \delta \left(\frac{1}{2} (LN \bar{U}^j)^T (LN \bar{U}^j) \right) \sigma_0^z dV \quad (17)$$

where the difference operator is given as: $L = \begin{bmatrix} \frac{\partial}{\partial z} & 0 & 0 \\ 0 & \frac{\partial}{\partial z} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} \end{bmatrix}$

On further simplifying Equation (17):

$$\int_{V_j} \delta \left(\frac{1}{2} (LN \bar{U}^j)^T (LN \bar{U}^j) \right) \sigma_0^z dV = \delta \bar{U}^{jT} \int_{V_j} ((LN)^T (LN)) \sigma_0^z dV \bar{U}^j \quad (18)$$

$$LN = k \begin{bmatrix} B_1 & B_2 & B_3 \end{bmatrix}$$

$$B_m = iN_m = \begin{bmatrix} iN_m(r, \theta) & & \\ & iN_m(r, \theta) & \\ & & -N_m(r, \theta) \end{bmatrix} \quad (19)$$

Therefore, the virtual work term in the axial initial stress field can be transformed into:

$$\int_{V_j} \delta e_2^T \sigma_0^z dV = \delta \bar{U}^j \int_{V_j} k^2 (N^{T*} N) \sigma_0^z dV \bar{U}^j \quad (20)$$

Then, the effect of the differential operator just cancels out, and finally, the matrix of element initial stress has:

$$k_0 = \int_{\Omega_j} N^{T*} \sigma_0^z N d\Omega_j \quad (21)$$

Generally, the axial force is assumed to be evenly distributed across the steel wire cross-section. Therefore, the $\sigma_0^z = \sigma_0^z = P/A$ element initial stress matrix and the element mass matrix have the same form, namely:

$$k_0 = \frac{\sigma_0^z}{\rho} m \quad (22)$$

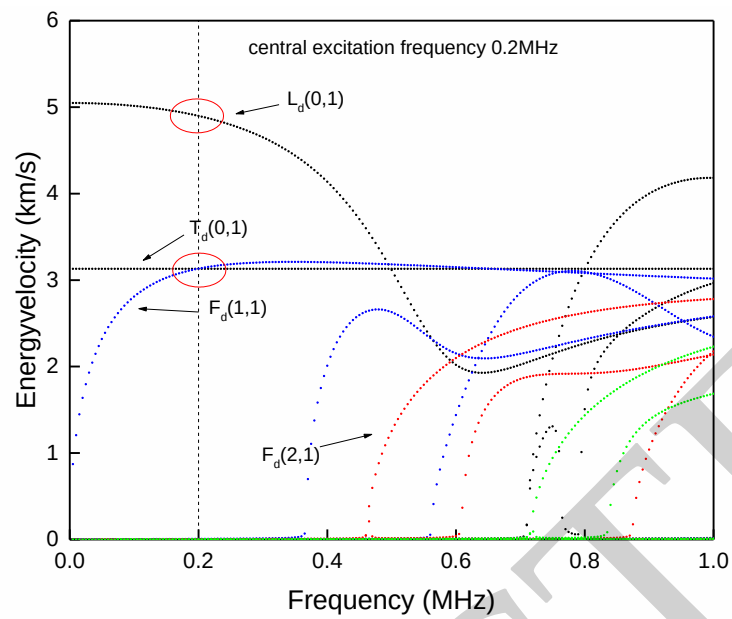
Finally, the semi-analytical frequency equation containing the initial stress matrix has [21]:

$$[K_1 + kK_2 + k^2(K_3 + K_0) - \omega^2 M]_M U = 0 \quad (23)$$

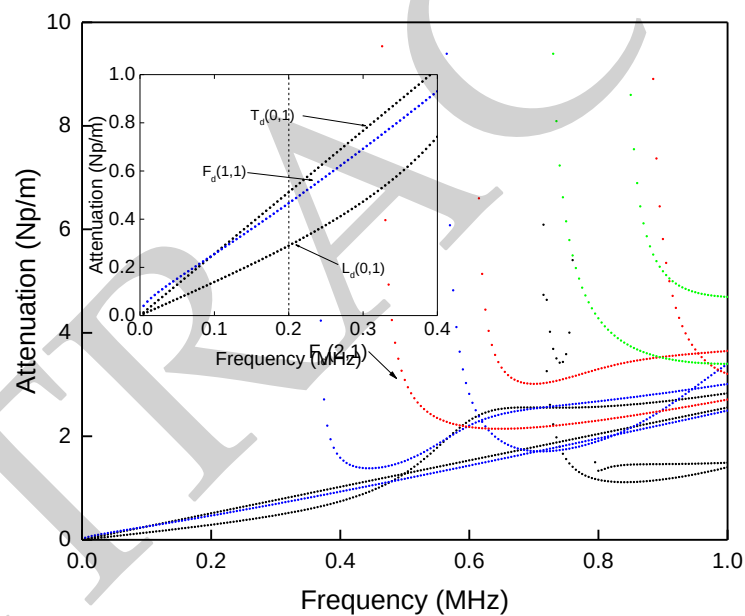
where K_0 is the overall initial stress matrix. It can be seen that K_0 is the modification of K_3 matrix.

Numerical Investigation

The external excitation unit force load is given on the wire cross-section's radial center node along the z-direction. The narrowband excitation force illustrating the tone burst excitation with a center frequency of 0.2 MHz is applied to obtain the corresponding SAFE results for steel wire under a viscoelastic condition. The energy velocity and attenuation dispersion curves are illustrated in Figure 15. The influence of tensile stress on energy velocity and attenuation is discussed in a detailed manner. The ultimate tensile stress (UTS) of high-strength steel wire used in actual engineering is 1860 MPa, and the stress on the cable is generally 0.3~0.4 of the UTS. The comparative analysis of initial stress uses 0.0, 0.2, 0.4, 0.6, and 0.8 times the UTS values to explore the effect of stress on wave propagation characteristics. Since the torsional mode occupies a small part of the AE signal, only the longitudinal and bending wave modes are considered. Figure 16a–d shows the variation curves of energy velocities, ΔC_e and attenuation, ΔAtt of $L_d(0, m)$ and $F_d(n, 1)$ modes with frequency under the four initial tensile stress conditions. A high initial tensile stress can increase the stiffness of the system (in this case, increase the corresponding stiffness of the K_3 matrix), thereby increasing the energy velocity and reducing the attenuation. However, this effect only occurs in relatively high-frequency bands, generally higher than the cut-off frequency of each mode, as shown by the dotted line in Figure 16. For modes in the low-frequency region that contain high attenuation factors, even if the attenuation factor decreases with the increasing tensile stress, the amount of energy velocity change may still be negative, such as 0–0.5 MHz in $L_d(0, 2)$ mode or 0–0.4 MHz in $F_d(2, 1)$ mode. The sharply concave part of the energy change curve or the attenuation factor's sharply protruding peak represents the energy curve's transition area. In this area, the energy velocity rapidly increases from the frequency axis to a specific maximum value.



(a) Energy velocity dispersion curves.



(b) Attenuation curve.

Figure 15. SAFE calculation results on a viscoelastic steel wire for narrowband tone burst excitation: (a) Energy velocity dispersion curves; (b) Attenuation curve.

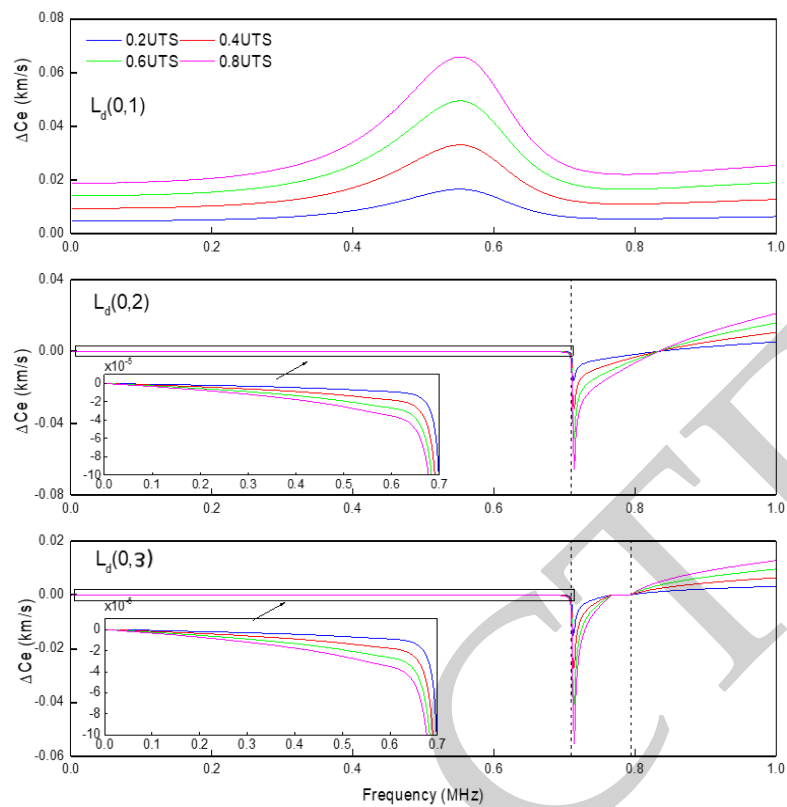
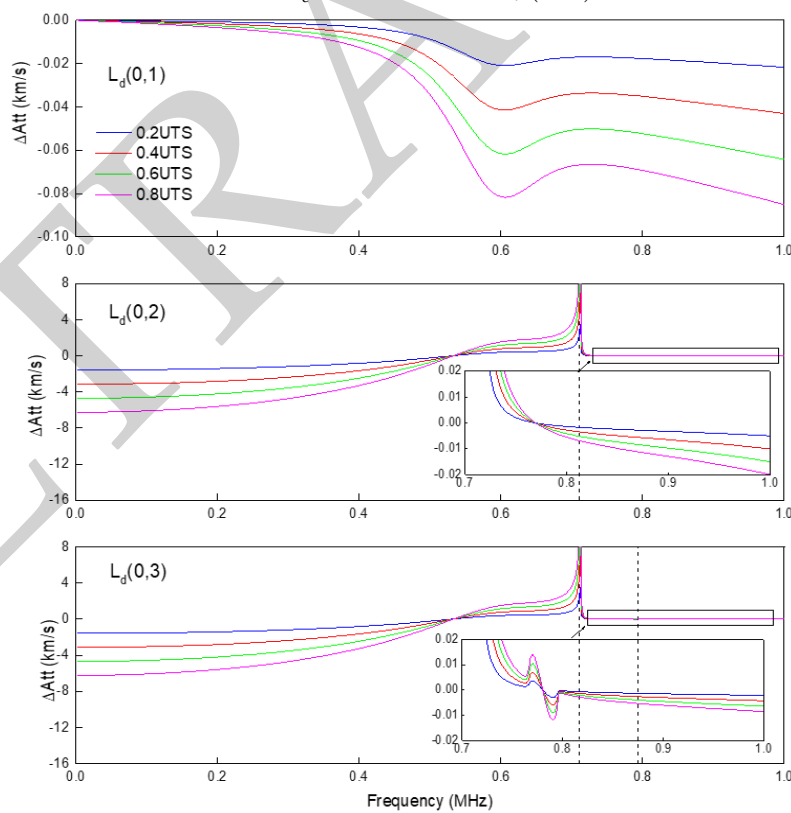
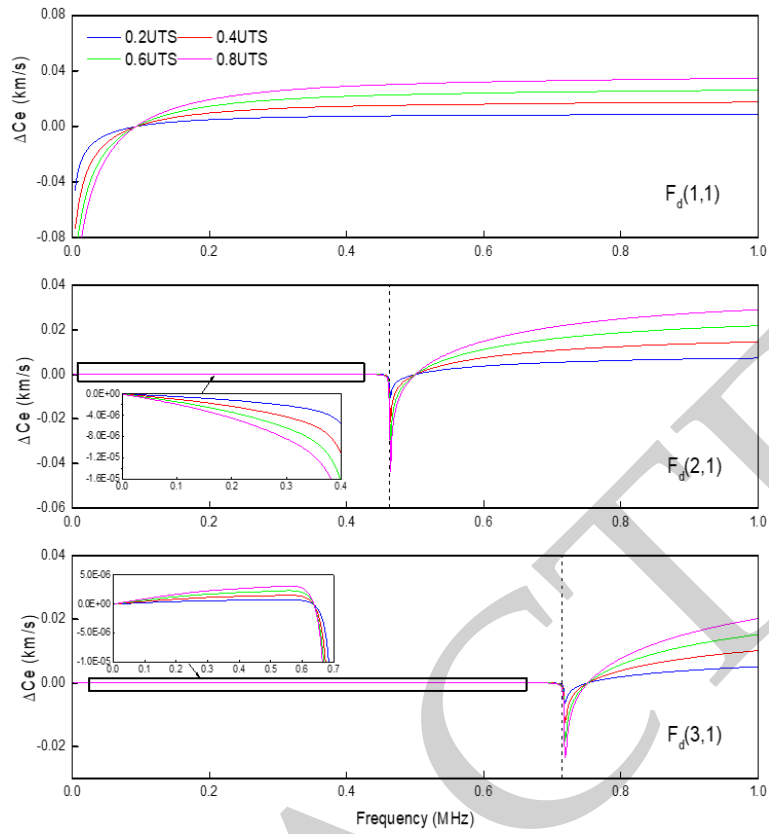
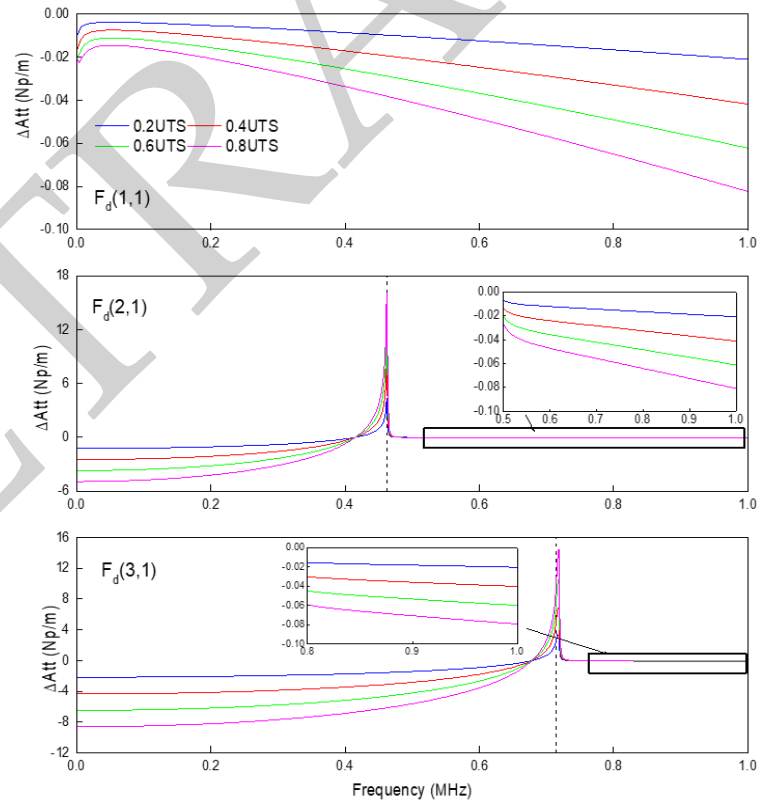
(a) ΔC_e variation for the $L_d(0,m)$ mode.(b) ΔAtt variation for $L_d(0,m)$ mode.

Figure 16. Cont.



(c) ΔC_e variation for $F_d(n,1)$ mode.



(d) ΔAtt variation for $F_d(n,1)$ mode.

Figure 16. Influence of initial tensile stress on energy velocity and attenuation: (a) ΔC_e variation for the $L_d(0,m)$ mode; (b) ΔAtt variation for $L_d(0,m)$ mode; (c) ΔC_e variation for $F_d(n,1)$ mode; (d) ΔAtt variation for $F_d(n,1)$ mode.

Fortunately, from a practical point of view, only those quasi-propagating modal initial tension forces have a clear and reasonable effect on them, which is worthy of mentioning. Figure 16 shows that the impact of initial tensile stress on energy velocity or attenuation is monotonous; i.e., they continue to increase or decrease as the stress level increases. This trend is still approximately linear because, at each frequency point, the interval of the target change amount under the four stress levels is the same, but this linear factor itself changes with frequency. Acoustoelastic constants can quantify this effect as it depends only on the frequency. It can be defined as:

$$S_{C_e}(f) = \left(\frac{C_e(f,\sigma) - C_e(f,0)}{C_e(f,0)\sigma} \right) \quad S_{Att}(f) = \left(\frac{Att(f,\sigma) - Att(f,0)}{Att(f,0)\sigma} \right) \quad (24)$$

This phenomenon was also verified through experiments, and similar conclusions were obtained by Chaki and Bourse [26]. Figure 17 shows that acoustoelastic curves are stable and smooth at higher frequencies, and spikes appear near the cut-off frequency. The steel wire exhibits an “anomalous” acoustoelastic behavior at low-stress levels (below 20% UTS), with group velocity increasing with stress. However, above 20% UTS, the rate of change of the relative group velocity with stress was measured. At larger stress levels that include typical service stresses for cable stays, however, the strands exhibit an acoustoelastic trend similar to that of the single wires in a relatively stress measurement. It could be argued that the strange behavior of the wire at low-stress levels is due to the existing manufacture-induced residual stress state.

5. Modal Selection for AE Monitoring

The primary issue comprised in AE monitoring is the attenuation of the acoustic signals. As it carries less energy, it gets mixed with noise, which causes significant difficulties in subsequent signal processing steps. Some modes with less attenuation should be suitable for AE monitoring. Besides, the modes that are susceptible to interference from surrounding steel wires in actual cables are also challenging to identify. On the one hand, energy is transferred to the adjacent steel wire through the relative movement of the steel wire that occurs on the steel wire's surface, similar to attenuation. On the other hand, the signal caused by friction and collision between the steel wires will also be continuously introduced into the system during the wave propagation so that the AE signal may be contaminated. Therefore, the selection of modes applicable to AE monitoring should follow the two low attenuation points and small external surface vibration. The only possibility is a longitudinal wave mode, as it has simple modal forms and a limited number of bending modes. Figure 18 shows the dispersion curve of the longitudinal wave mode up to 5 MHz. The red dots in Figure 18 are the maximum values in some energy velocity curves and their corresponding minimum values in attenuation. The relevant longitudinal wave modes, frequencies, and energy velocity values are listed in Figure 19. Obviously, for the $L_d(0,2)$, $L_d(0,3)$, $L_d(0,4)$, $L_d(0,5)$, $L_d(0,6)$, $L_d(0,7)$ modes, a significant vibration occurs inside the cross-section of the wire, but the part near the wire surface is relatively small. The figure illustrates the displacement path of radial response, U_r and axial response, U_z , respectively. Similar conclusions are also obtained in the computational simulation of the slab waveguide section [32].

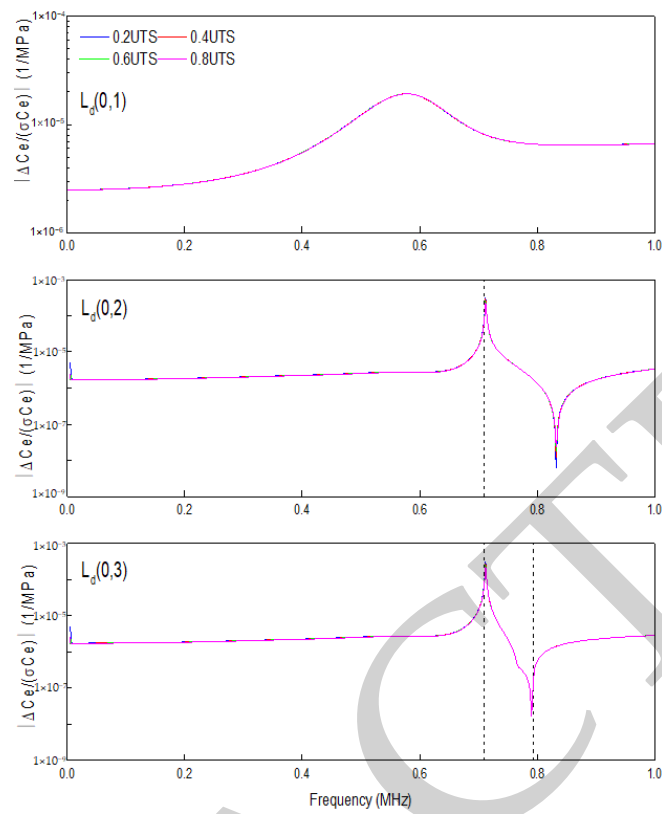
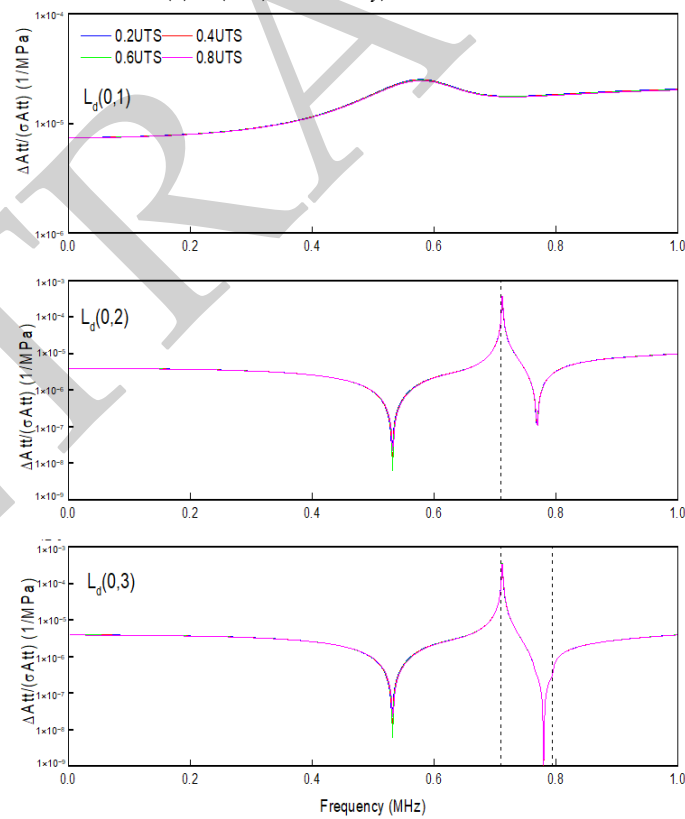
(a) $L_d(0,m)$ mode $S_{Ce}(f)$ absolute value.(b) $L_d(0,m)$ mode $S_{Att}(f)$ absolute value.

Figure 17. Cont.

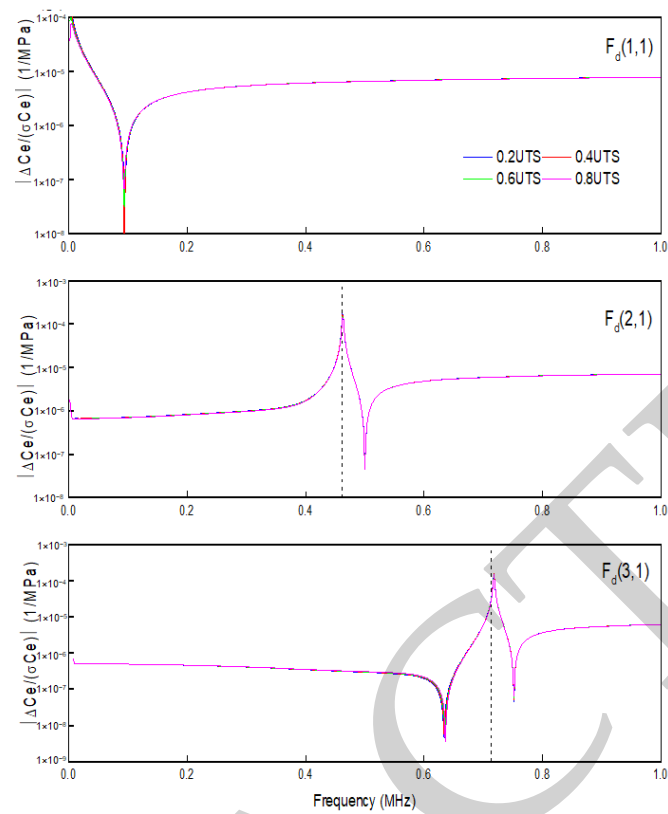
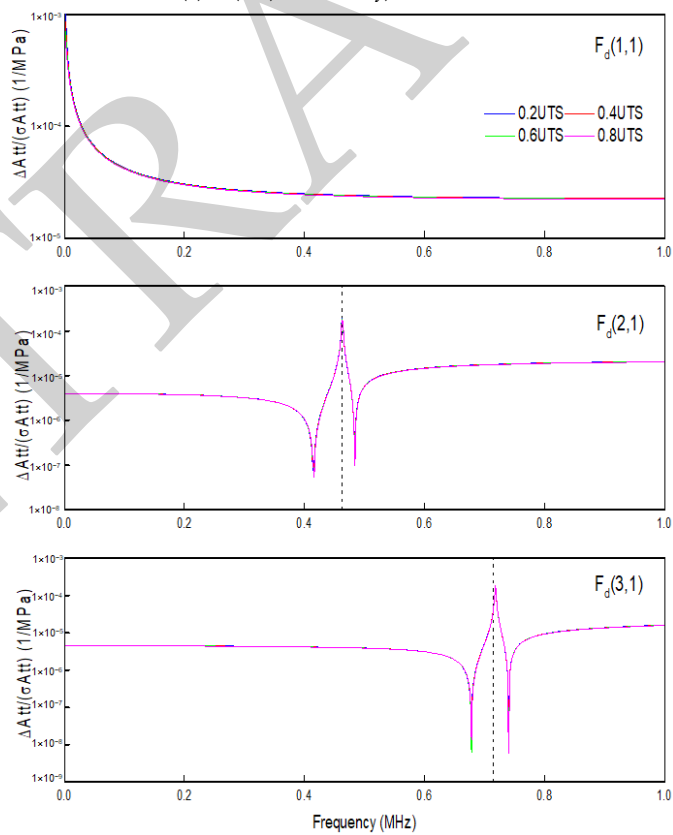
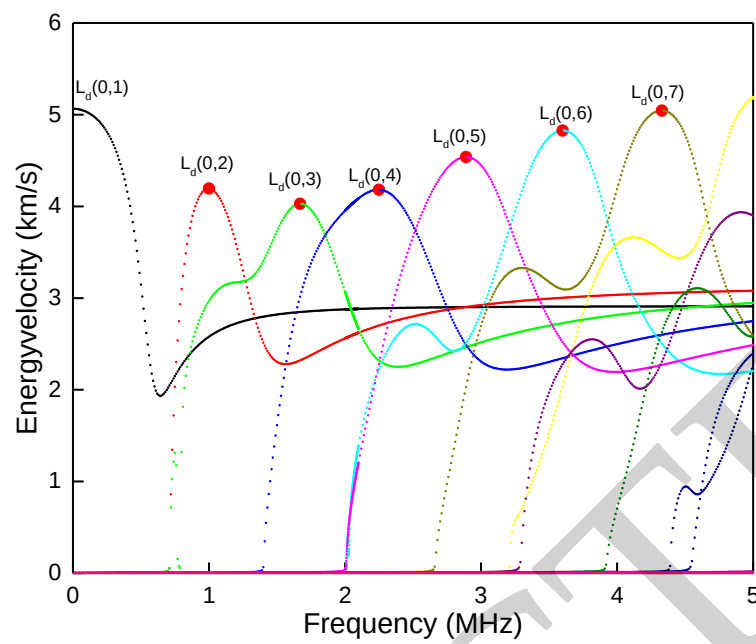
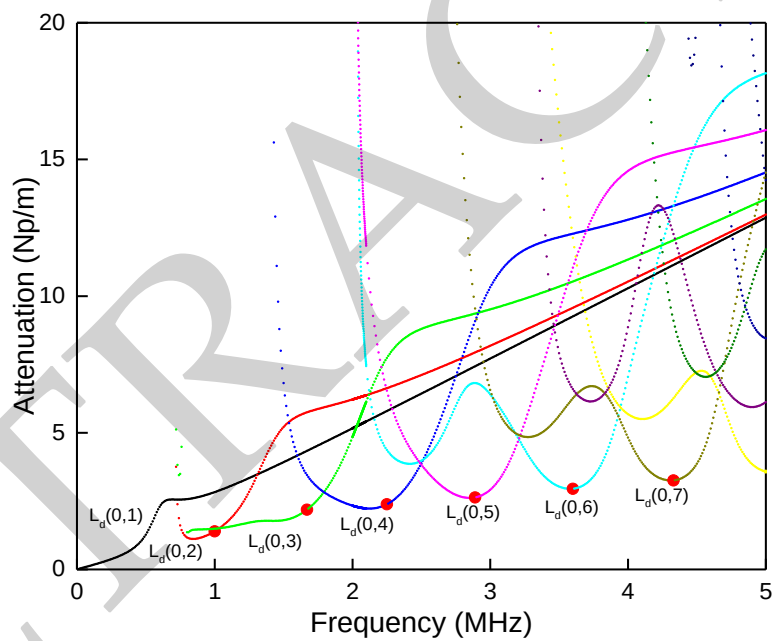
(c) $F_d(n,1)$ mode $S_{Ce}(f)$ absolute value.(d) $F_d(n,1)$ mode $S_{Att}(f)$ absolute value.

Figure 17. Acoustoelastic constant curves: (a) $L_d(0,m)$ mode $S_{Ce}(f)$ absolute value; (b) $L_d(0,m)$ mode $S_{Att}(f)$ absolute value; (c) $F_d(n,1)$ mode $S_{Ce}(f)$ absolute value; (d) $F_d(n,1)$ mode $S_{Att}(f)$ absolute value.



(a) Energy velocity curve.



(b) Attenuation curve.

Figure 18. Longitudinal mode dispersion curve for the damped waveguide: (a) Energy velocity curve; (b) Attenuation curve.

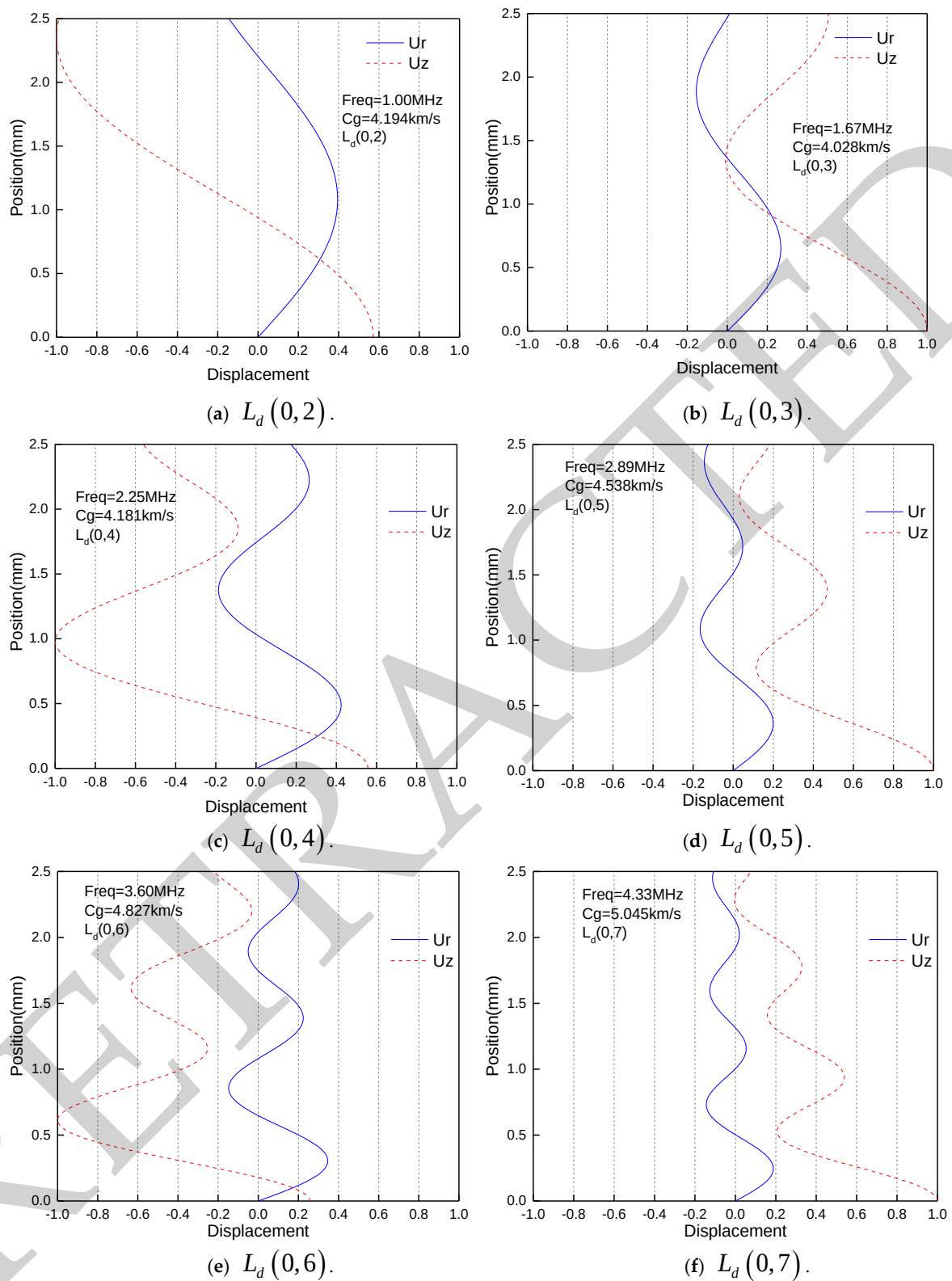


Figure 19. Longitudinal mode at a maximum energy velocity for the damped waveguide: (a) $L_d(0,2)$; (b) $L_d(0,3)$; (c) $L_d(0,4)$; (d) $L_d(0,5)$; (e) $L_d(0,6)$; (f) $L_d(0,7)$.

6. Conclusions

In this paper, the author presents the development and results of a method to calculate the characteristics of guided waves in a wire, with NDT and AE monitoring applications. The work includes the possibility of material damping in the waveguide and also of pre-stress. The axisymmetric SAFE method is used to study wave properties of a cylindrical waveguide, especially a high-strength steel wire in a bridge cable/transmission line conductor. This study considers the impact of two common factors, structural damping, and initial tensile stress, on the propagation characteristics. The following discussions are derived from the presented work:

- Each curve will extend downward from a cut-off frequency point to zero frequency without considering the structural damping. This part of the curve has a complex wavenumber, the imaginary part of which is the attenuation, and the real part still represents the fluctuation of space.
- By considering structural damping, the wavenumber at any point on the curve is complex, and modal curves are separated in space, which is easy to distinguish.
- Due to the complex nature of wavenumbers, the original definition of group velocity in undamped conditions is no longer practical.
- The energy velocity above the cut-off frequency is consistent with the group velocity without damping, and the portion below the cut-off frequency is almost zero. Contrary to the energy velocity, the attenuation below the cut-off frequency is substantial, indicating that the wave mode (evanescent wave) of this part cannot propagate over long distances and only exists near the excitation source. The attenuation factor above the cut-off frequency is small, reflecting its propagation phenomenon. Generally, the maximum value of the energy velocity curve corresponds to the attenuation curve's minimum value. The high-frequency mode of the same circumferential order mode will have a slightly higher attenuation.
- The intensity of the Poynting vector flowing in the cross-section is significant for each damped mode, and the attenuation factor is more significant at the higher frequency value of that particular mode.
- Finally, the influence of initial tensile stress on the energy velocity and attenuation factor is considered. The initial tensile stress can be calculated and analyzed by the semi-analytical stiffness matrix in a geometric stiffness matrix.
- There is a considerable initial tensile stress in the bridge cable's steel wire in the practical scenario. Without considering the effects of other stress fields and other deformations, the 0.2, 0.4, 0.6, and 0.8 times UTS are analyzed for the effect of initial stress conditions. It can be found that for propagating waves above the cut-off frequency, the initial tensile stress can slightly increase the energy velocity and reduce the attenuation factor. This effect is linear (acoustoelastic constant) at each frequency point, but this law is not evident for evanescent waves.
- In practical applications, since this effect has little influence on the propagation of a single wire, it can be ignored. The longitudinal wave modes considered in the high-frequency region are suitable for AE monitoring as it has a low attenuation factor and relatively small external surface vibration.
- The proposed formulation for analyzing the pre-stress field in the viscoelastic waveguide showed a possible way for guided wave-based NDT and health monitoring applications for pre-stressed bridge cables or overhead transmission line conductors. The author concludes that this study can help select a suitable mode with low attenuation characteristics that may be useful for monitoring AE events.

Funding: This research received no external funding.

Conflicts of Interest: The author declares no conflict of interest.

Appendix A

The displacement field function in the finite element format can be written as:

$$\mathbf{u}^j = \begin{bmatrix} N_1(r, \theta) & N_2(r, \theta) & N_3(r, \theta) \end{bmatrix} \begin{bmatrix} \bar{\mathbf{u}}_1^j \\ \bar{\mathbf{u}}_2^j \\ \bar{\mathbf{u}}_3^j \end{bmatrix} \exp(ikz - i\omega t) \quad (\text{A1})$$

where the interpolation function matrix $\mathbf{N}_m(r, \theta)$ is:

$$\mathbf{N}_m(r, \theta) = \begin{bmatrix} N_m(r) \cos(n\theta) & & \\ & N_m(r) \sin(n\theta) & \\ & & iN_m(r) \cos(n\theta) \end{bmatrix} \quad (\text{A2})$$

For any of the interpolation functions $N_m(r)$, a 3-point Lagrange interpolation function is used. The corresponding node displacement vector is:

$$\bar{\mathbf{u}}_m^j = \begin{bmatrix} u_{rm} & u_{\theta m} & u_{zm} \end{bmatrix}^T \quad (\text{A3})$$

Finally, the element strain vector can be derived as:

$$\boldsymbol{\varepsilon}^j = \begin{bmatrix} B_1 & B_2 & B_3 \end{bmatrix} \bar{\mathbf{u}}^j \exp(ikz - i\omega t) \quad (\text{A4})$$

Accordingly, the matrix, $\mathbf{B} = \begin{bmatrix} B_1 & B_2 & B_3 \end{bmatrix}$ can also be expressed as follows:

$$\mathbf{B} = \begin{bmatrix} b_{11} & b_{21} & b_{31} \end{bmatrix} \cos(n\theta) + k \begin{bmatrix} b_{12} & b_{22} & b_{32} \end{bmatrix} \cos(n\theta) + \begin{bmatrix} b_{13} & b_{23} & b_{33} \end{bmatrix} \sin(n\theta) + k \begin{bmatrix} b_{14} & b_{24} & b_{34} \end{bmatrix} \sin(n\theta) \quad (\text{A5})$$

The element stiffness matrix can be obtained by integrating over the cross-sectional domain:

$$\mathbf{k}^j = \int_0^{2\pi} \int_{R_j} \mathbf{B}^T \mathbf{D} \mathbf{B} r dr d\theta \quad (\text{A6})$$

where R_j in the integration domain represents the radial integration interval. The final element stiffness matrix is expressed as:

$$\mathbf{k}^j = \int_0^{2\pi} \int_{R_j} \mathbf{B}^T \mathbf{D} \mathbf{B} r dr d\theta = \mathbf{k}_1^j + k \mathbf{k}_2^j + k^2 \mathbf{k}_3^j \quad (\text{A7})$$

Similarly, the element mass matrix is calculated as:

$$\mathbf{m}^j = \int_0^{2\pi} \int_{R_j} \mathbf{N}^T \rho \mathbf{N} r dr d\theta \quad (\text{A8})$$

$$\mathbf{N}_m(r, \theta) = \mathbf{n}_{m1} \cos(n\theta) + \mathbf{n}_{m2} \sin(n\theta)$$

$$\mathbf{n}_{m1} = \begin{bmatrix} N_m & & \\ & 0 & \\ & & iN_m \end{bmatrix} \quad \mathbf{n}_{m2} = \begin{bmatrix} 0 & & \\ & N_m & \\ & & 0 \end{bmatrix} \quad (\text{A9})$$

The final element mass matrix can be shown as:

$$m^j = \int_0^{2\pi} \int_{R_j} N^T \rho N r dr d\theta = \pi \int_{R_j} \left\{ \begin{bmatrix} n_{11} & n_{21} & n_{31} \end{bmatrix}^T \rho \begin{bmatrix} n_{11} & n_{21} & n_{31} \end{bmatrix} + \begin{bmatrix} n_{12} & n_{22} & n_{32} \end{bmatrix}^T \rho \begin{bmatrix} n_{12} & n_{22} & n_{32} \end{bmatrix} \right\} r dr \quad (A10)$$

For the longitudinal wave mode, since its displacement field no longer contains a circumferential component, its vector can be simplified as:

$$\mathbf{u} = \begin{bmatrix} u_r & u_z \end{bmatrix}^T \quad (A11)$$

The degree of freedom is reduced from 3 to 2 on each node. For the torsional wave mode, there is only a circumferential displacement component, which can be further simplified to obtain the following:

$$\mathbf{u} = u_\theta \quad (A12)$$

Each node has only one degree of freedom. Considering the displacement field function, the strain vector has only two elements: $\varepsilon_{r\theta}$ and $\varepsilon_{\theta z}$. Accordingly, the shear stresses $\tau_{r\theta}$ and $\tau_{\theta z}$ are the only elements in the stress vector. Hence, the strain-stress relationship becomes:

$$\begin{bmatrix} \tau_{r\theta} \\ \tau_{\theta z} \end{bmatrix} = \mathbf{D} \begin{bmatrix} \varepsilon_{r\theta} \\ \varepsilon_{\theta z} \end{bmatrix} \quad (A13)$$

$$\mathbf{D} = \begin{bmatrix} \frac{E}{2(1+\nu)} & 0 \\ 0 & \frac{E}{2(1+\nu)} \end{bmatrix} \quad (A14)$$

where E is the elastic modulus of the material, and ν is Poisson's ratio. Consequently, the element stiffness and mass matrices are derived using Equations (A7)–(A10) for longitudinal and torsional wave modes.

References

1. Saravanan, T.J.; Gopalakrishnan, N.; Rao, N.P. Damage detection in structural element through propagating waves using radially weighted and factored RMS. *Measurement* **2015**, *73*, 520–538. [\[CrossRef\]](#)
2. Kumar, K.V.; Saravanan, T.J.; Sreekala, R.; Gopalakrishnan, N.; Mini, K.M. Structural damage detection through longitudinal wave propagation using spectral finite element method. *Geomech. Eng.* **2017**, *12*, 161–183. [\[CrossRef\]](#)
3. Achenbach, J. *Wave Propagation in Elastic Solids*; Elsevier: Amsterdam, The Netherlands, 2012.
4. Saravanan, T.J.; Gopalakrishnan, N.; Rao, N.P. Detection of damage through coupled axial–flexural wave interactions in a sagged rod using the spectral finite element method. *J. Vib. Control* **2017**, *23*, 3345–3364. [\[CrossRef\]](#)
5. Saravanan, T.J.; Gopalakrishnan, N.; Rao, N.P. Experiments on coupled axial–flexural wave propagation in a sagged rod with structural discontinuity using piezoelectric transducers. *J. Vib. Control* **2018**, *24*, 2717–2731. [\[CrossRef\]](#)
6. Armenàkas, A.E.; Gazis, D.C.; Herrmann, G. *Free Vibrations of Circular Cylindrical Shells*; Pergamon: Oxford, UK, 1969.
7. Saravanan, T.J. Investigation of guided wave dispersion characteristics for fundamental modes in an axisymmetric cylindrical waveguide using rooting strategy approach. *Mech. Adv. Mater. Struct.* **2020**, 1–11. [\[CrossRef\]](#)
8. Lowe, M.J. Matrix techniques for modeling ultrasonic waves in multilayered media. *IEEE Trans. Ultrason. Ferroelectr. Freq. Control* **1995**, *42*, 525–542. [\[CrossRef\]](#)
9. Nelson, R.B.; Dong, S.B.; Kalra, R.D. Vibrations and waves in laminated orthotropic circular cylinders. *J. Sound Vib.* **1971**, *18*, 429–444. [\[CrossRef\]](#)

10. Mace, B.R.; Duhamel, D.; Brennan, M.J.; Hinke, L. Finite element prediction of wave motion in structural waveguides. *J. Acoust. Soc. Am.* **2005**, *117*, 2835–2843. [[CrossRef](#)]
11. Serey, V.; Quaegebeur, N.; Micheau, P.; Masson, P.; Castaings, M.; Renier, M. Selective generation of ultrasonic guided waves in a bi-dimensional waveguide. *Struct. Health Monit.* **2019**, *18*, 1324–1336. [[CrossRef](#)]
12. Hayashi, T.; Song, W.J.; Rose, J.L. Guided wave dispersion curves for a bar with an arbitrary cross-section a rod and rail example. *Ultrasonics* **2003**, *41*, 175–183. [[CrossRef](#)]
13. Hayashi, T.; Tamayama, C.; Murase, M. Wave structure analysis of guided waves in a bar with an arbitrary cross-section. *Ultrasonics* **2006**, *44*, 17–24. [[CrossRef](#)] [[PubMed](#)]
14. Bartoli, I.; Marzani, A.; Di Scalea, F.L.; Viola, E. Modeling wave propagation in damped waveguides of arbitrary cross-section. *J. Sound Vib.* **2006**, *295*, 685–707. [[CrossRef](#)]
15. Damljanović, V.; Weaver, R.L. Propagating and evanescent elastic waves in cylindrical waveguides of arbitrary cross section. *J. Acoust. Soc. Am.* **2004**, *115*, 1572–1581. [[CrossRef](#)]
16. Shorter, P.J. Wave propagation and damping in linear viscoelastic laminates. *J. Acoust. Soc. Am.* **2004**, *115*, 1917–1925. [[CrossRef](#)]
17. Galán, J.M.; Abascal, R. Numerical simulation of Lamb wave scattering in semi-infinite plates. *Int. J. Numer. Methods Eng.* **2002**, *53*, 1145–1173. [[CrossRef](#)]
18. Mei, H.; Giurgiutiu, V. Guided wave excitation and propagation in damped composite plates. *Struct. Health Monit.* **2019**, *18*, 690–714. [[CrossRef](#)]
19. Li, L.; Haider, M.F.; Mei, H.; Giurgiutiu, V.; Xia, Y. Theoretical calculation of circular-crested Lamb wave field in single-and multi-layer isotropic plates using the normal mode expansion method. *Struct. Health Monit.* **2020**, *19*, 357–372. [[CrossRef](#)]
20. Marzani, A.; Viola, E.; Bartoli, I.; Di Scalea, F.L.; Rizzo, P. A semi-analytical finite element formulation for modeling stress wave propagation in axisymmetric damped waveguides. *J. Sound Vib.* **2008**, *318*, 488–505. [[CrossRef](#)]
21. Mazzotti, M.; Marzani, A.; Bartoli, I.; Viola, E. Guided waves dispersion analysis for pre-stressed viscoelastic waveguides by means of the SAFE method. *Int. J. Solids Struct.* **2012**, *49*, 2359–2372. [[CrossRef](#)]
22. Mu, J.; Rose, J.L. Guided wave propagation and mode differentiation in hollow cylinders with viscoelastic coatings. *J. Acoust. Soc. Am.* **2008**, *124*, 866–874. [[CrossRef](#)]
23. Gavrić, L. Computation of propagative waves in free rail using a finite element technique. *J. Sound Vib.* **1995**, *185*, 531–543. [[CrossRef](#)]
24. Loveday, P.W. Semi-analytical finite element analysis of elastic waveguides subjected to axial loads. *Ultrasonics* **2009**, *49*, 298–300. [[CrossRef](#)]
25. Chen, F.; Wilcox, P.D. The effect of load on guided wave propagation. *Ultrasonics* **2007**, *47*, 111–122. [[CrossRef](#)]
26. Chaki, S.; Bourse, G. Guided ultrasonic waves for non-destructive monitoring of the stress levels in pre-stressed steel strands. *Ultrasonics* **2009**, *49*, 162–171. [[CrossRef](#)] [[PubMed](#)]
27. Treysède, F. Elastic waves in helical waveguides. *Wave Motion* **2008**, *45*, 457–470. [[CrossRef](#)]
28. Treysède, F. Numerical investigation of elastic modes of propagation in helical waveguides. *J. Acoust. Soc. Am.* **2007**, *121*, 3398–3408. [[CrossRef](#)]
29. Saravanan, T.J. Convergence study on ultrasonic guided wave propagation modes in an axisymmetric cylindrical waveguide. *Mech. Adv. Mater. Struct.* **2020**, *1*–18. [[CrossRef](#)]
30. Biot, M.A. General theorems on the equivalence of group velocity and energy transport. *Phys. Rev.* **1957**, *105*, 1129. [[CrossRef](#)]
31. Quintanilla, F.H.; Lowe, M.J.S.; Craster, R.V. Full 3D dispersion curve solutions for guided waves in generally anisotropic media. *J. Sound Vib.* **2016**, *363*, 545–559. [[CrossRef](#)]
32. Pavlakovic, B.N.; Lowe, M.J.S.; Cawley, P. High-frequency low-loss ultrasonic modes in imbedded bars. *J. Appl. Mech.* **2001**, *68*, 67–75. [[CrossRef](#)]

Publisher’s Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



© 2020 by the author. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).