



# Article Lifetime Estimation Based Health Index and Conditional Factor for Underground Cable System

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**Abstract**: In this paper, a lifetime estimation method for underground cable systems is proposed by combining a health index (HI) and conditional factor (CF). The underground cable system consists of underground cable, joint, termination, manhole, and duct bank. The HI is an indicator to indicate the actual condition of underground cable components and systems whereas the CF is used to indicate different operating stresses of the system under different operating conditions such as percentage loading, electrical stresses, laying structure, environment, etc. The actual technical data as well as historical operating and testing records are applied. The weighting and scoring method with the analytical hierarchy process are used to classify an importance of underground cable components, testing methods, and criteria used in the HI and CF calculation. The annual calculated HIs are plotted to investigate the lifetime trending curve by using a polynomial function. The degradation curve based on calculated CF is estimated by using the Weibull distribution function. Finally, the remaining life of the underground cable system is determined by matching the lifetime trending curve with the degradation curve. Ten practical underground cable systems supplying power in a high voltage power delivery system are evaluated with effective results. The lifetime of the underground cable system cable system cable system and by using the factor of the underground cable system and the system is determined by matching the lifetime trending curve with the degradation curve. Ten practical underground cable systems supplying power in a high voltage power delivery system are evaluated with effective results. The lifetime of the underground cable system cable system cable system and supplying power in a high voltage power delivery system are evaluated.

**Keywords:** underground cable; lifetime estimation; health index; conditional factor; Weibull distribution; polynomial function

# 1. Introduction

Underground power cable systems have been widely used in many countries, not only in transmission and distribution systems but also in industrial areas. The number of cable installations keeps increasing to improve effectiveness, reliability, trustworthiness, cost, and risk of power systems as well as better aesthetic view of a community. Nevertheless, the increasing number of underground cable system failures has also been recognized. Both visible and invisible degradations of the cable system could be caused by installation defects, as well as electrical, thermal, and mechanical stresses as well as possible damages to installation sites and the operational environment [1,2]. Thus, to maintain the acceptable condition of a cable system, the utility needs to recognize the actual condition and the end of life of their own asset for proper management and effective planning of repair, renovation or replacement of the defective asset before damage [3]. Currently, many testing methods have been applied to assess the condition of underground cable systems and their components, such as partial discharge measurement to determine the type of defect [4] and localization technique [5,6], insulation resistance measurement and resistance of the earthing connection [7], ampacity and sheath voltage measurement [8], and thermography inspection [9], etc. Then, the quantitative health index, which regularly processes the inspection and testing results according to an organization's inspection interval to represent



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**Copyright:** © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). the actual condition of underground cable system, has been proposed in previous research works [10]. However, the proposed health index is static and probably only updated annually after the annual routine inspection and testing are performed. Since this static health index is annually evaluated and recorded in the central database, its decreasing trend can be observed from the plotting of its historical value against usage time and the remaining lifetime can be estimated [11]. This numerical technique is interesting, but it requires accuracy improvement to become an effective tool to facilitate the lifetime estimation of an underground cable system. In addition, the lifetime estimation of the underground cable system is of prime concern for utilities, especially as a novel technique to prevent the aging analysis of polymeric material from the cut sample of considered underground cable [12], which is nearly impossible to obtain from the highly significant cable route.

Therefore, this paper aims to estimate the remaining lifetime of underground cable systems based on predictive health index and the conditional factor to incorporate the degradation behavior of each underground cable system. Firstly, the future health index is predicted by applying the curve fitting technique to the plot of historical static health index values with usage time [13]. Theoretically, its end of lifetime can be estimated when the predictive health index is crossing the acceptable value. Then, to improve lifetime estimation accuracy, the conventional static health index is modified to the dynamic health index by incorporating the actual degradation of each individual cable route due to differences in operating condition, cable route configuration, network reliability, and operational environment [14,15], which is known as the conditional factor. Then, this modified or dynamic health index is plotted against usage time to accurately determine the remaining lifetime of each cable system. With the obtained remaining lifetime of each underground cable system, the organization can properly set up an effective plan for replacement of the existing underground cable routes based on available budgets and human resources [16].

The working procedure of this paper starts from the conventional static health index (HI) calculation for condition assessment of the underground cable system and its components by applying the weighting and scoring method (WSM) and the analytic hierarchy process (AHP). The scoring technique is used to transform the raw inspection and testing result from each test method to a quantitative value known as score, while the weighting technique is used to assign the numerical value representing the importance of each test method as well as the significance of each component in an underground cable system known as weighting value. To obtain the consensus of weighting determination in the organization, the analytic hierarchy process as a multi-criterion decision-making technique involving pairwise comparison is applied to solve complex decisions, which is difficult to quantify. The AHP technique is applied to brainstorm the opinions of the experts from various departments working with underground cable systems in an organization to determine the weighting value as a percentage of significance for all condition evaluation criteria as well as the weighting of each major component for condition assessment [10,17]. Five major components of underground cable systems (underground cable, joint, termination, manhole, and duct bank) are classified. Various test methods and corresponding results of all components were used. Thereafter, the annual HIs were plotted versus the time to obtain a lifetime trending curve. By using the polynomial function for curve fitting, the predictive health index can be determined. In addition, actual technical and historical operating data were also considered as conditional factors representing the degradation behavior regarding practical usage by using the Weibull distribution method [18]. Lastly, the lifetime trending curve of the underground cable system was adjusted by multiplying the health index with the conditional factor to obtain the dynamic health index trending curve with respect to usage time. Finally, the lifetime of the underground cable system can be successfully determined. The calculation procedure of the aforementioned process is represented in Figure 1.



Figure 1. Lifetime estimation diagram of underground cable system.

In Figure 2, an underground cable system in an industrial estate consists of underground cable, joint, termination, manhole, and duct bank, i.e., system B-B'. A failure of the underground cable system could cause a huge impact to customers due to power interruption in industrial processes. To avoid such unexpected power outages, percentage health index (%*HI*) determination is a factor used to indicate the condition of the underground cable system and its components for effective usage and maintenance planning.



Figure 2. Simplified underground cable system and diagram of five major components.

#### 2. Data Management System

Three significant data sets including technical information [3] and operating data as well as testing and visual inspection results were involved in lifetime estimation as described below.

#### 2.1. Technical Information

The technical information of all major components in a cable system is described as follows. At first, the technical data of the cable route are gathered including circuit name, system voltage and current ampacity, manufacturer, model type, installation date, number of terminators and manholes, and total length of the entire circuit. Then, the joint and termination's technical data consist of device number and circuit name, model and bonding method, manufacturer, installation location, and installation date. Next, the manhole's technical data consist of device number, designation route in manhole, location, manufacturer, and model type. Finally, the duct bank's technical data consist of name, starting and ending manhole, as well as numbers of a total, used, damaged, and spared duct. Then, the database of this data has been developed using MySQL (Bitrock, Inc., San Francisco, CA, USA) for web-application software to systematically collect the data of the existing and new installation of cable systems for further processes.

#### 2.2. Testing and Inspection Results

Basically, the aims of maintenance of underground cable systems are to detect and recognize the possible defects at the actual operating condition and to prevent unscheduled outage [19,20]. It is performed while the system is under energization [21]. In this work, four effective tests and inspections that are regularly performed according to utility practice consist of visual inspection, sheath current measurement [8], infrared thermography inspection [9], and partial discharge measurement [21] as presented in Figure 3. Further information about each testing method regarding considered parameters extracted from the measurement, condition classification, and its criteria are expressed in Table 1 [22].



Figure 3. Visual inspection, testing, and measurement of underground cable system.

Testing Method	Output Value Wei		Score				
resting method	Sulput value	WeightScore4 (Good)2 (Moderate)0 (Bad10No PD/coronaSurfaceInterna $< 50$ 50-300>3008 $<0.5$ $0.5-2$ >2StableSlightSignifica10 $<10$ 10-15>1510 $<7$ 7-10>108 $<5$ 5-10>105 $<10$ 10-252510NormalRepairedCracke4NormalStainedBroker10Normal-Bloate10NormalSmall crackBroker10NormalSmall crackBroker10NormalSmall crackBroker3CleanDirtyFloode3NormalSmall crackBroker3NormalSmall crackBroker <th>0 (Bad)</th>	0 (Bad)				
	PD pattern	10	No PD/corona	Surface	Internal		
Partial discharge	Amplitude (internal PD), (pC)		<50	50-300	>300		
i artiai discharge	Amplitude (surface PD), (nC)	8	< 0.5	0.5–2	>2		
	Trending of amplitude		Stable	Slight	Significant		
Infrared thermography	$\Delta T$ phase-ambient (°C)	10	<10	10–15	>15		
initiated thermography	$\Delta T$ phase-phase (°C)	10	<7	7–10	>10		
Sheath current	Increment of sheath current (%)	8	<5	5–10	>10		
Grounding resistance	Grounding resistance ( $\Omega$ )	5	<10	10–25	25		
	Cable jacket	10	Normal	Repaired	Cracked		
	Cable supporting structure	4	Normal	Stained	Broken		
	Cable shield grounding	8	Normal	Loose	Broken		
	Splice condition	10	Normal	-	Bloated		
	Termination condition	10	Normal	Dirty	Bloated		
	Manhole gate	7	Normal	Stained	Lost		
Visual inspection	Manhole wall	7	Normal	Small crack	Broken		
	Manhole floor	7	Normal	Small crack	Broken		
	manhole cleaning	3	Clean	Dirty	Flooded		
	Manhole ground connection	8	Normal	Loose	Broken		
	Duct bank water ingress	8	No water	Some leakage	High pressure		
	Duct bank general condition	8	Normal	Small crack	Broken		
	Number of available ducts	10	Many	A few	Unavailable		

Table 1. Testing and inspection methods with scoring and weighting for health index calculation.

# 2.3. Operating Information

To cope with an accuracy in lifetime estimation, the actual environment and operating condition of individual underground cable systems are significantly important. These analyses consider the actual operating condition and usage risk of the system. Important criteria to evaluate the difference in degradation behavior due to various practical usage of a cable system include usage time, loading condition, failure frequency, reparation rate, network reliability, and operational environment as presented in Table 2. It can be implied that if a cable system has long service life, high loading condition, and failure frequency while it is operating in an extreme environment, such as water flooding, poor ventilation, bad coverage soil; its lifetime should be lower than life expectation [23].

Considering Item	Waight	Score						
Considering item	weight	4 (Normal)	2 (Moderate)	0 (Risk)				
Usage time (y)	10	<20	20–30	>30				
Loading condition (%)	10	<60	60–80	>80				
Failure frequency (times/year)	8	0	1–3	>3				
Reparation rate (times/year)	7	<3	3–6	>6				
Network reliability	6	Network	Loop	Redial				
Length (km)	5	<1	1–3	>3				
Route configuration	5	<10	10–30	>30				
Operational environment	3	no	Road, building	Vibration				

Table 2. Criteria with scoring and weighting values for conditional factor assessment.

#### 3. Assessment Criteria with WMS Technique

After classification of underground cable system components, the associated testing and inspection methods of each component are identified as shown in Table 1. Similarly, the scores and weights of all testing criteria are identified by using the WSM technique. The score classification is based on international standards and practice of the utility performing cable system maintenance. The importance weight setting is assigned according to the importance and effectiveness of each inspection item to identify the severity of possible defects. This setting is based on a consensus of several experts in different departments in the focused organization involved with the underground cable system, such as the engineering, operation, and maintenance departments. The opinions of the experts are brainstormed together and with the aid of the AHP technique [10,17], the final weighting value can be assigned to each criterion. For the conditional factor evaluation, the criteria consisting of usage time, loading condition, failure frequency, reparation rate, network reliability, cable length and route configuration, as well as operational environment of the underground cable system are presented in Table 2. The scoring for operating criteria is also given in Table 2.

## 4. Health Index Calculation

The underground cable components are classified as five significant groups to facilitate efficient data collection and management, and simply HI calculation, which starts from an analysis of individual components in Section 4.1 and then computing the HI of the whole system in Section 4.2.

#### 4.1. Component HI Calculation

Firstly, the percentage HI representing the condition of each major component (%*HIC*) is evaluated by analyzing their relevant routine and inspection test results with the criteria by using Equation (1):

$$\% HIC = \frac{\sum_{i=1}^{n} (S_i \times W_i)}{\sum_{i=1}^{n} (S_{\max,i} \times W_i)} \times 100$$
(1)

where  $S_i$  is a score obtained from the test and inspection result *i*th,  $S_{max,i}$  is a maximum score of the test and inspection result *i*th,  $W_i$  is the weight representing the importance of the test and inspection results *i*th, *i* is the index of test and inspection results, and *n* is the total number of the test and inspection results.

#### 4.2. System HI Calculation

After %*HIC* of all components are calculated, a percentage HI condition of the underground system (%*HIS*) is evaluated by using Equation (2). The worst percentage HI from every component (% $HIC_{W,j}$ ) in each group along the cable route is selected as a representative of each major group to calculate the overall system HI of a system (%*HIS*) identified from 0% to 100 % from poor to good condition:

$$\%HIS = \frac{\sum_{j=1}^{m} (\%HIC_{W,j} \times W_j)}{100}$$
(2)

where  $%HIC_{W,j}$  is the worst component HI in each group of major component *j*th,  $W_j$  is the important weight of each group of major component *j*th, *j* is the index of each group of major component, and *m* is the total number of the major component groups.

#### 5. Conditional Factor Calculation

Conditional factor (*CF*) is proposed to improve the accuracy of lifetime estimation by considering the practical usage condition. This *CF* is used to adjust a slope of the degradation curve applied by the Weibull distribution function. The *CF* is based on practical and statistical operating records of the criteria in Table 1 and calculated by using Equation (3):

$$%CF = \frac{\sum_{c=1}^{p} (S_c \times W_c)}{\sum_{c=1}^{p} (S_{\max,c} \times W_c)} \times 100$$
(3)

where  $S_c$  is a score of the operating criterion *c*th,  $S_{max,c}$  is a maximum score of the operating criterion *c*th,  $W_c$  is the important weight of the operating criterion *c*th, *c* is the index of operating criterion, and *p* is the total number of operating criteria.

# 6. Lifetime Estimation

The lifetime of the cable system is determined by multiplying a predictive *%HIS* curve with a conditional factor obtained from the Weibull distribution function as shown in Figure 1. The lifetime estimation procedure is described in this section.

#### 6.1. Predictive HI by Applying Curve Fitting

After %*HIC* and %*HIS* calculation, the statistical %*HIS* record is plotted to observe and predict the %*HIS* trend of the underground cable system, which may show a slight decrease in the HI due to gradual degradation behavior according to both normal and stress aging. Then, a %*HIS* trending equation can be determined by using a regression technique for curve fitting of the previous %*HIS* to forecast the possible future %*HIS*. Then, this health trending equation can be used not only to analyze the degradation behavior, but also to predict the future %*HIS* from the observed trend to set up the proper maintenance tasks and optimize a constrained budget for the underground cable system. In Figure 4, the most appropriated curve fitting function is the 3rd order polynomial function with the highest coefficient of determination ( $R^2 = 0.8822$ ) when compared with three other functions such as the linear, exponential, and 2nd order polynomial functions.



**Figure 4.** Regression analysis by various curve fitting functions to predict the trend of health index. (a) Linear function, (b) exponential function, (c) 2nd order polynomial function, and (d) 3rd order polynomial function.

In [11], the third order polynomial distribution is also mentioned for lifespan prediction on different power equipment. Moreover, this selected function satisfies flexibility, monotonicity, smoothness, and continuity of health variation with time [24,25]. The polynomial function could be written as Equation (4):

$$g(t) = b_3 t^3 + b_2 t^2 + b_1 t + b_0 \tag{4}$$

All the parameters in Equation (4) are obtained from the regression analysis based on historical %*HIS*. The larger number of data collection for curve fitting could improve the accuracy and trustworthiness of the result. Finally, the %*HIS* trending curve can be plotted, and the upcoming %*HIS* can be predicted.

### 6.2. Degradation Behavior Accelerated by Operating Condition

According to differences in the degradation behavior of each cable system due to variation in operating condition, system configuration, and environmental impacts, it is well accepted to use the Weibull distribution function to analyze and illustrate the degradation curve of high voltage equipment and substation [26–28]. However, there are various types of Weibull distribution functions. In this work, a survival curve function as written in Equation (5) is selected because of its similarly to the inverse bathtub curve characteristic during the end-of-life period [29–31] and plotted in Figure 5.

$$h(t) = e^{-(t/\alpha)^{\beta}}$$
(5)



**Figure 5.** Weibull survival curve with different shape parameters to represent the difference in degradation behavior of underground cable system.

This function requires two parameters [28]. Firstly,  $\beta$  is called the shape parameter. It is used to adjust the slope of the curve, which can refer to degradation behavior of the cable system. In this work,  $\beta$  is substituted by the *CF* of each cable system and  $\beta_0$ . The  $\beta_0$  is the minimum value of shape parameter which illustrates an extreme degradation curve of the underground cable system. Therefore, the determination of  $\beta$  can be calculated by using Equation (6) to incorporate the practical usage condition of each cable system into account.

$$\beta = \beta_0 + \left(\frac{\% CF}{100} \times (10 - \beta_0)\right) \tag{6}$$

Secondly,  $\alpha$  is called the scale parameter. It represents the characteristic life that 36.78% of the population is expected to fail. Then, according to Figure 5, the scale parameter is 40 years, which implies the expected lifetime of the cable system [31].

In Figure 5, different shape parameters ( $\beta$ ) result in different degradation patterns while Table 3 shows a correlation between  $\beta$  and *CF*.

$\beta$ -Parameter	10	8	6	4	2
Conditional factor (%CF)	100	75	50	25	0

Table 3. Correlation between shape parameter and conditional factor.

It can be observed that *CF* as 100% yields the  $\beta$  as 10, for which the failure curve is the most appropriate. In contrast, the lowest  $\beta$  as 2 represents an abnormal shape of condition degradation because faster degradation occurred in an early stage due to the severe operating conditions. When the operating condition and environmental impacts are less severe, the degradation behavior is gradually decreased, and the lifetime is prolonged [18].

#### 6.3. Lifetime Curve Forecasting

In this step, the predictive %*HIS* curve is multiplied by the degradation curve to obtain a final lifetime estimation function y(t), as given in Equation (7), reflected in the difference in operating condition, system configuration, and environmental impacts in the period t (year). Finally, the end of life (*LT*) is estimated by using Equation (8), where *AP* is the acceptable limit of %*HIS* level and  $t_e$  is a calculated year beyond the *AP* as shown in Figure 6. The value of  $y(t_e)$  must be a lesser value than *AP* because the Equation (8) is used to find the cutting point of their two lines, which is the *LT*.

$$y(t) = g(t) \times h(t) \tag{7}$$





Figure 6. Lifetime curve estimation after the combination of predictive health index and conditional factor.

## 7. Results and Discussion

In this section, the results of %HIC calculation of five major components and the overall %*HIS* of the cable system as well as the %*CF* of 10 cable feeders are presented. The data of feeder F-01 provided in Tables 4-6 is used to demonstrate the calculation of %HIC, %HIS, %CF, and lifetime estimation as examples. The lifetime curve of F-01 is plotted in Figure 7 as a solid line, whereas the dashed line represents the ideal lifetime curve without operational and environmental stresses. In Figure 7, when the AP is defined at %HIS equal to 50%, the lifetime is estimated as 21 years.

Table 4. Calculation of cable system health index of feeder F-01.

Component Group	The Worst Component Health Index, <i>%HIC<sub>W,j</sub></i>	Weight, $W_j$	System Health Index, %HIS
Cable	46.88	30	
Joint	40.70	30	
Termination	100.00	25	75.38
Manhole	55.13	10	
Duct bank	50.00	5	

Table 5. Conditional factor calculation of feeder F-01.

Considering Item	Score, S <sub>c</sub>	Weight, W <sub>c</sub>	Conditional Factor, %CF	Shape Parameter, β
Usage time	2	10		
Loading condition	2	10	-	
Failure frequency	4	8	_	
Reparation rate	2	7	-	
Network reliability	0	6	- 33.5	4.68
Length	2	5	_	
Route configuration	0	5	_	
Operational environment	2	3	_	

Year, t	System Health Index, %HIS	HIS Fitting- Function, g(t)	Shape Parameter, $\beta$	Expected Lifetime, α	Weibull Function, h(t)	Lifetime Function, y(t)
2	96.97	97.01			0.99	97.01
4	95.11	95.11	-		0.99	95.11
6	95.11	94.23	_		0.99	94.21
8	93.83	93.69			0.99	93.64
10	91.06	92.84	4.68	40	0.99	92.70
12	91.06	91.01			0.99	90.68
14	87.57	87.53	_		0.99	86.88
16	85.91	81.75	_		0.99	80.62
18	67.16	72.98	-		0.98	71.25
20	59.28	60.58	-		0.96	58.24

Table 6. Calculated parameters for lifetime estimation of feeder F-01.



**Figure 7.** Plot of predictive health index multiplied by conditional factor for lifetime estimation of cable feeder F-01.

The worst *%HIC* of each major component of F-01 to F-10 is summarized and presented in Table 7. Finally, the *%HIS* of 10 feeders evaluated from the past 20 years are shown in Table 8. The adjusted *%HIS* of the best and the worst cable systems are plotted in Figure 8, in which the lifetime can be observed. The results show that the maximum expected lifetime is 37.90 years of feeder F-05 as the best condition, whereas the minimum expected lifetime is 21.03 years of feeder F-01 as the worst condition.

Moreover, this section shows the differences of degradation behavior of each system. For example, the systems as F-06 and F-07 have the same level of *%HIS* at the 20th year, but their expected lifetimes are different. The lifetime of F-06 is shorter than F-07 because its stresses in operation are more severe than those of F-07 as can be seen in Table 8. Thus, for any other power plants, there will be several systems of the same model, which have been put in service in the same year. They have the same level of *%HIS* at the latest year, but at the end their expected lifetime is not equal due to the differences in terms of operating and environmental conditions. Another case is the comparison of F-03 and F-06, in which it can be seen that although the latest *%HIS* of F-03 is higher than F-06, the evaluated lifetime of F-03 is shorter because the *%HIS* of F-03 dropped suddenly at the 19th year due to the increase in some minor defects in its system.

Component	Testing Method	Considering Value	Weight.	Score, S <sub>i</sub>									
Component	Testing Method	Considering value	W <sub>i</sub>	F-01	F-02	F-03	F-04	F-05	F-06	F-07	F-08	F-09	F-10
Cable	Visual inspection	Cable jacket	10	2	2	4	4	4	4	4	4	4	4
		Cable supporting structure	4	2	2	2	2	2	2	2	2	2	2
		Cable shield grounding	8	4	4	4	4	4	4	4	4	4	4
	Sheath current	increment of sheath current	10	0	4	4	4	4	4	4	4	4	4
	The worst component health	index ( $\%$ <i>HIC</i> <sub>W</sub> ) of cable		46.88	78.13	93.75	93.75	93.75	93.75	93.75	93.75	93.75	93.75
Joint	Visual inspection	Splice condition	10	4	4	4	4	4	4	4	4	4	4
	Partial discharge	PD pattern	10	0	4	4	4	4	4	4	4	4	4
		PD amplitude	8	0	4	4	4	4	4	4	4	4	4
	Infrared thermography	$\Delta T$ p-p or p-ambient	10	2	4	4	4	4	4	4	4	4	4
	Grounding resistance	Grounding resistance	5	2	2	2	4	4	2	2	4	2	4
	The worst component health	n index (% <i>HIC</i> <sub>W</sub> ) of joint		40.7	94.19	94.19	100	100	94.19	94.19	100	94.19	100
Termination	Visual inspection	Termination condition	10	4	4	4	4	4	2	2	4	4	4
	Partial discharge	PD pattern	10	4	4	4	4	4	4	4	4	4	4
		PD amplitude	8	4	4	4	4	4	4	4	4	4	4
	Infrared thermography	AT p-p or p-ambient	10	4	2	4	4	4	4	4	4	4	4
	Grounding resistance	Grounding resistance	5	4	4	4	4	4	2	2	4	4	2
The	e worst component health ind	dex (% <i>HIC</i> <sub>W</sub> ) of termination		100	88.37	100	100	100	82.56	82.56	100	100	94.19
Manhole	Visual inspection	Manhole gate	7	4	4	4	4	4	4	4	4	4	4
	1	Manhole wall	7	2	2	2	2	2	2	2	2	2	2
		Manhole floor	7	2	2	2	2	4	2	2	2	2	2
		Manhole cleanness	3	0	0	0	0	0	0	0	0	0	2
		Manhole	8	2	2	2	4	4	4	4	2	4	4
	Crounding registeres	ground connection	7	2	2	2	4	-	2	2	4	2	2
	Giotaliang resistance	Gibunding resistance	7				4				4		
T	he worst component health i	ndex (%HIC <sub>W</sub> ) of manhole		55.13	55.13	55.13	74.36	83.33	65.38	65.38	64.10	65.38	69.23
Duct bank	Visual inspection	Duct bank	8	4	4	2	2	2	2	2	2	2	4
		Duct bank water ingress	8	0	0	0	0	0	0	0	2	0	2
		number of available ducts	10	2	2	0	0	0	0	0	0	0	0
Th	ne worst component health ir	ndex (% <i>HIC</i> <sub>W</sub> ) of duct bank		50	50	15.38	15.38	15.38	15.38	15.38	30.07	15.38	46.15
	System health in	ndex (%HIS)		59.28	81.8	87.66	91.33	92.23	84.33	84.33	91.07	88.69	90.90

**Table 7.** Summary of testing and inspection results with their scoring and health index calculation of cable system and its components of 10 cable feeders.

**Table 8.** Summary of remaining life estimation results and related parameters of ten cable systems.

Decorded Veer	System Health Index, %HIS									
Kecorded fear	F-01	F-02	F-03	F-04	F-05	F-06	F-07	F-08	F-09	F-10
0	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
1	98.85	99.23	98.85	99.04	99.04	99.23	99.23	98.85	98.65	98.85
2	96.97	98.65	98.85	98.65	99.04	98.65	99.04	98.85	98.65	98.85
3	96.01	98.65	98.85	98.65	98.85	98.65	98.65	98.13	97.16	98.85
4	95.11	96.78	96.97	98.13	98.85	98.13	97.16	97.16	97.16	96.97
5	95.11	96.01	96.97	97.16	98.65	98.13	96.78	96.97	96.97	96.97
6	95.11	95.11	96.97	97.16	96.97	96.78	96.78	96.97	96.78	96.97
7	93.83	93.83	96.01	96.78	96.97	96.78	96.01	96.01	96.01	96.01
8	93.83	93.83	96.01	96.78	96.78	96.78	95.05	96.01	96.01	96.01
9	93.83	93.13	96.01	96.01	96.78	96.01	93.89	96.01	95.11	96.01
10	91.06	91.33	95.11	96.01	96.01	96.01	93.13	95.11	95.05	95.11
11	91.06	91.06	95.11	96.01	96.01	95.05	93.13	95.11	95.05	95.11
12	91.06	91.06	95.11	95.05	95.11	95.05	91.33	95.05	93.89	95.11
13	87.57	87.57	93.83	95.05	95.11	92.23	91.33	93.83	93.89	93.83
14	87.57	87.53	93.83	95.05	93.89	91.33	91.33	93.83	93.13	93.83
15	87.57	87.53	93.83	93.89	93.89	88.42	88.42	93.13	93.13	93.83
16	85.91	86.5	91.06	93.89	93.13	87.53	86.5	93.13	92.23	93.83
17	76.53	85.91	91.06	93.89	93.13	87.53	86.5	92.23	92.23	91.07
18	67.16	85.91	91.06	91.33	92.23	86.5	86.07	91.33	91.33	91.07
19	71.84	77.11	87.66	91.33	92.23	86.07	84.33	91.07	91.33	90.90
20	59.28	81.8	87.66	91.33	92.23	84.33	84.33	91.07	88.69	90.90

Recorded Year	System Health Index, %HIS										
	F-01	F-02	F-03	F-04	F-05	F-06	F-07	F-08	F-09	F-10	
Expected lifetime, $\alpha$ (yrs.)	40	40	40	40	40	40	40	40	40	40	
Shape parameter, $\beta$	4.67	6.15	6.52	6.52	8.37	6.52	7.41	7.41	6.89	7.41	
Estimated lifetime (yrs.)	21.03	29.42	29.88	32.96	37.90	32.62	34.19	34.63	32.33	34.01	
Coefficient (R <sup>2</sup> )	0.9608	0.9468	0.973	0.974	0.982	0.9743	0.987	0.987	0.9777	0.962	
Acceptable point, <i>AP</i> (%)	50	50	50	50	50	50	50	50	50	50	
Remaining life (yrs.)	1.03	9.42	9.88	12.96	17.90	12.62	14.19	14.63	12.33	14.01	

Table 8. Cont.



**Figure 8.** Lifetime curve and determination of the expected lifetime of the best and the worst cable system. (**a**) The best estimated lifetime curve of F-05 and (**b**) the worst estimated lifetime curve of F-01.

The proposed lifetime estimation method was well agreed by the utility. The failure records as well as the testing and inspection results of the cable system in that utility are systematically collected and recorded in the central database to verify the outcome of the proposed method and to adjust some parameters in the method to improve the accuracy. Currently, the worst condition of a cable feed F-01 shows the highest failure rate with detectable internal partial discharge at a cable joint. This leads to the shortest remaining lifetime of this cable. Even though further comparison between predictive remaining lifetime and symptom of defects leading to end of lifetime takes time for data collection due to different remaining lifetimes of each cable system, it is a mandatory step in future work to verify the usefulness of the proposed method.

Eventually, a further benefit is that the results can be used to categorize the systems for future planning and determination of the proper maintenance actions as urgent, monitor, and normal inspection based on their remaining lifetimes being lower than 1 year, between 1 to 10 years, and more than 10 years, respectively [7]. Finally, the organization can properly manage their available budget according to the known maintenance requirement and lifetime estimation result by taking actions such as fully replacing the cable when the system is in very poor condition and has very short remaining lifetime, paying more attention and increasing the maintenance cycle when the system has moderate condition, or continuing to adhere to the normal maintenance strategy when the system is satisfied and has a long remaining lifetime [8].

# 8. Conclusions

This paper proposes a new lifetime estimation method for underground cable systems by combining the conventional health index approach with an indicator of cable system degradation known as conditional factor as representative of the difference in various usage conditions of the cable system. This method is aimed to estimate the remaining lifetime of an underground cable system by combining the difference in degradation behavior and operating conditions with the conventional health index. The weighting and scoring method, analytical hierarchy process, polynomial and Weibull distribution functions were key elements in the evaluation process. The actual technical and operating data with historical testing records were stored in the central database via developed web application software. The condition assessment of the underground cable system was firstly performed by applying the weighting and scoring technique and the analytic hierarchy process to evaluate the health index of a cable system and its parts consisting of five major components: power cable, joint, termination, manhole, and duct bank. The corresponding test results of those five major components of any underground cable system were used for the condition assessment. Then, the annually calculated health indices of cable system of each cable feeder were periodically plotted versus time. The trending curve of such a health index of a cable system was observed and predicted by the third polynomial distribution function. Simultaneously, the technical data and operating data were also considered as conditional factors representing the degradation behavior in terms of practical usage by using Weibull distribution. Finally, the lifetime of the cable system can be successfully determined by multiplying the obtained health index from fitting function with the conditional factor estimated by the Weibull distribution function.

The result of the health index of five major components and the health index of a cable system as well as the conditional factor of ten cable feeders are presented. The difference of degradation behavior and the impact of different operating and environmental conditions on the expected lifetime have been investigated and described. The obtained results can be further used to categorize the systems for future maintenance and replacement planning and determination of the proper maintenance actions as urgent, monitor, and normal inspection according to their remaining lifetime and health index result. Finally, the organization can properly manage their available budget according to the obtained health index and lifetime estimation result of those cable systems by taking actions such as full replacement, paying more attention and increasing the maintenance cycle, or continually performing routine inspections.

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