

Combination of Compensations and Multi-Parameter Coil for Efficiency Optimization of Inductive Power Transfer System

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Abstract: A loosely coupled inductive power transfer (IPT) system for industrial track applications has been researched in this paper. The IPT converter using primary Inductor-Capacitor-Inductor (LCL) network and secondary parallel-compensations is analyzed combined coil design for optimal operating efficiency. Accurate mathematical analytical model and expressions of self-inductance and mutual inductance are proposed to achieve coil parameters. Furthermore, the optimization process is performed combined with the proposed resonant compensations and coil parameters. The results are evaluated and discussed using finite element analysis (FEA). Finally, an experimental prototype is constructed to verify the proposed approach and the experimental results show that the optimization can be better applied to industrial track distributed IPT system.

Keywords: inductive power transfer system; efficiency optimization; coil design; pickup coil

1. Introduction

Inductive power transfer (IPT) is the process of transferring power without wired interconnects. With an extra degree of freedom on electrical isolation and the absence of mechanical contact between the power supply side and the load, the IPT system has the advantages of low maintenance cost, high reliability, and the ability to operate in rugged environment [1–3].

A typical distributed IPT system is presented in Figure 1, which has been used in automotive industry for materials handling applications [4–6]. The primary magnetic structure is an elongated track loop carrying an AC current. And one or more Rail Guide Vehicles (RGV) with pickup coils are powered as they drive on the track and this is called on-line dynamic powering.

On-line dynamic powering is a promising technology that can help promote the adoption in variety of industrial applications [7,8]. But this mode have reduced coupling and are not as efficient as stationary powering [9,10]. Therefore, appropriate circuit design and coil design can ensure the desirable power demands.

A number of IPT power supply have been developed in previous studies. An LCL fixed-frequency resonant topology has been proven to be suitable for supplying a steady-state track current [11–14]. And series- and parallel-compensations has been carried out to circumvent low power transfer [15–18]. However, these compensations are often studied under some isolated constraints for optimal system efficiency and less consideration of the effect of pickup coil parameters on the system.

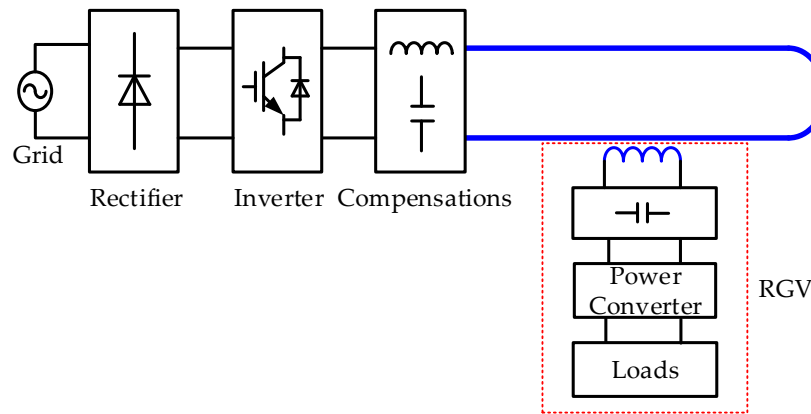


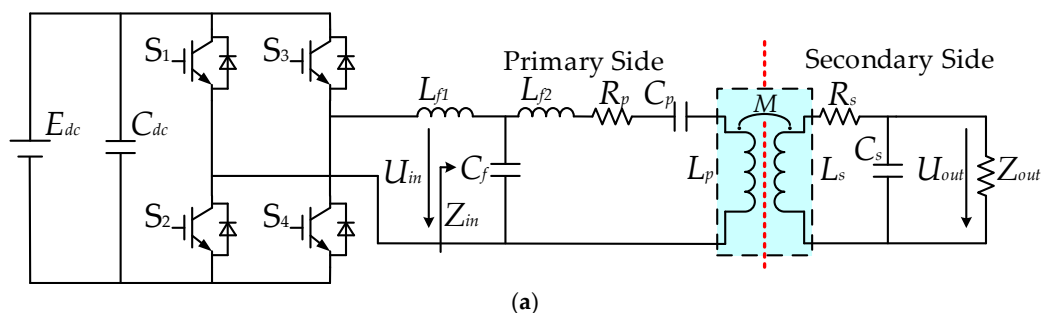
Figure 1. Industrial Rail Guide Vehicles (RGV) inductive power transfer system.

Secondary pickup coil design is also an important factor for improving system efficiency. Recent studies have analyzed the magnetic field characteristics and power transmission effect of different shapes of pickup coils, such as round, rectangular, double D type [19–22]. In loosely coupled IPT system, self-inductance and mutual inductance are more important parameters for coil design. The mathematical method has been present in some applications, which both the primary transmitting coil and secondary receiving coil are charge pads with multiple windings [23–25]. Less mathematical analysis was carried out for distributed IPT systems shown in Figure 1. This paper attempts to propose a coil analytical model and accurate expressions of self-inductance and mutual inductance for optimizing the system efficiency.

In this paper, a detailed analysis is proposed for combination of compensation network and coil design to achieve an optimal operating efficiency. And accurate coil analytical model and expressions of self-inductance and mutual inductance for the system are present in details. Consequently, optimization results are given by theoretical analysis and finite element analysis. The remainder of the paper is organized as follows. Section 2 presents the principle of LCL fixed-frequency resonant topology of the IPT system. And the influencing factors on the output efficiency are analyzed in details. Section 3 presents an analytical approach for accurate computing the self-inductance and mutual inductance between the track and pickup coils. Section 4 presents analysis results of multi-parameter coupling coil and the results are evaluated and discussed using finite element analysis. Finally, Section 5 presents the experimental results.

2. Efficiency Influencing Factors of IPT System

The topology of the IPT system is given in Figure 2. The phase-shifted pulse-width modulated full-bridge topology with Inductor-Capacitor-Inductor (LCL) network in Figure 2a is adopted at the primary side, and the LC parallel resonance circuit is adapted to at the secondary side. The switching signals, control signals, and electrical waveforms are shown in Figure 2b.



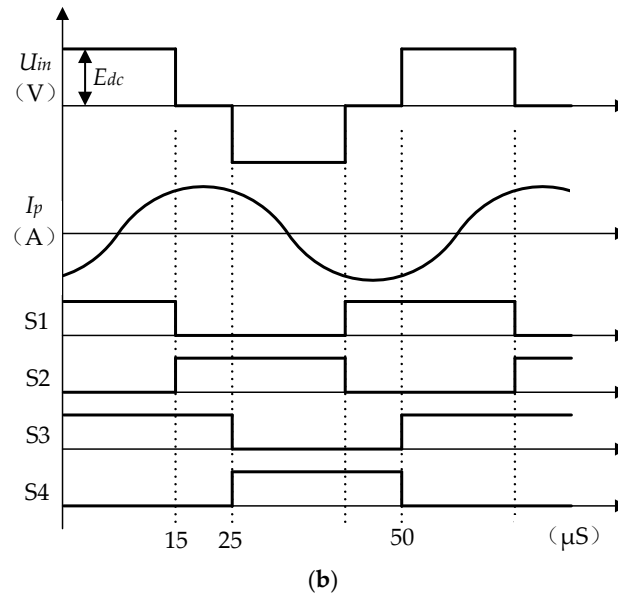


Figure 2. Topology of the inductive power transfer (IPT) system. (a) Power converter schematic of IPT system; (b) Switching signals, control signals, and electrical waveforms.

In the LCL resonant network, L_{f1} is the inductance at the inverter side, L_{f2} is the inductance at the track side, C_f is the resonant capacitance at the primary side. The parasitic resistances of the resonant components are assumed to be small and are therefore neglected. L_{f1} and C_f are tuned for operating at the switching frequency ω of the system. When the DC bus voltage E_{dc} keeps invariant, the track current I_p at the primary side is given by

$$I_p = \frac{U_{in}}{\omega L_{f2}} \quad (1)$$

U_{in} is the output voltage of the inverter bridge. From Equation (1), the track current I_p at the primary side can keep constant, which is independent of load, and the inverter only supplies the real power required by the load and any losses in the resonant tank.

According to the resonance compensating characteristics of the IPT system, the resonance condition at the primary and secondary side of the IPT system can be obtained.

$$\begin{cases} j\omega L_{f1} = \frac{1}{j\omega C_f} \\ L_{f1} = L_{f2} \\ j\omega (L_p - M^2/L_s) = \frac{1}{j\omega C_p} \\ j\omega L_s = \frac{1}{j\omega C_s} \end{cases} \quad (2)$$

Figure 3 presents the equivalent circuit of the inductive pickup coil at the secondary side, where the LC parallel resonance circuit is adopted. For simplified analysis, the circuit can be equivalent by Thevenin and Norton's Theorem. M is the mutual inductance between the primary track and secondary coil.

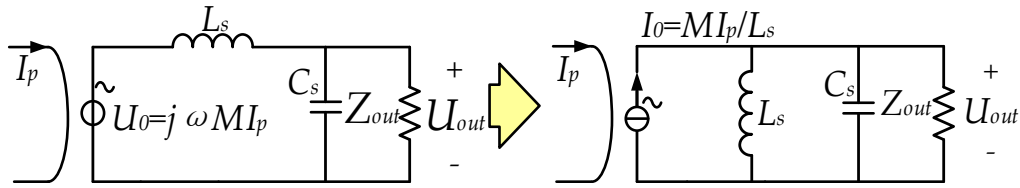


Figure 3. The equivalent circuit model at the secondary side.

Considering that the couple self-inductance L_s is larger than the internal resistance R_s of the pickup coil, the current I_s is given by

$$I_s = \frac{MI_p Z_{out}}{\omega L_s^2} \quad (3)$$

Z_{out} is the equivalent load impedance. According to the impedance analysis and the circuit theory, the power output P_{out} of the IPT system can be obtained.

$$P_{out} = \frac{M^2 U_{in}^2 Z_{out}}{L_{f1}^2 L_s^2 \omega^2} \quad (4)$$

Furthermore, the output efficiency can also be given as follows.

$$\eta = \frac{P_{in}}{P_{out}} = \frac{1}{1 + \frac{L_s^2 R_p}{M^2 Z_{out}}} \quad (5)$$

R_p is internal resistance of the track. When the quality factor of the parallel resonance at the secondary side is larger, R_s can not be neglected. Therefore, the output efficiency can be shown in Equation (6).

$$\eta = \frac{P_{out}}{P_{in} + I_s^2 R_s} = \frac{1}{1 + \frac{L_s^2 R_p}{M^2 Z_{out}} + \frac{R_s Z_{out}}{L_s^2 \omega^2}} \quad (6)$$

From Equation (6), the higher output efficiency η can be obtained when R_p , R_s are smaller in the system. Moreover, η is becoming higher with the increase of ω and M . However, the switching frequency is limited to 20–50 kHz, because ω is limited by the power grade and switching devices in medium or large frequency system.

Furthermore, in order to obtain the optimal output efficiency, Equation (6) is derivative and the optimization condition is given by.

$$\frac{L_s^2}{Z_{out}} = \sqrt{\frac{M^2 R_s}{\omega^2 R_p}} \quad (7)$$

It is clear that the optimal output efficiency η of the IPT system can be obtained only if Equation (7) can be established.

From Equations (6) and (7), the optimal output efficiency η is affected by M , L_s and R_s when other parameters of the IPT system at the primary side are fixed. And the output efficiency of the IPT system is shown in Figure 4.

M , L_s and R_s have a direct relation with coil design. Therefore, a proper analytical approach of coil design should be employed.

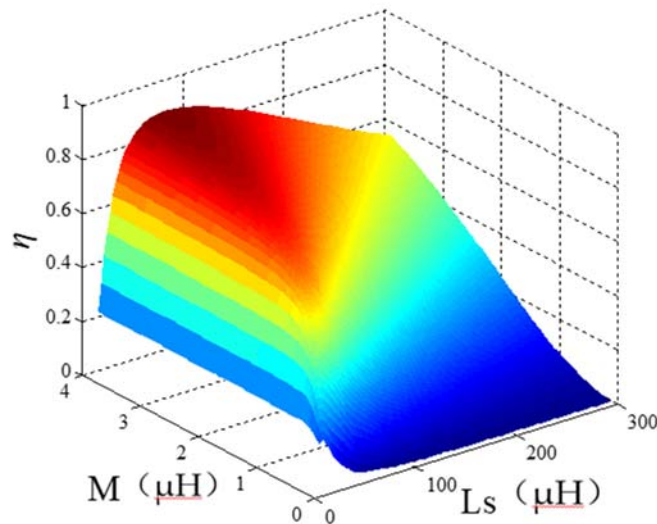


Figure 4. Output efficiency with M and L_s .

3. Accurate Computation of Coil Parameters

In this section, an analytical approach and mathematical expression is present for computing the self-inductance and mutual inductance between the track and pick-up coils. A rectangular plane coil model is shown in Figure 5 according to engineering requirements for RGV application.

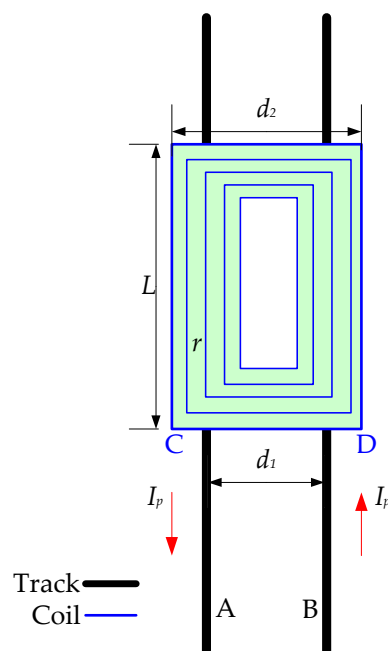


Figure 5. Magnetic field coupling model for RGV application.

3.1. Calculation of Self-Inductance

Figure 6 shows the equivalent plane diagram of the coil and the track. Magnetic flux density $B_{(x,y)}$ at any point of the rectangular coil can be given by applying Biot–Savart law.

$$B_{(x,y)} = \frac{\mu_0}{4\pi} \left[\frac{\frac{L}{2} + y}{x \sqrt{\left(\frac{L}{2} + y\right)^2 + x^2}} + \frac{\frac{L}{2} - y}{x \sqrt{\left(\frac{L}{2} - y\right)^2 + x^2}} \right] \quad (8)$$

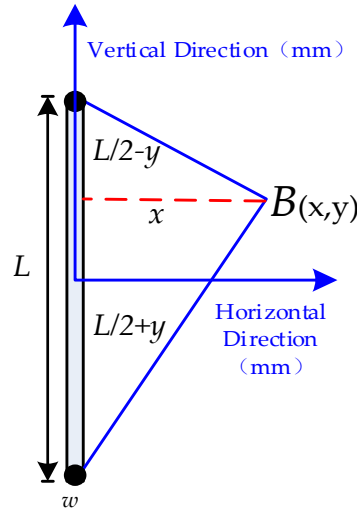


Figure 6. Equivalent diagram of the coil and track.

The length, width and wire diameter of the coil is L , d_2 and w respectively. Where the y -axis is in the direction of the track and the x -axis is perpendicular to the track direction.

When the current flows on one of the long side L of the rectangular coil, the magnetic flux ϕ_{11L} in the rectangular region is given by

$$\phi_{11L} = \int_{\frac{w}{2}}^{d_2 - \frac{w}{2}} \int_{\frac{L}{2} - \frac{w}{2}}^{\frac{L}{2} + \frac{w}{2}} B_{(x,y)} dy dx \quad (9)$$

Similarly, when the current flows the width side d_2 of the rectangular coil, the magnetic flux ϕ_{12d_2} in the rectangular area is given by

$$\phi_{12d_2} = \int_{\frac{L}{2} - \frac{w}{2}}^{\frac{L}{2} + \frac{w}{2}} \int_{\frac{w}{2}}^{d_2 - \frac{w}{2}} B_{(x,y)} dy dx \quad (10)$$

So the total magnetic flux of rectangular coil can be obtained.

$$\phi = 2(\phi_{11L} + \phi_{12d_2}) \quad (11)$$

The winding gap of the coil is r . From Figure 4, the j -turn length is $L - 2(j-1)r$, and the width is $d_2 - 2(j-1)r$. The track current I_P flowing each turn is the same. Therefore, the self-inductance L_{jj} of the j -th coil can be calculated from the magnetic flux passing through the j -th turn, and the mutual inductance L_{jk} among the winding turns is calculated by the magnetic flux of the k -th turn, where $L_{kj} = L_{jk}$. Therefore, the mutual inductance between the j -th and k -th turns is given by

$$L_{jk} = \frac{\phi_{jk}}{I_p} = \mu \frac{2}{\pi} \left\{ \sqrt{F^2 + G^2} - \sqrt{F^2 + K^2} - \sqrt{G^2 + K^2} + \sqrt{2}K + \right. \\ \left. \frac{F}{2} \ln \left[\left(\frac{F + \sqrt{F^2 + K^2}}{F + \sqrt{F^2 + G^2}} \right) \left(\frac{G}{K} \right) \right] + \frac{G}{2} \ln \left[\left(\frac{G + \sqrt{G^2 + K^2}}{G + \sqrt{F^2 + G^2}} \right) \left(\frac{F}{K} \right) \right] \right. \\ \left. + \frac{K}{2} \ln \left[\frac{(K + \sqrt{F^2 + K^2})(K + \sqrt{G^2 + K^2})}{FG(1 + \sqrt{2})^2} \right] \right\} \quad (12)$$

where $F = L(1 - \frac{w}{2L}) - (j+k-2)r$, $G = d_2(1 - \frac{w}{2d_2}) - (j+k-2)r$, $K = \frac{w}{2} - (j-k)r$.

When $j = k$, the inductance of the coil is the sum of self inductance and the inductance of the multi-turn winding. Therefore, the self-inductance L_s of N turn rectangle coil can be expressed as:

$$L_s = \sum_{j=1}^N \left(L_{jj} + 2 \sum_{\substack{k=j+1 \\ k \leq N}}^N L_{jk} \right) \quad (13)$$

3.2. Accurate Computation of Mutual Inductance

As shown in Figure 4, the flux linkage of the N turn coil is the sum of the flux generated by the track. The vertical surface equivalent diagram between the track and the coil is shown in Figure 7. d_1 is the track spacing. h is the distance between the coil and the track.

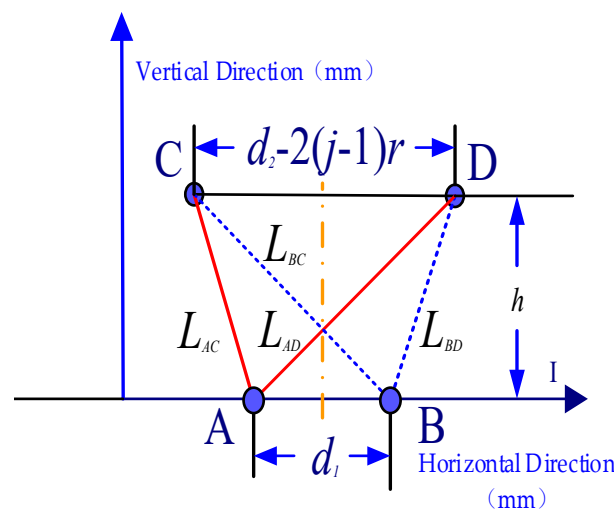


Figure 7. Vertical equivalent diagram between the track and the coil.

The magnetic flux produced by track A through the j -th coil area is given by

$$\phi_{21A} = \int_0^{L-2(j-1)r} dz \int_{L_{AC}}^{L_{AD}} \frac{\mu_0 I}{2\pi \rho} d\rho = \frac{\mu_0 I (L - 2(j-1)r)}{2\pi} \ln \frac{L_{AD}}{L_{AC}} \quad (14)$$

And the magnetic flux produced by track B through the j -th coil is given by

$$\phi_{21B} = - \frac{\mu_0 I (L - 2(j-1)r)}{2\pi} \ln \frac{L_{BD}}{L_{BC}} \quad (15)$$

where $L_{AC}^2 = h^2 + (\frac{d_2 - 2(j-1)r - d_1}{2})^2$, $L_{AD}^2 = h^2 + (\frac{d_1 + d_2 - 2(j-1)r}{2})^2$.

The magnetic flux through the j -th turn is:

$$\begin{aligned}\phi_{21} = \phi_{21A} + \phi_{21B} &= \frac{\mu_0 I (L - 2(j-1)r)}{2\pi} \ln \frac{L_{AD} L_{BC}}{L_{AC} L_{BD}} = \frac{\mu_0 I (L - 2(j-1)r)}{\pi} \ln \frac{L_{AD}}{L_{AC}} \\ &= \frac{\mu_0 I (L - 2(j-1)r)}{2\pi} \ln \frac{h^2 + (\frac{d_1 + d_2 - 2(j-1)r}{2})^2}{h^2 + (\frac{d_2 - 2(j-1)r - d_1}{2})^2}\end{aligned}\quad (16)$$

And the magnetic flux generated by track A and B on the N turn coil is:

$$\Psi_2 = \sum_{j=1}^N \phi_{21} = \sum_{j=1}^N \left(\frac{\mu_0 I (L - 2(j-1)r)}{2\pi} \ln \frac{h^2 + (\frac{d_1 + d_2 - 2(j-1)r}{2})^2}{h^2 + (\frac{d_2 - 2(j-1)r - d_1}{2})^2} \right) \quad (17)$$

Furthermore, the mutual inductance M between the track and the N -turn rectangular coil is:

$$M = \frac{\Psi_2}{I} = \sum_{j=1}^N \left[\frac{\mu_0 (L - 2(j-1)r)}{2\pi} \ln \frac{h^2 + (\frac{d_1 + d_2 - 2(j-1)r}{2})^2}{h^2 + (\frac{d_2 - 2(j-1)r - d_1}{2})^2} \right] \quad (18)$$

3.3. Internal Resistance Calculation of Track and Coil

The internal resistance R_s of coil can be calculated as follows:

$$R_s = \rho_{cu} \frac{2N(L + d_2 - Nr)}{S_s} \quad (19)$$

ρ_{cu} is the electrical resistivity and S_s is cross-sectional area of the coil. To improve the output efficiency, R_s should be as small as possible.

4. Efficiency Optimization Analysis of the IPT System

From Section 3, it is known that mutual inductance M and self-inductance L_s are related to the geometrical structure, spatial position, turns and wingding gap of the coil. The Equation (6) shows that the efficiency is not only related to the design of coil parameters, but also the circuit structure and resonance compensations. In this section, the efficiency optimization is present based on the proposed IPT topology.

4.1. Optimization Design Process

The design flowchart of the system is presented in Figure 8.

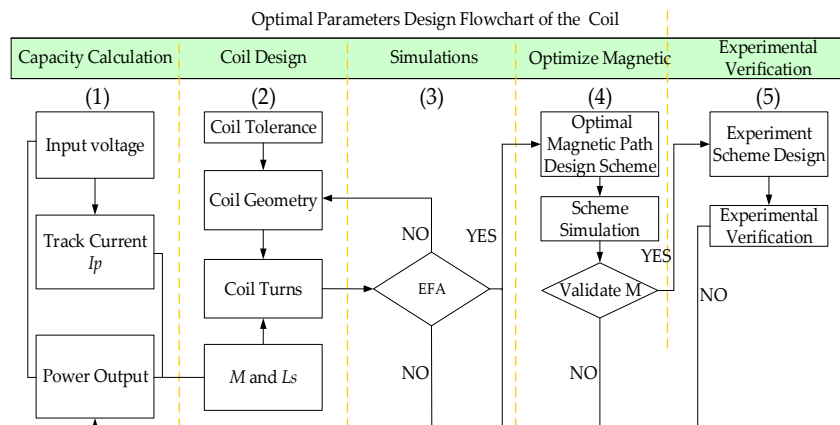


Figure 8. Design flowchart of the IPT system.

Firstly, optimization of the IPT system needs to consider the power requirements for RGV application, which determines the topology and compensations. And the coil design mainly considers the influence of coil tolerance, geometry and turns on mutual inductance and self-inductance. Furthermore the coil parameters are verified through finite element analysis for optimum efficiency. When the optimization of the coil is completed, the mutual inductance of the coil can be further improved through displacement the magnetic strip reasonably. Whether the above design meets the requirements also needs to be verified by experiments.

4.2. Optimization Analysis of Coil Parameters

To simplify the analytical calculations and to reduce the computation time, some assumptions are made based on industrial field, such as coil size and track spacing must meet the installation of RGV application. The parameters of IPT system are shown in Table 1.

Table 1. Experimental parameters of IPT system.

Parameters	Values
Switching Frequency f	20 kHz
Inductance $L_{f1} = L_{f2}$	80 μH
Resonant Capacitance C_f	0.5 μF
Self-inductance L_P	5 μH
Compensation Capacitance C_P	8 μF
Track Internal Resistance R_P	0.022 Ω
Inductive Coil Internal Resistance R_s	0.045 Ω
Output Power of pickup	400 W
output voltage of pickup	24 VDC

Combined with self-inductance calculation Equation (13) and mutual inductance calculation Equation (18), the effects of the winding gap r , the turns N to the self-inductance L_s and mutual inductance M are shown in Figure 9.

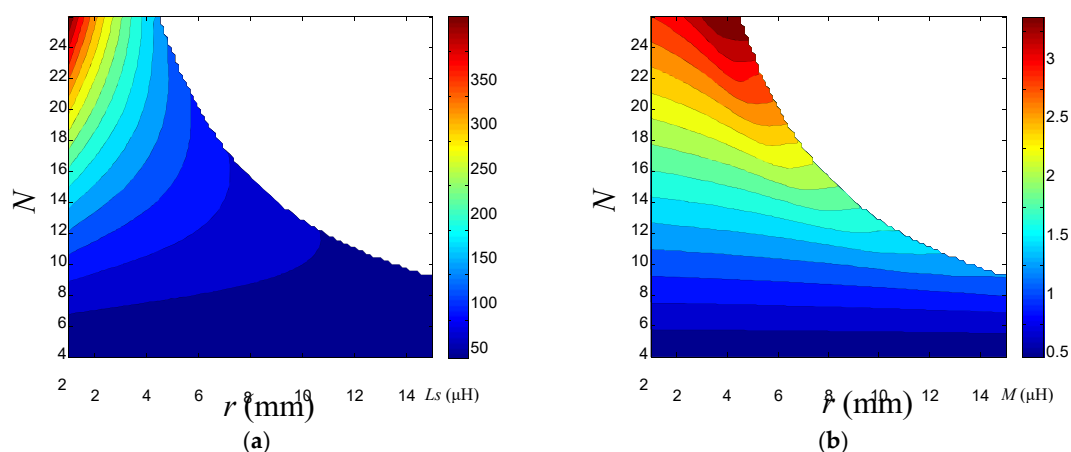


Figure 9. Calculated value of L_s and M with variable N and r . (a) N - r - L_s ; (b) N - r - M .

Furthermore, the relationship between the turns, winding gap and the output efficiency of the system is shown in Figure 10.

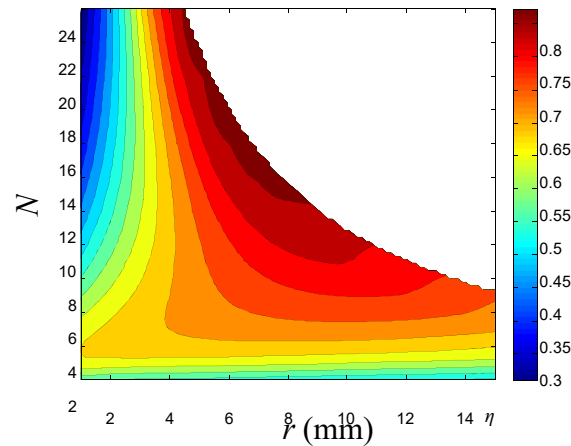


Figure 10. Output efficiency with variable N and r .

From the results in Figure 10, the optimum efficiency of the system is 81.2%. And the optimized coil parameters can be obtained as $N = 14$, $r = 7$ mm, $L_s = 61.2$ μH and $M = 1.91$ μH respectively.

The output efficiency of long-track-loop structure of on-line dynamic powering IPT system is lower than stationary system. This is because the inductance of the long track is so large that the switching frequency is usually limited to 20–50 kHz. Also the quality factor of the long loop is therefore lower than the stationary system for the effect of track internal resistance. However, flexible routing path makes the dynamic powering system suitable for industrial RGV applications.

At the same time, the output efficiency is also affected by vertical and horizontal migration. Output efficiency with misalignment is shown in Figure 11. Apparently the output efficiency decreases with the increase of migration.

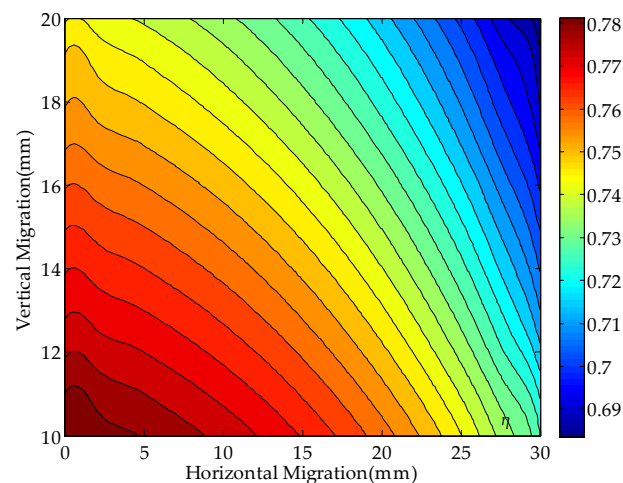


Figure 11. Output efficiency with misalignment.

4.3. Finite Element Analysis (FEA)

The 3D Maxwell finite element software is used to verify and analyze the coil parameters, so as to verify whether the coil parameters meet the optimum out efficiency.

FEA simulation model of coil is shown in Figure 12.

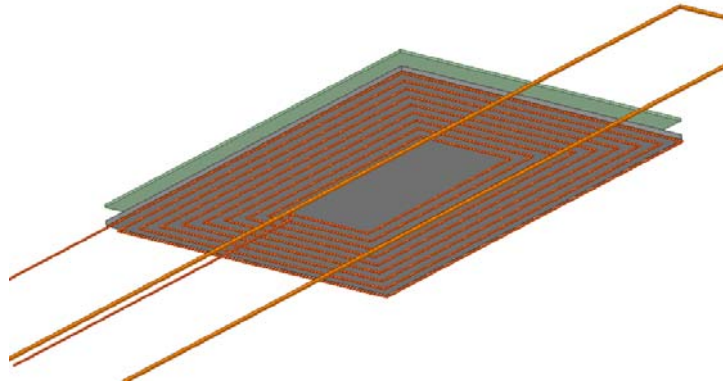


Figure 12. Finite element simulation model of coil.

The result of FEA is shown in Figure 13. It can be seen that the optimum output efficiency is basically consistent with the theoretical optimization analysis.

Proper placement of the magnetic strip over the coil can shorten the magnetic circuit, reducing the edge of the magnetic flux, thereby enhancing the mutual inductance between the track and the coil. The choices of magnetic stripe mainly consider the magnetization curve, magnetic loss, geometric size and so on.

FEA simulation model of coil with magnetic strip is shown in Figure 14. Ferrite PC40 magnetic strips are closed to the coil surface. The size of the magnetic stripe is 90 mm × 5 mm × 15 mm.

After adding the magnetic stripe, the value of M is 2.82 μH and the system optimum output efficiency can be improved as 85.6%.

Finally, the magnetic field radiation also can be evaluated with Finite Element Analysis (FEA) simulation results. The design satisfies the relevant standard of the International Commission on Non-Ionizing Radiation Protection (ICNIRP) magnetic field radiation under the actual working condition.

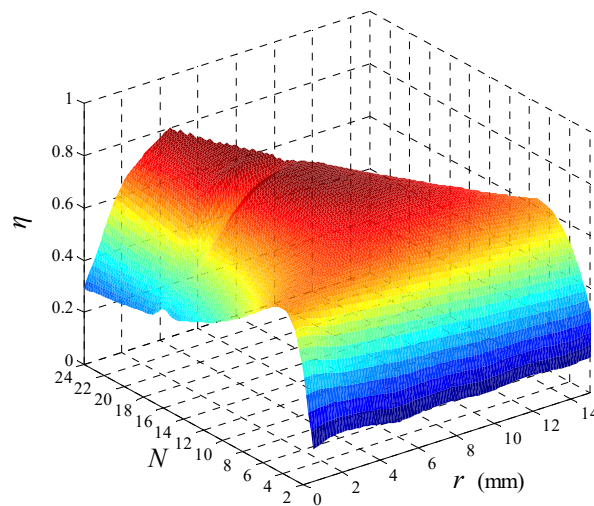


Figure 13. Results of finite element simulation.

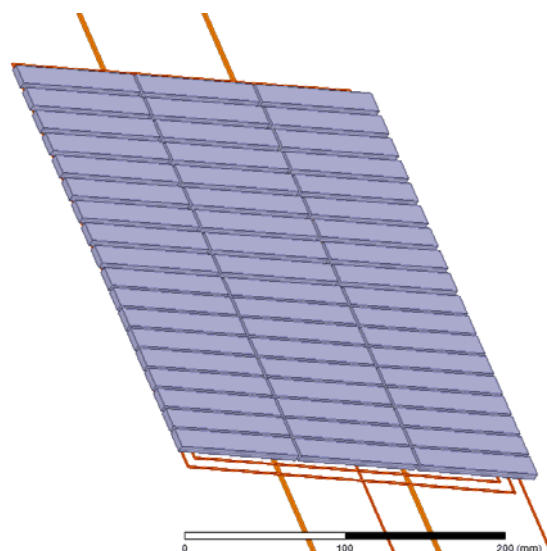


Figure 14. Model with placement of the magnetic strip.

The results with placement of the magnetic strip are shown in Figure 15.

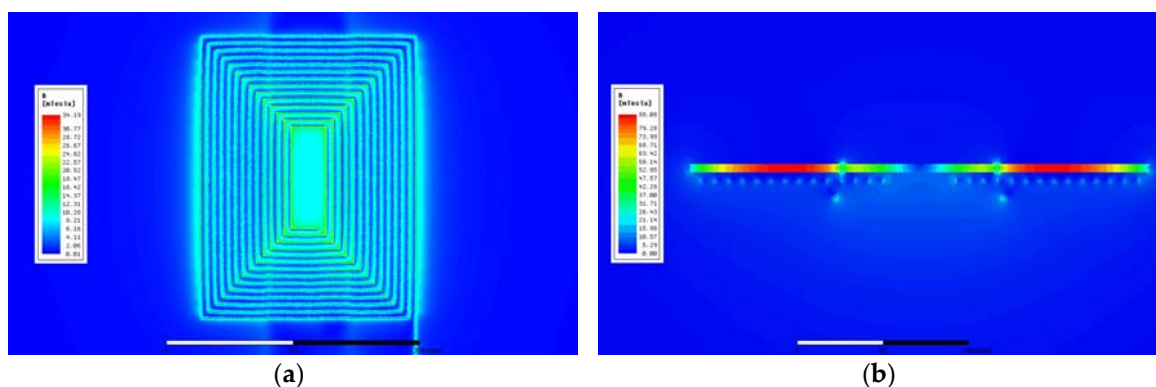


Figure 15. Finite Element Analysis (FEA) simulations with placement of the magnetic strip. (a) plan; (b) axial.

5. Experimental Results

A prototype is constructed to verify the proposed system and the experimental parameters are shown in Table 1.

IPT power supply and primary track with a RGV are shown in Figure 16.

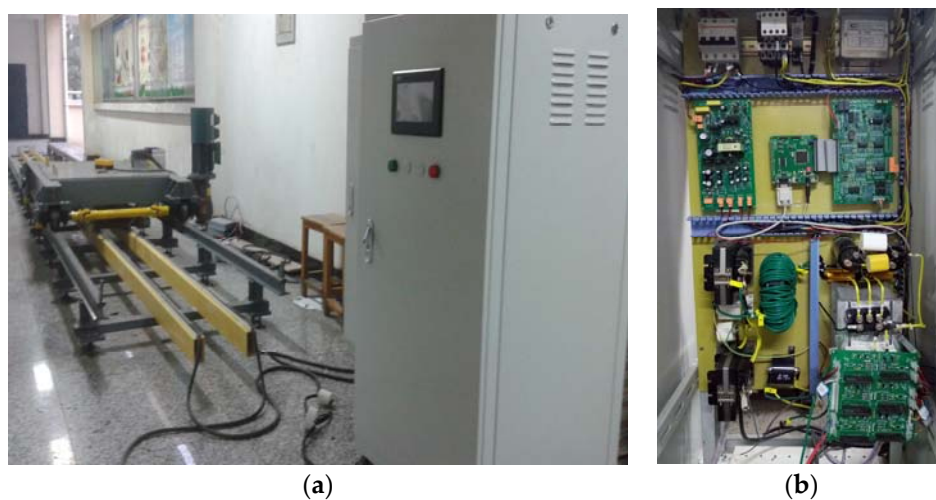


Figure 16. Experimental platform of IPT system: (a) experimental panorama of the platform; (b) the converter of the primary side.

And the structure and dimension of the pickup coil is shown in Figure 17.

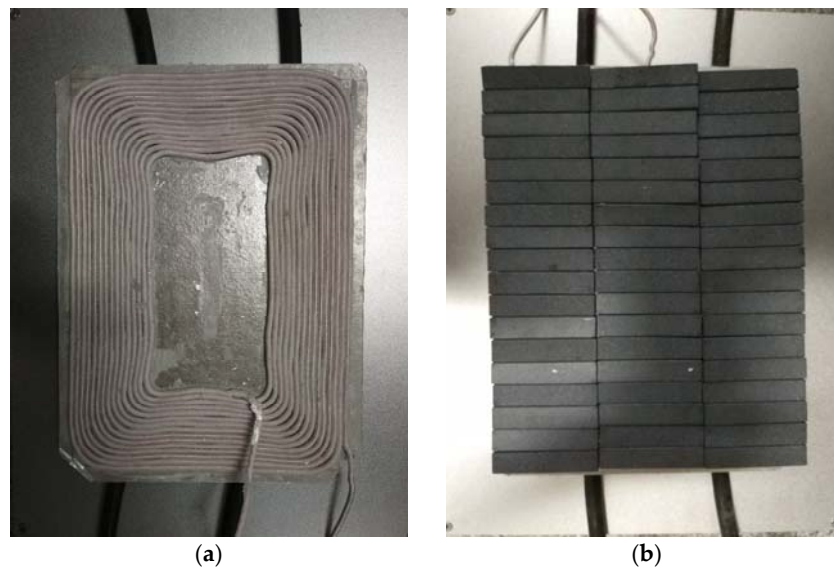
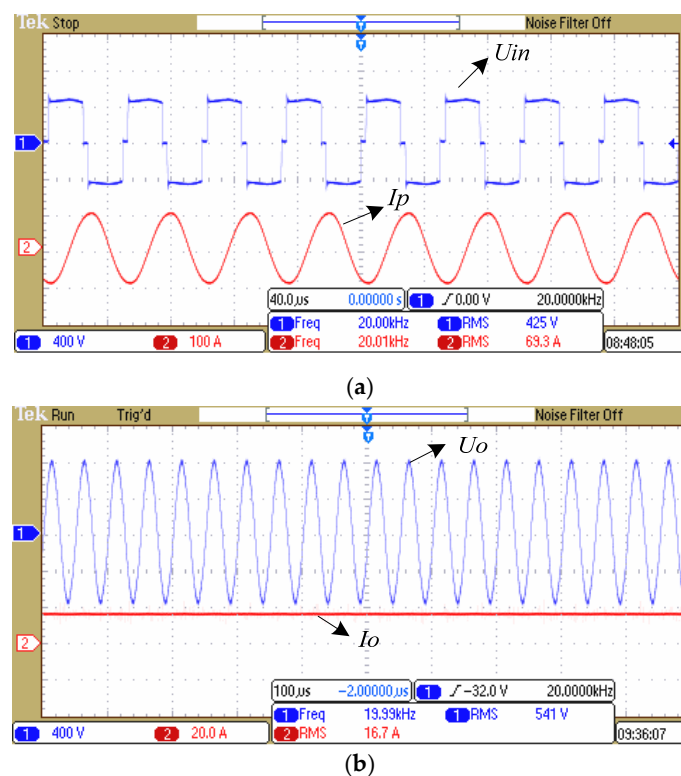


Figure 17. Pickup coil physical map. (a) couplings coil; (b) couplings coil with magnetic strips.

The experimental results of the IPT system are shown in Figure 18. In Figure 18a CH1 is the waveform of the voltage of the inverter bridge arms, and CH2 is the waveform of the track current I_p , which is an AC 20 kHz high-frequency sine wave. Similarly, resonant waveform at secondary side is presented in Figure 18b,c, where CH1 is the waveform of the LC resonant voltage at the secondary side, and CH2 is the waveform of the load current at half and full loads. A post-stage power converter is able to regulate the output AC voltage to a desired DC value. The output voltage of pickup is 24 VDC for RGV applications.



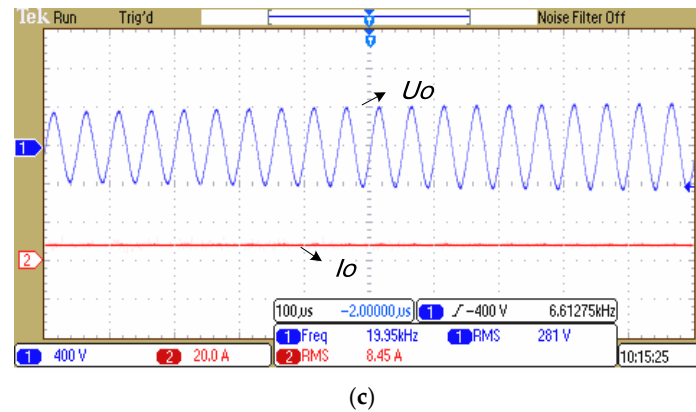


Figure 18. Experimental results of IPT system. (a) Waveform at the primary side (CH1:400 V/div, CH2:100 A/div, Time: 40 μ s/s); (b) Waveform at secondary side at full load (CH1:400 V/div, CH2:20 A/div, Time: 100 μ s/s); (c) Waveform at secondary side at half load (CH1:400 V/div, CH2:20 A/div, Time: 100 μ s/s).

Comparison of the output efficiency under different loads with the theoretical efficiency is shown in Figure 19. It is clear that the efficiency is slightly lower than the theoretical efficiency because of the effects of the circuit losses, the switching losses and the coil misalignment.

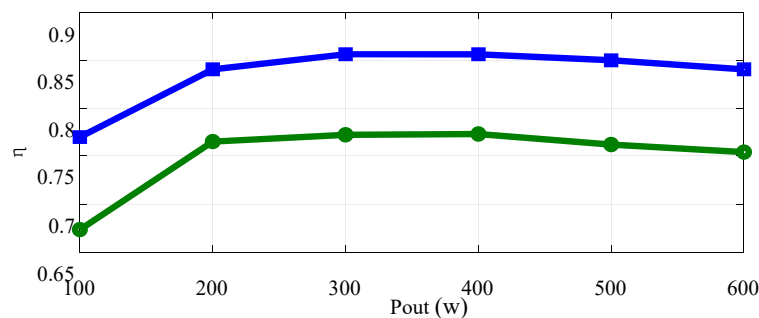


Figure 19. Output efficiency under variable loads.

6. Conclusions

In this paper, the multi-parameter optimization of an IPT system for industrial RGV application was presented. The optimal output efficiency is mainly affected by self-inductance and mutual inductance between primary track and secondary pick-up coil. Therefore, an accurate analytical method based on Biot–Savart law has been presented for estimating self-inductance and mutual inductance between the track and the coil. Furthermore, optimization for coil parameters has been present through analytical calculation and FEA simulation. The experimental results show a good agreement with analytical and FEA results.

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Conflicts of Interest: The authors declare no conflict of interest.

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