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A Cost-Effective Decentralized Control for AC-Stacked Photovoltaic Inverters

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Abstract: For an AC-stacked photovoltaic (PV) inverter system with N cascaded inverters, existing control methods require at least N communication links to acquire the grid synchronization signal. In this paper, a novel decentralized control is proposed. For N inverters, only one inverter nearest the point of common coupling (PCC) needs a communication link to acquire the grid voltage phase and all other $N - 1$ inverters use only local measured information to achieved fully decentralized local control. Specifically, one inverter with a communication link utilizes the grid voltage phase and adopts current control mode to achieve a required power factor (PF). All other inverters need only local information without communication links and adopt voltage control mode to achieve maximum power point tracking (MPPT) and self-synchronization with grid voltage. Compared with existing methods, the communication link and complexity is greatly reduced, thus improved reliability and reduced communication costs are achieved. The effectiveness of the proposed control is verified by simulation tests.

Keywords: AC-stacked PV inverters; PV generation; decentralized control; self-synchronization

1. Introduction

Renewable energy generation is drawing more and more attention in the past decades [1–5]. AC-stacked photovoltaic (PV) inverter architecture is now considered a promising PV generation configuration [6–12]. It facilitates the integration of low voltage (LV) PV generators into medium/high voltage (MV/HV) grid due to its AC-stacked characteristic. LV PV generation units can be connected to the MV/HV grid directly by the AC-stacked PV inverters with no need for a step-up transformer, which leads to improved energy conversion efficiency. Compared with the traditional multilevel cascaded H-bridge topology, each AC-stacked PV inverter has an independent output LC filter, which makes it much easier for coordinating all PV inverter units [6,7]. In this way, distributed control methods or even fully decentralized control methods are much easier to implement, which means the communication complexity is much lower and the system's reliability is higher. In this way, the AC-stacked PV inverter system has great potential for large-scale MV/HV grid-connected distributed PV generation. So, to explore new decentralized control methods with min-communication requirement for AC-stacked inverters makes a lot of sense. And the motivation of this paper is to propose a min-communication decentralized control for AC-stacked PV inverters.

Recently, some low-bandwidth communication-based controls for AC-stacked PV inverters have been investigated [8–12]. In Reference [8], a distributed autonomous control is first proposed without a central controller. Grid voltage phase from a phase locked loop (PLL) is transmitted to

all inverters to realize synchronization and maximum power point tracking (MPPT) operation by low-bandwidth communications. However, reactive power and power factor (PF) control are not discussed. To realize flexible power control and satisfactory PF, distributed active power and reactive power control methods are improved in Reference [9], where all AC-stacked inverters are controlled in voltage mode. Furthermore, references [10,11] propose a hybrid current-voltage control scheme with low-bandwidth communication. In References [5,6], one inverter in the AC-stacked PV inverter string is controlled as a current source to serve as a reactive power compensation unit and other inverters are controlled as voltage sources. A controllable PF is achieved by this hybrid control framework. Different from References [8–11], each AC-stacked inverter string has a central controller to coordinate all local controllers of inverters in Reference [12]. The voltage phase reference of each inverter is generated by combining the common current phase and the transmitted power factor from central controller. As the transmitted information is a slow DC component, a low-bandwidth communication link is required for each inverter.

Although existing control methods achieve MPPT and PF regulation, they all require at least N communication links for N inverters to acquire the synchronization signal from grid references [8–12]. As a result, system reliability is limited by high communication complexity. On the other hand, increased communication cost is unavoidable. Similar to the need to explore distributed/decentralized control approaches to solving the optimal power flow problem in power system references [13,14], how to design a decentralized control algorithm for AC-stacked PV inverters is necessary.

In view of the overview above, this paper proposes a min-communication decentralized control method to greatly improve system reliability and lower the communication cost. The contributions of the proposed control method are listed as follows:

- (1) It reduces the communication links to a great extent compared with existing control methods. Only one communication link is needed. Thus, system reliability is greatly improved and communication cost is reduced;
- (2) It achieves voltage self-synchronization with grid voltage with no need for PLL;
- (3) It can achieve a desirable unity PF or a required non-unity PF;
- (4) It achieves MPPT of all cascaded inverters under symmetrical conditions and partial shading;
- (5) It is available under grid voltage sag and grid frequency fluctuation.

The rest of this paper is organized as follows: In Section 2, the system configuration is described and the mathematical model of the AC-stacked PV inverter system is derived. In Section 3, the proposed control method is presented and analyzed in detail. In Section 4, simulation results under different conditions are provided to verify the effectiveness of the proposed control. Conclusions are finally drawn in Section 5. To make this paper clearer, variables and parameters used in this paper are listed in the nomenclature below.

2. System Modeling

The configuration of the AC-stacked PV inverter system studied in this paper is shown in Figure 1. The whole system consists of n series-connected PV inverter units, where each inverter has an independent output LC filter. These AC-stacked inverters are then connected to the utility grid directly without a step-up transformer. In each PV inverter unit, local PV panels are directly tied to the input port of an inverter. This type of system architecture aims to integrate LV distributed PV generators into the power grid directly with high energy conversion efficiency. Moreover, this topology makes it possible for distributed or decentralized control to be realized since output of each inverter is at AC line frequency.

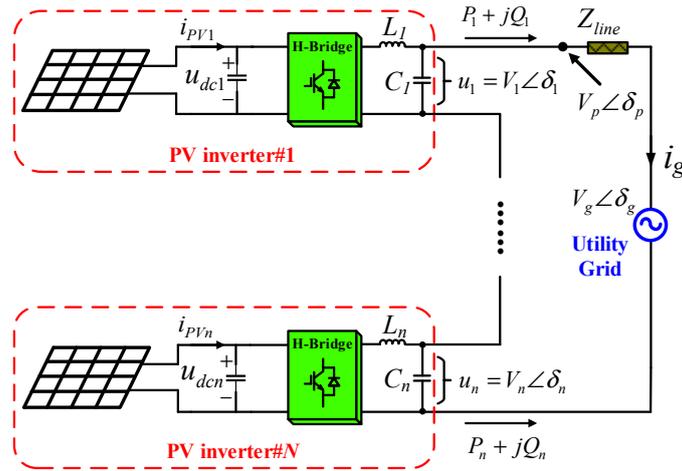


Figure 1. Configuration of AC-stacked photovoltaic (PV) inverter system.

In Figure 1, $V_1 \sim V_n$ and $\delta_1 \sim \delta_n$ are amplitudes and phase angles of the inverters' output voltages. V_g and δ_g represent amplitude and phase angle of the grid voltage, respectively. V_p and δ_p are voltage amplitude and phase at the PCC. L_{line} is the line inductance, its amplitude and angle are denoted as $|L_{line}|$ and θ_{line} . $i_{PV1} \sim i_{PVn}$ and $u_{dc1} \sim u_{dcn}$ represent the PV output currents and PV output voltages. $L_1 \sim L_n$ and $C_1 \sim C_n$ are the parameters of output LC filters. From Figure 1, the output active power and reactive power of i -th ($i = 1, 2, \dots, n$) inverter, which are denoted as P_i and Q_i , can be calculated as

$$P_i = \text{Re} \left\{ \frac{V_i e^{j\delta_i}}{2} \left(\frac{V_p e^{j\delta_p} - V_g e^{j\delta_g}}{|L_{line}| e^{j\theta_{line}}} \right)^* \right\} \quad (1)$$

$$Q_i = \text{Im} \left\{ \frac{V_i e^{j\delta_i}}{2} \left(\frac{V_p e^{j\delta_p} - V_g e^{j\delta_g}}{|L_{line}| e^{j\theta_{line}}} \right)^* \right\} \quad (2)$$

There is a factor 1/2 in Equations (1) and (2) because V_i , V_p and V_g are all amplitude values, instead of RMS (Root Mean Square) values. For this AC-stacked PV inverter architecture, the voltage at the PCC is the sum of $u_1 \sim u_n$:

$$V_p e^{j\delta_p} = \sum_{j=1}^n V_j e^{j\delta_j} \quad (3)$$

By substitution of Equation (3) into Equations (1) and (2), P_i and Q_i are derived as

$$P_i = \sum_{j=1}^n \frac{V_i V_j}{2|Z_{line}|} \cos(\delta_{line} + \delta_i - \delta_j) - \frac{V_i V_g}{2|Z_{line}|} \cos(\delta_{line} + \delta_i - \delta_g) \quad (4)$$

$$Q_i = \sum_{j=1}^n \frac{V_i V_j}{2|Z_{line}|} \sin(\delta_{line} + \delta_i - \delta_j) - \frac{V_i V_g}{2|Z_{line}|} \sin(\delta_{line} + \delta_i - \delta_g) \quad (5)$$

3. Proposed Decentralized Control

3.1. Schematic Overview of the Proposed Decentralized Control

The overall schematic overview of the proposed decentralized control is presented in Figure 2. It is noted that only one communication link is needed to transmit the grid voltage phase to inverter#1. Inverter#1 is controlled as a current source to carry out PF regulation and track its maximum power point (MPP). Inverter#1 can achieve a desired PF according to practical requirements.

All other inverters are controlled as voltage sources locally and independently to achieve MPPT and self-synchronization. They need only local information and they need no grid synchronization signal.

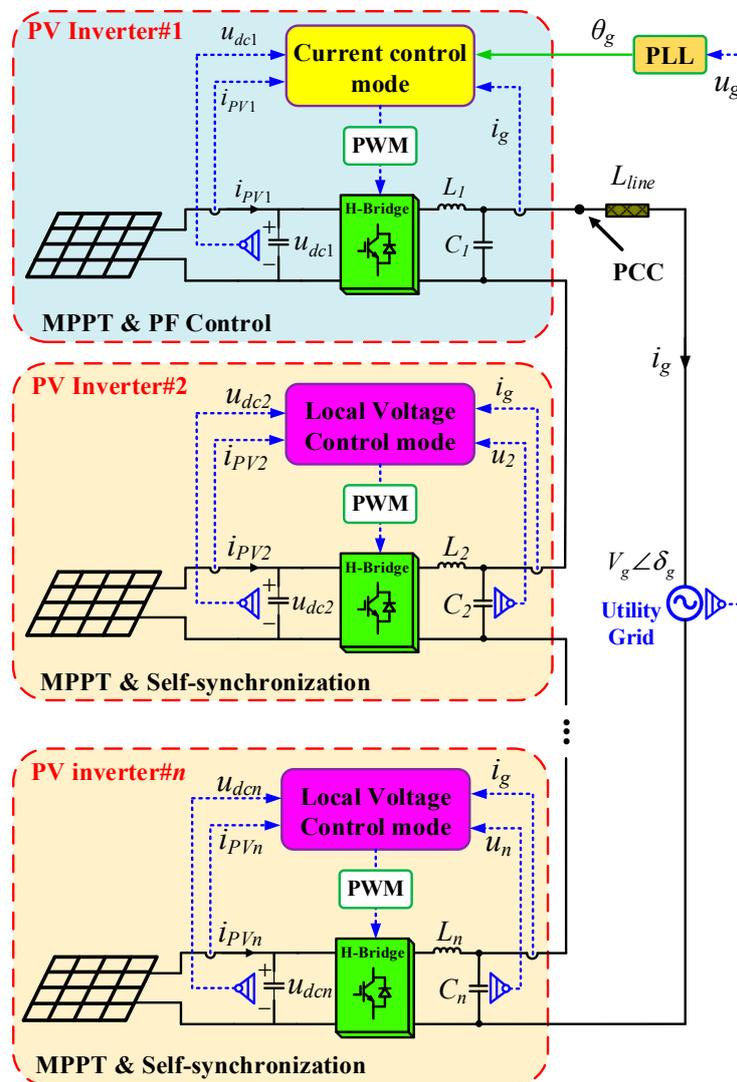


Figure 2. Overall control framework of the proposed method.

3.2. Proposed Decentralized Control

The control diagram of inverter#1 is shown in Figure 3. Inverter#1 is controlled as a current source to serve as a current regulation unit for the AC-stacked PV inverter string while tracking its MPP. The front-end DC-link voltage reference u_{dc1}^{ref} is provided by the MPPT controller. In order to realize the desired PF, the line current phase reference is determined by the grid voltage phase θ_g from a PLL. Then the output current reference i_g^* is synthesized by I_g^* , θ^* and θ_g . θ^* is the system PF angle, which is set according to the practical PF requirement. Thus, the proposed method can achieve different PFs by setting different values of θ^* . Finally, the line current is regulated to its reference value by a proportional (PR) controller.

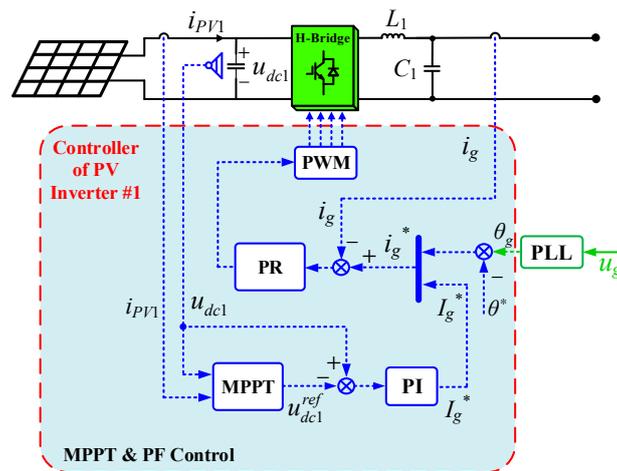


Figure 3. Control diagram of inverter#1.

For inverter# i ($i = 2, 3, \dots, n$), the detailed control diagram is presented in Figure 4. Inverter# i is responsible for building up the voltage at the PCC while outputting its maximum power available. The proposed control for inverter# i aims to achieve self-synchronization and MPPT without communication links. As shown in Figure 4, the core of proposed control is designed as

$$\begin{cases} V_i = \frac{V_g}{n} + \left(K_{Pi} + \frac{K_{Ii}}{s} \right) (u_{dci} - u_{dci}^{ref}) \\ \omega_i = \omega^* + \left(k_{Pi} + \frac{k_{Ii}}{s} \right) (\sin \theta^* - \sin \theta_i) \end{cases} \quad (i = 2, 3, \dots, n) \quad (6)$$

where V_i and ω_i represent the output voltage amplitude reference and angular frequency reference of inverter# i respectively. V_g and ω^* are the rated grid voltage amplitude and rated grid angular frequency. u_{dci} is the front-end DC-link voltage of inverter# i and u_{dci}^{ref} is the DC-link voltage reference provided by MPPT controller. K_{Pi} and K_{Ii} are the proportional and integral (PI) coefficients of the DC-link voltage controller. θ_i and θ^* are real-time PF angle of inverter# i and its reference. θ^* can be flexibly set according to the system PF requirement. k_{Pi} and k_{Ii} are the proportional and integral coefficients of the frequency controller. The designed frequency controller can realize frequency self-synchronization with the grid frequency.

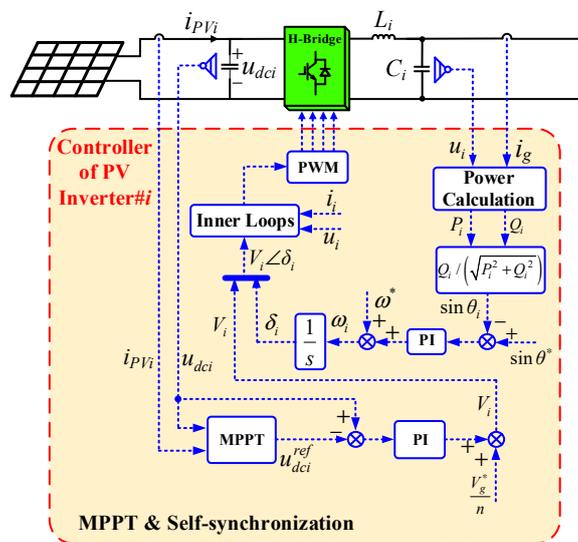


Figure 4. Control diagram of inverter# i ($i = 2, 3, \dots, n$).

As the DC-link voltage controller is a PI regulator, V_i can be regulated autonomously to form the voltage at the PCC and match the grid voltage. In this way, the proposed method is adaptable even when grid voltage sag happens. Additionally, Equation (7) must hold in steady state:

$$u_{dci} = u_{dci}^{ref} \quad (7)$$

Equation (7) reveals that MPPT operation is ensured in steady state. On the other hand, Equation (8) must hold in steady-state:

$$\omega_i = \omega^* \quad (8)$$

In other words, Equation (9) must hold to reach a steady state:

$$\left(k_{pi} + \frac{k_{li}}{s}\right)(\sin \theta^* - \sin \theta_i) = 0 \quad (9)$$

Since frequency controller is a PI controller, Equation (10) must hold in steady state.

$$\sin \theta^* = \sin \theta_i \quad (10)$$

This indicates that the frequency of each inverter will be synchronous with grid frequency in a steady state and the output voltage of each inverter will be in phase with grid voltage in a steady state. Moreover, From Equations (6)–(10) and Figure 4, MPPT of inverter# i is achieved by regulating its output voltage amplitude and self-synchronization with grid voltage is achieved by adjusting the output angular frequency according to its own PF angle. No communication links are involved and PLL is not needed.

3.3. Steady-State Analysis and Self-Synchronization Mechanism

According to the description in Section 3.2, the proposed method is adaptable under grid voltage sag and grid frequency fluctuation. On the other hand, it can also meet different PF requirements. In practical PV grid-connected applications, unity PF is often required. So, we take the unity PF condition as an example to analyze the control mechanism. Similar analysis can also be adapted in other non-unity PF conditions.

With the proposed control for PV inverter#1, the line current is regulated and becomes in phase with the grid voltage in steady state to satisfy the unity PF requirement. As the line current is a common signal for all the AC-stacked PV inverters, inverter# i ($i = 2, 3, \dots, n$) can thus self-synchronize its output voltage with the grid voltage indirectly by synchronizing its output voltage with the line current locally. So, we set $\sin \theta^* = 0$ in Equation (6) for inverter# i to synchronize with grid voltage under unity PF operation requirement.

The detailed self-synchronization mechanism in Equation (6) can be illustrated by Figure 5.

- Initially, the system is operating in steady-state. The steady-state phasor diagram is shown in Figure 5a. Output voltages of inverter#2~inverter# n , line current and the grid voltage are all in phase in a steady state. Small amount of reactive power consumed by the line impedance is compensated by inverter#1 and unity PF of this grid-connected system is ensured;
- When disturbances occur, power angle of inverter# i will change. For example, $\theta_i > 0$ as shown in Figure 5b. According to Equation (6), the angular frequency reference $\omega_i = (\omega^* - k_i \sin \theta_i) < \omega^*$. And thus the relative angular frequency between u_i and u_g is: $\Delta\omega_i = (\omega_i - \omega^*) = -k_i \sin \theta_i < 0$;
- As a result, θ_i will decrease until $\theta_i = 0$ and self-synchronization of inverter# i is achieved;
- Similar analysis can be applied to the condition where $\theta_i < 0$ occurs as shown in Figure 5c. From the analysis above, self-synchronization of u_i with the grid voltage u_g is achieved with the proposed control.

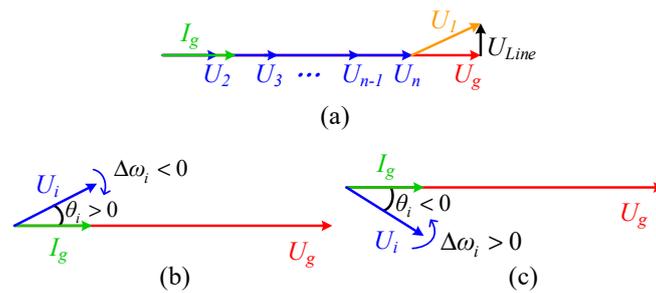


Figure 5. (a) Steady-state phasor diagram; (b) Self-synchronization process of inverter#*i* when $\theta_i > 0$; (c) Self-synchronization process of inverter#*i* when $\theta_i < 0$.

4. Simulation Results

To verify the correctness and effectiveness of the proposed control method, four simulation tests in different operation conditions are conducted. The simulation model consists of three AC-stacked PV inverters. Simulation parameters are listed in Table 1.

Table 1. Simulation Parameters.

Symbol	Value	Symbol	Value
V_g	311 V	$K_{P2} = K_{P3}$	1.8
ω^*	$2\pi \times 50$ rad/s	$K_{I2} = K_{I3}$	6
$\sin\theta^*$	0 & 0.392	$k_{P2} = k_{P3}$	7
L_{line}	300 μ H	$k_{I2} = k_{I3}$	0.2
$C_{DC1} = C_{DC2} = C_{DC3}$	4000 μ F	-	-

4.1. Symmetrical Condition and Partial Shading

To evaluate the steady-state and dynamic performances of the proposed control, both symmetrical condition and partial shading condition are simulated. Before $t = 2$ s, the symmetrical operation condition is simulated. At $t = 2$ s, different partial shadings are imposed on PV inverter#2 and PV inverter#3 simultaneously. Simulation results are shown in Figure 6.

Before $t = 2$ s, the output active power of the inverters P_1 , P_2 and P_3 are equal in Figure 6a, since the system operates under symmetrical conditions. In Figure 6c, steady-state DC-link voltages of all the inverters are the same, which indicates all PV inverter units operates at MPP. In Figure 6b, output voltages of inverter#2 and inverter#3 are identical, while output voltage of inverter#1 is a little different to compensate the line reactive power. After $t = 2$ s, P_2 drops from 1500 W to 1400 W and P_3 drops to 1200 W while P_1 stays unchanged in Figure 6a, because different shadings are imposed on inverter#2 and inverter#3 simultaneously. The DC-link voltages u_{dc2} and u_{dc3} drop to different steady-state values accordingly, shown in Figure 6c, still operating at the MPP. In Figure 6b, u_2 and u_3 are still in phase while their amplitudes are different, owing to their different maximum power outputs. In addition, amplitude of u_1 is the highest, because it generates the highest active power and compensates the line reactive power to regulate system PF. Figure 6d shows that the line current and grid voltage are always in phase in different steady states. So, unity PF of the system is achieved in both symmetrical and partial shading conditions. Moreover, the steady-state line current amplitude after $t = 2$ s is smaller than the current amplitude before $t = 2$ s, since total active power injected to the grid is smaller when partial shading happens. Output voltages in transient states are shown in Figure 6e, the output voltages of the inverters response immediately according to the control algorithm in Equation (6). Grid voltage and line current in transient states are presented in Figure 6f. It is clear that the amplitude of the transient line current transient is not too high and the phase angle of line current is also in phase with the grid voltage. So, required unity PF is ensured in the transient state.

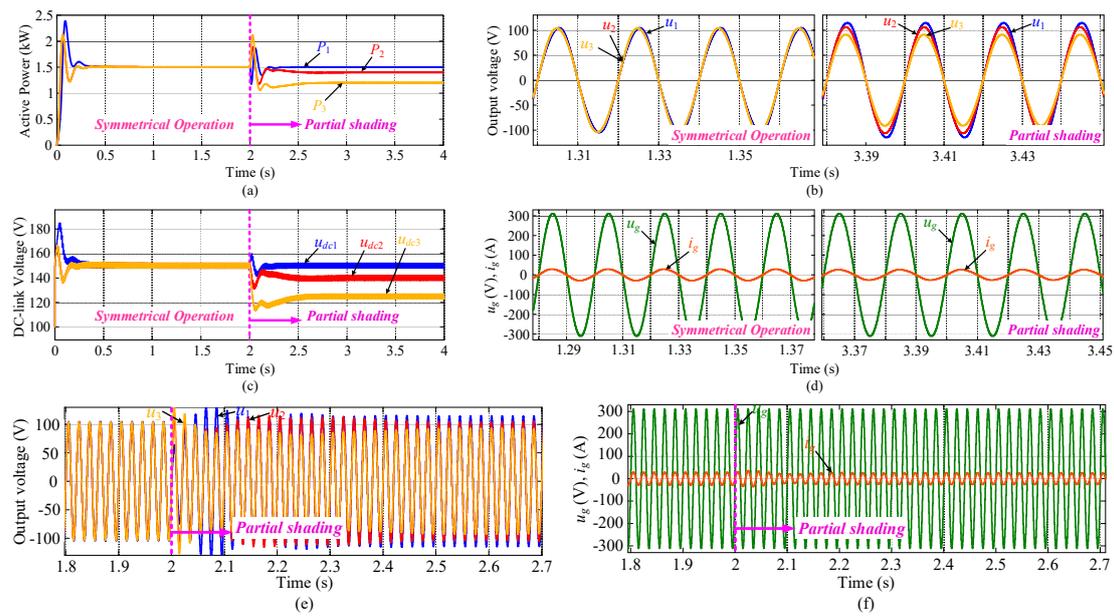


Figure 6. Simulation results under symmetrical condition and partial shading condition. (a) Active power; (b) Steady-state output voltages; (c) DC-link voltages; (d) Grid voltage and line current in steady state; (e) Output voltages in transient state; (f) Grid voltage and line current in transient state.

4.2. Grid Voltage Sag Condition

To demonstrate the feasibility of the proposed method under grid faults, a simulation test under 10% grid voltage sag is carried out. Before $t = 1$ s, the system operates under rated grid voltage condition. At $t = 1$ s, 10% grid voltage sag is simulated. Simulation results are shown in Figure 7.

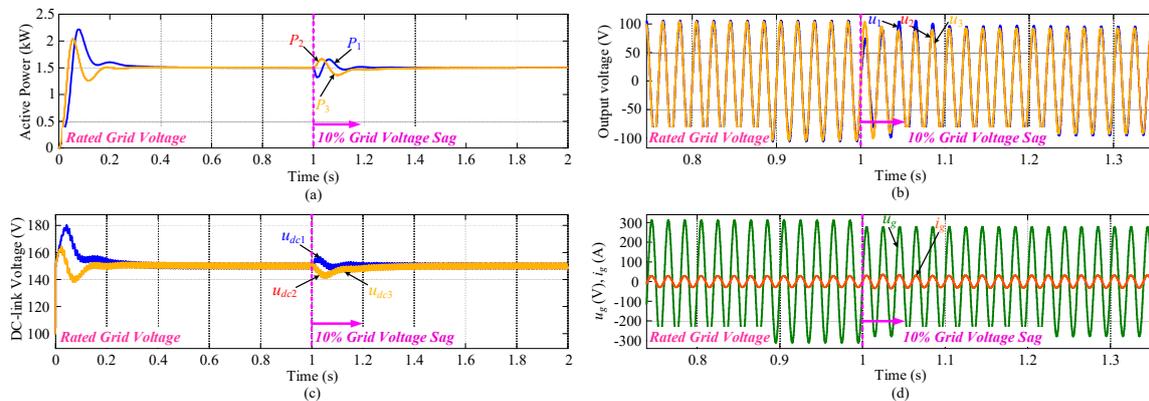


Figure 7. Simulation results under 10% grid voltage sag condition. (a) Active power; (b) Steady-state output voltages; (c) DC-link voltages; (d) Grid voltage and line current in steady state.

From Figure 7a,c $P_1 \sim P_3$ are identical and DC-link voltages $u_{dc1} \sim u_{dc3}$ reach the same steady-state value during $t = 0 \sim 1$ s, which indicates that the system operates under symmetrical conditions and achieves MPPT. In Figure 7b, output voltages of inverter#2 and inverter#3 are identical before $t = 1$ s, while output voltage of inverter#1 is a little different to compensate for the line reactive power. Figure 7d shows that grid voltage and line current are inphase and a satisfactory unity PF is achieved, where the grid voltage is at its rated value. At $t = 1$ s, 10% grid voltage sag is implemented which can be seen in Figure 7d. During this process, output voltage of inverter#1 reacts immediately to compensate for the grid voltage sag as shown in Figure 7b. Meanwhile, inverter#2 and inverter#3

reduce their output voltage amplitudes gradually according to Equation (6). Eventually, $u_1 \sim u_3$ reach new steady-state values to match the sagged grid voltage. In Figure 7d, the amplitude of line current increases to a higher steady-state value after $t = 1$ s to maintain the maximum active power output of all PV inverters and line current is still inphase with the grid voltage to satisfy unity PF requirement. From Figure 7a,c the steady-state values of $P_1 \sim P_3$ and DC-link voltages $u_{dc1} \sim u_{dc3}$ stay unchanged after $t = 1$ s despite 10% grid voltage sag. So, MPPT operation of all PV inverters are still ensured and self-synchronization of inverter#2 and inverter#3 are realized. Thus, the proposed method is immune to the grid voltage fault.

4.3. Grid Frequency Fluctuation Condition

To verify the feasibility of the proposed method under grid frequency fluctuation, a simulation test with random grid frequency variation is performed. Initially, the system operates under rated grid frequency condition. Then random frequency fluctuation is simulated. Simulation results are shown in Figure 8.

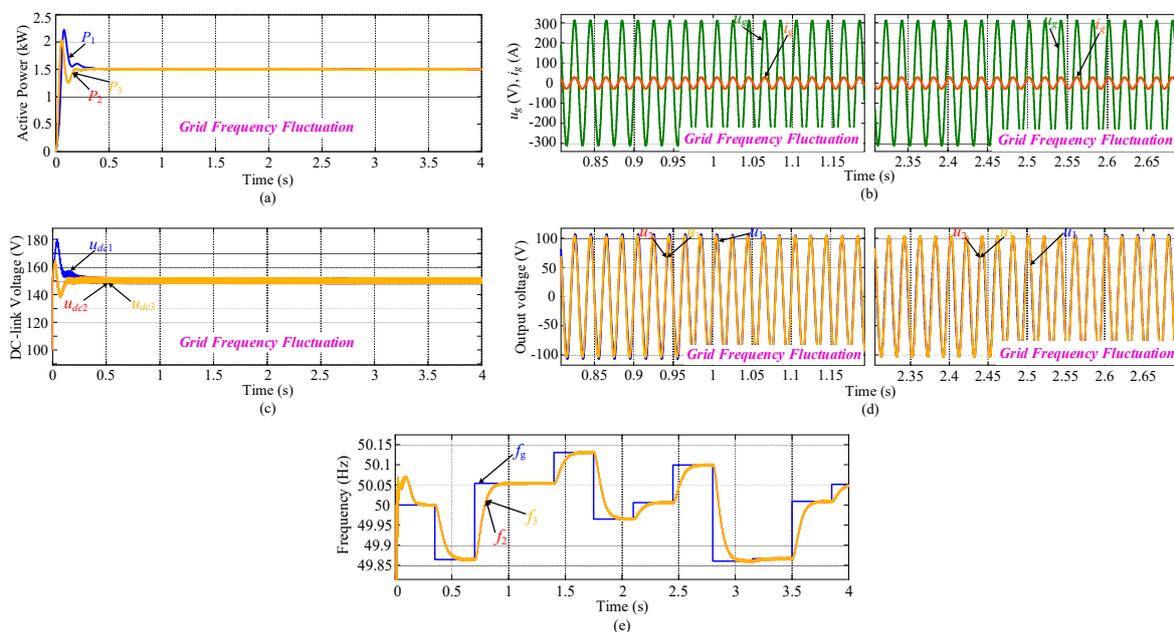


Figure 8. Simulation results under grid frequency fluctuation. (a) Active power; (b) Grid voltage and line current; (c) DC-link voltages; (d) Output voltages; (e) Frequencies.

From Figure 8a,c $P_1 \sim P_3$ are identical and DC-link voltages $u_{dc1} \sim u_{dc3}$ reach the same steady-state value, which indicates that the system operates under symmetrical condition and achieves MPPT. In Figure 8d, output voltages of inverter#2 and inverter#3 are identical, while output voltage of inverter#1 is a little different to compensate the line reactive power. Figure 8b shows that grid voltage and line current are inphase and a desired unity PF is achieved. The frequencies of the system are shown in Figure 8e. In the beginning, grid frequency is the rated value. $f_2 \sim f_3$ are 50 Hz tracking the rated grid frequency. Then, grid frequency varies randomly. Accordingly, $f_2 \sim f_3$ follow to change and track the real-time grid frequency tightly. Thus, the proposed control method is adaptable to the grid frequency fluctuation and can self-synchronize the inverters' frequencies with the grid frequency. So, the proposed control method can maintain the stability of the system even when grid frequency fluctuation occurs.

4.4. No-Unity PF Operation

In most grid-connected PV generation applications, unity PF is required. However, no-unity PF and Volt/Var capability of the inverters are required. To verify the PF controllability of the proposed method, a simulation test with a required PF = 0.92 is performed. To achieve PF = 0.92, we just need to set $\theta^* = 0.4027$ in Equation (6). Simulation results are shown in Figure 9.

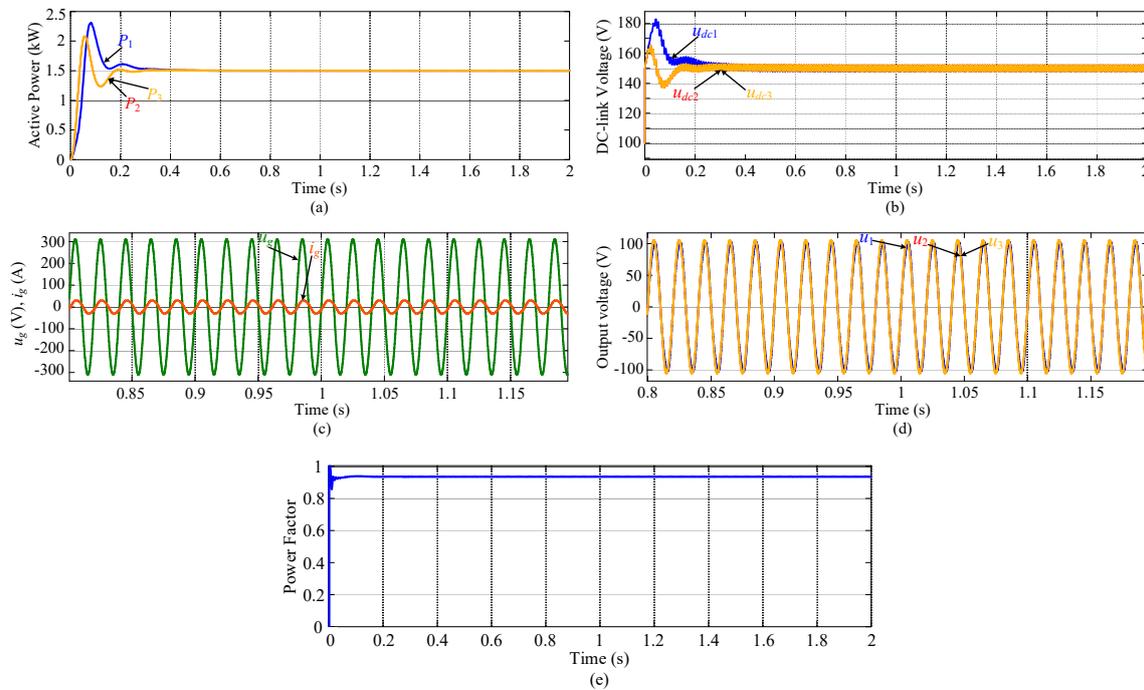


Figure 9. Simulation results under grid frequency fluctuation. (a) Active power; (b) DC-link voltages; (c) Grid voltage and line current; (d) Output voltages; (e) Power factor (PF).

From Figure 9a,b $P_1 \sim P_3$ are identical and DC-link voltages $u_{dc1} \sim u_{dc3}$ reach the same steady-state value, which indicates that the system operates under symmetrical condition and achieves MPPT. In Figure 9d, output voltages of inverter#2 and inverter#3 are identical, while output voltage of inverter#1 is a little different to compensate the line reactive power. Figure 9c shows that grid voltage and line current are not inphase and a no-unity PF is achieved. The system PF is shown Figure 9e. Obviously, the required PF = 0.92 is achieved.

From the simulation results and analysis above, we can see the advantages and performances of the proposed control method clearly. For an AC-stacked PV inverter system with N inverters, the main advantages and performances of the proposed control method in comparison with the existing control methods are summarized in Table 2.

Table 2. Comparison with Existing Control Methods.

Items	Proposed Decentralized Control	Existing Control Methods
Number of Communication Links	1	N
Communication Cost	Low	High
Communication Complexity	Low	High
Reliability in Case of Communication Faults	High	Low
Synchronization Method	By Self-synchronization Mechanism	By Centralized Communication
Global MPPT Operation	Yes	Yes
Operation Under Grid Voltage Sag	Yes	Yes
Operation Under Grid Frequency Fluctuation	Yes	Yes

5. Conclusions

This paper proposes a one-communication-link decentralized control for AC-stacked PV inverter system. It achieves the following objectives:

- (1) It reduces the communication complexity to a great extent compared with existing control methods. Specifically, it reduces $N - 1$ communication links for a system with N inverters. Thus system reliability is greatly improved and communication cost is reduced;
- (2) It achieves voltage self-synchronization with grid voltage;
- (3) It can achieve a desirable unity PF or a required non-unity PF;
- (4) It achieves MPPT of all cascaded inverters under symmetrical conditions and partial shading;
- (5) It is available under grid voltage sag and grid frequency fluctuation.

Simulation tests under symmetrical/partial-shading condition, grid voltage sag condition, grid frequency fluctuation condition and non-unity PF requirement condition have verified the effectiveness of the proposed control method. Beyond this study, the possibilities of new ideas will be inspired in future cascaded-type distributed generation systems.

For better operation of the AC-stacked PV inverter system in practical application situation, seeking for optimal configuration of the energy storage system in this architecture and corresponding control methods with high reliability are very important and meaningful. This aspect will be explored in our future work.

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Nomenclature

u_{dci}	DC-link voltage of i -th inverter
i_{pVi}	PV current of i -th inverter
L_{line}	Line inductance
C_{DCi}	Capacitor in DC side
i_g	Line current
$V_g \angle \delta_g$	Grid voltage
i_g^*	Line current reference
u_{dc}^{ref}	DC-Link voltage reference
θ_i	Power angle of i -th inverter
V_g^*	Rated grid voltage amplitude
ω^*	Rated grid frequency
V_i	Output voltage amplitude reference of i -th inverter
ω_i	Angular frequency of i -th inverter
u_i	Output voltage amplitude of i -th inverter
K_{pi}, K_{Ii}	Proportional and integral coefficients of DC voltage controller
k_{pi}, k_{Ii}	Proportional and integral coefficients of frequency controller

References

1. Hou, X.; Sun, Y.; Han, H.; Liu, Z.; Yuan, W.; Su, M. A fully decentralized control of grid-connected cascaded inverters. *IEEE Trans. Power Del.* **2018**. [[CrossRef](#)]
2. Sun, Y.; Hou, X.; Yang, J.; Han, H.; Su, M.; Guerrero, J.M. New perspectives on droop control in AC microgrid. *IEEE Trans. Ind. Electron.* **2017**, *64*, 5741–5745. [[CrossRef](#)]

3. Hou, X.; Sun, Y.; Han, H.; Liu, Z.; Su, M.; Wang, B.; Zhang, X. A General Decentralized Control Scheme for Medium/High Voltage Cascaded STATCOM. *IEEE Trans. Power Syst.* **2018**. [[CrossRef](#)]
4. Liu, Z.; Su, M.; Sun, Y.; Li, L.; Han, H.; Zhang, X.; Zheng, M. Optimal criterion and global/sub-optimal control schemes of decentralized economical dispatch for AC microgrid. *Int. J. Electr. Power Energy Syst.* **2019**, *104*, 38–42. [[CrossRef](#)]
5. Li, L.; Ye, H.; Sun, Y.; Han, H.; Li, X.; Su, M.; Guerrero, J.M. A communication-free economical-sharing scheme for cascaded-type microgrids. *Int. J. Electr. Power Energy Syst.* **2019**, *104*, 1–9. [[CrossRef](#)]
6. Nuotio, M.; Ilic, M.; Liu, Y.; Bonanno, J.; Verlinden, P.J. Innovative AC photovoltaic module system using series connection and universal low-voltage micro inverters. In Proceedings of the 2014 IEEE 40th Photovoltaic Specialist Conference (PVSC), Denver, CO, USA, 8–13 June 2014; pp. 1367–1369.
7. Bhowmik, S. Systems and Methods for Solar Photovoltaic Energy Collection and Conversion. U.S. Patent 9,531,293, 27 December 2016.
8. Lu, F.; Choi, B.; Maksimovic, D. Autonomous control of series-connected low voltage photovoltaic microinverters. In Proceedings of the 2015 IEEE 16th Workshop on Control and Modeling for Power Electronics (COMPEL), Vancouver, BC, Canada, 12–15 July 2015; pp. 1–6.
9. Zhang, L.; Sun, K.; Li, Y.W.; Lu, X.; Zhao, J. A Distributed Power Control of Series-connected Module Integrated Inverters for PV Grid-tied Applications. *IEEE Trans. Power Electron.* **2017**, 7698–7707. [[CrossRef](#)]
10. Jafarian, H.; Cox, R.; Enslin, J.H.; Bhowmik, S.; Parkhideh, B. Decentralized Active and Reactive Power Control for an AC-Stacked PV Inverter with Single Member Phase Compensation. *IEEE Trans. Ind. Appl.* **2018**, *54*, 345–355. [[CrossRef](#)]
11. Jafarian, H.; Bhowmik, S.; Parkhideh, B. Hybrid Current-/Voltage-Mode Control Scheme for Distributed AC-Stacked PV Inverter with Low-Bandwidth Communication Requirements. *IEEE Trans. Ind. Electron.* **2018**, *65*, 321–330. [[CrossRef](#)]
12. He, J.; Li, Y.; Wang, C.; Pan, Y.; Zhang, C.; Xing, X. Hybrid Microgrid With Parallel- and Series-Connected Microconverters. *IEEE Trans. Power Electron.* **2018**, *33*, 4817–4831. [[CrossRef](#)]
13. Hadi Amini, M.; Bahrami, S.; Kamyab, F.; Mishra, S.; Jaddivada, R.; Boroojeni, K.; Weng, P.; Xu, Y. Decomposition Methods for Distributed Optimal Power Flow: Panorama and Case Studies of the DC Model. *Class. Recent Asp. Power Syst. Optim.* **2018**, 137–155. [[CrossRef](#)]
14. Mohammadi, A.; Mehrtash, M.; Kargarian, A. Diagonal Quadratic Approximation for Decentralized Collaborative TSO+DSO Optimal Power Flow. *IEEE Trans. Smart Grid.* **2018**, *1*. [[CrossRef](#)]



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