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Small-Signal Performance of Type 4 Wind Turbine Generator-Based Clusters in Power Systems

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Abstract: The impact of Type 4 wind turbine generator (WTG)-based 10 million megawatt clusters (TMMC) on small-signal dynamics of power systems was investigated using the second-generation generic models (GM) of Western Electricity Coordinating Council (WECC). A WTG participation index (WTG PI) was defined to investigate the impact of Type 4 WTGs on the traditional interarea electromechanical modes. To identify the new electromechanical modes dominated by Type 4 WTGs, an identification factor (IF) was also defined using participation factors. Given the increasing penetration of Type 4 WTGs replacing synchronous generators, the changed law of damping and frequencies of the traditional interarea modes was also investigated using the WTG PI. One new type of electromechanical mode dominated by Type 4 WTGs was identified by using the defined IF. These new modes can be divided into two categories: strong-interaction modes and weak-interaction modes, depending on the number of participating WTGs. The strong-interaction modes dominated by Type 4 WTGs can result in widely spread power oscillations in power systems. The results of small-signal analysis were validated by time domain simulation and mode detection.

Keywords: generic model (GM); wind turbine generators (WTGs); damping ratio; small-signal stability

1. Introduction

The Type 4 wind turbine generator (WTG)-based 10 million megawatt cluster (TMMC) has been put into operation in the northwest China Grid. The Type 4 WTG-based TMMC consist of dozens of wind farms that are centrally integrated into one area of a power system. Its total capacity is greater than 10 million megawatts. The capacity of Type 4 WTGs is increasing recently, and they account for more than one-third of the total capacity of wind turbine generators in China. However, Type 4 WTGs are connected to power systems using electronic converters. This is different from the traditional synchronous generators that are directly connected to power systems. The mechanical dynamics of Type 4 WTGs are completely decoupled from power systems. Thus, they cannot provide inertia response for the connected power systems, which may cause the dynamic damping of the connected power systems to become so weak that it is difficult to damp out the power oscillation during small-signal events. In other words, Type 4 WTG-based TMMCs have a significant impact on the electromechanical dynamic performance of power systems. Industrial circles have shown concerns about the impact of Type 4 WTG-based TMMCs on small-signal performance of power systems in China. Therefore, it is urgent to investigate the impact of Type 4 WTG-based TMMCs on small-signal performance of power systems.

Using a single machine infinite bus system, some works addressed the modal characteristics of Type 4 WTGs themselves [1–3], but they did not investigate the impact of Type 4 wind turbine generators on the small-signal stability of power systems by using a multimachine power system. The supplementary frequency and oscillation control loops of Type 4 WTGs have been presented for emulating inertia response by using a single machine infinite bus system as well [4–6]. In terms of the small-signal stability for multimachine power systems, a previous study focused on the impact of Type 3 WTGs on small-signal stability of power systems. However, compared with Type 3 WTGs, Type 4 WTGs have a different impact on the small-signal stability of power systems. The previous conclusions for Type 3 WTGs are not applicable for Type 4 WTGs. A thorough survey of literature shows that the potential impact of Type 4 WTG-based TMMCs on the electromechanical behavior of power systems has received little study.

The impact of the combination of Type 3 WTGs, Type 4 WTGs and utility-scale photovoltaic systems on the small-signal stability of power systems has been investigated by using the first-generation generic models (GMs) of Western Electricity Coordinating Council (WECC) and General Electric models in production-level power systems [7]. Most previous studies adopted custom models [1–3] or the first-generation GMs of WTGs for analysis of small-signal stability [7]. They were hardly validated by measured data. Additionally, the active power control seemed to be too simple for the first-generation Type 4 GM; the reactive power control of the first-generation GM does not cater to various reactive power injection options of various designs [8]. These above defects of the first-generation Type 4 GM can result in the incorrect results.

The WECC developed the second-generation GMs for representing wind farms after the first-generation GMs had been implemented for several years [8–15]. The second-generation GMs improved the above limitations of the first-generation GMs. Also, the second-generation GMs have been verified through a large number of field-measured data. As such, the second-generation GMs can reliably describe the electromechanical dynamics of WTGs from different manufacturers. No literature has been found with regard to adopting the second-generation GMs to study the influence of Type 4 WTGs on the small-signal stability of power systems.

Despite that the commercial software of power system simulation PSS/E [16] was used to conduct the analysis, the contributions of this work are:

(1) The identification of two undocumented types of electromechanical modes dominated by Type 4 WTGs: strong-interaction modes and weak-interaction modes.

Almost all Type 4 WTGs connected to power systems participate in the strong-interaction modes; with the increase of wind penetration levels, their damping gradually becomes weak, and finally negative. The strong-interaction modes can result in widely spread power oscillations in power systems. However, the weak-interaction modes are only related to a few WTGs, and the damping of weak-interaction modes is almost constant with the increase of wind generation penetration. Therefore, the strong-interaction modes of Type 4 WTGs have a significant impact on the security of power systems, but this is not the case for the weak-interaction modes.

(2) The second-generation GMs of Type 4 WTGs were used to implement a simulation analysis in a moderate-scale test bed of the IEEE 16-machine 68-bus standard test system. Each wind farm in the TMMC was represented by a Type 4 equivalent WTG using the second-generation GM. The impact of Type 4 WTG-based TMMC on the small-signal performance of power systems was firstly investigated in this work using the second-generation GM.

The rest of the paper is organized as follows. Section 2 presents the fundamental basis of the modal-based small-signal stability analysis used in this work. Section 3 presents the framework of the second-generation of Type 4 WTGs. With the increasing penetration level of Type 4 WTGs, two new kinds of modes dominated by Type 4 WTGs are identified and characterized in Section 4. Finally, the conclusions are summarized in Section 5.

2. Theory of Small-Signal Stability Analysis with WTGs

2.1. Small-Signal Stability Theory

Similar to the conventional power systems, the electromechanical dynamics of power systems involving WTGs can be also described as differential algebraic equations. Nonlinear first-order ordinary differential equations are used to describe the dynamic characteristics of the components concerned. The quasi-steady-state behavior of a transmission network is represented by nonlinear algebraic equations [7]. Assuming the steady-state equilibrium point of the system is not a singularity of network equations, these differential algebraic equations can be linearized as a standard formulation:

$$\Delta \dot{x} = A \Delta x \quad (1)$$

where A is the Jacobian matrix of the linearization equation of differential algebraic equations.

According to the Lyapunov stability theory, the sign of the eigenvalues of the Jacobian matrix determines the stability of the linearized system. Traditional synchronous generators (SG) are directly connected to the alternative current (AC) power network. The rotor flux is directly fixed to the rotor. When the rotor is disturbed, the rotor flux linkage changes with the actual physical position of the rotor, so that the generator rotor oscillates to induce power oscillation and synchronization stability issues. The traditional power oscillation modes of power systems only involve electromechanical modes governed by synchronous generators. Therefore, the previous study of the power oscillation of power systems only focused on traditional electromechanical modes governed by SGs. A traditional electromechanical mode corresponds to a pair of complex eigenvalues, $\lambda_i = \sigma_i + j\omega_i$. Its damping ratio is defined as $\zeta_i = -\sigma_i / \sqrt{\sigma_i^2 + \omega_i^2}$.

The eigenvalues satisfy

$$\begin{cases} A \mathbf{u}_i = \lambda_i \mathbf{u}_i \\ \mathbf{v}_i A = \lambda_i \mathbf{v}_i \end{cases} \quad (2)$$

where \mathbf{u}_i is the i th column of the right eigenvector matrix, u of A ; \mathbf{v}_i is the i th row of the left eigenvector matrix, v of A ; they are respectively called the right and left eigenvectors. The relationship between the right and the left eigenvectors can be expressed as $v = u^{-1}$.

The normalized right eigenvector \mathbf{u}_i and the left eigenvector \mathbf{v}_i are combined to form the participation matrix p , which is used to measure the degree of correlations between modes and state variables. The k th row i th column of elements of the participating matrix p can be expressed as,

$$p_{ki} = u_{ki} v_{ki} \quad (3)$$

where p_{ki} is called the participation factor. The participation factor is dimensionless and used to measure the degree of mutual involvement between the i th mode and the k th state variable.

2.2. Impact of Type 4 WTGs on Traditional Electromechanical Modes

For n synchronous generators in power systems, there are usually $(n - 1)$ electromechanical modes. In order to assess the impact of Type 4 WTGs on traditional interarea electromechanical modes, the participation of Type 4 WTGs in traditional interarea electromechanical mode i can be determined through a WTG participation index (PI):

$$\text{WTG } PI_i = \left| \frac{\sum_{\text{WTG}} p_{ki}}{\sum_{\text{All}} p_{ki}} \right| \quad (4)$$

where $\sum_{\text{All}} p_{ki}$ denotes the summation of participation factors of all state variables of the system affecting mode i ; $\sum_{\text{WTG}} p_{ki}$ denotes the sum of participation factors of the state variables of WTGs affecting mode i ; p_{ki} greater than 0.1 is used to calculate $\text{WTG } PI_i$ and p_{ki} smaller than 0.1 is negligible.

If $WTG PI_i \approx 0$, the Type 4 WTGs in the TMMC have no participation in traditional interarea electromechanical modes. If not, the Type 4 WTGs have an impact on traditional interarea electromechanical modes.

2.3. Identification of Electromechanical Modes Dominated by Type 4 WTGs

The rotor oscillations of permanent magnet synchronous generators (PMSG) will result in the power oscillation and synchronization stability issues when they are directly connected to AC networks. However, the PMSGs of Type 4 WTGs are integrated into power systems using electronic converters. Previously, it was believed that mechanical dynamics of Type 4 WTGs are completely decoupled from the power grid so that Type 4 WTGs' electromechanical oscillations cannot spread into the connected power system. However, this paper draws the conclusion that the electromechanical oscillations of PMSGs of Type 4 WTGs may spread into the connected power system.

The electromechanical modes of Type 4 WTGs should be strongly related to the mechanical state variables of the drive-train model, $wtgt_a$, such as ω_t , ω_g , δ_t and δ_g . However, a large number of oscillation modes can be solved by Equation (3), but only a few of them are dominated by the PMSGs of Type 4 WTGs. To identify the electromechanical modes dominated by Type 4 WTGs, the identification factor (IF) of the mechanical state variables of Type 4 WTGs in mode i , λ_i , is defined using participation factors:

$$IF_i = \left| \frac{\sum_{\omega_g, \omega_t, \delta_g, \delta_t} p_{ki}}{\sum_{All} p_{ki}} \right| \quad (5)$$

where $\sum_{\omega_g, \omega_t, \delta_g, \delta_t} p_{ki}$ denotes the sum of participation factors of the mechanical state variables (ω_t , ω_g , δ_t and δ_g) of WTGs affecting mode i .

In general, if $IF_i \approx 1$, the corresponding mode is the electromechanical mode dominated by Type 4 WTGs; on the contrary, if $IF_i \ll 1$, it is a non-electromechanical mode. The performance of the new electromechanical modes participating in power oscillations can be verified by time-domain simulation and signal detection.

3. Second-Generation Generic Models of Type 4 WTGs

During 2009–2014, due to the need for generic, standard and publicly available models for variable generation technologies, WECC developed second-generation GMs for representing wind farms/WTGs. The second-generation GMs have improved the defects of first-generation GMs by controlling the structure, function, portability and other aspects. The second-generation GMs were validated through a large number of field data. This shows that the second-generation GMs can reliably describe the electromechanical time-scale dynamics of wind farms/WTGs in large-scale power systems. The submodels— $repc_a$, $reec_a$, $regc_a$ and $wtgt_a$ —are illustrated in c–f of Figure 1, respectively. I_{pcmd} and I_{qcmd} are the active and reactive current commands; U_{term} is the generator terminal voltage; U_{ref}/U_{reg} is the optional remote control bus voltage.

The second-generation GMs of Type 4 WTGs are divided into Type 4A and Type 4B models [8–15], as shown in Figure 1a,b. The Type 4A model consists of the generator/converter model ($regc_a$), electrical control model ($reec_a$), shaft model ($wtgt_a$) and plant-level controller model ($repc_a$). The Type 4B model includes all components, except for the shaft model ($wtgt_a$). When power grid faults occur, if the electromagnetic power output of the WTG involves a significant torsional oscillation, it is appropriate to use the Type 4A model; if not, then the Type 4B model is used. The Type 4A model preserves the influence of the electromechanical modes of PMSGs, while the Type 4B model neglects the influence of the electromechanical modes of PMSGs. In this study, the Type 4A model was used to study the effect of electromechanical oscillation modes of Type 4 WTGs. The details of Type 4A models can be found in [8].

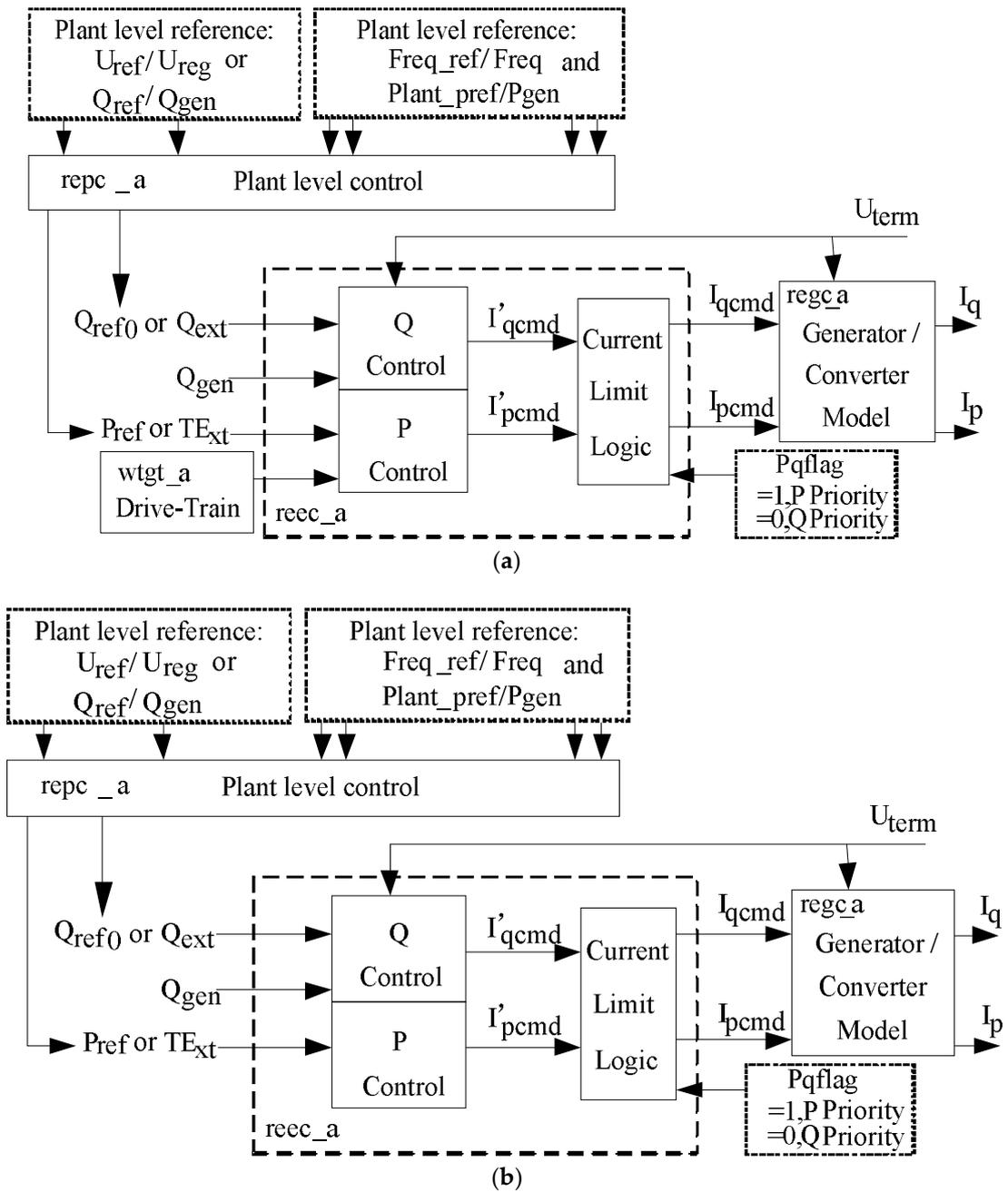


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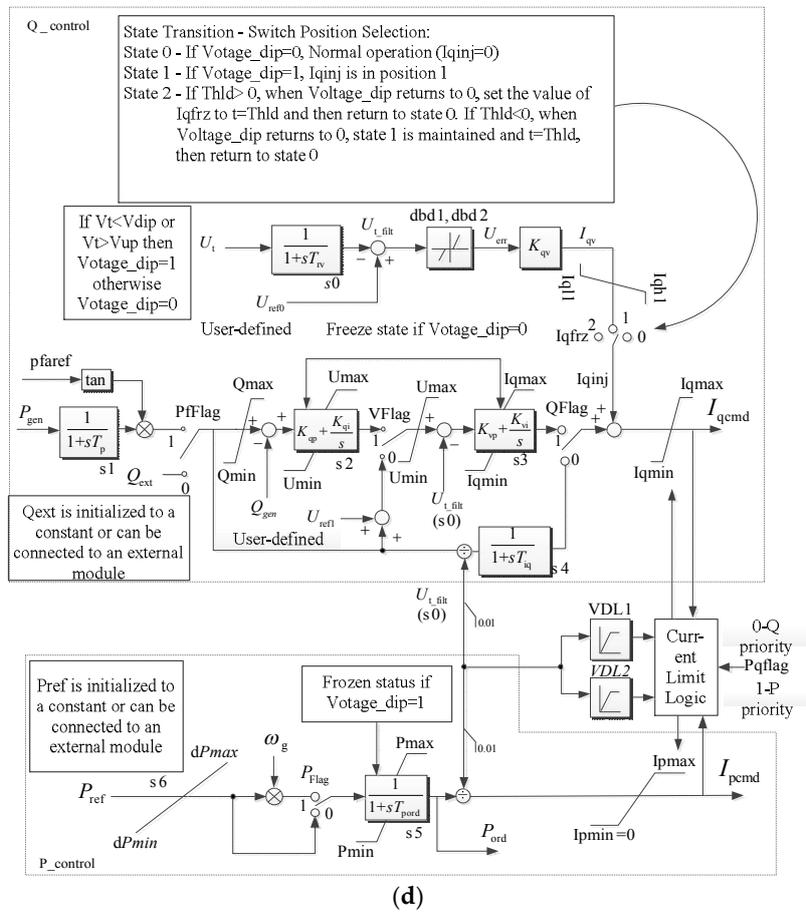
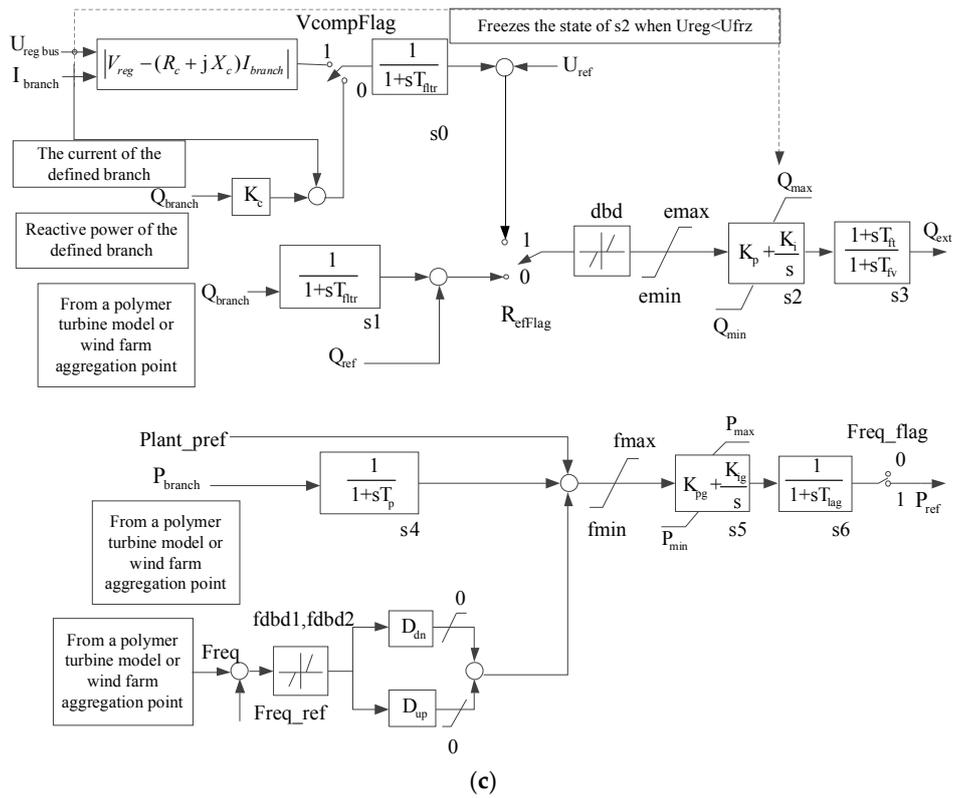


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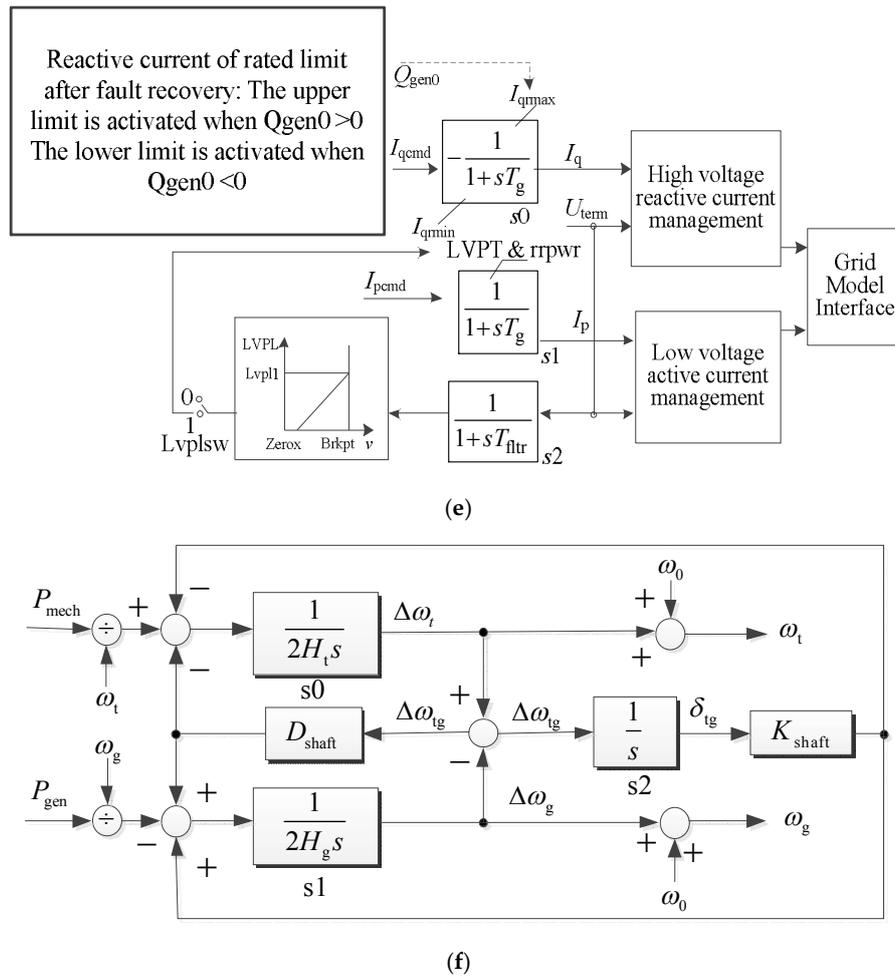


Figure 1. Second-generation generic model (GM) of Type 4 wind turbine generators (WTGs): (a) Type 4A; (b) Type 4B; (c) repc_a; (d) reec_a; (e) regc_a; (f) wtgt_a.

The flag R_{effFlag} is set in repc_a. The voltage control is implemented when $R_{\text{effFlag}} = 1$, while the constant reactive power control is realized when $R_{\text{effFlag}} = 0$.

The input of reec_a is derived from the active power reference P_{ref} and the reactive power reference Q_{ext} , both of which are obtained by the repc_a. The output of reec_a is the active current command (I_{pcmd}) and the reactive current command (I_{qcmd}), which transfer to the repc_a. The internal part of reec_a consists of three parts: active power control (generates the command I_{pcmd}), reactive power control (generates the command I_{qcmd}) and converter current limit logic, which limits the active and reactive currents to the current rating of the converter inside.

The active current command I_{pcmd} and the reactive current command I_{qcmd} are the inputs of regc_a. The outputs of the model are the active current I_p and reactive current I_q injected into the grid model. In Figure 1e, T_g represents the active and reactive current injection time constants and the T_{filt} represents the voltage filter time constant.

The submodel, wtgt_a, is a double mass model that consists of two shafts: the wind turbine shaft and the generator shaft. The symbols involved are explained as follows: H_t is the turbine inertia; H_g is the generator inertia time constant; F_{req1} is the frequency of the first torsional mode. D_{shaft} is the coefficient of the shaft mechanical damping; K_{shaft} is the shaft spring coefficient; P_{mech} is the mechanical power from the wind turbine; P_{gen} is the electromagnetic output power of the generator; ω_t and ω_g are the speeds of the LV of the wind turbine and the generator; $\Delta\omega_{\text{tg}} = \omega_t - \omega_g$; δ_t is the angle deviation of the turbine; δ_{tg} is the angle deviation of the generator and $\delta_{\text{tg}} = \delta_t - \delta_g$.

4. Simulation Analysis and Verification

The IEEE 16-machine 68-bus system [17] was adopted to implement the simulation analysis. The system consists of five areas: the New England test system (NETS), the New York power system (NYPS) and its three adjacent systems, as shown in Figure 2. Among them, the New England system (NETS) is Area 1 comprising nine generators, named G1–G9. The system power flows, SG models, their parameters and excitation systems and power system stabilizers (PSS) are described in [17].

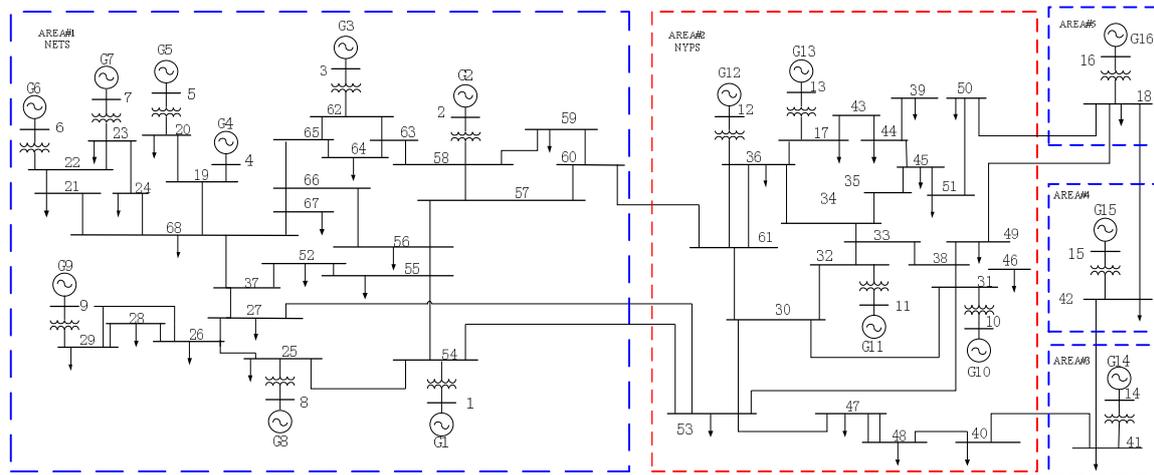


Figure 2. IEEE 16-machine 68-bus system diagram: with the increasing of wind penetration, the synchronous generators (SGs) of the New England test system (NETS) are gradually replaced by Type 4 WTGs; its behavior is similar to the 10 million megawatt cluster (TMMC).

The PSS/E was adopted to implement the simulation analysis. Fifteen electromechanical modes in the original system were identified and are listed in Table 1. Among these electromechanical modes, four interarea modes, their corresponding eigenvalues, oscillation frequencies, damping ratios and associated generators are shown in the first four lines in bold in Table 1. From Table 1, it can be observed that interarea modes are involved with several interarea SGs—their frequencies change from 0.3619 to 0.7926 Hz—but only a few local SGs participate in the other 11 local modes, with frequencies between 1.0113 and 1.7944 Hz.

Table 1. Eigenvalues of 16-machine 68-bus original system.

Mode	Eigenvalues	Frequency (Hz)	Damping Ratio	Participation Generator
1	-0.2625 ± 4.9801	0.7926	0.0526	15, 14, 16
2	-0.1878 ± 3.6787	0.5855	0.0510	13, 16, 14, 6, 12,
3	-0.1645 ± 3.2708	0.5206	0.0502	16, 14, 13
4	-0.0642 ± 2.2737	0.3619	0.0282	15, 14, 16, 13
5	-0.4311 ± 6.3543	1.0113	0.0677	3, 2, 6, 5, 7, 4
6	-0.1499 ± 6.6674	1.0612	0.0225	9, 3, 8
7	-0.4443 ± 6.9603	1.1078	0.0637	12, 13
8	-0.5850 ± 7.0540	1.1227	0.0826	5, 6, 7, 4
9	-0.2895 ± 7.7299	1.2303	0.0374	10, 9, 1, 8, 12
10	-0.6337 ± 7.8369	1.2473	0.0806	2, 3
11	-0.3960 ± 8.1306	1.2940	0.0487	10, 1, 8, 9
12	-0.9023 ± 9.0836	1.4457	0.0989	7, 6
13	-0.7164 ± 9.2516	1.4724	0.0772	8, 1
14	-0.9341 ± 9.5130	1.5140	0.0977	4, 5
15	-0.7562 ± 11.2750	1.7944	0.0669	11, 10

4.1. Impact of the Increasing Penetration Levels of Type 4 WTGs on Traditional Interarea Modes

The capacities of generators G1–G9 in the NETS area of the system are 250, 545, 650, 632, 505, 700, 560, 540, 800 MW. To study the impact of the Type 4 WTG-based TMMC on the small-signal performance of power systems, the synchronous generators, G9–G2, in the NETS area are gradually replaced by the equivalent Type 4 WTGs. The eight penetration levels in the NETS area change from 15.44% to 95.18%. The details of the eight penetration levels and the replaced synchronous generators are shown in Table 2. When the largest WTG penetration level of the NETS area is 95.18%, the penetration level of the whole system is 27.7%. In this case, the NETS area is analogous to a Type 4 WTG-based TMMC.

Table 2. Replaced units and corresponding penetration levels in the New England test system (NETS) area.

Penetration Levels	15.44%	25.86%	36.67%	50.17%	59.92%	72.12%	84.66%	95.18%
Replaced Generators	G9	G9, G8	G9, G8, G7	G9, G8, G7, G6	G9, G8, G7, G6, G5	G9, G8, G7, G6, G5, G4	G9, G8, G7, G6, G5, G4, G3	G9, G8, G7, G6, G5, G4, G3, G2

We analyzed and compared the modes for all penetration levels in Table 2. When one conventional synchronous generator is replaced by one Type 4 equivalent WTG, a pair of electromechanical modes relating to the conventional synchronous generator disappears. Moreover, a pair of new electromechanical modes relating to Type 4 WTGs appears. Four interarea modes are still available despite replacement of some conventional synchronous generators in the NETS area, but their damping ratios and frequencies change with increasing penetration levels.

Figure 3 shows that the damping ratios of the four interarea modes vary as the penetration level of Type 4 WTGs in the TMMC increases. It can be observed from Figure 3 that the damping ratio of Mode 1 is generally constant before the penetration level reaching 72.12%, and then it fluctuates with the penetration level increasing in the TMMC. The damping ratio of Mode 2 increases with the increase of the WTG penetration level. However, when the WTG penetration level increases to 84.66%, the damping ratio of Mode 2 begins to decrease. The damping ratios of Modes 3 and 4 fluctuate as the WTG penetration level increases. A high Type 4 WTG penetration level may cause Modes 3 and 4 to become unstable. It can be observed from Figure 3 that, with the increase of the penetration level, the changed law of the damping of interarea modes is inconsistent.

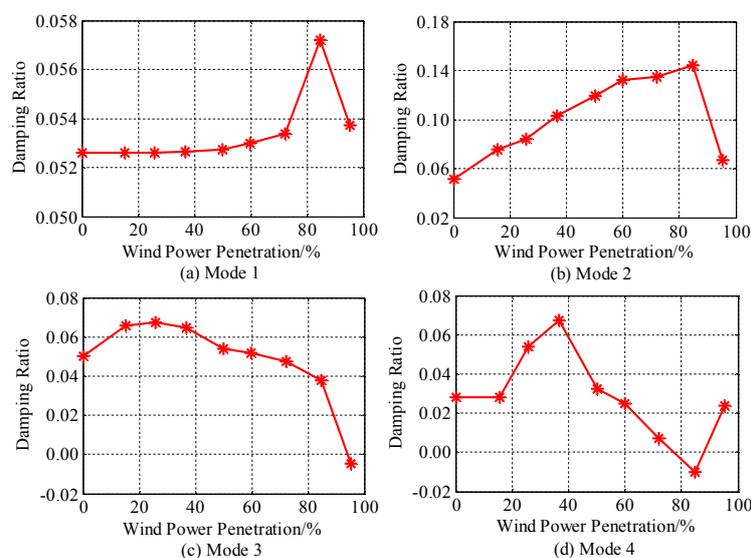


Figure 3. Damping ratios of interarea modes. (a) Mode 1; (b) Mode 2; (c) Mode 3; (d) Mode 4.

Figure 4 shows that the frequencies of interarea modes change with the increase of WTG penetration levels. The frequency of Mode 1 fluctuates with the increase of penetration levels, while the frequencies of Modes 2, 3 and 4 increase with the increase of penetration levels. The changed law of the damping of interarea modes is also inconsistent with the increase of penetration levels.

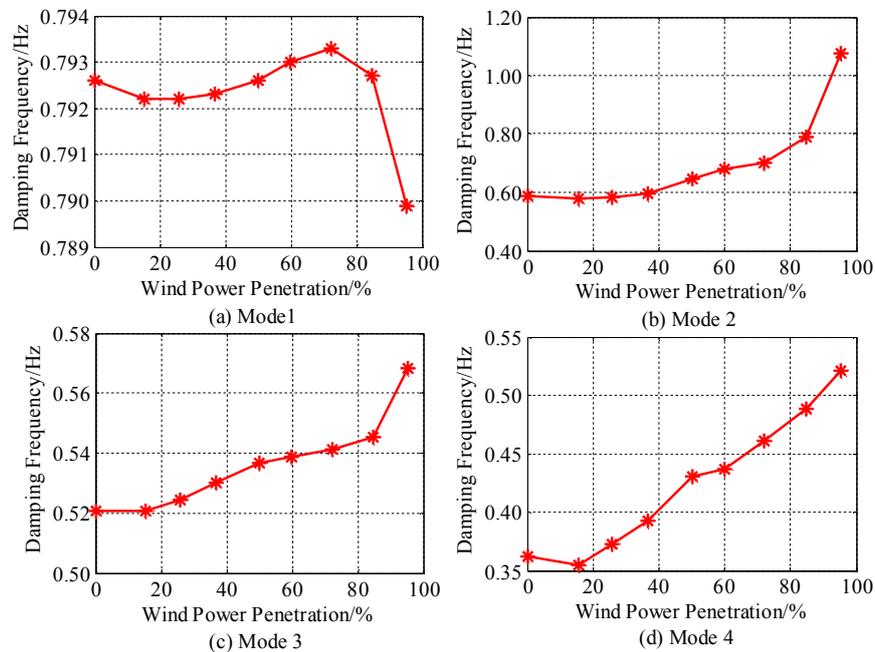


Figure 4. Frequencies of interarea modes vs. wind power penetration. (a) Mode 1; (b) Mode 2; (c) Mode 3; (d) Mode 4.

Table 3 shows that the state variables of Type 4 WTGs hardly participate in the traditional interarea electromechanical modes. Thus, there is no dynamic interaction between Type 4 WTGs and traditional interarea electromechanical modes. The impact of Type 4 WTGs on traditional interarea modes mainly depends on the system layout, the WTG penetration levels and the replaced synchronous generators, but not on the dynamic interaction of Type 4 WTGs and SGs.

Table 3. WTG participation index (PI_i) of interarea modes for the case with the penetration level 50.17% in the NETS area.

Mode #	WTG PI_i
1	0/5.428
2	0/8.239
3	0/3.2
4	0/5.55

In summary, there is no dynamic interaction between Type 4 WTGs and SGs by interarea modes. With the increase in penetration level in the NETS area, the SGs that participate in the area modes may be replaced. Thus, for each penetration level, the participation SGs are different for the area modes. This can result in an inconsistent law, where the damping ratios or frequencies of four interarea modes may increase or decrease with the increase of penetration levels. Thus, integration of Type 4 WTGs into production-level power systems may result in the increase of damping of some interarea modes, but the decrease of damping of others. It is difficult to find a law of the influence of the Type 4 WTGs on damping and frequencies of the key modes of production-level power systems.

4.2. Investigation of New Electromechanical Modes Dominated by Type 4 WTGs

As stated above, when one equivalent Type 4 WTG replaces one synchronous generator, a pair of electromechanical modes strongly relating to the synchronous generator vanishes, but a pair of new electromechanical modes strongly relating to the Type 4 WTG appears. The new type of electromechanical modes can be identified by IF_i , defined by Equation (5). Table 4 lists the new modes for each penetration level, participating WTGs in descending order of participation factors and identification factors of these new modes.

The numerators of identification factors, IF_i , are equal to their denominators in Table 4. This shows that the new electromechanical modes are dominated by the mechanical state variables of Type 4 WTGs. For each penetration level, there exists one electromechanical mode that has the lightest damping and strong interaction with most Type 4 WTGs. They are akin to the conventional interarea modes, but with frequencies higher than conventional interarea modes, here called strong-interaction modes in bold in Table 4. The other several modes are only related to a few WTGs with heavier damping, and they are akin to the conventional local modes, here called weak-interaction modes. The new electromechanical modes involving both strong- and weak-interaction modes have a weak correlation with the electrical control of full converters of Type 4 WTGs.

Table 4. New modes dominated by Type 4 WTGs for different penetration levels in the NETS area.

Penetration Levels	Eigenvalues	Damping Ratio	Frequency	Participating WTGs	IF_i
15.44%	-0.4440 ± 13.701	0.0324	2.1805	G9	1.97/1.97
25.86%	-0.4428 ± 13.702	0.0323	2.1807	G9, G8	2.1/2.1
	-0.4638 ± 13.693	0.0339	2.1793	G8	1.97/1.97
36.67%	-0.4425 ± 13.702	0.0323	2.1807	G9, G8, G7	2.1/2.1
	-0.4591 ± 13.694	0.0335	2.1795	G7	1.97/1.97
	-0.4638 ± 13.693	0.0338	2.1793	G8	1.97/1.97
50.17%	-0.4378 ± 13.706	0.0319	2.1813	G9, G7, G6	3.43/3.43
	-0.4479 ± 13.701	0.0327	2.1806	G9, G7, G6	4.63/4.63
	-0.4627 ± 13.693	0.0338	2.1793	G9, G7	3.55/3.55
	-0.4637 ± 13.693	0.0339	2.1793	G8	1.97/1.97
59.92%	-0.4374 ± 13.706	0.0319	2.1814	G9, G7, G6	3.24/3.24
	-0.4478 ± 13.701	0.0327	2.1806	G9, G7, G6	5.1/5.1
	-0.4627 ± 13.693	0.0338	2.1793	G6, G7	3.59/3.59
	-0.4636 ± 13.693	0.0338	2.1793	G8	1.97/1.97
	-0.4657 ± 13.691	0.0340	2.1791	G5	1.97/1.97
72.12%	-0.3981 ± 13.729	0.0290	2.1850	G6, G7, G9, G4, G5	6.91/6.91
	-0.4452 ± 13.701	0.0325	2.1806	G9, G7	2.19/2.19
	-0.4575 ± 13.696	0.0334	2.1798	G4, G5, G7, G6	4.4/4.4
	-0.4636 ± 13.693	0.0338	2.1793	G8	1.97/1.97
	-0.4625 ± 13.693	0.0338	2.1793	G6, G7	3.61/3.61
	-0.4641 ± 13.692	0.0339	2.1792	G5, G4	3.15/3.15
84.66%	-0.3601 ± 13.743	0.0262	2.1872	G7, G6, G9, G4, G5, G3	7.28/7.28
	-0.4450 ± 13.701	0.0325	2.1806	G9, G7	2.07/2.07
	-0.4571 ± 13.696	0.0334	2.1798	G4, G5, G7, G3, G6	6.06/6.06
	-0.4582 ± 13.696	0.0334	2.1797	G3, G4	2.26/2.26
	-0.4635 ± 13.693	0.0338	2.1793	G8	1.97/1.97
	-0.4624 ± 13.693	0.0337	2.1793	G6, G7	3.55/3.55
	-0.4640 ± 13.692	0.0339	2.1792	G5, G4	3.17/3.17
95.18%	-0.0854 ± 13.747	0.0062	2.1878	G6, G7, G9, G4, G3, G5, G2	8.53/8.53
	-0.4448 ± 13.701	0.0324	2.1806	G9	1.97/1.97
	-0.4510 ± 13.699	0.0329	2.1803	G3, G2, G7, G6	4.13/4.13
	-0.4573 ± 13.696	0.0334	2.1798	G4, G5, G7, G6	3.17/3.17
	-0.4616 ± 13.693	0.0337	2.1794	G7, G3	3.32/3.32
	-0.4635 ± 13.693	0.0338	2.1793	G8	1.97/1.97
	-0.4621 ± 13.692	0.0337	2.1792	G6, G7	3.58/3.58
	-0.4638 ± 13.692	0.0339	2.1791	G5, G4	3.17/3.17

Figure 5a,b show that the damping ratios and frequencies of the strong-interaction modes change with the increasing penetration levels. The new type of strong-interaction mode is governed by most Type 4 WTGs. With the increase of penetration level, the damping of the strong-interaction mode gradually decreases and finally becomes negative because the number of its participating WTGs increases. Their oscillation frequencies are higher than conventional interarea modes. The detailed performance of strong-interaction modes need to be further investigated.

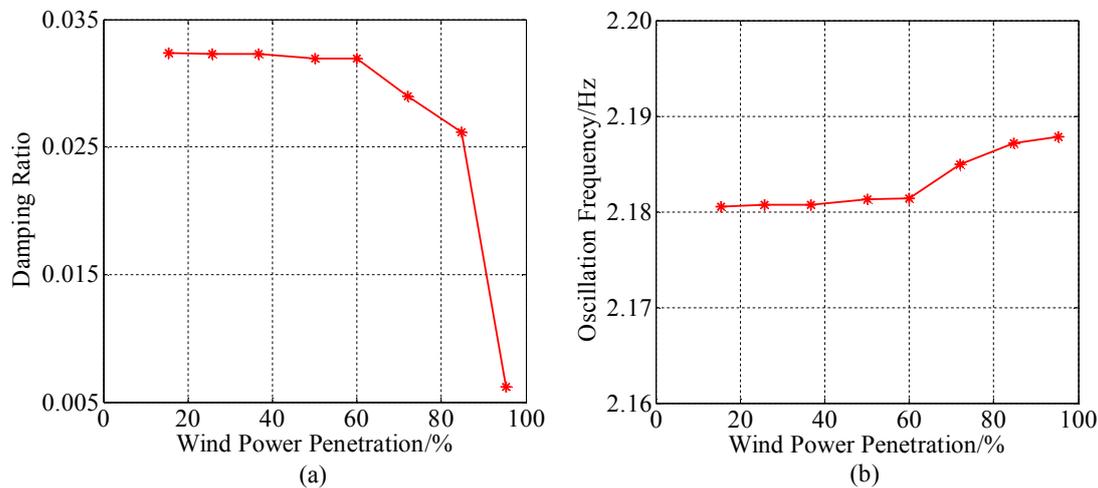


Figure 5. Damping ratio and frequency of the strong-interaction mode vs. wind power penetration. (a) the damping ratios of the strong-interaction modes; (b) the frequencies of the strong-interaction modes.

For the wind power penetration level 50.17%, at which G6–G9 are replaced, Table 5 shows the first participation factors larger than 0.1, the corresponding participating WTGs and variables for the strong-interaction mode. It can be seen from Table 5 that the strong-interaction mode strongly relates to equivalent WTGs—G9, G7 and G6. It is also observed from the first larger participation factors that the strong-interaction mode closely relates to δ_t and ω_g of Type 4 WTGs. Therefore, the strong-interaction modes dominated by Type 4 WTGs result from a strong interaction between the power angle and speed of the Type 4 WTGs.

Table 5. Participating WTGs and state variables of the strong-interaction mode for the penetration level 50.17% in the NETS area.

Participation Factor	Generator	Module	Related State Variables
1.00000	G9	wtgt_a	The twist angle of the shaft (δ_t)
0.97162	G9	wtgt_a	Generator speed deviation ($\Delta\omega_g$)
0.40640	G7	wtgt_a	The twist angle of the shaft (δ_t)
0.39469	G7	wtgt_a	Generator speed deviation ($\Delta\omega_g$)
0.33489	G6	wtgt_a	The twist angle of the shaft (δ_t)
0.32535	G6	wtgt_a	Generator speed deviation ($\Delta\omega_g$)

For the wind power penetration level of 50.17%, a three-phase short-circuit fault was applied to bus 49 for a duration period of 0.01 s and then cleared. The power oscillation curves of the related generators and the tie line for 15 s are shown in Figures 6 and 7. Figure 6 shows the active power and reactive power curves of the WTGs G9 and G7. Figure 7 illustrates the active power curves of the interarea tie lines 27–53 and 60–61. The power oscillation curve was analyzed by using the Prony program [18,19] to identify the modes of the power oscillations.

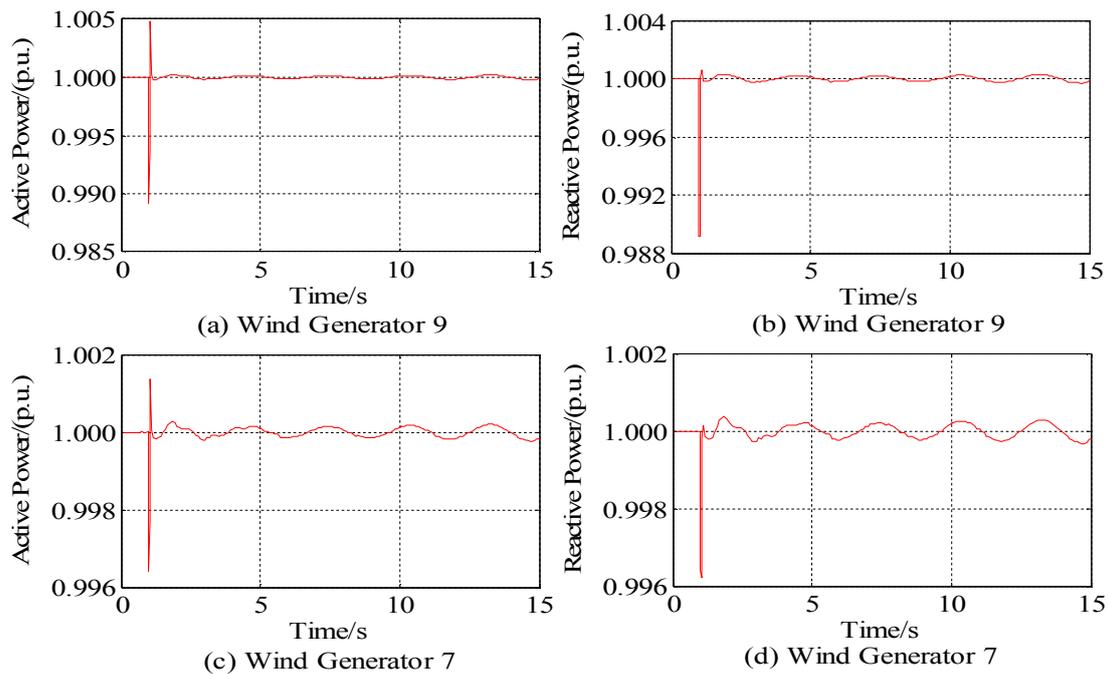


Figure 6. Power oscillation of WTGs G9 and G7 under the penetration level of 50.17%. (a) the active power curves of the WTGs G9; (b) the reactive power curves of the WTGs G9; (c) the active power curves of the WTGs G7; (d) the reactive power curves of the WTGs G7.

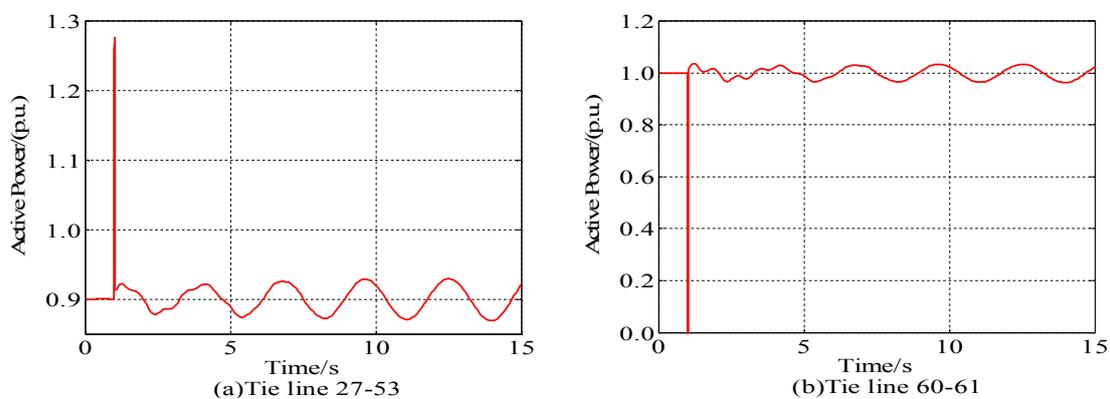


Figure 7. Power curve of tie lines for 27–53 and 60–61 under 50.17% wind power penetration. (a) the active power curves of the interarea tie lines 27–53; (b) the active power curves of the interarea tie lines 60–61.

Table 6 shows the Prony analysis results of the power oscillations of Type 4 equivalent WTGs and the interarea tie line. It can be also observed from Table 6 that two oscillation components appear in power oscillations of WTGs and tie lines 27–53, 54–53, 60–61. One oscillation component of about 0.34 Hz is the conventional interarea electromechanical Mode 4. Another oscillation component of about 2.183 Hz is the strong- or weak- interaction mode of the Type 4 WTGs in Table 5. These results show that the new electromechanical modes dominated by WTGs are similar to the traditional electromechanical modes dominated by SGs. They can result in widely spread power oscillations into the grid through the full converter.

In the traditional power system, its power oscillation propagates from the electromechanical modes dominated by SGs. However, according to the above small-signal analysis and signal detection of the time-domain simulation, the new electromechanical modes dominated by the

mechanical dynamics of Type 4 WTGs may cause widely spread power oscillations in power systems. The characteristics of these new electromechanical modes are akin to the traditional electromechanical modes dominated by SGs. Moreover, according to the analysis results of Figure 5, with the increase of WTG penetration level, the strong interaction between Type 4 WTGs can result in instability of strong-interaction modes dominated Type 4 WTGs, which was not involved in any previous theoretical analysis. Previous theoretical analysis usually believed that Type 4 WTGs are isolated from the grid through the electronic converters and that their electromechanical dynamics are decoupled from power systems. However, the above analysis in this paper presents a different result.

Table 6. Results of Prony analysis under the case with the penetration level 50.17%.

Measured Power	Main Modes	Frequency	Damping Ratio
Active power of G9	-0.0250 ± 2.1603	0.344	0.0116
	-0.0520 ± 13.8788	2.210	0.0037
Reactive power of G9	0.0230 ± 2.1164	0.337	-0.0109
	-2.6000 ± 13.2508	2.110	0.1925
Active power of G8	0.0240 ± 2.1478	0.342	-0.0112
	-0.0560 ± 13.6276	2.170	0.0041
Reactive power of G8	-0.0320 ± 2.1352	0.340	0.0150
	-6.1000 ± 13.0624	2.080	0.4231
Active power of G7	0.0620 ± 2.1540	0.343	-0.0288
	-0.6000 ± 13.5648	2.160	0.0442
Reactive power of G7	0.0290 ± 2.1415	0.341	-0.0135
	-0.0350 ± 14.9464	2.380	0.0023
Active power of G6	0.0320 ± 2.1415	0.341	-0.0149
	-1.2000 ± 14.8836	2.370	0.0804
Reactive power of G6	0.0490 ± 2.1917	0.349	-0.0224
	-3.0000 ± 13.502	2.150	0.2169
Active power of tie line 27–53	0.0100 ± 2.1729	0.346	-0.0046
	-1.8000 ± 13.8788	2.210	0.1286
Active power of tie line 54–53	0.0150 ± 2.1854	0.348	-0.0069
	-2.0000 ± 15.4488	2.460	0.1284
Active power of tie line 60–61	0.0230 ± 2.1603	0.344	-0.0106
	-2.1000 ± 13.7532	2.190	0.1509

5. Conclusions

Under the background that the Type 4 WTG-based TMMC has operated in the Northwest Power Grid in China, this paper analyzes the impact of the Type 4 WTG-based TMMCs on small-signal stability using the second-generation GMs of WECC. Integration of the Type 4 WTG-based TMMC into power systems not only has an important impact on the conventional electromechanical modes, but also brings in two new types of electromechanical modes related to the Type 4 WG-based TMMC. The detailed conclusions are given as follows.

(1) There is no dynamic interaction between Type 4 WTGs and SGs. Due to replacement of SGs, the increasing penetration of Type 4 wind power generators may result in stronger damping or also instability of a significant mode. There is no law for the impact of Type 4 WTGs replacing SGs on traditional electromechanical modes.

(2) Although the PMSGs of the Type 4 WTGs are isolated from the grid by their grid-connected converters, one new type of electromechanical mode, strongly dominated by the mechanical states of Type 4 WTGs, is introduced into power systems. The new type of mode is strongly determined by the rotor angle and velocity of the Type 4 WTGs. It can be divided into strong-interaction modes and

weak-interaction modes. Multiple equivalent Type 4 WTGs participate in the strong-interaction modes. Also, the strong-interaction modes may lose stability with the increase of penetration. Thus, the strong-interaction modes of Type 4 WTGs have significant impact on the operation security of power systems.

The performance of the new electromechanical modes dominated by Type 4 WTGs need to be further investigated.

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Nomenclature

WTG	Wind turbine generator
TMMC	Ten million megawatt cluster
GM	Generic model
WECC	Western Electricity Coordinating Council
IF	Identification factor
regc_a	Generator/converter model
reec_a	Electrical control model
wtgt_a	Shaft model of wind turbine generator
repc_a	Plant-level controller model
SG	Synchronous generator
AC	Alternative current
PI	Participation index
PMSG	Permanent magnet synchronous generators
NETS	New England test system
NYPS	New York power system
PSS	Power system stabilizer

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