



# Elucidating the Photocatalytic Behavior of TiO<sub>2</sub>-SnS<sub>2</sub> Composites Based on Their Energy Band Structure

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11**Table S1.** FFD matrix for removal (M1) and conversion (M2) of diclofenac by solar/TiO2-SnS2-COMM12process after 60 min exposure.

|      | Vari  | ables | Experime | ntal results | Respo              | onse, Y               |
|------|-------|-------|----------|--------------|--------------------|-----------------------|
| Exp. | $X_1$ | $X_3$ | ΔDO      | CF, %        | $Y_1$              | Y2                    |
| #    | coded | coded | removal  | conversion   | ΔDCF, %<br>removal | ΔDCF, %<br>conversion |
| 1    | -1    | -1    | 68.68    | 53.89        | 72.61              | 57.63                 |
| 2    | 0     | -1    | 12.89    | 11.27        | 6.84               | 5.41                  |
| 3    | 1     | -1    | 2.01     | 1.36         | 4.14               | 3.47                  |
| 4    | -1    | 0     | 80.98    | 66.06        | 78.06              | 63.40                 |
| 5    | 0     | 0     | 6.42     | 5.34         | 8.68               | 7.40                  |
| 6    | 1     | 0     | 1.71     | 1.07         | 2.38               | 1.67                  |
| 7    | -1    | 1     | 82.18    | 68.10        | 81.17              | 67.02                 |
| 8    | 0     | 1     | 4.39     | 3.44         | 8.19               | 7.24                  |
| 9    | 1     | 1     | 1.07     | 0.44         | -1.73              | -2.27                 |

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**Table S2.** BBD matrix for removal (M3) and conversion (M4) of diclofenac by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-COMM/H<sub>2</sub>O<sub>2</sub> process after 60 min exposure.

|      | Variables |       |       | Experime  | ntal results | Respo                   | Response, Y             |  |  |
|------|-----------|-------|-------|-----------|--------------|-------------------------|-------------------------|--|--|
| Exp. | $X_1$     | $X_2$ | $X_3$ | ΔD        | CF, %        | $Y_1$                   | $Y_2$                   |  |  |
| #    | andad     | andod | andod | nom orral | convion      | $\Delta \text{DCF}$ , % | $\Delta \text{DCF}$ , % |  |  |
|      | coded     | coueu | coueu | removal   | conversion   | removal                 | conversion              |  |  |
| 1    | -1        | -1    | 0     | 79.41     | 68.04        | 77.37                   | 64.93                   |  |  |
| 2    | 1         | -1    | 0     | 1.80      | 1.17         | 5.26                    | 6.50                    |  |  |
| 3    | -1        | 1     | 0     | 90.11     | 85.78        | 86.65                   | 80.44                   |  |  |
| 4    | 1         | 1     | 0     | 3.19      | 2.93         | 5.23                    | 6.05                    |  |  |
| 5    | -1        | 0     | -1    | 71.99     | 56.34        | 76.50                   | 63.47                   |  |  |
| 6    | 1         | 0     | -1    | 5.13      | 4.92         | 4.14                    | 3.61                    |  |  |
| 7    | -1        | 0     | 1     | 78.05     | 66.77        | 79.04                   | 68.08                   |  |  |
| 8    | 1         | 0     | 1     | 2.37      | 2.26         | -2.13                   | -4.87                   |  |  |
| 9    | 0         | -1    | -1    | 11.45     | 11.27        | 8.98                    | 7.25                    |  |  |
| 10   | 0         | 1     | -1    | 15.56     | 15.31        | 14.52                   | 13.51                   |  |  |
| 11   | 0         | -1    | 1     | 6.99      | 2.24         | 8.03                    | 4.04                    |  |  |
| 12   | 0         | 1     | 1     | 9.27      | 8.82         | 11.74                   | 12.84                   |  |  |
| 13   | 0         | 0     | 0     | 6.64      | 4.55         | 6.65                    | 4.55                    |  |  |
| 14   | 0         | 0     | 0     | 6.64      | 4.52         | 6.65                    | 4.55                    |  |  |
| 15   | 0         | 0     | 0     | 6.66      | 4.58         | 6.65                    | 4.55                    |  |  |

|      | Vari  | ables | Experime | ntal results | Response, Y      |                       |  |
|------|-------|-------|----------|--------------|------------------|-----------------------|--|
| Exp. | $X_1$ | $X_3$ | ΔDO      | CF, %        | $Y_1$            | <b>Y</b> <sub>2</sub> |  |
| #    | codod | coded | romoval  | conversion   | $\Delta DCF$ , % | $\Delta DCF$ , %      |  |
|      | coueu | coueu | Temoval  | conversion   | removal          | conversion            |  |
| 1    | -1    | -1    | 71.78    | 58.26        | 69.18            | 58.85                 |  |
| 2    | 0     | -1    | 48.04    | 45.00        | 54.95            | 45.73                 |  |
| 3    | 1     | -1    | 9.98     | 8.33         | 5.67             | 7.01                  |  |
| 4    | -1    | 0     | 88.04    | 75.35        | 87.79            | 73.56                 |  |
| 5    | 0     | 0     | 73.47    | 57.70        | 70.56            | 57.44                 |  |
| 6    | 1     | 0     | 15.11    | 13.67        | 18.28            | 15.71                 |  |
| 7    | -1    | 1     | 89.71    | 76.21        | 92.56            | 77.41                 |  |
| 8    | 0     | 1     | 76.32    | 58.76        | 72.33            | 58.28                 |  |
| 9    | 1     | 1     | 15.93    | 14.27        | 17.07            | 13.55                 |  |

15**Table S3.** FFD matrix for removal (M4) and conversion (M5) of diclofenac by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT16process after 60 min exposure.

**Table S4.** BBD matrix for removal (M7) and conversion (M8) of diclofenac by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT/H<sub>2</sub>O<sub>2</sub> process after 60 min exposure.

|      |        | Variables   |        | Experime | ntal results | Response, Y             |            |  |
|------|--------|-------------|--------|----------|--------------|-------------------------|------------|--|
| Exp. | $X_1$  | $X_1$ $X_2$ |        | ΔD       | CF, %        | $Y_1$                   | $\gamma_2$ |  |
| #    | لممامم | لملمه       | لممامم |          |              | $\Delta \text{DCF}$ , % | ΔDCF, %    |  |
|      | coded  | coded       | coded  | removal  | conversion   | removal                 | conversion |  |
| 1    | -1     | -1          | 0      | 91.50    | 82.29        | 95.15                   | 79.54      |  |
| 2    | 1      | -1          | 0      | 10.73    | 7.94         | 8.15                    | 7.30       |  |
| 3    | -1     | 1           | 0      | 94.57    | 91.02        | 97.15                   | 91.66      |  |
| 4    | 1      | 1           | 0      | 41.40    | 16.52        | 37.74                   | 19.27      |  |
| 5    | -1     | 0           | -1     | 89.40    | 69.85        | 84.86                   | 70.07      |  |
| 6    | 1      | 0           | -1     | 12.82    | 7.57         | 14.51                   | 5.68       |  |
| 7    | -1     | 0           | 1      | 91.02    | 79.89        | 89.33                   | 81.78      |  |
| 8    | 1      | 0           | 1      | 8.73     | 1.77         | 13.27                   | 1.54       |  |
| 9    | 0      | -1          | -1     | 37.53    | 24.54        | 38.42                   | 27.07      |  |
| 10   | 0      | 1           | -1     | 50.98    | 41.23        | 52.94                   | 40.36      |  |
| 11   | 0      | -1          | 1      | 40.73    | 31.23        | 38.77                   | 32.10      |  |
| 12   | 0      | 1           | 1      | 56.71    | 45.43        | 55.82                   | 42.90      |  |
| 13   | 0      | 0           | 0      | 53.33    | 39.38        | 53.47                   | 39.70      |  |
| 14   | 0      | 0           | 0      | 53.32    | 39.44        | 53.47                   | 39.70      |  |
| 15   | 0      | 0           | 0      | 53.77    | 40.28        | 53.47                   | 39.70      |  |

<sup>19</sup> 

Table S5. Specific surface area of constituents of studied TiO<sub>2</sub>-SnS<sub>2</sub> composites.

| Material             | BET surface area, m <sup>2</sup> g <sup>-1</sup> |
|----------------------|--|
| TiO <sub>2</sub> P25 | 50 ± 15 [1]                                      |
| SnS2 MKN-900         | $0.83 \pm 0.01$                                  |
| TiO <sub>2</sub> -HT | $128.39 \pm 1.87$                                |
| SnS <sub>2</sub> -HT | $22.62 \pm 0.29$                                 |

Table S6. Model equations of derived RSM models for DCF removal and conversion by solar/TiO<sub>2</sub> SnS<sub>2</sub> without and with an oxidant H<sub>2</sub>O<sub>2</sub>.

| Process         | Catalyst<br>type | Model<br># | Model equation  |
|-----------------|------------------|------------|---|
| solar/TiO2-SnS2 | COMM             | M1         | $Y_1 = 8.68 - 37.84 \times X_1 + 31.54 \times X_{1^2} + 0.68 \times X_3 - 1.17 \times X_{3^2} - 3.61 \times X_1 \times X_3$ |

|                  |      | M2   | $Y_2 = 7.40 - 30.86 \times X_1 + 25.14 \times X_{1^2} + 0.91 \times X_3 - 1.07 \times X_{3^2} -$  |
|------------------|------|------|---|
|                  |      | IVIZ | $3.78 \times X_1 \times X_3$  |
|                  |      |      | $Y_3 = 6.65 - 38.38 \times X_1 + 32.78 \times X_{1^2} + 2.31 \times X_2 + 4.21 \times X_{2^2} -$  |
|                  |      | M3   | $0.93 \times X_3 - 0.037 \times X_{3^2} - 2.33 \times X_1 \times X_2 - 2.20 \times X_1 \times X_3 - 0.46 \times$  |
| solar/TiO2-      | COMM |      | $X_2 \times X_3$  |
| $SnS_2/H_2O_2$   | COMM |      | $Y_4 = 4.55 - 33.20 \times X_1 + 29.05 \times X_{1^2} + 3.76 \times X_2 + 5.88 \times X_{2^2} -$  |
|                  |      | M4   | $0.97 \times X_3 - 1.02 \times X_{3^2} - 3.99 \times X_1 \times X_2 - 3.27 \times X_1 \times X_3 + 0.64 \times$   |
|                  |      |      | $X_2 \times X_3$  |
|                  |      | M5   | $Y_5 = 70.56 - 34.75 \times X_1 - 17.52 \times X_{1^2} + 8.69 \times X_3 - 6.91 \times X_{3^2} - $  |
| color/TiOs SpSs  | UТ   |      | $3.00 \times X_1 \times X_3$  |
| S01a1/1102-31132 | 111  | M6   | $Y_6 = 57.44 - 28.93 \times X_1 - 12.80 \times X_{1^2} + 6.27 \times X_3 - 5.43 \times X_{3^2} -$   |
|                  |      |      | $3.00 \times X_1 \times X_3$  |
|                  |      |      | $Y_7 = 53.47 - 36.60 \times X_1 + 5.04 \times X_{1^2} + 7.90 \times X_2 + 1.03 \times X_{2^2} +$  |
|                  |      | M7   | $0.81 \times X_3 - 8.02 \times X_{3^2} + 6.90 \times X_1 \times X_2 - 1.43 \times X_1 \times X_3 + 0.63 \times X_1 \times X_2 - 1.43 \times X_2 \times X_3 + 0.63 \times X_2 \times X_2 \times X_3 + 0.63 \times X_2 \times X_3 \times X_3 + 0.63 \times X_2 \times X_3 \times X_3 \times X_3 \times X_3 + 0.63 \times X_3 \times X_$           |
| solar/TiO2-      | ЦΤ   |      | $X_2 \times X_3$  |
| $SnS_2/H_2O_2$   | 111  |      | $Y_8 = 39.70 - 36.16 \times X_1 + 6.95 \times X_{1^2} + 6.02 \times X_2 + 2.79 \times X_{2^2} +$  |
|                  |      | M8   | $1.89 \times X_3 - 6.88 \times X_{3^2} - 0.036 \times X_1 \times X_2 - 3.96 \times X_1 \times X_3 - 0.62 \times X_1 \times X_2 - 0.02 \times X_2 \times X_2 - 0.026 \times X_2 \times X_2 \times X_2 - 0.026 \times X_2 \times X$ |
|                  |      |      | $X_2 \times X_3$  |

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**Table S7.** Analysis of variance (ANOVA) of RSM models M1 and M2 predicting removal and conversion of diclofenac by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-COMM process after 60 min exposure (transformed and non-transformed response values).

| With non-transformed values |                      |          |           |            |          |          |         |         |           |         |  |  |
|-----------------------------|----------------------|----------|-----------|------------|----------|----------|---------|---------|-----------|---------|--|--|
| Eastor                      | Statistical analysis |          |           |            |          |          |         |         |           |         |  |  |
| ractor                      | SS                   |          | df        |            | Μ        | MSS      |         | F       |           | 1       |  |  |
| (coded)                     | <b>M1</b>            | M2       | <b>M1</b> | M2         | M1       | M2       | M1      | M2      | <b>M1</b> | M2      |  |  |
| Model                       | 10638.661            | 7044.065 | 5         | 5          | 2127.732 | 1408.813 | 67.919  | 48.417  | 0.0028*   | 0.0045* |  |  |
| $X_1$                       | 8591.707             | 5715.815 | 1         | 1          | 8591.707 | 5715.815 | 274.255 | 196.438 | 0.0005*   | 0.0008* |  |  |
| $X_{1^2}$                   | 2.737                | 1263.719 | 1         | 1          | 2.737    | 1263.719 | 0.087   | 43.431  | 0.7868    | 0.0071* |  |  |
| $X_2$                       | 52.105               | 4.977    | 1         | 1          | 52.105   | 4.977    | 1.663   | 0.171   | 0.2876    | 0.7070  |  |  |
| $X_{2^2}$                   | 1989.379             | 2.297    | 1         | 1          | 1989.379 | 2.297    | 63.503  | 0.079   | 0.0041*   | 0.7970  |  |  |
| $X_1 \times X_2$            | 2.732                | 57.258   | 1         | 1          | 2.732    | 57.258   | 0.087   | 1.968   | 0.7870    | 0.2553  |  |  |
| Residual                    | 93.982               | 87.292   | 3         | 3          | 31.327   | 29.097   |         |         |           |         |  |  |
| Total                       | 10732.643            | 7131.357 | 8         | 8          |          |          |         |         |           |         |  |  |
|                             |                      |          |           | <b>T</b> 4 |          |          |         |         |           |         |  |  |

| With | transformed values  |
|------|---------------------|
|      | Statistical analysi |

| Easter           | Statistical analysis |        |           |    |       |        |         |         |         |         |  |  |
|------------------|----------------------|--------|-----------|----|-------|--------|---------|---------|---------|---------|--|--|
| (coded)          | SS                   |        | df        |    | MSS   |        | F       |         | р       |         |  |  |
|                  | M1                   | M2     | <b>M1</b> | M2 | M1    | M2     | M1      | M2      | M1      | M2      |  |  |
| Model            | 0.796                | 28.833 | 5         | 5  | 0.159 | 5.767  | 103.142 | 67.386  | 0.0015* | 0.0028* |  |  |
| $X_1$            | 0.731                | 27.534 | 1         | 1  | 0.731 | 27.534 | 473.293 | 321.747 | 0.0002* | 0.0004* |  |  |
| $X_{1^2}$        | 0.013                | 0.091  | 1         | 1  | 0.013 | 0.091  | 8.181   | 1.059   | 0.0646  | 0.3791  |  |  |
| $X_2$            | 0.034                | 0.725  | 1         | 1  | 0.034 | 0.725  | 21.817  | 8.478   | 0.0185* | 0.0619  |  |  |
| $X_{2^2}$        | 0.001                | 0.015  | 1         | 1  | 0.001 | 0.015  | 0.505   | 0.172   | 0.5287  | 0.7058  |  |  |
| $X_1 \times X_2$ | 0.018                | 0.469  | 1         | 1  | 0.018 | 0.469  | 11.915  | 5.476   | 0.0409* | 0.1012  |  |  |
| Residual         | 0.005                | 0.257  | 3         | 3  | 0.002 | 0.086  |         |         |         |         |  |  |
| Total            | 0.801                | 29.090 | 8         | 8  |       |        |         |         |         |         |  |  |

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p<0.05 means that model or model term is significant

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Table S8. Analysis of variance (ANOVA) of RSM models M3 and M4 predicting removal and ersion of diclofenac by solar/TiO2-SnS2-COMM/H2O2 process after 60 min exposure (transformed

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|----|---|
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|    |   |

| conversion of diciofenaci | y solar/1102-51 | 152-COIVIIVI/H2 | O <sub>2</sub> process and | er 60 min exp | osure (trar |
|---------------------------|-----------------|-----------------|----------------------------|---------------|-------------|
| and non-transformed resp  | oonse values).  |                 |                            |               |             |

| With non-transformed values |                      |            |    |            |               |               |         |         |           |              |  |
|-----------------------------|----------------------|------------|----|------------|---------------|---------------|---------|---------|-----------|--------------|--|
| Easton                      | Statistical analysis |            |    |            |               |               |         |         |           |              |  |
| ractor<br>(coded)           | , SS                 |            | df |            | MSS           |               | F       |         | р         |              |  |
| (coueu)                     | M3                   | <b>M</b> 4 | M3 | <b>M</b> 4 | M3            | M4            | M3      | M4      | M3        | <b>M</b> 4   |  |
| Model                       | 15881.136            | 12260.441  | 9  | 9          | 1764.571      | 1362.271      | 98.879  | 30.899  | < 0.0001* | 0.0007*      |  |
| $X_1$                       | 11785.644            | 8820.169   | 1  | 1          | 11785.644     | 8820.169      | 660.420 | 200.058 | < 0.0001* | < 0.0001*    |  |
| $X_{1^2}$                   | 3966.537             | 3115.435   | 1  | 1          | 3966.537      | 3115.435      | 222.269 | 70.664  | < 0.0001* | $0.0004^{*}$ |  |
| $X_2$                       | 42.769               | 113.390    | 1  | 1          | 42.769        | 113.390       | 2.397   | 2.572   | 0.1823    | 0.1697       |  |
| $X_{2^2}$                   | 65.323               | 127.863    | 1  | 1          | 65.323        | 127.863       | 3.660   | 2.900   | 0.1139    | 0.1493       |  |
| $X_3$                       | 6.956                | 7.515      | 1  | 1          | 6.956         | 7.515         | 0.390   | 0.170   | 0.5598    | 0.6968       |  |
| $X_{3^2}$                   | 0.005                | 3.854      | 1  | 1          | 0.005         | 3.854         | 0.000   | 0.087   | 0.9874    | 0.7794       |  |
| $X_1 \times X_2$            | 21.655               | 63.776     | 1  | 1          | 21.655        | 63.776        | 1.213   | 1.447   | 0.3208    | 0.2829       |  |
| $X_1 \times X_3$            | 19.409               | 42.870     | 1  | 1          | 19.409        | 42.870        | 1.088   | 0.972   | 0.3448    | 0.3694       |  |
| $X_2 \times X_3$            | 0.844                | 1.618      | 1  | 1          | 0.844         | 1.618         | 0.047   | 0.037   | 0.8364    | 0.8556       |  |
| Residual                    | 89.228               | 220.440    | 5  | 5          | 17.846        | 44.088        |         |         |           |              |  |
| Total                       | 15970.365            | 12480.881  | 14 | 14         |               |               |         |         |           |              |  |
|                             |                      |            |    | W          | ith transform | med values    |         |         |           |              |  |
| Factor                      |                      |            |    |            | Statis        | stical analys | sis     |         |           |              |  |
| (coded)                     | SS                   |            | df |            | MSS           |               | 1       | F       | p         | ,            |  |
| (coucu)                     | M3                   | <b>M4</b>  | M3 | M4         | M3            | M4            | M3      | M4      | M3        | <b>M</b> 4   |  |
| Model                       | 24.376               | 27.235     | 9  | 9          | 2.708         | 3.026         | 98.253  | 22.738  | < 0.0001* | 0.0015*      |  |
| $X_1$                       | 21.982               | 21.975     | 1  | 1          | 21.982        | 21.975        | 797.443 | 165.123 | < 0.0001* | < 0.0001*    |  |
| $X_{1^2}$                   | 1.345                | 2.331      | 1  | 1          | 1.345         | 2.331         | 48.806  | 17.514  | 0.0009*   | 0.0086*      |  |
| $X_2$                       | 0.208                | 0.999      | 1  | 1          | 0.208         | 0.999         | 7.555   | 7.510   | 0.0404*   | 0.0408*      |  |
| $X_{2^2}$                   | 0.093                | 0.103      | 1  | 1          | 0.093         | 0.103         | 3.362   | 0.776   | 0.1262    | 0.4188       |  |
| $X_3$                       | 0.362                | 0.963      | 1  | 1          | 0.362         | 0.963         | 13.138  | 7.235   | 0.0151*   | 0.0433*      |  |
| $X_{3^2}$                   | 0.302                | 0.456      | 1  | 1          | 0.302         | 0.456         | 10.939  | 3.430   | 0.0213*   | 0.1232       |  |
| $X_1 \times X_2$            | 0.050                | 0.118      | 1  | 1          | 0.050         | 0.118         | 1.821   | 0.888   | 0.2351    | 0.3893       |  |
| $X_1 \times X_3$            | 0.181                | 0.224      | 1  | 1          | 0.181         | 0.224         | 6.570   | 1.686   | 0.0505    | 0.2508       |  |
| $X_2 \times X_3$            | 0.000                | 0.283      | 1  | 1          | 0.000         | 0.283         | 0.006   | 2.130   | 0.9433    | 0.2043       |  |
| Residual                    | 0.138                | 0.665      | 5  | 5          | 0.028         | 0.133         |         |         |           |              |  |
| Total                       | 24.513               | 27.901     | 14 | 14         |               |               |         |         |           |              |  |

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Table S9. Analysis of variance (ANOVA) of RSM models M5 and M6 predicting removal and conversion of diclofenac by solar/TiO2-SnS2-HT process after 60 min exposure.

| Factor   | Statistical analysis |          |    |    |          |          |         |              |         |          |  |  |
|--|----------------------|----------|----|----|----------|----------|---------|--------------|---------|----------|--|--|
| (code  | SS                   |          | df |    | MSS      |          | F       |              | р       |          |  |  |
| d)   | M5                   | M6       | M5 | M6 | M5       | M6       | M5      | M6           | M5      | M6       |  |  |
| Model  | 8444.841             | 5679.537 | 5  | 5  | 1688.968 | 1135.907 | 43.308  | 279.397      | 0.0054* | 0.0003*  |  |  |
| $X_1$  | 7245.976             | 5020.347 | 1  | 1  | 7245.976 | 5020.347 | 185.799 | 1234.84<br>6 | 0.0009* | <0.0001* |  |  |
| $X_{1^2}$  | 614.018              | 327.830  | 1  | 1  | 614.018  | 327.830  | 15.744  | 80.636       | 0.0286* | 0.0029*  |  |  |
| $X_2$  | 453.327              | 236.213  | 1  | 1  | 453.327  | 236.213  | 11.624  | 58.101       | 0.0422* | 0.0047*  |  |  |
| $X_{2^2}$  | 95.634               | 59.073   | 1  | 1  | 95.634   | 59.073   | 2.452   | 14.530       | 0.2153  | 0.0317*  |  |  |
| $X_1 \times X_2$   | 35.886               | 36.074   | 1  | 1  | 35.886   | 36.074   | 0.920   | 8.873        | 0.4082  | 0.0587   |  |  |
| Resid<br>ual   | 116.997              | 12.197   | 3  | 3  | 38.999   | 4.066    |         |              |         |          |  |  |
| Total  | 8561.837             | 5691.734 | 8  | 8  |          |          |         |              |         |          |  |  |
| $\frac{1}{2}$ * $v < 0.05$ means that model or model term is significant |                      |          |    |    |          |          |         |              |         |          |  |  |

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34 35

**Table S10.** Analysis of variance (ANOVA) of RSM models **M7** and **M8** predicting removal and conversion of diclofenac by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT/H<sub>2</sub>O<sub>2</sub> process after 60 min exposure .

| Lester           | Statistical analysis |            |            |           |            |            |            |              |          |           |  |  |
|------------------|----------------------|------------|------------|-----------|------------|------------|------------|--------------|----------|-----------|--|--|
| Factor           | SS                   |            | df         |           | MSS        |            | F          |              | р        |           |  |  |
| (coded)          | M7                   | <b>M</b> 8 | <b>M</b> 7 | <b>M8</b> | <b>M</b> 7 | <b>M</b> 8 | <b>M</b> 7 | <b>M8</b>    | M7       | <b>M8</b> |  |  |
| Model            | 11783.8<br>82        | 11252.799  | 9          | 9         | 1309.320   | 1250.311   | 67.906     | 164.620      | 0.0001*  | <0.0001*  |  |  |
| $X_1$            | 10717.6<br>58        | 10457.913  | 1          | 1         | 10717.66   | 10457.913  | 555.855    | 1376.92<br>3 | <0.0001* | <0.0001*  |  |  |
| $X_{1^2}$        | 93.846               | 178.300    | 1          | 1         | 93.846     | 178.300    | 4.867      | 23.476       | 0.0785   | 0.0047*   |  |  |
| $X_2$            | 498.655              | 290.338    | 1          | 1         | 498.655    | 290.338    | 25.862     | 38.227       | 0.0038*  | 0.0016*   |  |  |
| $X_{2^2}$        | 3.943                | 28.701     | 1          | 1         | 3.943      | 28.701     | 0.205      | 3.779        | 0.6700   | 0.1095    |  |  |
| $X_3$            | 5.201                | 28.624     | 1          | 1         | 5.201      | 28.624     | 0.270      | 3.769        | 0.6257   | 0.1099    |  |  |
| $X_{3^2}$        | 237.463              | 174.949    | 1          | 1         | 237.463    | 174.949    | 12.316     | 23.034       | 0.0171*  | 0.0049*   |  |  |
| $X_1 \times X_2$ | 190.432              | 0.005      | 1          | 1         | 190.432    | 0.005      | 9.876      | 0.001        | 0.0256*  | 0.9801    |  |  |
| $X_1 \times X_3$ | 8.156                | 62.772     | 1          | 1         | 8.156      | 62.772     | 0.423      | 8.265        | 0.5441   | 0.0348*   |  |  |
| $X_2 \times X_3$ | 1.598                | 1.540      | 1          | 1         | 1.598      | 1.540      | 0.083      | 0.203        | 0.7850   | 0.6714    |  |  |
| Residua<br>l     | 96.407               | 37.976     | 5          | 5         | 19.281     | 7.595      |            |              |          |           |  |  |
| Total            | 11880.2<br>89        | 11290.775  | 14         | 14        |            |            |            |              |          |           |  |  |

36

\*p<0.05 means that model or model term is significant



Figure S1. Diffuse reflectance spectra of immobilized TiO<sub>2</sub>-SnS<sub>2</sub> composites with different SnS<sub>2</sub> wt%;
 commercial (COMM) (A) and hydrothermal (HT) (B)



41 Figure S2. Determination of pHpzc values TiO<sub>2</sub>-SnS<sub>2</sub>-COMM (A) and TiO<sub>2</sub>-SnS<sub>2</sub>-HT (B) composites.

42



Figure S3. Kinetics of DCF removal by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-COMM process; TiO<sub>2</sub>-SnS<sub>2</sub>-COMM prepared
 by immobilization using AEROXIDE TIO<sub>2</sub> P25 and SnS<sub>2</sub> MKN-900 (Experimental conditions listed in
 Table 1, and experimental matrix provided by FFD, Table S1, Supplementary material).



49 Figure S4. Kinetics of DCF removal by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-COMM/H<sub>2</sub>O<sub>2</sub> process; TiO<sub>2</sub>-SnS<sub>2</sub>-COMM
 50 prepared by immobilization using AEROXIDE TIO<sub>2</sub> P25 and SnS<sub>2</sub> MKN-900 (Experimental conditions 1 listed in Table 1, and experimental matrix provided by BBD, Table S2, Supplementary material).

- 52
- 53



55 **Figure S5.** Kinetics of DCF removal by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT process; TiO<sub>2</sub>-SnS<sub>2</sub>-HT prepared by 56 hydrothermal method (Experimental conditions listed in Table 1, and experimental matrix provided 57 by FFD, Table S3, Supplementary material).



Figure S6. Kinetics of DCF removal by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT/H<sub>2</sub>O<sub>2</sub> process; TiO<sub>2</sub>-SnS<sub>2</sub>-HT prepared by
 hydrothermal method (Experimental conditions listed in Table 1, and experimental matrix provided
 by BBD, Table S4, Supplementary material).

- 63
- 64



**Figure S7.** Comparison of DCF conversion using TiO<sub>2</sub>-SnS<sub>2</sub>-COMM and TiO<sub>2</sub>-SnS<sub>2</sub>-HT without H<sub>2</sub>O<sub>2</sub> (**A**) and with H<sub>2</sub>O<sub>2</sub> addition (**B**) under solar radiation at conditions set by FFD (Tables 1, and S1 and S3, Supplementary material) and BBD (Tables 1, and S2 and S4, Supplementary material), respectively.



Figure S8. Residual diagnostics of model M6 for the prediction of the conversion of DCF by solar/TiO<sub>2</sub>-SnS<sub>2</sub>-HT/H<sub>2</sub>O<sub>2</sub> process: (A) observed *vs.* predicted plot, (B) normal probability plot, and (C) internally studentized residuals *vs.* predicted values plot.

## Detailed Experimental section related to (1) Determination of semiconducting properties by electrochemical measurements, and (2) Calculations and procedure used in RSM modeling

#### 77 1. .Determination of semiconducting properties by electrochemical measurements

Circular shaped titanium samples (Alfa Aesar, 99.9 wt.% Ti) were abraded with 1000 grit SiC
 papers, ultrasonically cleaned with ethanol and redistilled water and served as solid substrates for

80 TiO<sub>2</sub>-HT and SnS<sub>2</sub>-HT pure components, as well as for TiO<sub>2</sub>-SnS<sub>2</sub>-COMM and TiO<sub>2</sub>-SnS<sub>2</sub>-HT

81 composites immobilization as was described in the Experimental section, subsection 2.2. 82 Photocatalysts synthesis and immobilization (main text). As prepared substrates were embedded in a 83 Teflon holder, with an area, A=1 cm<sup>2</sup> exposed to the solution and were used as working electrodes.

84 All electrochemical measurements were performed in a conventional three-electrode cell: the 85 working electrode was Ti coated electrode, the counter electrode was a large area platinum electrode 86 and the reference electrode, to which all potentials in the paper are referred, was Ag | AgCl in 3.0 mol 87  $dm^{-3}$  KCl (E = 0.208 V vs. standard hydrogen electrode). The electrolyte was 3% NaCl solution, pure 88 or spiked with DCF (0.1 mM). A Solartron potentiostat/galvanostat 1287 with FRA 1260 controlled 89 by CorrWare® and ZView® softwares was used in these measurements.

90 The structure of the solid liquid interface, i.e., the structure of the TiO<sub>2</sub>-SnS<sub>2</sub> catalysts electrolyte 91 solution interface (TiO<sub>2</sub>-SnS<sub>2</sub>-COMM and TiO<sub>2</sub>-SnS<sub>2</sub>-HT composite films on titanium substrate) was 92 investigated at the open circuit potential  $(E_{ocp})$  using electrochemical impedance spectroscopy (EIS) 93 performed in the frequency range from 100 kHz to 5 mHz at an *ac* voltage amplitude of ±5 mV. The 94 experimental data were fitted using the complex non-linear least squares (CNLS) fit analysis software 95 [2] and values of the elements of the proposed electric equivalent circuit (EEC) were derived with  $\chi^2$ 96 values less than 5  $\times$  10<sup>-3</sup> (errors in parameter values of 1–3%).

97 Due to the frequency dispersion (mostly attributed to the "capacitance dispersion"), the 98 capacitor in EECs was replaced with the constant phase element (CPE). The impedance of CPE is 99 defined as  $Z(CPE)=[Q(j\omega)^n]^{-1}$ , where  $j\omega$  is the complex variable for sinusoidal perturbations with 100  $\omega = 2\pi f$ , and *n* is the exponent of CPE, while *Q* is the frequency–independent parameter of CPE, which 101 represents a pure capacitance when n = 1 [3]. Values of 0.70 < n < 1 indicate inhomogeneities at the 102 microscopic level at the metal electrolyte interface (surface roughness, adsorbed species, etc.) [4,5]. 103 The numerical values of interfacial capacitances, C were calculated using the Brug's relation, valid 104

when the ohmic (electrolyte) resistance,  $R_{\Omega}$  is much smaller than the charge–transfer resistance [3]:

$$C = \left( Q \cdot R_{\Omega}^{1-n} \right)^{1/n} \tag{1}$$

105 The electronic-semiconducting properties of TiO2-HT, SnS2-HT, TiO2-SnS2-COMM and TiO2-106 SnS2-HT catalyst films were investigated by Mott–Schottky method [6]. The capacitance values of the 107 titanium | composite film | solution interface, required for Mott–Schottky analysis, were obtained from 108 EIS measurements. The imaginary part of impedance  $(Z_{imag})$  was recorded as a function of the 109 electrode potential and the frequency (ranging from 3000-30 Hz). The potential was swept in the 110 negative direction from 0 V at a sweep rate of 50 mV s<sup>-1</sup>. The rapid cathodic scan of 50 mV s<sup>-1</sup> was 111 used to avoid the change in the film thickness during measurements [7]. From the measured Zimag 112 values, it was possible to calculate CPE parameter  $Q = -1/\omega Z_{imag}$  taking into account the angular 113 frequency,  $\omega = 2\pi f$ . From Q value and CPE exponent n and R<sub>Ω</sub>, the effective interfacial capacitance, C, 114 was calculated using the expression developed by Brug et al. [3]; eq. (1). The C values consist of the 115 series combination of Helmholtz double layer capacitance (CH) with the parallel combination of the

116 space–charge capacitance  $(C_{sc})$  and is equal to:

$$C^{-1} = C_{\rm H}^{-1} + C_{\rm sc}^{-1} \tag{2}$$

117 All capacitance values were corrected taking Helmholtz capacitance to be 50  $\mu$ F cm<sup>-2</sup> [8].

118 To avoid the frequency dispersion of the effective interfacial capacitance in MS tests and 119 eliminate the contribution of the surface states, the data obtained at seven frequencies (ranging from 120 3000-30 Hz) were analyzed according to the procedure proposed by Harrington et al. [8,9]. Detailed 121 description of Devine-Harrington procedure can be found in literature [10-12]. By applying 122 Devine-Harrington procedure, the characteristic frequency was determined to be 1000 Hz. Hence the

123 results provided refer to this frequency.

#### 124 2. .Calculations and procedure used in RSM modeling

125 The influence of pH, [H<sub>2</sub>O<sub>2</sub>] and SnS<sub>2</sub> wt % within TiO<sub>2</sub>-SnS<sub>2</sub> composites, on DCF removal and 126 conversion was correlated by means of response surface modeling (RSM). The values of process 127 parameters are represented by independent variables: X1, X2 and X3 (Table 1, main text), and 128 according to the number of parameters to be varied within solar driven photocatalytic treatment, 129 experimental matrices were expressed by 3<sup>2</sup> FFD for solar/TiO<sub>2</sub>-SnS<sub>2</sub> (Tables S1 and S3, respectively) 130 and BBD for solar/TiO<sub>2</sub>-SnS<sub>2</sub>/H<sub>2</sub>O<sub>2</sub> processes (Tables S2 and S4, respectively). DCF removal and 131 conversion extents after 60 min exposure to solar irradiation were chosen as processes responses (Y). 132 The combined influence of studied parameters on processes performance is described by quadratic 133 polynomial equations, i.e. RSM models [13], and evaluated by the (i) analysis of variance (ANOVA) 134 considering following statistical parameters: Fisher F-test value (F), its probability value (p), 135 regression coefficients (pure;  $R^2$ , adjusted;  $R_{adl}^2$ , predicted;  $R_{pre^2}$ ), *t*-test value, and (ii) graphical based 136 analysis, so-called "residual diagnostic" (RD): including normal probability test, Levene's test, and 137 constant variance test. The calculations were performed by STATISTICA 12.7, StatSoft&Dell; and 138 Design-Expert 10.0, StatEase, software packages.

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