

Article

Analysis of Cantilever Triple-Layer Piezoelectric Harvester (CTLPH): Non-Resonance Applications

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Abstract: In this research, a design guideline for a kinetic energy converter using a cantilever triple-layer piezoelectric harvester (CTLPH) for low-frequency applications is presented. By combining the constitutive and internal energy equations, the analytical equations for harvested voltage and power were developed. It was also found that frequency of motion, applied tip force, piezoelectric coefficients, geometrical dimensions, and mechanical properties of layers play significant roles in the performance of the harvester. Having characterised the voltage regulator module, LTC3588, the dependency of output voltage on both the storage and output capacitors of the LTC3588 was investigated. An experimental measurement using the optical method was carried out to determine the applied tip force. Furthermore, the performance of the CTLPH in low frequencies (<3.3 Hz) for various resistive loads was investigated. It was found that both excitation frequency and external resistance load are effective on the maximum generated power. The developed CTLPH shows the optimum power of 17.31 μW at the external resistance of 20 k Ω , which is highly appropriate for micropower devices with at least 3.2 Hz of kinetic vibration in their environment.

Keywords: piezoelectric; low-frequency; tip-force; cantilever beam; triple-layer beam; non-resonance harvester; reciprocated motion; tip-mass; LTC3588

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1. Introduction

Research on the creation of micropower generators was recently driven by biomedical implants, the internet of things (IoT), and the monitoring of the health of structures in severe environments [1]. Micro-power-consuming devices of the next generation include CMOS, biomedical implants, and MEMS sensors [2]. Even while high energy density lithium-ion batteries are now reasonably priced to use in the majority of electrical equipment, replacing them can be difficult in specific situations. To address the problem of battery replacement, researchers are working to create self-powered modules using carbon nanotubes [3]. For instance, detecting sensors are essential components to alert about the possibility of fire in inaccessible mountainous areas. It is nearly impossible to replace or recharge the batteries of these sensors due to their remote locations. To address the ever-increasing need for battery power replacement via harvesters, researchers developed various devices to convert environmental energy to electricity via small solar panels, electrostatic, electromagnetic, reverse electrowetting effects [4], and smart materials. However, each system comes with its specific drawbacks. Solar is not suitable for cloudy days or nights, whereas electrostatic is limited by its low-energy density [5]. Most electromagnetic harvesters suffer from bulky coils [6], and reverse electrowetting requires a complex and costly structure [7]. Among smart materials, piezoelectric shows the highest energy density and is used as a harvester, actuator [8,9], sensor [1], and vibration absorber for lightweight structures [10–13], etc.

Despite high energy density, piezoelectric harvesters suffer from low longevity. The main reason for the short life span is microstructural cracks. It was shown that triple-layer structures could be a potential solution to enhance the output voltage and the life

span of piezoelectric harvesters [14]. For example, the effectiveness of energy harvesters in vivo environments, with an excitation frequency of 2 Hz, was demonstrated by coupling the pacemaker's battery with the harvester. Since the required power of the pacemaker is roughly 30 μ W, the array of 100-harvester was helpful to elongate the pacemaker's longevity by 1.5 years [15]. As another application, Shi proposed an ultra-low frequency (<1.4 Hz) energy harvester floating on the water's surface using a piezoelectric cantilever beam and generating 6.32 mW [16]. However, no analytical design procedure was proposed for the harvester in this research. Qin et al [17] proposed a branch structure mechanism to apply force to a two-layer piezoelectric harvester to enhance the output voltage. Despite low-frequency excitation, it suffers from a complex structure.

In terms of modelling, Smits et al [18] derived the constitutive equations for piezoelectric bimorph with both series and parallel electrical branch structure mechanisms. DeVoe et al [19] presented a model to predict the static behavior of a cantilever beam made of elastic and piezoelectric layers. However, the matrix inversion used in the presented method complicates the model. Weinburge presented a simpler mathematical model while the effect of the electromechanical coupling coefficient was ignored; it was because of the small value electromechanical coupling coefficient of a maximum of 12% for lead zirconate titanate (PZT) [20]. Wang et al. employed internal energy and constitutive equations to estimate the tip deflection of the cantilever triple-layer actuators with a series of electrical connections of electrodes [21]. The development of new materials with higher electromechanical coupling coefficients (e.g., $K_{31} = 0.38$ for PZT-5H) directed Tadmor et al to reform Weinburge and Wang equations by highlighting the effect of large electromechanical coupling coefficients in the equations [22]. Ismail et al corrected the model by considering the geometry of the beam [23]. A model for a multi-layer energy piezoelectric harvester using carbon and glass fibers was developed by Lu et al [24]. However, the analysis of this harvester is based excitation, which is suitable for high-frequency applications.

In this paper, we aim to provide a guideline for designing a low-frequency cantilever triple-layer piezoelectric harvester (CTLPH) with tip excitation and tip mass. Moreover, the piezoelectric layers are electrically connected in parallel. Therefore, in the first step, we will investigate the effective parameters of the output voltage of the energy storage module, which is coupled with the CTLPH. We will find the relationship between the output voltage and applied tip force, the geometrical and electromechanical properties, and the length of the harvester. To verify the derived analytical equations, the tip force will be measured with an optical method using a laser displacement sensor. Finally, the voltage and power of a prototype CTLPH for various resistance loads and frequencies will be measured.

2. Principle of Operation

The schematic structure of the developed energy converter device consists of an active element (i.e., CTLPH), and its excitation mechanism is shown in Figure 1a. The excitation mechanism is an acrylic slider connected to a Scotch yoke to make a reciprocated mechanism. The CTLPH is made of an elastic substrate sandwiched by two piezoelectric layers with a tip mass that is fixed on the wall of a U-shaped acrylic channel. The tip mass of the cantilever beam is a cylindrical permanent magnet (NdFeB-N35, $\varnothing 5 \times 5$ mm). The slider is made of a permeant magnet bound to an acrylic slider. The directions of the polarity of permanent magnets, on both the slider and CTLPH, are a way that there is a repulsive force between them. The reciprocating motion (Figure 1b) of the slider causes the bending deflection of CTLPH.

This deflection leads to the accumulation of charges on the electrodes and induces a voltage across the electrodes. The real photo of the structure is shown in Figure 1c.

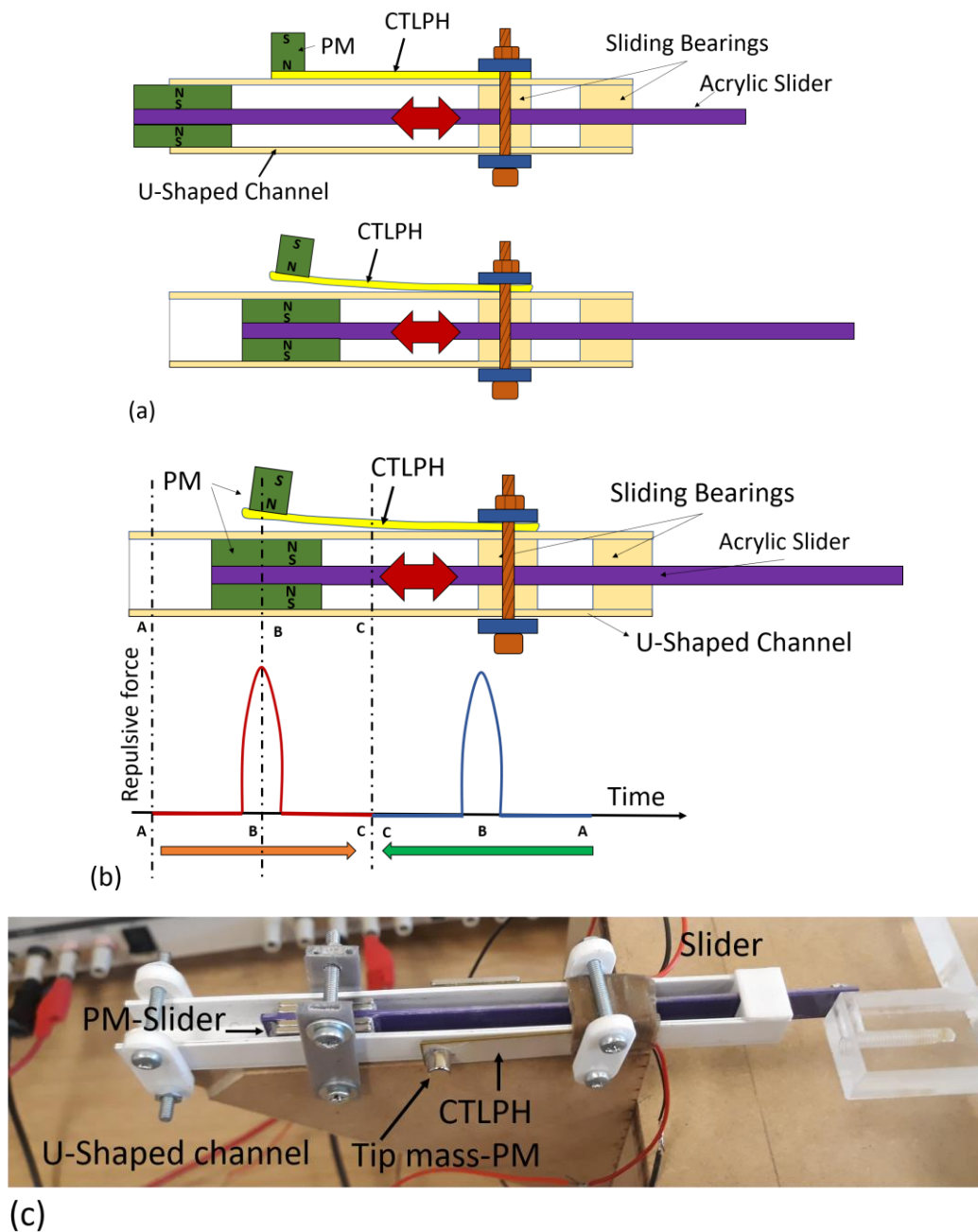


Figure 1. The CTLPH (a) A schematic, (b) bending deflection in a reciprocating motion, and (c) a real mechanism.

3. Theoretical Analysis

3.1. Assumptions and Constitutive Equations

In this research, a symmetrical cantilever triple-layer piezoelectric harvester with a tip mass was designed, built, and modelled. The CTLPH (Figure 2a) can be modelled by the Euler–Bournoulli beam with effective length (L) and width (W_b). This beam is deformed by a uniformly distributed body force of $p(x)$ and an applied tip force of F . The tip force is caused by a repulsive force between the slider magnet and the tip magnet of the CTLPH. The coordinate system is in a way that x or 1 axis is in the length direction, y or 2 axis is in the width direction, and z or 3 axis is in the thickness direction of the CTLPH. The transverse vibration causes the deflection of $w(x,t)$ in the y -direction. The beam has an arbitrary cross-section, $A(x)$, and is made of three layers of piezoelectric–substrate–piezoelectric. Considering $I(x)$ as the moment of inertia about the z -axis and $E(x)$ as the effective elastic

modulus of the triple-layer beam, the bending stiffness of the beam is $EI(x)$. The CTLPH is loaded by a mechanical force that causes a distribution of shear force $Q(x,t)$ and moment $M(x,t)$ along the CTLPH. Figure 2b shows a side view of an infinitesimal element of the CTLPH positioned at x . Based on the selected coordinate system, the tip force and lateral vibration are in the y direction. The central layer is a substrate made of an elastic material with a thickness of t_s . The substrate is coated with piezoelectric layers with thickness t_p . As with [19,20], we assume that the layers are bonded strongly so that there is no slip between them. Moreover, each part of the CTLPH is in static equilibrium. The radius of curvature ($R_o(x)$) induced by the applied tip force is much larger than the CTLPH's thickness, and the cross-section of the CTLPH is constant in a rectangular shape. Figure 2c,d also indicates the different arrangements of the CTLPH in terms of the polarization direction of piezoelectric layers and their electrical connections. The CTLPH is called parallel if the piezoelectric layers are electrically connected, as shown in Figure 2c, and the piezoelectric layers have the same polarization direction. However, if electrical connections are similar to Figure 2d, and the piezoelectric layers have the anti-polarization direction, the CTLPH is called a series. The electrodes of piezoelectric layers are perpendicular to the y direction. Both length (L) and width (W_b) of the CTLPH are much larger than the total thickness ($t_s + 2t_p$). If a tip force is applied to the beam, the electromechanical equations for the piezoelectric layers are [18]:

$$\text{the upper layer, } \begin{cases} e_u^p = \frac{\sigma_u^p}{E_u^p} - d_{31}E_3 & (a) \\ D_3^p = -d_{31}\sigma_u^p + \epsilon_{33}^p E_3 & (b) \end{cases} \quad (1)$$

$$\text{the lower layer, } \begin{cases} e_l^p = \frac{\sigma_l^p}{E_l^p} + d_{31}E_3 & (a) \\ D_3^p = d_{31}\sigma_l^p + \epsilon_{33}^p E_3 & (b) \end{cases} \quad (2)$$

where the superscripts p represent the piezoelectric elements, while subscripts u and l indicate the upper and lower layers. The e_u^p and σ_u^p are the strain and stress of the lower piezoelectric layer in x or 1 direction, which is along with the length of the CTLPH; d_{31} , E_u^p , and ϵ_{33}^p are transverse piezoelectric coefficient, the elastic modulus of the upper piezoelectric constant electric field, and the permittivity at constant stress, respectively. D_3^p and E_3 are electric displacement and electric field across electrodes in z or 3 direction. The substrate is made of homogeneous elastic material without coupling effect to other fields. Then, the relationship between strain and stress for the substrate can be obtained by Equation (3).

$$\text{the substrate layer, } e_s = \frac{\sigma_s}{E_s}. \quad (3)$$

where the superscript 's' represents the substrate elastic elements, and e_s , σ_s and E_s are the strain, stress, and elastic modulus of the substrate layer.

3.2. Bending Stiffness

When a tip force is applied to the CTLPH, it will bend. Due to the strong glue between layers, the positive strain of the lower/upper layer will continuously change to the negative strain in the upper/lower layer. The neutral axis (NA) with zero strain is located in the mid of the substrate layer. Assuming that the coordinate system is coincident with the mid-plane of the substrate, $Y_{NA} = 0$. If the curvature radius of the neutral plane at position x is $R_o(x)$, the strain of the i th piezoelectric layer can be calculated from Equation (4) [25]:

$$e_1^p = \frac{L_i - L_{NA}}{L_{NA}} = \frac{(R_o(x) - y)\theta - R_o(x)\theta}{R_o(x)\theta} = -\frac{y}{R_o(x)}. \quad (4)$$

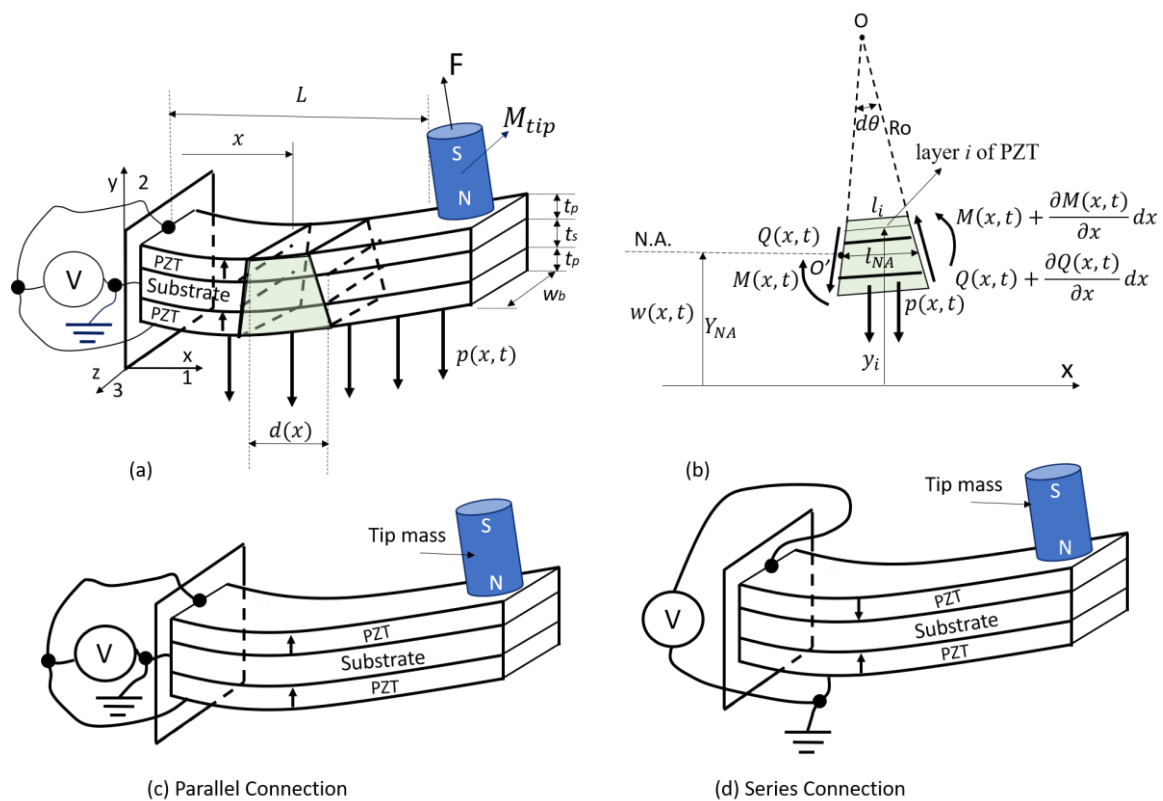


Figure 2. (a) A cantilever triple-layer piezoelectric harvester in transverse vibration. (b) Free-body diagram of a small element. (c) Parallel connection. (d) Series connection.

The bending moment of the internal stresses of an infinitesimal element in the CTLPH with the length of dx and cross-section of $w_b dy$ can be derived by Equation (5).

$$M = - \int_{-(t_p + \frac{t_s}{2})}^{-(\frac{t_s}{2})} \sigma_l w_b dy - \int_{-\frac{t_s}{2}}^{\frac{t_s}{2}} \sigma_s w_b dy - \int_{\frac{t_s}{2}}^{t_p + \frac{t_s}{2}} \sigma_u w_b dy. \quad (5)$$

Substituting (1b) in (1a) and considering the same piezoelectric material for the upper and lower layers ($E_u^p = E_l^p = E_p$), leads to

$$D_3^p = \frac{y E^p}{R_o(x)} d_{31} + (\epsilon_{33}^\sigma - d_{31}^2 E_p) E_3. \quad (6)$$

By substituting Equation (6) in (1b), the σ_u can be obtained from

$$\sigma_u = - \frac{y}{R_o(x)} E_p + d_{31} E_p E_3. \quad (7)$$

Similarly, the stress of the lower layer, σ_l , can be found in Equation (8):

$$\sigma_l = - \frac{y}{R_o(x)} E_p - d_{31} E_p E_3. \quad (8)$$

By replacing stress from Equations (3), (7), and (8) in Equation (5), $M(x)$ can be calculated from

$$M(x) = - \int_{-(t_p + \frac{t_s}{2})}^{-(\frac{t_s}{2})} \left(- \frac{y}{R_o(x)} E_p - d_{31} E_p E_3 \right) w_b dy - \int_{-\frac{t_s}{2}}^{\frac{t_s}{2}} \left(- \frac{y}{R_o(x)} \right) E^s w_b dy - \int_{\frac{t_s}{2}}^{t_p + \frac{t_s}{2}} \left(- \frac{y}{R_o(x)} E_p + d_{31} E_p E_3 \right) w_b dy. \quad (9)$$

After simplification, $M(x)$ can be presented by (10):

$$M(x) = \frac{w_b}{12R_o(x)} \left[2E_p \left(3t_s^2 t_p + 6t_p^2 t_s + 4t_p^3 \right) + E_s t_s^3 \right] - d_{31} E_p w_b E_3 \left(t_s t_p + t_p^2 \right). \quad (10)$$

or by Equation (11) in a simpler form:

$$M(x) = \frac{w_b}{12R_o(x)} \lambda - \Delta. \quad (11)$$

where λ and Δ are functions of geometrical dimensions and the elastic modulus of layers, defined by Equations (12) and (13).

$$\lambda \stackrel{\text{def}}{=} 2E_p \left(3t_s^2 t_p + 6t_p^2 t_s + 4t_p^3 \right) + E_s t_s^3. \quad (12)$$

$$\Delta \stackrel{\text{def}}{=} d_{31} E_p w_b E_3 \left(t_s t_p + t_p^2 \right). \quad (13)$$

The explicit relationship for radius curvature, $R_o(x)$, can be derived from Equation (11).

$$\frac{1}{R_o(x)} = \frac{12[M(x) + \Delta]}{w_b \lambda}. \quad (14)$$

It is well known that the relationship between the applied bending moment, $M(x,t)$, and the bending deformation $w(x,t)$ can be calculated by Equation (15) [26].

$$M(x,t) = EI(x) \frac{\partial^2 w(x,t)}{\partial x^2} = \frac{EI(x)}{R_o(x)} \quad (15)$$

The bending stiffness for the harvester ($E_3 = 0$) can be deduced from a comparison of Equations (10) and (15). Then $EI(x)$ can be simplified by Equation (16):

$$EI(x) = \frac{w_b}{12} \left[2E_p \left(3t_s^2 t_p + 6t_p^2 t_s + 4t_p^3 \right) + E_s t_s^3 \right] = \frac{w_b}{12} \lambda. \quad (16)$$

3.3. Output Voltage and Power

Based on the thermodynamic equilibrium equations, the internal energy of any differential volume element of the triple-layer harvester positioned at x , can be calculated by the internal energy of the upper piezoelectric, substrate, and lower piezoelectric layers given by Equation (17) [21].

$$dU_{beam} = dU_u^p + dU_s + dU_l^p. \quad (17)$$

The individual internal energy of the upper piezoelectric layer can be calculated by

$$dU_u^p = \frac{1}{2} e_u^p \sigma_u^p + \frac{1}{2} D_3^p E_3. \quad (18)$$

Replacing e_u^p and D_3^p by Equation (1), yields to

$$dU_u^p = \frac{1}{2} \frac{\sigma_u^{p2}}{E_p} - d_{31} \sigma_u^p E_3 + \frac{1}{2} \epsilon_{33}^\sigma E_3^2. \quad (19)$$

Substituting (1a) and Equation (4) in Equation (19) yields to

$$dU_u^p = \frac{1}{2} \left(\frac{y^2}{R_o^2} E_p - d_{31}^2 E_p E_3^2 + \epsilon_{33}^\sigma E_3^2 \right). \quad (20)$$

The same process for lower piezoelectric and substrate yields to

$$dU_l^p = \frac{1}{2}e_l^p\sigma_l^p + \frac{1}{2}D_3^pE_3 = \frac{1}{2}\left(\frac{y^2}{R_o^2}E_p - d_{31}^2E_pE_3^2 + \epsilon_{33}^\sigma E_3^2\right) \quad (21)$$

and

$$dU_s = \frac{1}{2}e_s\sigma_s = \frac{1}{2}E_s e_s^2 = \frac{y^2}{2R_o^2}E_s. \quad (22)$$

The total internal energy of the beam can be calculated by spatial integrating Equation (17) over the whole volume of the beam:

$$U_{beam} = \int_0^L \int_0^{w_b} \left[\int_{-(\frac{t_s}{2}+t_p)}^{-\frac{t_s}{2}} dU_l^p + \int_{-\frac{t_s}{2}}^{\frac{t_s}{2}} dU_s + \int_{\frac{t_s}{2}}^{\frac{t_s}{2}+t_p} dU_l^p \right] dx dy dz. \quad (23)$$

Replacing Equations (20)–(22) in Equation (23) leads to

$$U_{beam} = \int_0^L \int_0^{w_b} \left[\int_{-(\frac{t_s}{2}+t_p)}^{-\frac{t_s}{2}} \frac{1}{2} \left(\frac{y^2}{R_o^2} E_p - d_{31}^2 E_p E_3^2 + \epsilon_{33}^\sigma E_3^2 \right) + \int_{-\frac{t_s}{2}}^{\frac{t_s}{2}} \left(\frac{y^2}{2R_o^2} E_s \right) \right. \\ \left. + \int_{\frac{t_s}{2}}^{\frac{t_s}{2}+t_p} \frac{1}{2} \left(\frac{y^2}{R_o^2} E_p - d_{31}^2 E_p E_3^2 + \epsilon_{33}^\sigma E_3^2 \right) \right] dx dy dz. \quad (24)$$

As stated in Equation (14), the curvature radius is a function of the moment. The applied periodic tip force causes a moment at each section in x , presented by Equation (25). The diameter of the tip mass magnet is neglected in Equation (25).

$$M(x) = F(L - x). \quad (25)$$

Substituting Equation (25) in Equation (14) yields to

$$\frac{1}{R_o(x)} = \frac{12(FL - Fx + \Delta)}{w_b \lambda}. \quad (26)$$

By considering the electromechanical coupling coefficient, $k_{31} (= d_{31}^2 E_p / \epsilon_{33}^\sigma)$, the total internal energy of the beam, Equation (24), can be simplified by

$$U_{beam} = \int_0^L \left[\frac{\lambda w_b}{24(R_o(x))^2} - w_b \epsilon_{33}^\sigma t_p E_3^2 (1 - k_{31}^2) \right] dx. \quad (27)$$

For parallel electrical connection of electrodes we have ($E_3 = V/t_p$), where V is externally applied voltage, V , substituting Equations (13) and (26) in Equation (27) and integrating over the length of the beam, yields to

$$U_{beam} = \frac{2F^2 L^3}{w_b \lambda} + \frac{6L^2}{\lambda} d_{31} E_p (t_s + t_p) F V \\ + \left[\frac{\epsilon_{33}^\sigma}{t_p} w_b L (1 - k_{31}^2) + \frac{6L}{\lambda} d_{31}^2 E_p^2 w_b (t_s + t_p)^2 \right] V^2. \quad (28)$$

The generated charge value on the electrodes because of externally applied voltage, V , and tip force, F , can be calculated by differentiating internal energy to V :

$$Q = \frac{\partial U_{beam}}{\partial V} = \frac{6L^2}{\lambda} d_{31} E_p (t_s + t_p) F \\ + 2 \left[\frac{\epsilon_{33}^\sigma}{t_p} w_b L (1 - k_{31}^2) + \frac{6L}{\lambda} d_{31}^2 E_p^2 w_b (t_s + t_p)^2 \right] V. \quad (29)$$

For a harvester under external tip force with no external applied voltage ($V = 0$), the generated charge can be calculated by Equation (30):

$$Q = \frac{\partial U_{beam}}{\partial V} = \frac{6L^2}{\lambda} d_{31} E_p (t_s + t_p) F. \quad (30)$$

The tip deflection, δ , of the beam under externally applied voltage, V , and tip force F can be calculated as

$$\delta = \frac{\partial U_{beam}}{\partial F} = \frac{4FL^3}{w_b \lambda} + \frac{6L^2}{\lambda} d_{31} E_p (t_s + t_p) V. \quad (31)$$

Thus, for the harvester under external tip force with no external applied voltage ($V = 0$), tip deflection can be calculated by Equation (32):

$$\delta = \frac{4FL^3}{w_b \lambda}. \quad (32)$$

By replacing Equations (12) and (16) in Equation (32), the well-known relationship between tip deflection and tip force can be confirmed in Equation (33) [26]:

$$\delta = \frac{FL^3}{3EI}. \quad (33)$$

In the energy regulator module (Figure 3a), the generated voltage by the CTLPH is rectified by a germanium bridge diode. The rectified voltage is stored in a parallel capacitor called a storage capacitor, C_{in} . With the use of Equation (30) and considering ($L w_b$) as the surface of the electrode, the voltage across the storage capacitor can be calculated as [27]

$$V_{in} = \frac{Q}{C_{piezo} + C_{in}}. \quad (34)$$

By substituting Equation (30) in Equation (34) and assuming $C_{piezo} \gg C_{in}$, Equation (34) can be presented as Equation (35):

$$V_{in} = \frac{6L^2 d_{31} E_p (t_s + t_p) F}{\lambda C_{in}}. \quad (35)$$

It is obvious that any piezoelectric material with a larger d_{31} can generate a higher voltage. As shown in Figure 3b, the external load, a purely electrical resistance, is parallel to the output capacitor (C_{out}) of the voltage regulator module, LTC3588. In Figure 4, the discharging voltage level of the C_{out} , ΔV_{out} , is the voltage difference between the fully charged condition (i.e., point A) and the partially discharged condition (i.e., point B). Based on the energy conservation principle, the stored energy in C_{out} is equal to the dissipated energy on the external load, E_{out} , which can be calculated by Equation (36):

$$E_{out} = \frac{1}{2} C_{out} (\Delta V_{out})^2. \quad (36)$$

Depending on the resistor values in the RC circuit of Figure 3b, the discharge period, T_{dis} , varies. Therefore, the power dissipated on the resistor can be calculated by Equation (37):

$$P = \frac{E_{out}}{T_{dis}} = \frac{C_{out} (\Delta V_{out})^2}{2 T_{dis}} \quad (37)$$

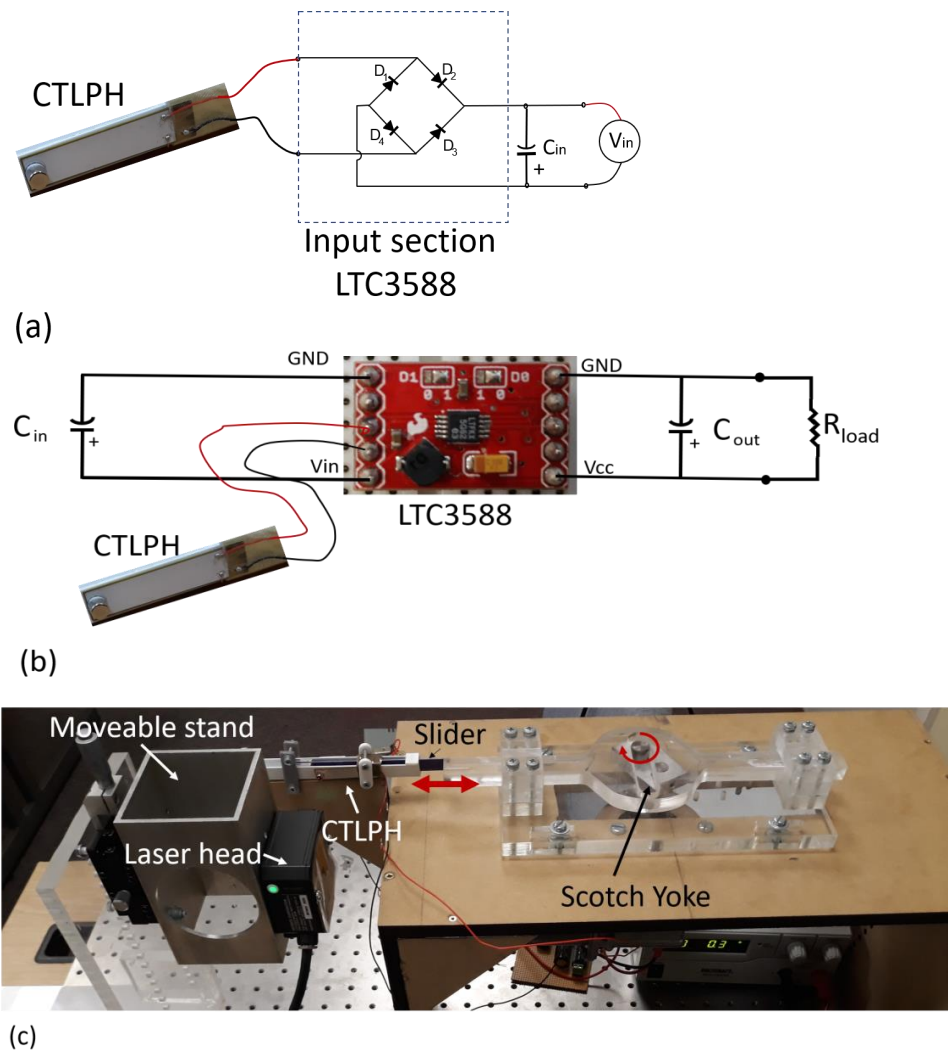


Figure 3. Performance evaluation. (a) Germanium diode bridge (1N34A) of the input section of LTC3588. (b) Connection of energy regulator module, LTC3588. (c) Driving and measurement setup.

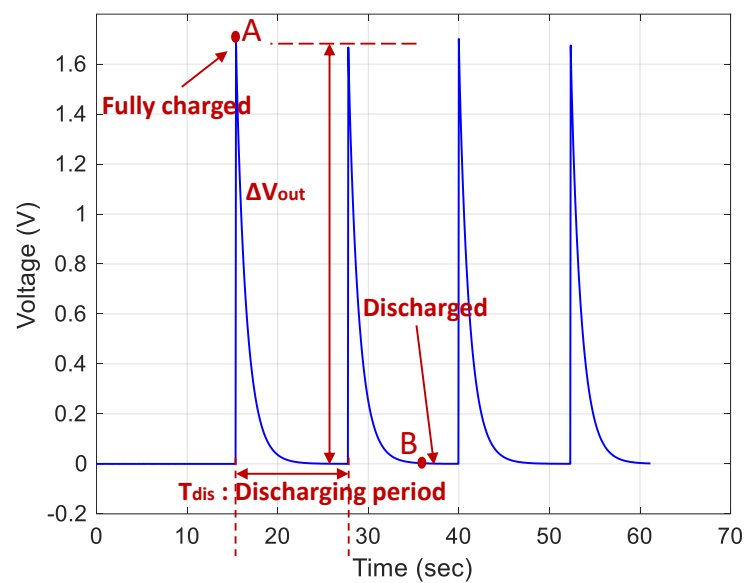


Figure 4. Discharging voltage versus time when LTC3588 is connected to the external load $R_{load} = 20 \text{ k}\Omega$; $C_{in} = 22 \text{ }\mu\text{F}$; $C_{out} = 47 \text{ }\mu\text{F}$; and $f = 2.88 \text{ Hz}$.

4. Methodology

To examine Equation (35), the effect of C_{in} on V_{in} , the input section of LTC3588 should be simulated by using a diode bridge. Then, a germanium diode bridge (1N34A) was employed to rectify the CLTPH output and store it in various C_{in} , (Figure 3a). LTC 3588 was also used to regulate the output voltage of the CLTPH (Figure 3b). To investigate the performance of the harvester, a reciprocated mechanism, depicted in Figure 3c, was employed. In this mechanism, a slider with a tip magnet is coupled with a Scotch yoke to generate a reciprocated motion with adjustable frequency. The variable low frequency (1–3.2 Hz) of the reciprocating motion is achievable by changing the energizing voltage of the DC motor. The specifications of the employed CTLPH are presented in Table 1. As shown in Figure 3c, a very sensitive laser displacement sensor, model HK-052, measures the vibration amplitude at the tip of the beam and the tip displacement (δ) without mechanical contact [28]. To collect the data, the National Instrument data acquisition card BNC-2110 was employed. To compare the results, the triple-layer harvester is composed of a brass strip ($t_s = 0.11$ mm, $E_s = 110$ GPa) that is sandwiched between two PZT-5H layers ($t_p = 0.225$ mm, $E_p = 60$ GPa). The material constants of PZH-5H are given by $d_{31} = -270 \times 10^{-12}$ C/N, $k_{31} = 0.38$, and $\epsilon_{33}^T/\epsilon_0 = 3500$ [29].

Table 1. Parameters of employed CTLPH sample in the experiment.

	Substrate Layer	Piezoelectric Layer	Tip Mass	Triple-Layer Beam
Material	Brass	PZT-5H	NdFeB-N35	PZT-Brass-PZT
Dimensions (mm)	$40 \times 10 \times 0.11$	$40 \times 10 \times 0.225$	$\varnothing 5 \times 5$	$40 \times 10 \times 0.56$
Elastic modulus (GPa)	110	60	38	—
Density (kg/m ³)	7800	6500	7500	—
Mass (kg)	0.00034	0.00058	0.00075	0.0015

5. Results and Discussion

5.1. Tip Force

The analytical relationship of Equation (35) predicts the effect of applied force, F , material properties (i.e., elastic modulus, electromechanical coupling coefficient), geometrical dimensions (i.e., the thickness of layers and length of the beam), and the storage capacitance (C_{in}) on generated voltage by the harvester. The values of all of the parameters can be found in the catalog of the piezoelectric material manufacturer or can be measured. Figure 5 shows the tip deflection of the CTLPH when the slider reciprocates at various low frequencies. The maximum deflection for all frequencies is about 2.7 mm. In the next step, considering the values in Table 1, bending stiffness, EI , can be computed as $0.0088 \text{ N}\cdot\text{m}^2$ using Equation (16). By replacing the bending stiffness value ($EI = 0.0088 \text{ N}\cdot\text{m}^2$) and maximum tip deflection $\delta_{max} = 2.7$ mm, in (33), the maximum applied tip force can be specified, $F = 3EI \times \delta/L^3 = 3 \times 0.0088 \times 0.0027/0.035^3 = 1.66 \text{ N}$.

5.2. Storage or Input Voltage

In this section, the performance of the employed CTLPH (specifications in Table 1) was investigated when it was connected to the germanium diode bridge. As depicted in Figure 4a by changing the storage capacitors (C_{in}), the voltage across the storage capacitors (V_{in}) was measured. Figure 6 shows V_{in} versus time for a variety of C_{in} values; the higher C_{in} , the lower the storage voltage. Figure 7 shows V_{in} versus C_{in} at a given time of 2 s. This figure confirms that the stored voltage (V_{in}) has a reverse relationship with C_{in} , as Equation (35) suggests.

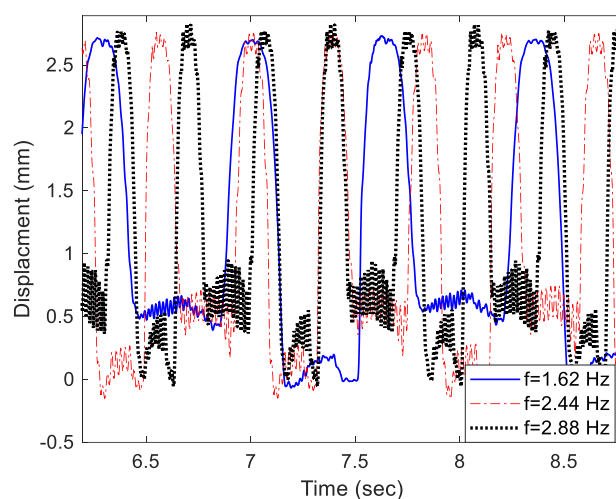


Figure 5. Tip deflection measurement of CTLPH at various slider frequencies.

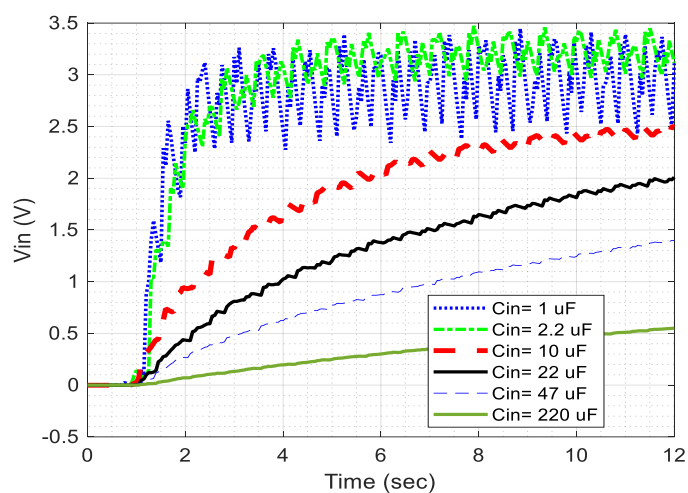


Figure 6. Storage voltage (V_{in}) vs. time for various storage capacitors (C_{in}); $f = 3.3$ Hz.

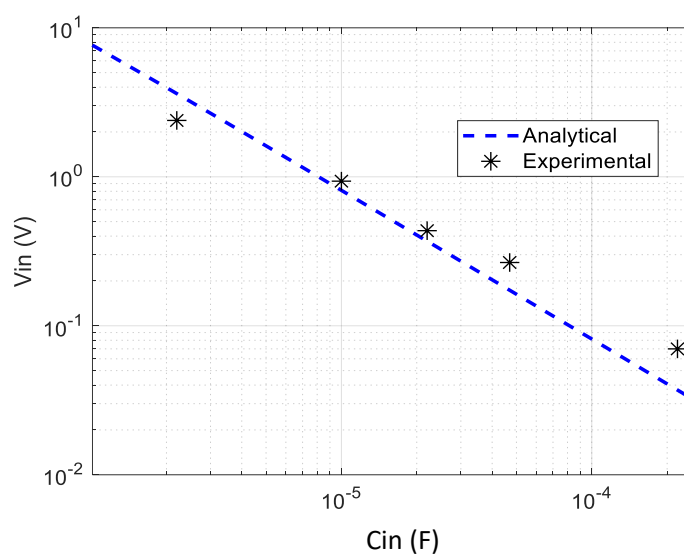


Figure 7. Effect of the storage capacitor (C_{in}) on the storage voltage (V_{in}) after 2 s; $f = 3.3$ Hz.

5.3. Output Voltage and Power with LTC3588

In this section, an energy storage module, LTC3588, is employed to regulate the output harvested voltage and power. Since the employed storage module is commercialised and its simulator is not available, it was required to characterise it. Then, the output terminals of the CTLPH were connected to the input terminals of the LTC3588 and the effect of the variable parameters, such as motion frequencies (up to 3.2 Hz), storage capacitors (C_{in}), output capacitors (C_{out}), and resistive loads were investigated. The rectified voltage (after the germanium diode bridge) is stored in the storage capacitor (C_{in}). In each reciprocated motion, generated by the Scotch Yoke, the bending deflection of the CTLPH increases the accumulated charges on the C_{in} , which is proportional to V_{in} .

5.3.1. Effect of Frequency

Figure 8 shows that the output voltage increases steeply across the C_{out} terminals when the CTLPH is bent by variable frequency. Since the output voltage of LTC3588 is set at 3.3 V, the output voltage cannot exceed this value. This figure highlights that higher frequency causes faster charging and reaches the set value of 3.3 V. The generated charge in low frequency (e.g., $f = 1.62$ and 1 Hz) does not generate a voltage in the monitoring period of 120 s.

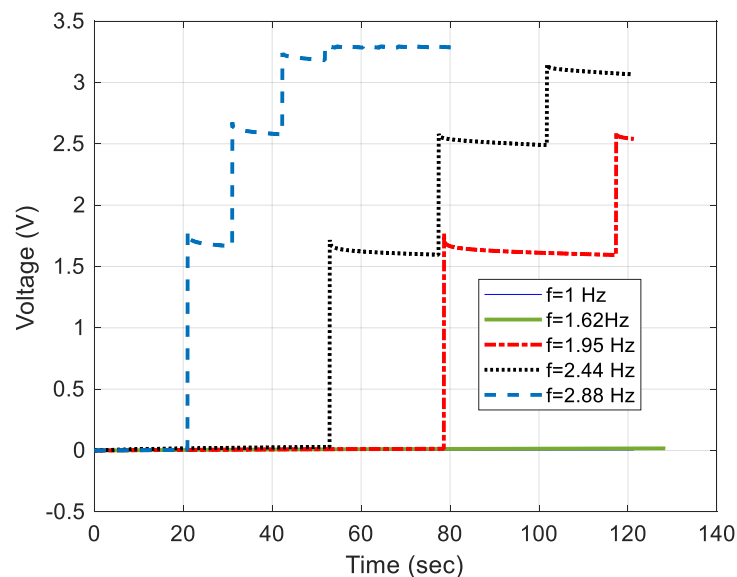
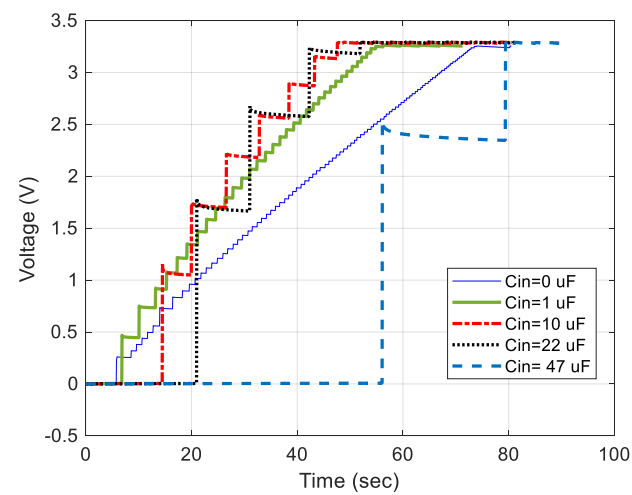


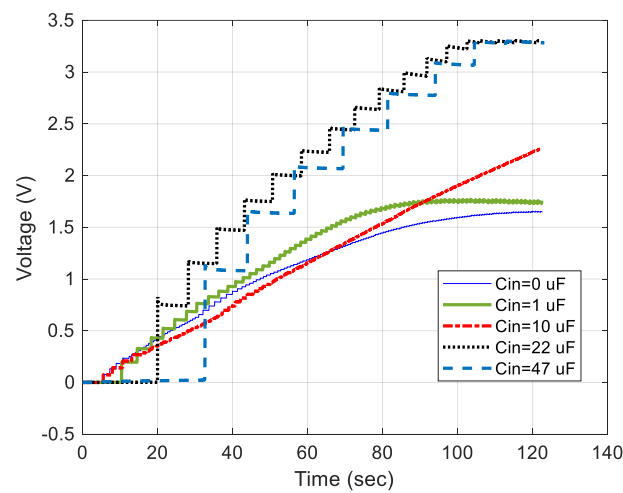
Figure 8. Frequency effect on the open circuit output voltage of LTC3588; $C_{in} = 22 \mu\text{F}$, $C_{out} = 47 \mu\text{F}$.

5.3.2. Effect of Storage and Output Capacitors

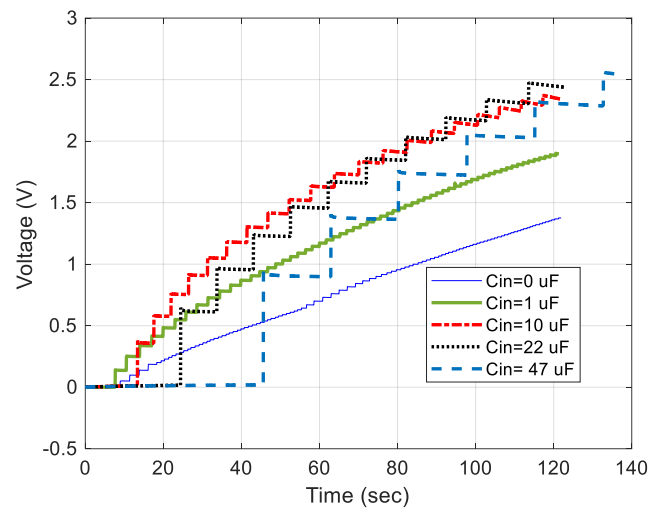
The effect of the storage capacitor, C_{in} , and output capacitor, C_{out} , on the output voltage (V_{out}) is manifested in Figure 9 when the slider moves at 2.88 Hz in an open circuit condition. For the same charge generated by the CTLPH, a lower C_{in} , causes a larger V_{in} . By increasing the C_{in} , more charges need to be stored to reach the threshold voltage value. In other words, a higher charging period causes later charge transportation to the output capacitor. Comparison of Figure 9a–c for any C_{in} (e.g., for $C_{in} = 22 \mu\text{F}$) show lower C_{out} , which leads to higher V_{out} .



(a)



(b)



(c)

Figure 9. The output voltage of LTC3588 versus time for different values of C_{in} and for open circuit; $f = 2.88 \text{ Hz}$ (a) $C_{out} = 47 \mu\text{F}$, (b) $C_{out} = 220 \mu\text{F}$, and (c) $C_{out} = 330 \mu\text{F}$.

5.3.3. Effect of Resistive Load

To investigate the effect of load (i.e., resistive type) on the output power of the CTLPH, we measured the generated energy and power for one discharging period, T_{dis} . Figure 10 emphasises again the role of C_{out} to provide output voltage with a lower ripple or smaller ΔV_{out} .

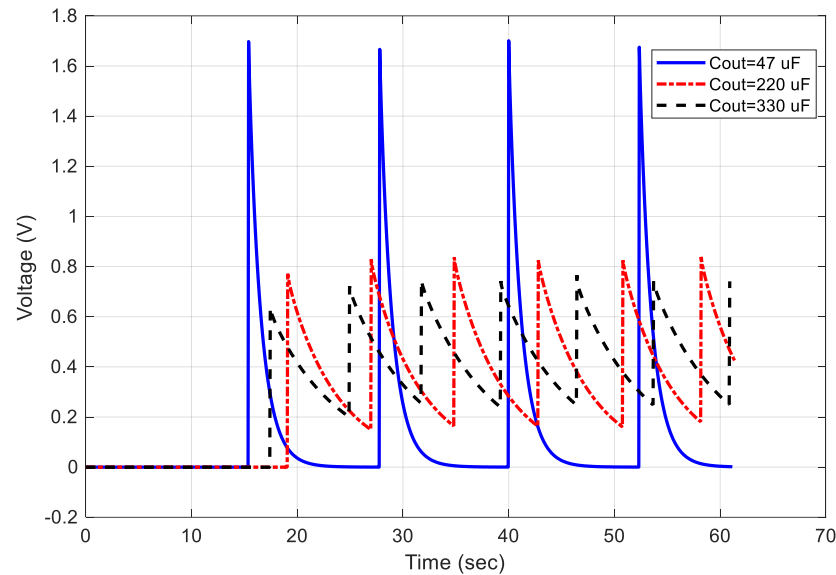


Figure 10. The output voltage of LTC3588 versus time for different values of C_{out} , when LTC3588 is connected to the external load $R_{load} = 20 \text{ k}\Omega$; $C_{in} = 22 \text{ }\mu\text{F}$; and $f = 2.88 \text{ Hz}$.

Figure 11 also highlights the electrical resistive load effect on the discharging period, T_{dis} , where larger resistance increases T_{dis} . Changing load value affects both the ΔV_{out} and T_{dis} . By substituting the measured values of ΔV_{out} and T_{dis} in Equation (37), the generated power of each resistive load, R_{load} , can be calculated (Figure 12). When the load is small, the voltage drop across the load is low (e.g., in a short circuit condition the output voltage is zero). By increasing the external resistive load, the output voltage (voltage drop across the external load) varies. Furthermore, higher excitation frequency causes a faster storage or voltage raise. Figure 12 shows that the power will reach its maximum value in a specific resistance and mitigates in the higher values. As an example, ΔV_{out} was measured at 1.9 V for $R = 20 \text{ k}\Omega$ at the frequency of 3.2 Hz. By substituting the measured value of ΔV_{out} in (36), the discharge energy from the output capacitor ($C_{out} = 47 \text{ }\mu\text{F}$) is 84.83 μJ . Considering $T_{dis} = 4.9 \text{ s}$, it causes a power of 17.31 μW . Similarly, the maximum power for 2.44 and 2.88 Hz at 20 k Ω would be 2.23 and 5.48 μW , respectively. In other words, the maximum output power of the CTLPH combined with LTC3588 module is realised when it is connected to a 20 k Ω external load. In other words, the proposed CTLPH in this research with 17.31 μW output power is a good candidate to empower microelectronic sensors or biomedical implants (e.g., 30 μW pacemakers). Compared with other harvesters presented in Table 2, the highest power density of this work (i.e., 77.2 $\mu\text{W}/\text{cm}^3$) can be related to many factors, such as piezoelectric coefficient (d_{31}) or amplitude of applied tip force (as shown in Equation (35)). Although higher applied force can generate higher voltage, it leads to more microstructural cracks and lower longevity of the harvester. Therefore, a trade-off between lifespan and power density should be considered for real-life applications.

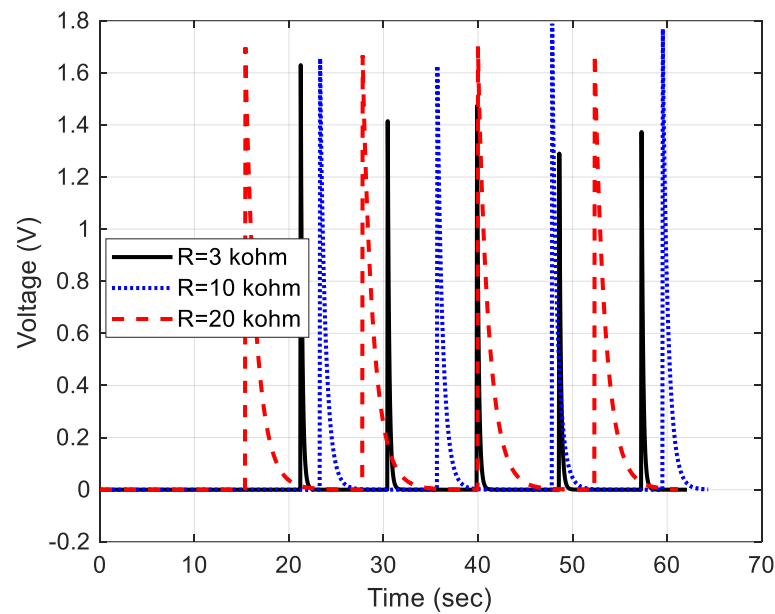


Figure 11. Sample of discharging voltage of LTC3588 when connected to the various external load; $C_{in} = 22 \mu\text{F}$; $C_{out} = 47 \mu\text{F}$; and $f = 2.88 \text{ Hz}$.

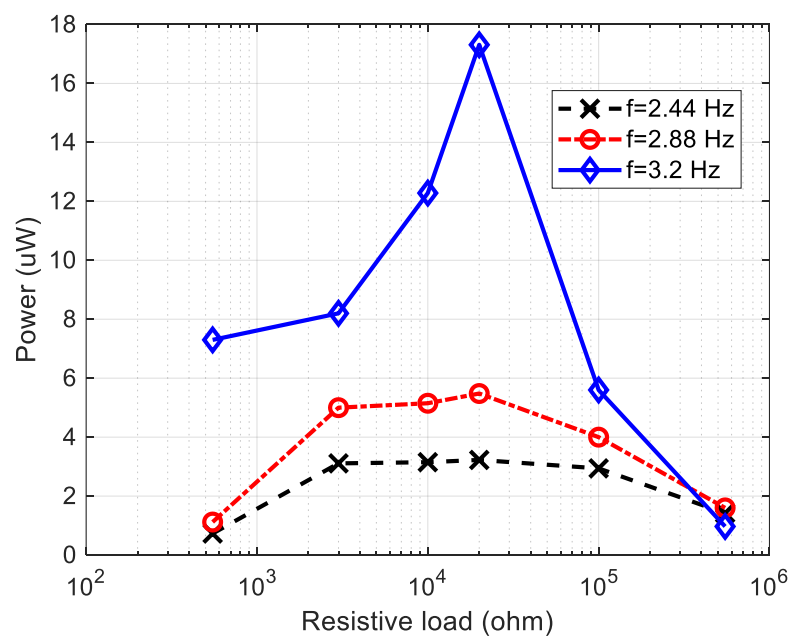


Figure 12. Generated power versus external resistance load for different motion frequencies; $C_{in} = 22 \mu\text{F}$; and $C_{out} = 47 \mu\text{F}$.

Table 2. Comparison of the output power of similar piezoelectric harvester.

Ref.	Dimensions (mm)	Material	Frequency (Hz)	Power (μW)	Resistance ($\text{M}\Omega$)	Power Density ($\mu\text{W}/\text{cm}^3$)
[30]	$160 \times 85 \times 85$	Unknow PZT	2.03	13290	0.54	11.5
[31]	$40 \times 70 \times 35$	PVDF	3.4	65.8	15	0.67
[32]	$48 \times 10 \times 65$	Unknow PZT	1	35	3	1.12
[33]	$300 \times 200 \times 250$	PZT 5J	2.5	146	0.5	0.00973
This work	$40 \times 10 \times 0.56$	PZT-5H	3.2	17.31	0.02	77.2

6. Conclusions

A design guideline for kinetic energy conversion of a cantilever triple-layer piezoelectric harvester (CTLPH) for a low-frequency excitation is presented. The effective parameters of CTLPH were determined by combining constitutive equations with internal energy equations, resulting in the prediction of output voltage and power generated by the harvester. The model revealed that the frequency of motion, applied tip force, piezoelectric coefficients, geometrical dimensions, and mechanical properties of the layers are all critical to the performance of the CTLPH. Furthermore, the dependency of output voltage on the storage (C_{in}) and output capacitor of the energy storage module, LTC3588, is investigated. An impractical measurement method without mechanical contact is employed to specify the applied tip force. The performance of the CTLPH in low frequencies (<3.3 Hz) for various resistive loads is also investigated. It was demonstrated that both the excitation frequency and external resistance load have an impact on the maximum generated power. The developed CTLPH generates the optimum power of 17.31 μ W at the external resistance of 20 k Ω , which is suitable for micropower implanted devices operating in environments with a minimum vibration frequency of 3.2 Hz.

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