

Article

Annual Heating and Hot Water Load Reduction Effect of Air-Based Solar Heating System Using Thermal Simulation

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Abstract: This study examines the effect of an air-based solar heating system that can be used directly for convection heating while minimizing thermal leakage. To compare the effect of reducing the heating and hot water load when using the system, a simulation model of the system is created, and annual load calculations are performed. The results of the simulation study show that the annual heating load is reduced by 5.39 GJ and the hot water load is reduced by 10.32 GJ when using the air-based solar heating system, resulting in a 48.3% annual load reduction effect. In addition, by analyzing the thermal balance of the indoor space based on the application of the air-based solar heating system, the problem of the existing system is elucidated. In order to improve the performance of the system as shown in the thermal balance, it is necessary not only to improve the performance of the collector, but also to review its thermal storage, insulation, and proper control.

Keywords: solar energy; air-based solar heating system; simulation; heating and hot water; heat balance

1. Introduction

Renewable energy from various sources is being utilized more efficiently because of the continuous increase in energy demand, environmental deterioration because of greenhouse gas emissions, and increasing fuel prices. Because the energy consumed in the building sector is approximately 40% of the total energy consumption, increased use of renewable energy in buildings is required to reduce the use of fossil fuels. Numerous studies have been conducted into the feasibility of using renewable energy sources such as geothermal, solar photovoltaic, and solar heat energy. Of these, solar methods will be the best option for future energy needs because of their availability, accessibility, cost effectiveness, and capacity [1].

Studies on solar heating have been actively conducted since the 1970s. Previously, thermal efficiency testing and the control of liquid-type flat-plate collectors were the primary focus of studies. Bliss reported the variables that affect the thermal efficiency of a flat-plate-type solar collector as a heat exchanger. By deriving the calculation formula of the collector, it was possible to easily compare various collectors [2]. Hill proposed a test method for determining the thermal efficiency of solar collectors. In this study, the energy generated by the collector was determined by measurements, and the results were compared to the solar radiation incident upon the collector to calculate the heat collector efficiency [3].

In a study on the performance of a solar collector via simulations, Dorfling reported a convective and conductive heat transfer model of a collector with linear low-density polyethylene microcapillary films and investigated the feasibility by comparing it with an experimental model [4]. Wei proposed a single large integrated wickless heat pipe as opposed to separate parallel heat pipes. A heat transfer

model of the proposed system was developed and compared with the experimental results. It was confirmed that the performance improvement was similar to that of the existing system [5]. Hussein reported a theoretical analysis of wickless heat pipe flat-plate solar collectors. It was observed that the performance of the suggested system was sensitive to the inlet temperature, the absorber material and thickness, the heat pipe pitch, and the condenser length [6]. Alvarez reported an experimental analysis and a numerical model of a flat-plate solar collector. The proposed collector was compared with the existing commercial collector, and the thermal efficiency curve of the new collector was created using a thermal model [7].

In recent years, photovoltaic and thermal (PV/T) systems have been attracting increasing attention as they not only collect solar heat, but also produce electricity. Huang [8] and He [9] evaluated the performance of a PV/T system through experiments and proposed ways to improve its performance. In addition, studies are underway to increase the thermal efficiency of PV/T systems by applying CPC (Compound Parabolic Concentrator) [10] and flat-box aluminum-alloys [11]. Bergene [12] and Zondag [13] accurately predicted changes in thermal efficiency depending on conditions by constructing a performance prediction model of a PV/T system. There is widespread research into the development trends, classification, and performance of PV/T systems [14–18]. By applying a PV/T system that can produce electricity and heat at the same time, solar energy can be utilized more efficiently for the energy reduction of housing.

Liquid-type systems are widely used to convert solar energy entering the roof into thermal energy. However, air is the ultimate receiver of energy, and there is no problem of leakage; therefore, air can be used by the ventilation system. For these reasons, the use of air-based solar heating systems has increased rapidly in recent years in Japan, where convective heating is predominant. In PV/T systems, there is increasing research on the performance evaluation of systems using air as a thermal medium via experiments and simulations [19–24]. Recently, there has been an increasing amount of research on the proposal and performance evaluation of heating systems using an air-based solar heating system [25–27]. However, most of the studies on the air-based solar system to date have mostly focused on the performance of the system itself, rather than the effect of applying it to buildings [28–30]. In the case of solar energy, it is important to understand not only the performance of the system itself but also the performance when applied to a building, because it is available only for a certain period of time, is difficult to control, and the utilization efficiency changes depending on the conditions of the building [20].

In this study, we propose an air-based solar heating system that uses hot air from solar heat for room heating and hot water supply, and the thermal performance is also evaluated. Thermal models of the air-based solar heating system are first developed, referencing current studies. The simulation models are validated from the results of an experiment at the scale of an actual house. We investigate the performance of an annual scale through a simulation of this system. In addition, by confirming the balance of the movement of solar heat introduced to the room, this basic data for the improvement of the system can be used in the future.

2. Simulation Conditions

The simulation in this study determines the season first based on the weather data and determines the operation mode based on the collecting air temperature of the solar collector. The operation mode consists of heating, heating after hot water supply, exhaust after hot water supply, indoor circulation, and shutdown. In the case of the hot water supply mode, the collecting air exchanges heat with the hot water tank, and in the heating mode, the collected air enters the underfloor space. Finally, the surface temperature, air temperature, heat flux, and load in the building are calculated. The simulation flow in this study is shown in Figure 1. The Excel-based thermal load analysis (ExTLA) is used as a thermal load simulation in this study [31]. By performing an iterative calculation (up to 32,767 times) in Microsoft Excel, the convergence criterion is met when the change in the value of the calculation result is no greater than the set maximum change value. Divergence is prevented

by using the alleviation coefficient. Based on the properties calculated from the upper cells, ExTLA calculates solar-radiation-related items, calculates the node temperature inside the wall, and then calculates the room temperature (including ventilation and latent heat). For the purposes of improving the calculation speed and convenience of use, calculation conditions such as weather conditions and air conditioning settings are input into the “input sheet”, the composition of the building and the characteristics of the members are input into the “setting sheet”, the calculated result of the previous time step is listed on the “T0 sheet”, and the thermal load calculation for the building and equipment is shown on the “T1 sheet”. The items to be calculated can be set as required and can output periodic and daily data for the building and equipment, as required.

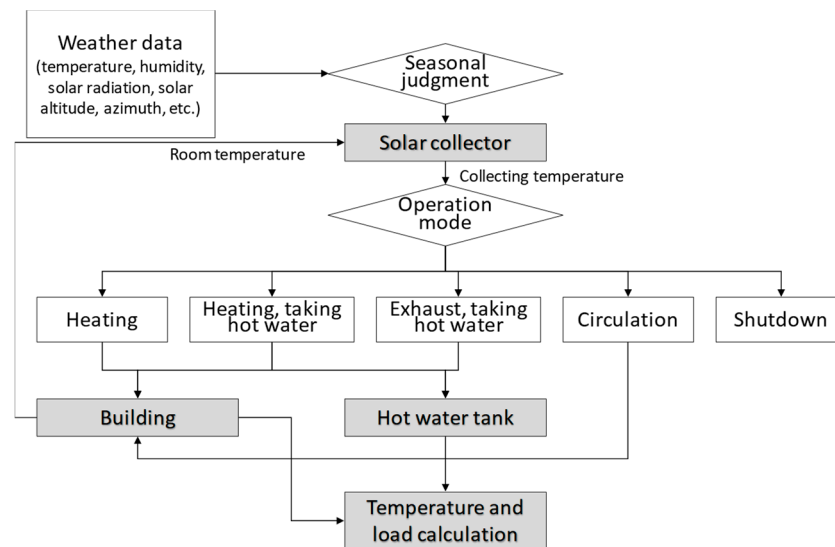


Figure 1. Simulation flow chart.

The target building is a Japanese standard house of the Japanese energy saving standard (next-generation energy saving standard) [32]. The solar collector is set based on the latitude of Tokyo (35.4° N). Assuming that there are surrounding buildings, the solar transmittance of the window on the first floor is set to zero. Figure 2 and Table 1 show the building information. In this simulation, a four-person family is targeted, and 450 L per day of hot water consumption is assumed [32]. Tables 2–4 present the simulation conditions, indoor heat generation, and hot water supply usage, respectively. The areas of the preliminary collector and glass heat collector are set as 45 m^2 and 15 m^2 , respectively. The hot water storage tank is set to a 1000 L capacity.

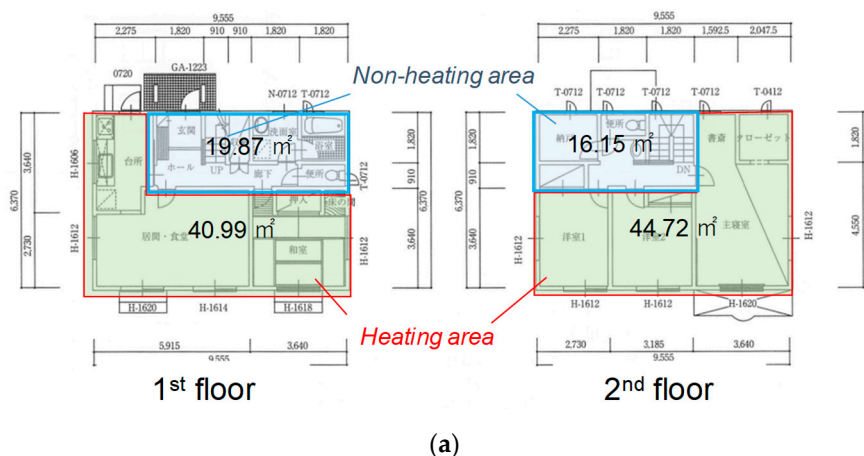


Figure 2. Cont.

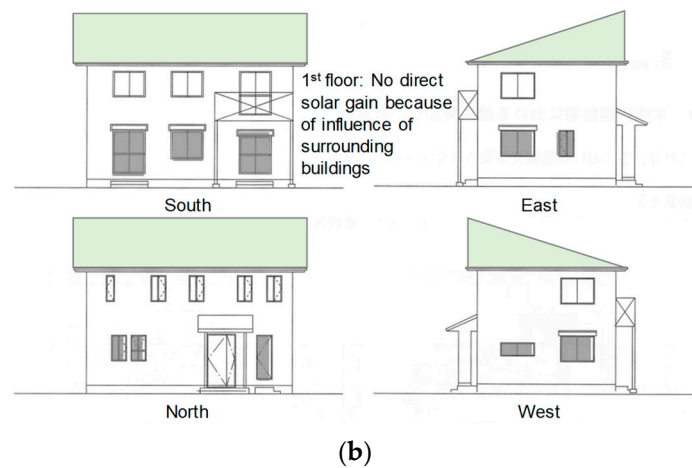


Figure 2. Target building (units: mm). (a) plan; (b) elevation. Reproduced from [32], publisher: 2010.

Table 1. Specification of target building.

Area	Total floor area: 121.73 m ² Heating area of 1st floor: 40.99 m ² , Non-heating area of 1st floor: 19.87 m ² Heating area of 2nd floor: 44.72 m ² , Non-heating area of 2nd floor: 16.15 m ²
Volume	328.06 m ³ (including underfloor space)
Insulation of each part	Ceiling: glasswool 18 kg m ⁻³ , $t = 210$ mm Wall: glasswool 16 kg m ⁻³ , $t = 100$ mm Roof: glasswool 32 kg m ⁻³ , $t = 50$ mm Basis concrete: extruded polystyrene foam, $t = 50$ mm
Window	Plain double-glazed glass (U_w : 4.65 W m ⁻² K ⁻¹)
Overall heat transfer coefficient (U_A-value)	0.83 W m ⁻² K ⁻¹
Overall coefficient of heat transfer of hot water tank	0.70 W m ⁻² K ⁻¹ (insulation: 50 mm, thermal conductivity: 0.036 W m ⁻¹ K ⁻¹)

Table 2. Simulation conditions.

Weather data	Expanded AMeDAS (Automated Meteorological Data Acquisition System) data standard (2000) Tokyo
Heating setpoint	20 °C
Heating schedule	07:00 to 10:00, 12:00 to 14:00, 16:00 to 23:00
Inclination angle of collector	Latitude of Tokyo (35.4° N)
Calculation	Preliminary calculation: from January 1 to April 30, Target period: May 1 to April 30 of following year
Time step	1 h
Usage of hot water	450 L per day (40 °C for using hot water)
Internal heat gain	13.26 kWh per day
Collector area	Preliminary collector: 45 m ² , glass collector: 15 m ²
Flow rate of air	Volume flow rate of air: 780 m ³ h ⁻¹

Table 3. Internal heat gains for simulation.

	Equipment [W]				Occupants [W] 60 W Per Person				Lighting [W]			
	1F Heating	1F Non-Heating	2F Heating	2F Non-Heating	1F Heating	1F Non-Heating	2F Heating	2F Non-Heating	1F Heating	1F Non-Heating	2F Heating	2F Non-Heating
1:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
2:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
3:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
4:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
5:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
6:00	66.9	41.5	18.0	-	0.0	-	240.0	-	0.0	0.0	0.0	-
7:00	84.3	41.5	18.0	-	60.0	-	180.0	-	22.6	101.6	0.0	-
8:00	269.1	95.1	18.0	-	120.0	-	0.0	-	97.5	171.8	0.0	-
9:00	270.6	57.0	18.0	-	60.0	-	0.0	-	52.5	101.3	0.0	-
10:00	167.8	41.5	293.1	-	60.0	-	0.0	-	115.0	174.3	105.0	-
11:00	117.4	41.5	18.0	-	0.0	-	0.0	-	17.5	76.0	0.0	-
12:00	66.9	41.5	18.0	-	0.0	-	0.0	-	0.0	0.0	0.0	-
13:00	185.2	41.5	18.0	-	60.0	-	0.0	-	67.5	34.9	0.0	-
14:00	218.7	41.5	18.0	-	60.0	-	0.0	-	52.5	47.5	0.0	-
15:00	66.9	41.5	18.0	-	0.0	-	0.0	-	0.0	0.0	0.0	-
16:00	66.9	41.5	18.0	-	0.0	-	0.0	-	0.0	0.0	0.0	-
17:00	167.8	41.5	18.0	-	60.0	-	0.0	-	35.1	98.3	0.0	-
18:00	218.7	41.5	18.0	-	120.0	-	0.0	-	70.0	64.3	0.0	-
19:00	303.9	41.5	18.0	-	120.0	-	60.0	-	70.0	104.6	35.0	-
20:00	269.1	41.5	18.0	-	180.0	-	0.0	-	80.0	111.0	35.0	-
21:00	269.1	41.5	63.0	-	180.0	-	60.0	-	120.0	148.2	52.5	-
22:00	269.1	148.8	445.5	-	120.0	-	60.0	-	70.0	267.4	122.5	-
23:00	242.9	41.5	118.3	-	60.0	-	120.0	-	70.0	273.3	140.0	-
0:00	242.9	95.1	49.8	-	60.0	-	180.0	-	35.1	79.8	87.5	-

Table 4. Hot water usage. Reproduced from [32], publisher: 2010.

Time	Usage [L]	Time	Usage [L]
06:30	3	20:15	15
06:35	3	20:20	15
07:20	10	20:25	15
07:25	3	20:30	15
07:30	3	20:35	15
08:25	3	20:45	150
09:30	3	21:15	20
10:15	3	21:20	3
12:45	5	21:25	25
12:50	10	21:30	25
13:45	3	21:45	3
16:00	3	22:00	10
17:15	3	22:05	10
18:00	3	22:15	3
18:15	3	22:30	25
19:15	3	22:35	25
19:20	3	23:00	3
19:25	3	23:05	3

3. Simulation Model of Solar Collector

Using the calculation model of the air-based solar heat collector, the temperature of the heat medium of the collector and the heat collection intensity were calculated [33]. Figure 3 shows a conceptual diagram of the collector model. The outlet temperature and heat collection intensity of the collector can be calculated from the inlet temperature, the sol-air temperature, and the coefficient of heat transfer of the collector by Equations (1) and (2). The sol-air temperature corresponding to the collector is obtained from Equation (4) and Table 5. The sol-air temperature on the outside air side (T_{coleu}) was calculated by the solar radiation amount and the night radiation of the outside surface of the collector, and the outside air temperature. The sol-air temperature on the indoor side (T_{coled}) was set to the room-side surface temperature of the collector. In the case of a preliminary collector, it was calculated by neglecting solar-radiation transmission and the thermal resistance of surface material. The k_d and k_u in Equation (4) represent the ratio of the thermal transmittance on the indoor side (K_{cd}) or the outdoor side (K_{cu}) to the overall thermal transmittance (K_c) of the collector. The thermal transmittance on the outdoor side (K_{cu}) and the thermal transmittance on the indoor side (K_{cd}) are determined by the heat resistance of the collector panel and the heat transfer due to the air flow, and the calculation method is expressed in Equations (5)–(8). The coefficient of heat transfer by convection is calculated by the wind speed using the Jurges equation.

$$T_{fout} = T_{cole} - (T_{cole} - T_{fin}) \exp(-K_c A_c / c_f G_f) \quad (1)$$

$$Q_c = c_f G_f (T_{fout} - T_{fin}) = c_f G_f \varepsilon_c (T_{cole} - T_{fin}) \quad (2)$$

$$\varepsilon_c = 1 - \exp(-K_c A_c / c_f G_f) \quad (3)$$

$$T_{cole} = k_u T_{coleu} + k_d T_{coled} \quad (4)$$

$$K_{cu} = K_{su} f_{cu}, K_{cd} = K_{sd} f_{cd} \quad (5)$$

$$f_{cu} = \alpha_c W_{sd} b_{12} + \alpha_c W_{su} b_{22} \quad (6)$$

$$f_{cd} = \alpha_c W_{sd} b_{11} + \alpha_c W_{su} b_{21}$$

$$b_{11} = (\alpha_r + \alpha_c + K_{su}) / Det, b_{12} = \alpha_r / Det, \quad (7)$$

$$b_{21} = \alpha_r (W_{su} / W_{sd}) / Det, b_{22} = (\alpha_r W_{su} / W_{sd} + \alpha_c + K_{sd}) / Det$$

$$Det = (\alpha_r A_{su} / A_{sd} + \alpha_c + K_{sd})(\alpha_r + \alpha_c + K_{su}) - \alpha_r^2 (A_{su} / A_{sd}) \quad (8)$$

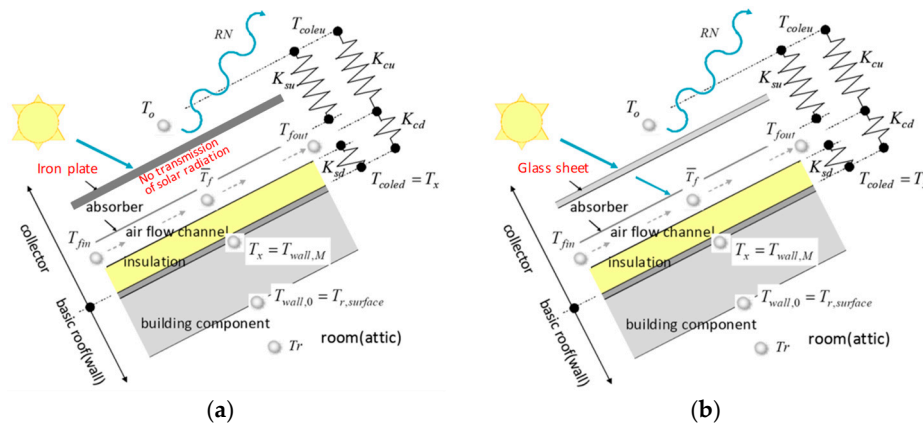


Figure 3. Air-based solar heat collector model: (a) preliminary collector; (b) glass collector. Reproduced from [33], publisher: 2019.

Table 5. Parameters used in air-based solar heat collector calculations. Reproduced from [33], publisher: 2019.

	K_{su}	K_{sd}	K_c	$T_{co,eu}$	$T_{co,ed}$	SG	$T_{co,le}$
Glass collector	$1/(r_a + 1/\alpha_o)$	$1/r_b$	$K_{cu} + K_{cd}$	$SG/K_{su} - R_{sky,c}/\alpha_o + T_o$	T_x	$(\tau_g a_{su} I)_e$	$k_u = K_{cu}/K_c$
Preliminary collector	α_o					$(a_{su} I)_e$	$k_d = K_{cd}/K_c$

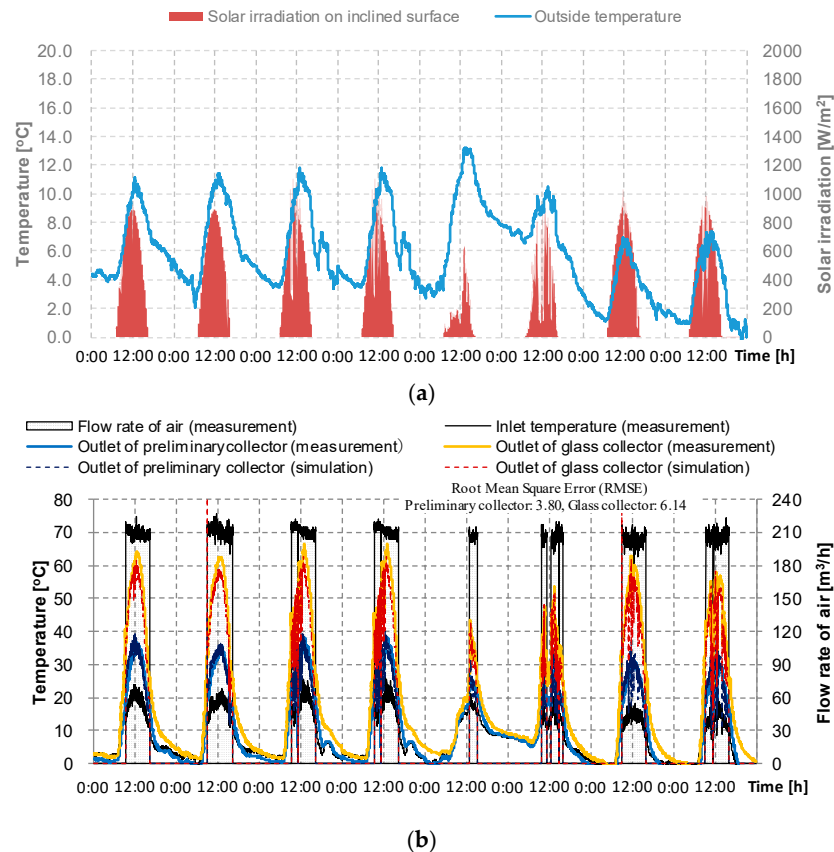
To investigate the accuracy of the calculation model of the air-based solar heat collector, the collector outlet temperatures from the experiment and simulation were compared under the same conditions of outside temperature, inlet temperature, and volume flow rate of air. Figure 4 shows the target collector of the experiment [20]. Table 6 shows the measurement instruments used in this study. Figure 5 shows the results for 8 days (December 23–30, 2013) for a preliminary collector area of 3.45 m² and a glass collector area of 1.32 m². It is surmised that the marginal difference between the two outlet temperatures is influenced by both the temperature distribution on the back surface of the collectors and equipment measurement errors. However, in this study into the effect of the presence of the solar heat collector, the accuracy of the simulation is assumed to be sufficient.



Figure 4. Target collector. Reproduced from [20], publisher: 2018.

Table 6. Measurement equipment.

	Item	Count	Sensor	Accuracy
Weather observation	Outside temperature, relative humidity (RH)	Each 1	Thermometer, hygrometer (−40–60 °C, 0–100% RH)	±1.0%
	Amount of solar radiation (horizontal)	1	Pyrheliometer (ISO9060 Second Class)	±0.5%
	Amount of solar radiation (inclined)	1	Pyrheliometer (ISO9060 Second Class)	±0.5%
	Wind direction, velocity	1	Anemometer (0–40 m/s, 0–355°)	±1.0%
	Longwave radiation	1	Long wavelength radiometer (sensitivity 42.2 mV kW ^{−1} m ^{−2})	±0.5%
	SAT (Sol-air temperature) (horizontal, inclined)	Each 1	Thermocouple	±1.0 °C
Collector	Inlet and outlet temperature	6	Thermocouple	±1.0 °C
	PV panel backside temperature	8	Thermocouple	±1.0 °C
	Air temperature of aeration layer	8	Thermocouple	±1.0 °C
	Duct temp. of ridge of a roof	4	Thermocouple	±1.0 °C
	Handling box temperature	4	Thermocouple	±1.0 °C
	Flow rate of air in the duct	1	Ultrasonic flow meter	±1.0%
	Flow rate of air in solar collection and return duct	Each 1	Pitot tube system	±1.0%
	Duct temperature	5	Thermocouple	±1.0 °C

**Figure 5.** Accuracy of air-based solar collector model (December 23–30, 2013). (a) weather data; (b) temperature and flow rate.

4. Performance of the Air-Based Solar Heating System

4.1. Simulation Results for Typical House (Non-Solar Heat Collection)

In order to verify the improvement of the indoor thermal environment and the effect of load reduction according to the application of the air-based solar heating system, a general house without a solar heating system was calculated first. Figures 6–8 show the results for 5 days when solar heat

was available during January when the ambient temperature was low. Figure 6 shows the ambient temperature and the solar irradiance at the solar collector (south, inclination angle 35.4°) in the target period. As shown in Figure 7, in the case of the first floor where direct gain through the window is not available, the indoor temperature could not reach the heating set temperature (20°C) during the entire target period. In contrast, in the case of the second floor, the indoor temperature exceeded 20°C due to the use of solar heat in the daytime, but the room temperature rapidly dropped at night due to lack of thermal storage. Figure 8 shows the hot water supply load during the target period. The hot water supply load was 8612–9167 W at 21:00 when the usage amount of hot water was a maximum, and an average 59.73 MJ per day is required for the hot water supply.

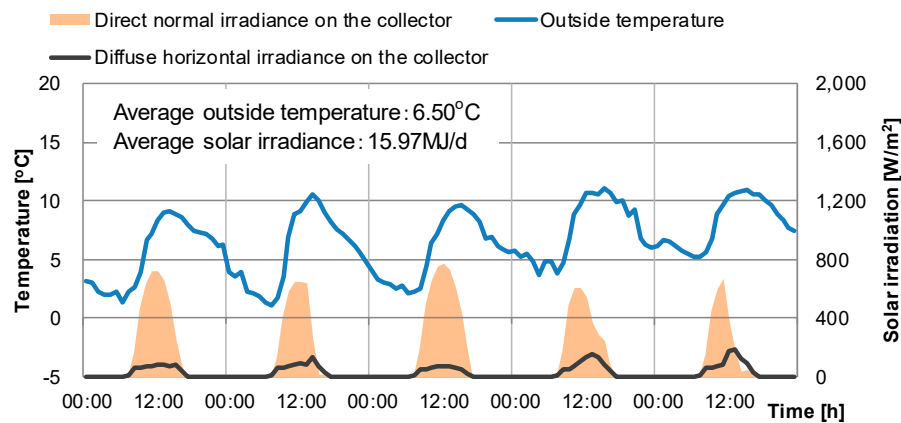
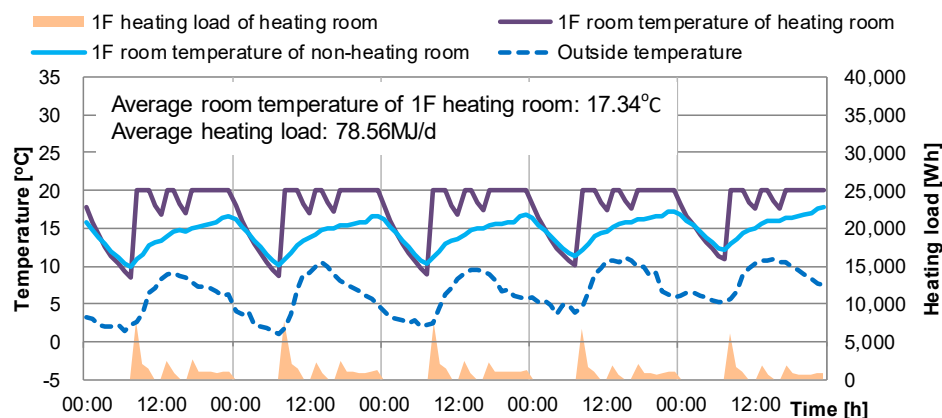
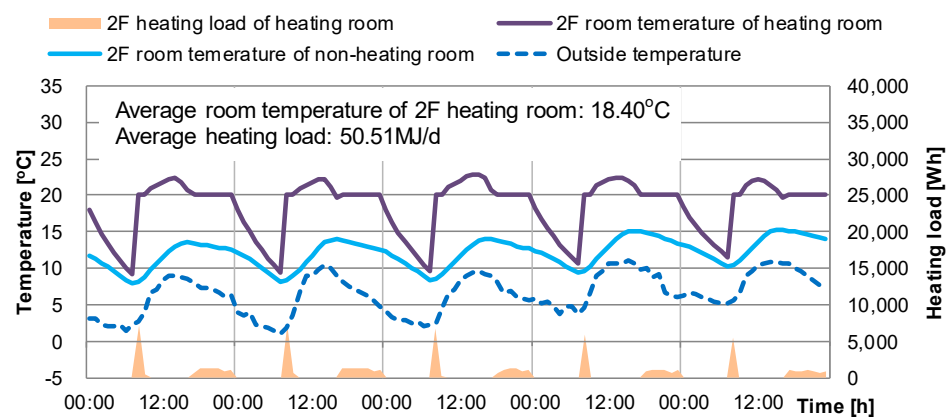


Figure 6. Weather conditions (January 7–11).



(a)



(b)

Figure 7. Room temperature results of a typical house. (a) First floor; (b) Second floor.

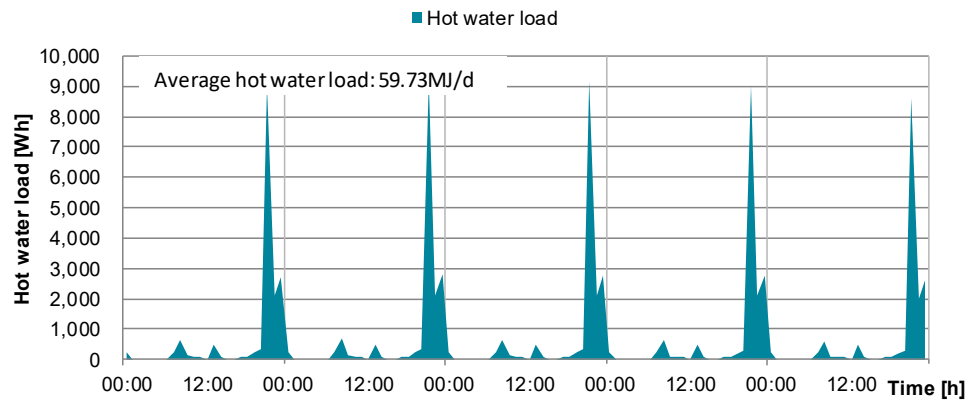


Figure 8. Hot water supply load of a typical house.

4.2. Simulation Results for the Air-Based Solar Heating System

The indoor thermal environment for the application of the air-based solar heating system was calculated. Figure 9 shows the control of the air-based solar heating system used in this study. First, the seasons are determined based on the ambient temperature at 5:00 am, and heating, hot water supply, indoor circulation, and shutdown are judged based on room temperature, the outlet temperature of the collector, the temperature of the underfloor and so on. Figure 10 shows a conceptual diagram of the studied air-based solar heating system.

By applying the air-based solar heating system, the room temperature increases because heated air is blown into the room during the day, as shown in Figure 11. In the case of the first-floor heating room, the average room temperature increased from 17.34 °C to 19.44 °C—i.e., by about 2.1 °C—and the heating load was reduced by 42.5% from 78.56 MJ per day to 45.21 MJ per day. In the case of the second-floor heating room, the indoor temperature increased from 18.4 °C to 19.5 °C and the heating load decreased by about 18.6% from 50.51 MJ per day to 41.14 MJ per day. It is considered that the effect of reducing the load on the first floor is larger because the original heat load of the second floor is not large due to the solar radiation, and the heated air first flows into the first floor.

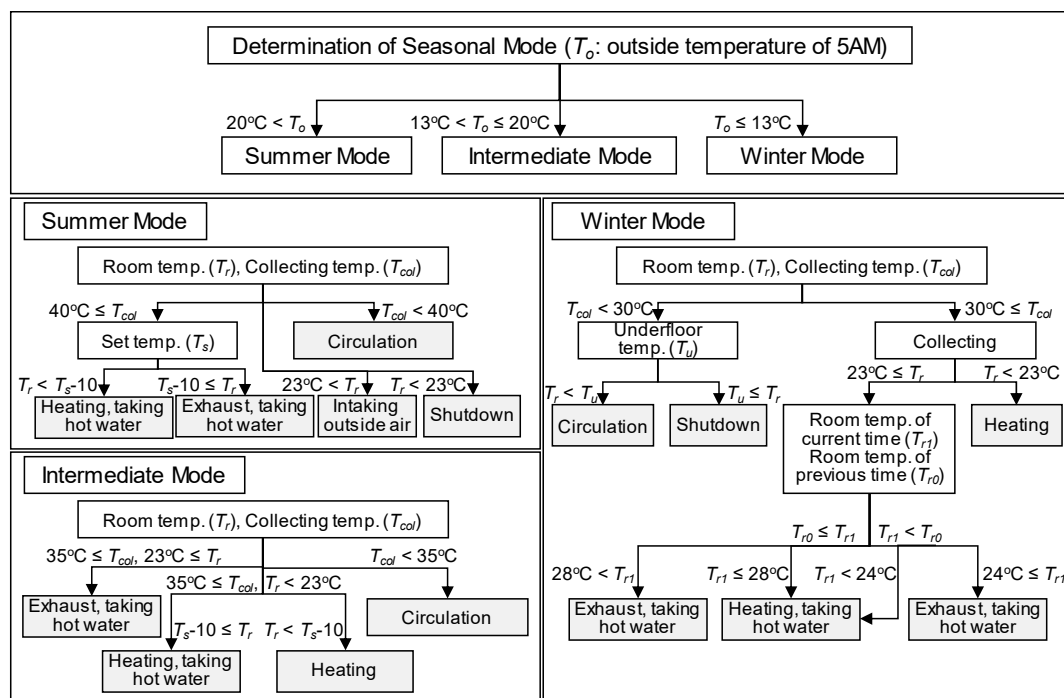


Figure 9. Operation control of air-based solar heat collection system.

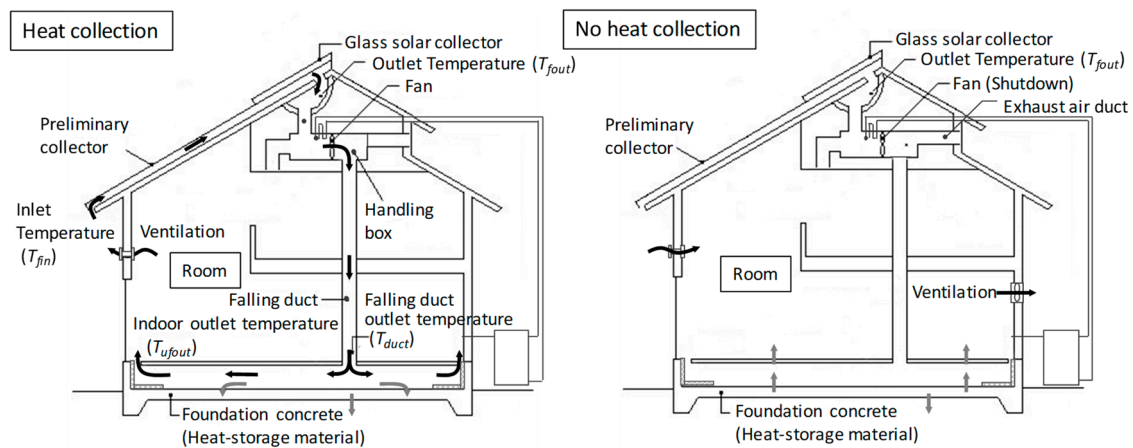


Figure 10. Conceptual diagram of the air-based solar heat collecting system.

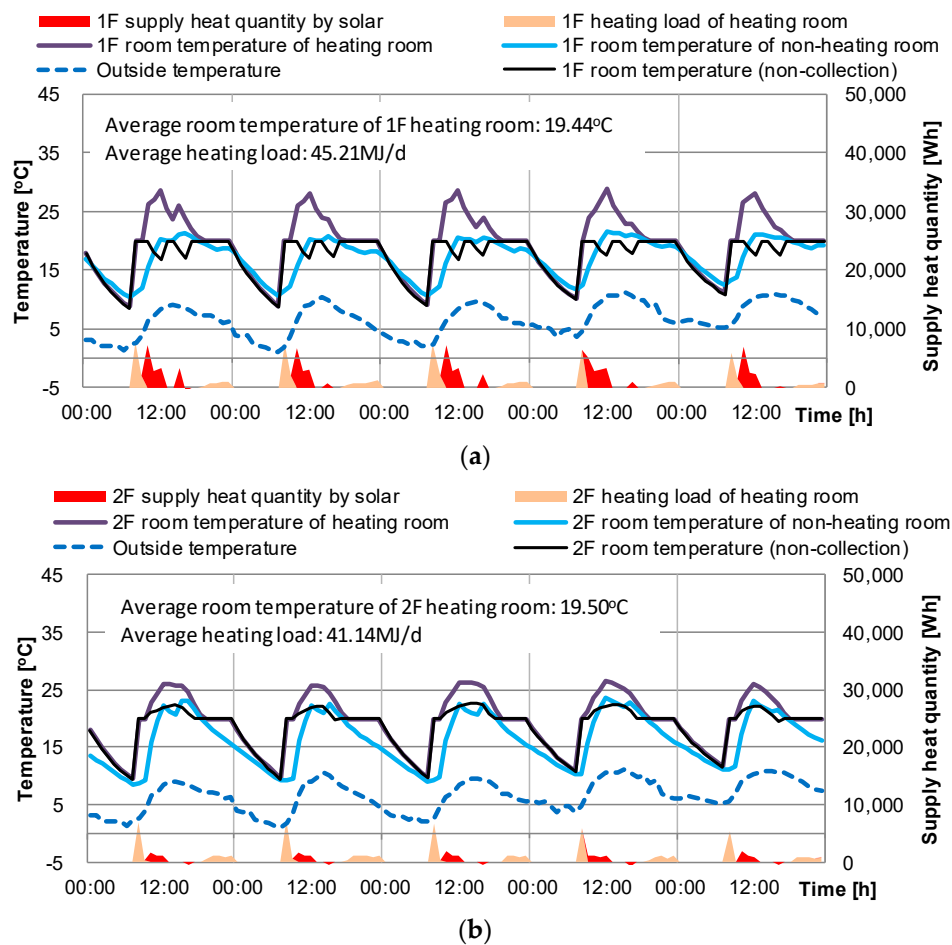


Figure 11. Room temperatures of the air-based solar system. (a) First floor; (b) Second floor.

However, due to the influx of the collected air, the room temperature was overheated up to 28.8 °C during the winter daytime. On the other hand, during non-heating at night, the room temperature dropped to a minimum of 8.9 °C. These results indicate the temperature imbalance during solar heat utilization and the necessity of thermal storage. At that time, the temperature inside the hot water storage tank (Figure 12), based on the hot water mode, increased by 16.1 °C to 34.1 °C by heat exchange with solar heat. Figure 13 shows the inlet and the outlet temperatures of the collector and the heat collector efficiency from January 7–11. The air temperature increased up to 71.0 °C by solar heat collection, and the average heat collector efficiency was 28.3%. Figure 14 shows the heat flux from heat

collection of the air-based solar system. The heat input to the room by the solar heat collector was 11.71 GJ, but 5.99 GJ was used to raise the indoor room temperature and 5.73 GJ was supplied to the underfloor space. Of the heat supplied to the underfloor space, only 1.23 GJ (about 21.5%) was used as thermal storage, and 0.53 GJ of this was heat loss.

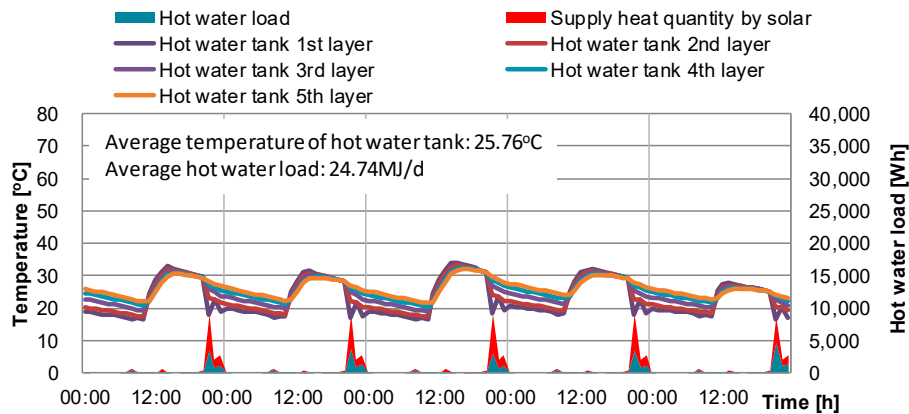


Figure 12. Temperature inside the hot water storage tank of the air-based solar system.

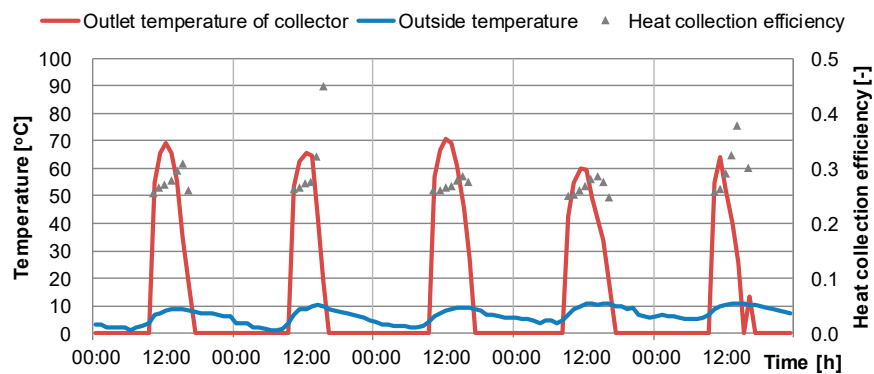


Figure 13. Outlet temperature of the collector and heat collector efficiency of the air-based solar system.

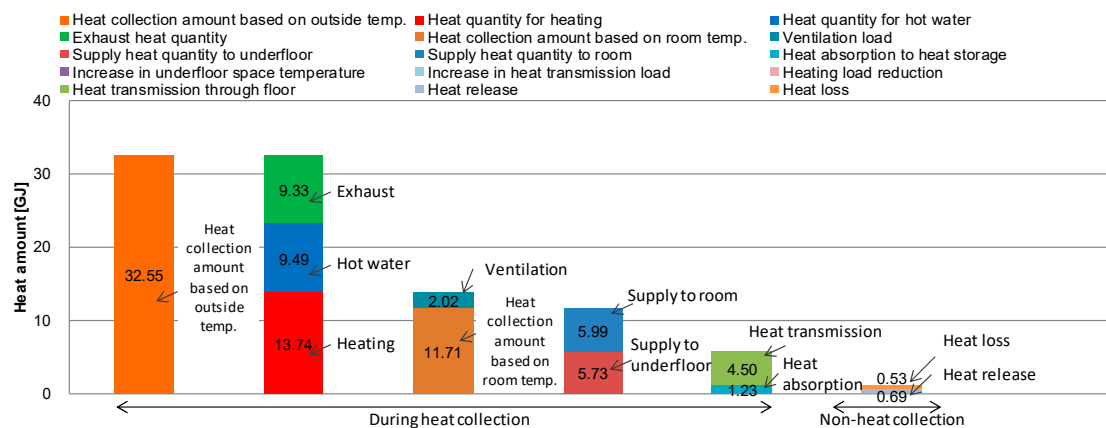


Figure 14. Heat flow from the heat collection of the air-based solar system.

As shown in Table 7, by using the air-based solar heating system, the annual indoor heating load was reduced by 5.39 GJ and the annual hot water load reduced by 10.32 GJ in the target building of this study. As a result, the annual load is reduced by about 48.3% by using the air-based solar heating system.

Table 7. Load reduction effect of the air-based solar heating system.

	Solar Irradiation on Inclined Surface [GJ]	Solar System Efficiency [%]	1F Heating Load [GJ]	2F Heating Load [GJ]	Hot Water Load [GJ]	Reduction of Heating Load [GJ]	Reduction of Hot Water Load [GJ]	Reduction Rate of Load [%]
Typical house (no solar collection)	-	-	9.72	6.92	15.87	-	-	-
Air-based solar heating system	292.9	24.5	5.67	5.58	5.55	5.39	10.32	48.3%

Figure 15 shows the flow of heat collected by the air-based solar heat collecting system. The heat collection amount can be calculated based on the outside air temperature, the collector outlet temperature, to which the temperature increased because of heat collection, and the flow rate of air at the time of heat collection. Heat exchange caused by heat collection is performed for hot water in the handling box, and the internal temperature of the hot water storage tank is increased. The air in the handling box is exhausted outdoors after exchanging heat with the hot water supply when it is used for heating by blowing into the living room through the underfloor space, depending on the room temperature condition or when the room temperature is high. However, because the amount of heat entering the room for heating use is a calorific value based on the outside air temperature, it is divided into a ventilation load and a room temperature standard heat collection amount when entering the room. The room-temperature-based heat collection amount includes the amount of heat transferred directly to the living room space by convection during heat collection, the temperature increase in the underfloor space, the amount of heat absorption to the heat storage body (such as foundation concrete and additional heat storage), and the amount from the underfloor space to the living room (such as the amount of heat flowing through the floor). After heat collection stops, the heat absorbed by the regenerator generates heat loss to the outside air and the ground, and the remaining heat dissipates to the underfloor space. The calculation of each element is shown in Equations (9)–(18).

$$Q_{out} = (T_{fout} - T_{fin})V_c c_p a T_{(h)} \quad (9)$$

$$Q_{hw} = (T_{hout} - T_{hin})F_h c_p m T_{(h)} \quad (10)$$

$$Q_{ht} = (T_{duct} - T_{fin})V_c c_p a T_{(h)} \quad (11)$$

$$Q_{in} = (T_{duct} - T_{in})V_c c_p a T_{(h)} \quad (12)$$

$$Q_v = (T_{in} - T_{fin})V_c c_p a T_{(h)} \quad (13)$$

$$Q_r = (T_{under} - T_{in})V_c c_p a T_{(h)} \quad (14)$$

$$Q_{under} = (T_{duct} - T_{under})V_c c_p a T_{(h)} \quad (15)$$

$$Q_f = (T_{floor} - T_{in})\alpha_c A_{floor} T_{(h)} \quad (16)$$

$$Q_{ab} = (T_{under} - T_{hs})\alpha_c A_{hs} T_{(h)} \quad (17)$$

$$Q_{ra} = (T_{hs} - T_{under})\alpha_c A_{hs} T_{(h)} \quad (18)$$

Figure 16 shows the thermal balance of the energy supplied to the room and the heat loss to the outside in the winter. During this period, the amount of indoor heat supplied by heat collection rises to 13.74 GJ; however, as the room temperature increases, the heat losses from the wall, the roof, the window, and the room ventilation load increase. Results indicate that the heating load is reduced by 5.23 GJ by the air-based solar heating system. We confirmed that the room temperature of the first floor reached a maximum of 20 °C or greater. This result indicates that the solar heat collection causes daytime overheating. To increase the annual load reduction effect of the air-based solar heating

system, it is necessary to not only increase the amount of solar heat collection, but also to solve the problems of heat loss because of overheating in the daytime and room temperature decreasing at night using thermal storage. In addition, it is necessary to study the control of the system that balances the reduction of exhaust heat and the utilization of solar heat for heating and hot water supply. Although it is possible to increase the heat collection amount by increasing the heat collection area, it is essential to increase the heat collection performance of the heat collector for use on a limited roof area. To increase the heat storage performance, insulation can be installed to reduce heat loss from the heat storage body to the outside, stored heat can be radiated into the indoor space, the heat capacity of the heat storage can be increased, and the heat flow rate can be increased via increases in wind speed and surface area. In the system operation control, suitable control varies depending on the balance between the heating load and hot water supply load based on the weather conditions, building performance, and hot water supply usage amount of the installation area. For example, in a case in which the heating load is small but the hot water supply load is large, it is possible to increase the annual load reduction amount by the preferential use of the collected heat for hot water supply.

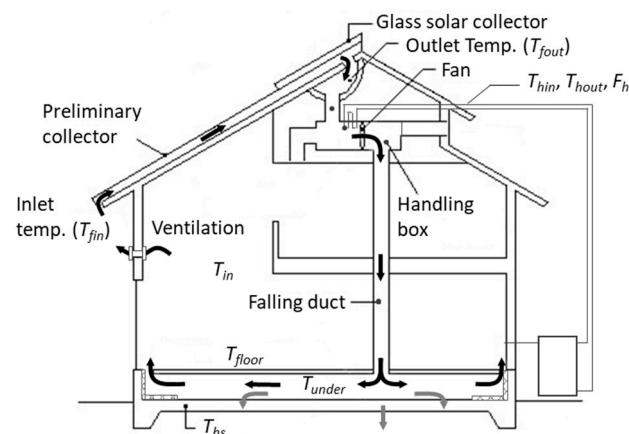


Figure 15. Conceptual diagram of the heat balance calculation.

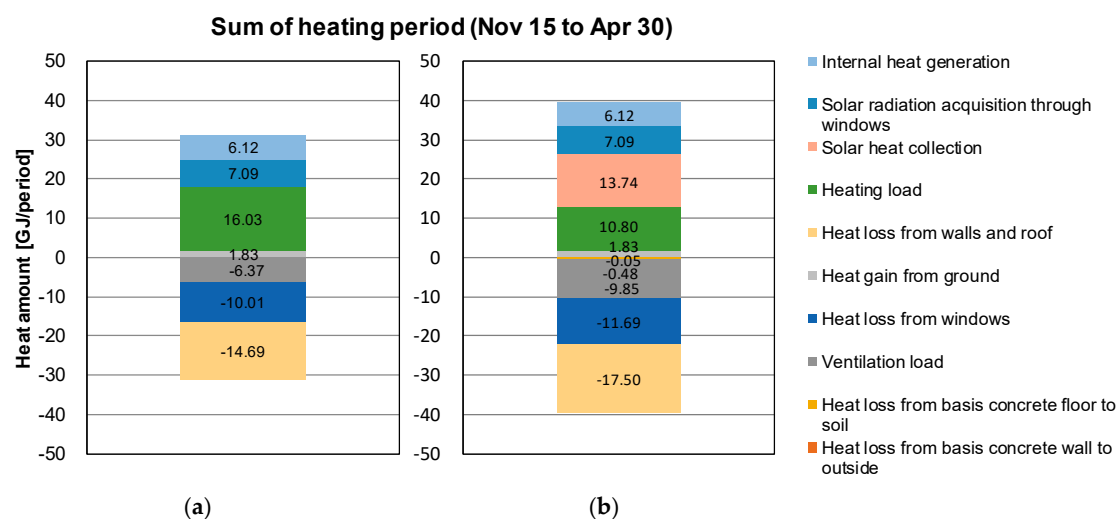


Figure 16. Heat balance of heat supply and heat loss in winter: (a) typical house (non-heat collection); (b) house with an air-based solar system.

5. Conclusions

In this study, a roof-integrated air-based solar collection system is proposed. The proposed system is used for heating or hot water depending on the seasonal and indoor temperature conditions. Especially in Japan, where convective heating is dominant, the system is considered to be highly

utilized. In this study, an annual thermal simulation was conducted to determine the performance of an air-based solar heat collecting system. The system was developed based on previous studies into solar thermal system simulation models. The accuracy of the simulation model was evaluated by comparison with experimental results, and the validity of the simulation was confirmed.

To analyze the effect of the air-based solar heating system proposed in this study, the indoor temperature, heating load, and hot water load of a typical house with no solar heating system and a house with the proposed system were calculated. The annual heating load was reduced by 5.39 GJ and the hot water load was reduced by 10.32 GJ when using the air-based solar heating system, which was a 48.3% annual load reduction. In addition, by confirming the heat balance based on solar heat collection, the possibility of improving the performance of the existing system was shown. In the future, we will propose system improvements by investigating changes to the collector, control, and insulation, and with the addition of thermal storage.

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Nomenclature

A_c	Collector area [m^2]
A_{floor}	Surface area of room floor [m^2]
A_{hs}	Surface area of heat storage [m^2]
A_{sd}, A_{su}	Area of collector frontside and backside, respectively [m^2]
a_{su}	Absorption rate of solar collector [-]
c_f	Specific heat of air static pressure [$\text{J kg}^{-1} \text{K}^{-1}$]
cp_a	Volume-specific heat of air [$\text{J m}^{-3} \text{K}^{-1}$]
cp_m	Specific heat of heating medium [$\text{J kg}^{-1} \text{K}^{-1}$]
F_h	Mass flow rate of heating medium in handling box [kg s^{-1}]
G_f	Mass flow rate of air [kg s^{-1}]
I	Solar irradiation on inclined surface [W m^{-2}]
K_c	Overall coefficient of heat transfer of collector [$\text{W m}^{-2} \text{K}^{-1}$]
K_{cu}	Overall coefficient of heat transfer on the outdoor side [$\text{W m}^{-2} \text{K}^{-1}$]
K_{cd}	Overall coefficient of heat transfer on the indoor side [$\text{W m}^{-2} \text{K}^{-1}$]
k_d	Ratio of the heat transmittance on the indoor side [-]
k_u	Ratio of the heat transmittance on the outdoor side [-]
Q_{ab}	Heat absorption to heat storage [Wh]
Q_c	Heat collection intensity [Wh]
Q_f	Heat transmission [Wh]
Q_{ht}	Heat amount to heating [Wh]
Q_{hw}	Heat amount to hot water supply [Wh]
Q_{in}	Heat collection amount referenced to room temperature [Wh]
Q_{out}	Heat collection amount referenced to outside temperature [Wh]
Q_r	Heat supply to room [Wh]
Q_{ra}	Heat radiation from heat storage [Wh]
$T_{(h)}$	Time period [h]
Q_{under}	Heat supply to underfloor space [W]
Q_v	Ventilation load [W]
r_a	Thermal resistance of hollow layer [$\text{m}^2 \text{K W}^{-1}$]
r_b	Thermal resistance of surface material [$\text{m}^2 \text{K W}^{-1}$]
R_{skyc}	Longwave radiation to sky [W m^{-2}]
T_{cole}	Sol-air temperature of collector [$^{\circ}\text{C}$]

T_{coled}	Sol-air temperature on the indoor side [°C]
T_{coleu}	Sol-air temperature on the outside air side [°C]
T_{duct}	Outlet temperature of air in handling box [°C]
T_{fin}	Collector inlet temperature, outside temperature [°C]
T_{floor}	Surface temperature of room floor [°C]
T_{fout}	Collector outlet temperature [°C]
T_{fin}	Collector inlet temperature [°C]
T_{hin}	Inlet temperature of heating medium in handling box [°C]
T_{hout}	Outlet temperature of heating medium in handling box [°C]
T_{hs}	Surface temperature of thermal storage [°C]
T_o	Outside temperature [°C]
T_{under}	Underfloor space temperature [°C]
T_x	Collector backside temperature [°C]
V_c	Volume flow rate of air in collection [$\text{m}^3 \text{s}^{-1}$]
W_{sd}, W_{su}	Width of collector frontside and backside, respectively [m]
α_c	Coefficient of heat transfer by convection [$\text{W m}^{-2} \text{K}^{-1}$]
α_o	Overall coefficient of heat transfer [$\text{W m}^{-2} \text{K}^{-1}$]
α_r	Coefficient of heat transfer by radiation [$\text{W m}^{-2} \text{K}^{-1}$]
ϵ_c	Thermal efficiency of heat exchanger in collector [-]
τ_g	Solar transmittance of glazing [-]

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