



Article Selective Catalytic Removal of High Concentrations of NO_x at Low Temperature

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Abstract: Three vanadium-based catalysts were used to remove high concentrations of nitrogen oxides, and the catalysts' performance of de-NO_x and anti-H₂O under the high concentrations of NO_x were investigated. The V-Mo-W/TiO₂ catalysts were tested under 1500 mL/min gas flow (GHSV = 500 h⁻¹, 2.4% NO₂, 4.78% NH₃, 13% O₂, 4% H₂O, 5% CO₂) and characterized by BET, SEM, EDS, XRD, XPS, H₂-TPR, and NH₃-TPD; then, their physical and chemical properties were analyzed. The results showed that under the influence of H₂O, the NO_x conversion of the V-Mo-W/TiO₂ catalysts remained above 97% at 200–280 °C indicating that the catalysts had high catalytic activity and strong water resistance. The analysis of the characterization results showed that the larger specific surface area of the catalyst, the higher acid content, stronger redox ability, and higher V⁴⁺ and V³⁺ content were the reasons for the high NO_x conversion. The surface area decreased and the microstructure become smoother after the reaction, which may be caused by thermal sintering, but the overall morphology did not change. Comparing the H₂-TPR and NH₃-TPD of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ before and after NH₃-SCR reaction, it was found that the reduction peak and the intensity of the acid sites of the sample had not changed, which indicated that the catalyst had good anti-sintering performance and a long lifetime. This is significant for followup long-term engineering application experiments.

Keywords: high concentration; NOx; SCR; V-Mo-W; NH3

1. Introduction

Extensive use of fossil fuels produce pollutants such as nitrogen oxides [1–3], causing great damage to the environment. The generated NO_x causes environmental problems such as acid rain, photochemical smog, and ozone layer destruction [4–6] and great harm to human health. Therefore, how to efficiently remove NO_x has become a hot spot in environmental management.

In the treatment of nitrogen oxides, the commonly used technology is selective catalytic reduction (SCR) [7,8], in which the selective reduction of NO_x with NH_3 as a reductant [9] under the action of a catalyst is one of the most effective and widely used NO_x removal technologies. With NH_3 as the reductant, the reaction equations [10] are mainly divided into the following categories:

- (1) The standard SCR reaction: $4NH_3 + 4NO + O_2 = 4N_2 + 6H_2O_2$;
- (2) The NO₂-SCR reaction: $4NH_3 + 2NO_2 + O_2 = 3N_2 + 6H_2O$;
- (3) The fast SCR reaction: $4NH_3 + 2NO + 2NO_2 = 4N_2 + 6H_2O$.

For NH₃-SCR technology, its crux is the NH₃-SCR catalyst [11–13]. In today's industry, the most widely used catalyst is V-W/TiO₂ [14–16]. The V-W/TiO₂ catalyst has good catalytic activity at a mid-range temperature and outstanding performance in sulfur resistance. The studies in [17,18] found that the VOx in the V/TiO₂ catalyst mainly existed in the form



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). of monomeric vanadyl species and polymeric vanadyl species, and the NH₃-SCR activity is higher in the form of polymeric vanadyl species. Yadolah et al. [19] studied the effect of anatase TiO₂ on the performance of VOx-TiO₂ by in situ spectroscopies, arguing that the ability to form V-pairs appeared to be the only requirement for catalytic activity. At present, the surface acidity and thermal stability of the V/TiO₂ catalysts have mainly been improved by introducing W [20–22], Mo [23,24], or Si, thereby enhancing their NH₃-SCR activity. Lai et al. [25] studied the catalytic active sites, reaction mechanism, and reaction kinetics in the NH₃-SCR process through the V₂O₅-WO₃/TiO₂ catalyst. Chen et al. [26] found that the doping of W promoted electron transfer, thereby generating more highly active V⁴⁺ and V³⁺. Pan et al. [27] used the sol–gel method to support Si on V₂O₅/TiO₂ for modification and found that the number of acid sites and oxidation performance of Si-doped V₂O₅/TiO₂ catalysts improved, thereby improving the catalytic activity for denitrification. In addition, Kobayashi et al. [28] used the coprecipitation method to prepare V₂O₅/SiO₂-TiO₂ and found that the catalytic activity of the catalyst was improved, and its durability was greatly increased.

However, the production process of nitric acid, uranyl nitrate, etc., introduces the problem of high concentrations of NO_x in flue gas. In the production of uranium oxide by denitration of uranyl nitrate, the reaction is "UO₂ (NO₃)₂·6H₂O \rightarrow UO₃ + 1.86NO₂ + 0.14NO + 0.57O₂ + 6H₂O" [29]. In the industrial production of UO₃, it will decompose to produce ultra-high concentrations of NO_x, which far exceed the national standard. The waste gas generated in the production process of uranyl nitrate is mainly N₂, CO₂, NO₂, O₂, and H₂O, and the temperature is usually 200–500 °C; after some NO₂ is removed by spraying water, the NO₂ concentrations used are small, but the volumetric space velocity is large, which differs from most engineering.

Therefore, in this paper, high concentrations of nitrogen oxides were used for NH₃-SCR experiments, the NH₃-SCR efficiency of vanadium-titanium catalysts in an environment with high concentrations of nitrogen oxides was studied through a fixed-bed reactor, and the NH₃-SCR activity of V-W-Mo/TiO₂ was tested by comparative experiments. The microstructural changes before and after the reaction of the catalyst were analyzed.

2. Experiment

2.1. Catalysts' Preparation

We studied the removal of NO_x from the exhaust gas produced during uranyl nitrate denitrification to produce UO₃ by NH₃-SCR. After investigation, three common commercial catalysts were selected for the NH₃-SCR experiments, which have been widely applied in flue gas denitrification projects and provide a reference for subsequent projects. The catalysts were prepared by the mixing process of an SCR honeycomb denitration catalyst [30], and the structures of the three catalysts are shown in Figure 1. The three catalysts used in the experiments were composed of V, Mo, W, Al, Si, Ti elements, etc. In addition to Ti, V, Mo, and W, the Al, Si, and other elements can enhance the mechanical properties of the catalyst. The catalysts were named $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ (V: 1.6 wt%, Mo: 1.7 wt%, W: 1.8 wt%), $V_{2.7}Mo_{3.0}W_{1.0}/TiO_2$ (V: 2.7 wt%, Mo: 3.0 wt%, W: 1.0 wt%), and $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$ (V: 1.6 wt%, Mo: 2.5 wt%), W: 0.5 wt%) respectively.

2.2. Catalysts' Characterization

X-ray Diffraction (XRD) was performed on a D8 ADVANCE X-ray diffractometer with a Cu K α radiation source, 2 θ were measured in the range of 10–90° in steps of 5°. The specific areas and pore sizes were measured in a Micromeritics ASAP 2020 analyzer and subjected to isothermal N₂ adsorption-desorption measurements at 220 °C. The morphology and microstructure were observed by Scanning Electron Microscope (SEM) and Energy-dispersive X-ray Spectroscopy (EDS) on a TESCAN G0AIA3 XMH. The X-ray Photoelectron Spectroscopy (XPS) was performed on the Thermo Scientific ESCALAB 250 Xi instrument, and the data of samples were calibrated using the C1s peak (284.8 eV). The Temperature Programmed Desorption of ammonia (NH₃-TPD) study was performed on an AutoChem II 2920 instrument; first, 0.1 g of the sample was pretreated in helium at 250 °C for 60 min. Then, after the sample was cooled to 80 °C, 5% NH₃ in helium was purged to the tube at a flow rate of 30 mL/min for 2 h; then, the temperature was raised from 80 to 600 °C at a rate of 10 °C/min in helium. The Temperature Programmed Reduction of hydrogen (H₂-TPR) data were acquired by an AutoChem II 2920 instrument; first, 0.1 g samples were pretreated in O₂ flow at 300 °C for 1 h. After the temperature of the samples was cooled to 30 °C, 10% H₂ in argon was flowed through the tube at a flow rate of 50 mL/min, as the temperature was raised from room temperature to 900 °C at a rate of 10 °C/min.



Figure 1. The structures of the three catalysts: (a) $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$; (b) $V_{2.7}Mo_{3.0}W_{1.0}/TiO_2$; (c) $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$.

2.3. Activity Test

The activity test of the catalyst was carried out on the fixed-bed catalyst evaluation device, as shown in Figure 2. The catalyst sample volume was 180 cm³ (30 mm × 30 mm × 200 mm with 30 holes). The total gas flow was 1500 mL/min, and the volumetric space velocity (GHSV) = 500 h⁻¹, in which the content of NO₂ was 2.4%, NH₃ varied with the ratio of NH₃:NO₂, O₂ was 13%, H₂O was 4%, CO₂ was 5%, and the balance gas was N₂. The catalyst was first heated to 200 °C in a nitrogen atmosphere. When the temperature remained unchanged, the mixed gas was passed into the reactor for the catalytic reaction, and a flue gas analyzer was used at the outlet of the reactor for exhaust gas detection. Due to the presence of NO₂ and H₂O in the inlet flue gas, some NO was produced in the gas and entered the reactor. The efficiency of the catalyst was calculated according to the following formula:

NO_x conversion (%) =
$$\left(1 - \frac{[NO_x]_{out}}{[NO_x]_{in}}\right) \times 100 (NO_x = NO + NO_2)$$
 (1)



Figure 2. Schematic diagram of the experimental apparatus for catalytic performance.

3. Results and Discussion

3.1. Catalytic Activity Evaluation

Figure 3 shows the change in the catalytic performance of $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$ with the ratio of NH₃:NO₂ at 220 °C. No matter the change in the ratio of NH₃:NO₂, the catalytic activity of NH₃-SCR of $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$ was excellent, and the NO_x conversion reached more than 96%. As the ratio of NH₃:NO₂ increased, the NO_x conversion also increased; however, when the ratio of NH₃:NO₂ exceeded 1.5, the increase in the rate of NO_x conversion became smaller.



Figure 3. The relationship between the de-NO_x efficiency of $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$ and the ratio of NH₃:NO₂ at 220 °C.

Figure 4 shows the NH₃-SCR catalytic performance of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂, V_{2.7}Mo_{3.0}W_{1.0}/TiO₂, and V_{1.6}Mo_{2.5}W_{0.5}/TiO₂ at 200–280 °C, when the ratio of NH₃:NO₂ was 2. At high concentrations of nitrogen oxides and 4% H₂O, the catalytic activity of the NH₃-SCR of the three catalysts in the range of 200–280 °C was generally excellent, and the NO_x conversion reached more than 97%. Among them, the catalytic activity of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ was the highest. The three catalysts showed strong anti-H₂O ability.



Figure 4. The NO_x conversion of the three catalysts.

3.2. *Characterization of the Catalysts* 3.2.1. BET

According to the experiment, the samples of the three catalysts were subjected to BET characterization test to understand the changes in the specific surface area, pore volume, and average pore diameter of each catalyst before and after the reaction, so as to better study and analyze the catalysts. The BET test results are shown in Table 1:

Table 1. BET test results of the three catalysts.

| Catalyst | | Surface Area (m ² /g) | Surface Area Reduction Percentage (%) | Pore Volume (cm ³ /g) | Pore Size (nm) |
|---|-----------------------------------|-------------------------------------|--|-------------------------------------|----------------|
| V _{1.6} Mo _{1.7} W _{1.8} /TiO ₂ | before reaction after reaction | 75.23 70.95 | 5.69 | 0.267 0.250 | 11.54 11.64 |
| V _{2.7} Mo _{3.0} W _{1.0} /TiO ₂ | before reaction after reaction | 70.90 66.66 | 5.98 | 0.284 0.297 | 13.32 12.88 |
| V _{1.6} Mo _{2.5} W _{0.5} /TiO ₂ | before reaction after reaction | 83.14 63.94 | 23.09 | 0.303 0.251 | 12.59 12.39 |

As shown in Table 1, the surface area of these three catalysts was around 70–80 m²/g, and the V_{1.6}Mo_{2.5}W_{0.5}/TiO₂ had the highest surface area, which was 83.14 m²/g; however, after the reaction, the surface area of the three catalysts decreased, and the surface area of V_{1.6}Mo_{2.5}W_{0.5}/TiO₂ decreased the most, followed by V_{2.7}Mo_{3.0}W_{1.0}/TiO₂, and V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ decreased the least. This may be one of the reasons for the highest catalytic activity of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂. In addition, the pore volume and pore size of the three catalysts were not significantly different, which also indicated that the activity of the three catalysts before and after the NH₃-SCR reaction, the catalysts after the reaction had decreased, but the difference was not large. The reason for the decrease in surface area may be the valence change of the V and Mo atoms and thermal sintering [31].

3.2.2. Morphology Evolution

The SEM/EDS images in Figures 5 and 6, respectively, display the morphology and sizes of the V-rich, Mo-rich, and W-rich particles of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before and after the NH₃-SCR reaction. It can be seen from Figure 5a that the combination of the active components and the catalyst was good, the catalyst surface before the NH₃-SCR reaction was smooth, and the structure was relatively tight. As shown in Figure 6a, the microstructure of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ became smoother after the NH₃-SCR reaction; however, it can be seen that the morphology of the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ did not change much after the NH₃-SCR reaction, and the original structure was basically maintained. The stability of the catalyst was high, which was also reflected in the activity test. Comparing the EDS images before and after the NH₃-SCR reaction, the V and Mo elements were uniformly distributed in the catalyst, but the W element appeared agglomerated after the NH₃-SCR reaction, which may be caused by thermal sintering [31].

3.2.3. XRD

In order to better determine the material structure of the catalyst, the catalyst crystal was further tested by the XRD characterization method. It can be seen from Figure 6a–c that the XRD peak patterns of the three catalysts were basically the same, and the main structural substances were TiO₂. Comparing the XRD images of the three catalysts before and after the NH₃-SCR reaction, it can be found that the crystal changed little after the reaction. As shown in Figure 7a–c, the presence of anatase TiO₂ peaks can be clearly observed in the XRD images, and the X-ray diffraction peaks appeared at 25.3°, 37.8°, 48°, 54°, 55°, 62.8°, 69°, 70.3°, and 75°. The peak shape was sharp, the intensity was large, and the crystallinity was good. At the same time, no other diffraction peaks were detected. This

showed that the metal oxides of V and Mo were evenly dispersed on the surface of the TiO_2 support, and the crystal form of the support was not affected [32]. This was consistent with the characterization results of the SEM and EDS.



Figure 5. Morphology of the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before reaction. (a) SEM image, 10.0 kx; (b) EDS image V element dispersion; (c) EDS image Mo element dispersion; (d) EDS image W element dispersion.



Figure 6. Morphology of the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ after reaction. (a) SEM image, 10.0 kx; (b) EDS image V element dispersion; (c) EDS image Mo element dispersion; (d) EDS image W element dispersion.

Intensity/a.u

10



Figure 7. XRD pattern of three catalysts: (a) $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$; (b) $V_{2.7}Mo_{3.0}W_{1.0}/TiO_2$; (c) $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$.

60

V_{1.6}Mo_{2.5}W_{0.5}/TiO₂ before reaction

70

80

3.2.4. XPS

 $1\overline{0}$

20

30

40

2θ/ degree (c)

50

Figure 8a shows the XPS spectra of O1s for the samples. The peak at 530 eV was attributed to lattice oxygen (O_{β}), while the peak at 532 eV corresponded to chemisorbed oxygen (O_{α}). The ratios of $O_{\alpha}/(O_{\alpha} + O_{\beta})$ of the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$, $V_{2.7}Mo_{3.0}W_{1.0}/TiO_2$, and $V_{1.6}Mo_{2.5}W_{0.5}/TiO_2$ were 0.127, 0.220, and 0.143, respectively. The chemisorbed oxygen played an important role in the oxidation reactions due to its high mobility, and high O_{α} content can promote "fast SCR" reactions [33]. Figure 9a shows the XPS spectra of O1s for $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$, in which the content of O_{α} increased after the NH₃-SCR reaction. As shown in Table 2, the ratio of $O_{\alpha}/(O_{\alpha} + O_{\beta})$ in the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ after the NH₃-SCR reaction increased from 12.74% to 16.36%, which was helpful for the stability of the reactivity of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$.



Figure 8. Deconvoluted XPS spectra of the three catalysts: (a) O1s; (b) Mo3d; (c) V2p.

Table 2. The chemical states and the ratios of the relative concentrations of O, V, and Mo for different catalysts.

| Catalyst | Ο _β (%) | O _α (%) | $O_{\alpha}/(O_{\alpha} + O_{\beta})$ (%) | $(V^{3+} + V^{4+})/V^{5+}$ (%) | Mo ⁶⁺ /(Mo ⁶⁺ + Mo ⁵⁺ + Mo ⁴⁺) (%) |
|---|--------------------|--------------------|---|--------------------------------|--|
| $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before reaction | 87.3% | 12.7% | 0.127 | 2.967 | 0.392 |
| $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ after reaction | 83.6% | 16.4% | 0.164 | 6.541 | 0.600 |
| V _{2.7} Mo _{3.0} W _{1.0} /TiO ₂ | 78.1% | 21.9% | 0.220 | 1.985 | 0.627 |
| V _{1.6} Mo _{2.5} W _{0.5} /TiO ₂ | 85.7% | 14.3% | 0.143 | 2.901 | 0.894 |

Figure 8b shows the XPS spectra of Mo3d for the catalysts. The peaks at 230.5 eV and 232.8 eV were peaks of Mo^{4+} , the peaks at 231.5 eV and 234.6 eV were attributed to Mo^{5+} , and the peaks of Mo^{6+} corresponded to the binding energies of 232.9 and 235.9 eV. As shown in Table 2, the $Mo^{6+}/(Mo^{6+} + Mo^{5+} + Mo^{4+})$ ratio of the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ was the smallest, which was 0.392. As shown in Figure 9b, the ratio of $Mo^{6+}/(Mo^{6+} + Mo^{5+} + Mo^{4+})$ increased after the SCR reaction, because an increase in the content of V^{4+} and Mo^{6+} resulted from the transfer of electrons in the Mo-O-V species between V^{5+} and Mo^{4+} and Mo^{5+} , the imbalance of which charged oxygen deficiency, which was beneficial to the catalyst activity [34].

Figure 8c shows the XPS spectra of V2p for the samples, and Figure 9c shows the XPS spectra of V2p for the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before and after reaction. The peaks around 517.3 eV and 525.4 eV were characteristic peaks of V⁵⁺, the peaks around 516.3 eV and 523.7 eV corresponded to V⁴⁺, and the peaks at 515.1 eV and 522.5 eV were assigned to V³⁺. It can be seen from Table 2 that the ratio of $(V^{3+} + V^{4+})/V^{5+}$ of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ was 2.97, which was higher than other catalysts. According to the literature, low-valence vanadium oxides can easily adsorb oxygen to generate reactive oxygen species during the

SCR reaction, which was significant for the low-temperature SCR activity [35,36]. It can be seen from Table 2 that the ratio of $(V^{3+} + V^{4+})/V^{5+}$ in the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ increased after the NH₃-SCR reaction, which was helpful for the catalytic activity. The V⁴⁺ and V⁵⁺ on the surface of the NH₃-SCR catalyst mainly existed in the form of V-OH, and V = O. NO was oxidized to NO₂, and V⁵⁺ = O was reduced to V⁴⁺ - OH, both of which promoted the fast SCR reaction, thereby improving the low-temperature activity of the catalyst [37].



Figure 9. Deconvoluted XPS spectra of the V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ before and after reaction: (**a**) O1s; (**b**) Mo3d; (**c**) V2p.

3.2.5. H₂-TPR

H₂-TPR was carried out on the three catalyst samples, respectively, and the test results are shown in Figure 10a. The V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ had two reduction peaks. The reduction peak at around 500 °C corresponded to the reduction of the VO_x and MoO_x species on the V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ [38,39], while the reduction peak at 619 °C was attributed to the reduction of the TiO₂ (Ti⁴⁺ \rightarrow Ti³⁺) or V-O-Ti species [40,41]. The peak areas of the other two catalysts were comparable to those of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂, but the temperature of the reduction peak of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ was lower than that of the other two catalysts, which indicated that the reduction performance of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ was before and after reaction, which were located around 502 °C and 619 °C, respectively. The position of the reduction peak did not occur, which indicated that the catalytic activity of V_{1.6}Mo_{1.7}W_{1.8}/TiO₂ was relatively stable.



Figure 10. H₂-TPR profiles of the three catalysts: (a) the three fresh catalysts and (b) $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before and after reaction.

3.2.6. NH₃-TPD

As shown in Figure 11a, the catalyst of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ showed NH₃ desorption peaks at 207 °C and 447 °C. Affected by the partial NH⁴⁺ bound to the weakly acidic site (Brønsted acid), the NH₃ desorption peak of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ at 207 °C was the same as that of the other two catalysts, which was mainly attributed to the bridge structure of MoO_x or MoO_x and VO_x [42]; the NH₃ desorption peak at 447 °C was attributed to the desorption of the coordinated NH₃ bound to the strongly acidic site (Lewis acid). Compared with the other two catalysts, the strong acid site of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ was more intense, and the desorption temperature was lower. The higher the acidity of the catalyst, the more catalytically active the centers were, which was conducive to the progress of the catalytic reaction. As shown in Figure 11b, the NH₃ desorption peak of $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ remained basically unchanged after the NH₃-SCR reaction, which indicated that the catalyst had good stability.



Figure 11. NH₃-TPD of the three catalysts: (a) the three fresh catalysts and (b) $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ before and after reaction.

4. Conclusions

In summary, this study focused on examining the activity of the three catalysts used for NH₃-SCR at high concentrations of NO_x and on understanding the physical and chemical

properties of the catalysts that play an important role in catalysis at high concentrations of NO_x . Three catalysts were tested for NH_3 -SCR catalytic activity and the microstructure changes before and after the NH_3 -SCR reaction were analyzed using microscopic characterization methods. The conclusions include:

- (1) Under high concentration NO_x and $4\%H_2O$, the three vanadium-based catalysts all showed excellent de- NO_x activity, and the NO_x conversion reached more than 97% at 200–280 °C.
- (2) After the NH₃-SCR reaction, the valence changes in the V and Mo atoms and thermal sintering may lead to changes in the microstructure of the catalyst and thus reduce its lifetime.
- (3) The higher content of V⁴⁺ and V³⁺ and active oxygen on the surface of the catalysts were beneficial to the fast SCR reaction, which improved the low-temperature activity of the catalyst.
- (4) After the NH₃-SCR reaction, neither the microstructure of the catalyst intensely changed nor the acid content or the intensity of the reduction peak changed, which indicated that the $V_{1.6}Mo_{1.7}W_{1.8}/TiO_2$ had strong stability.

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