

Supplementary Materials

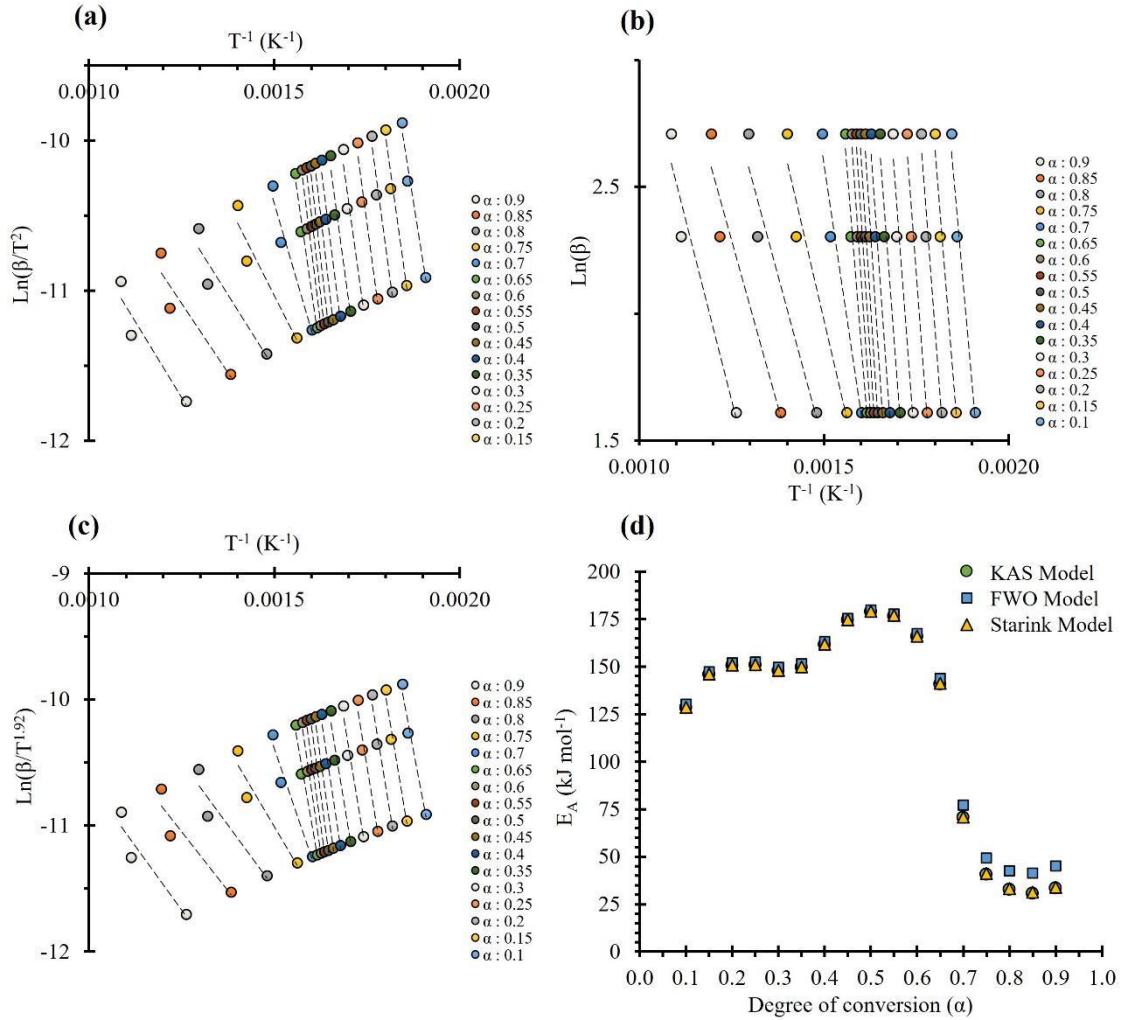


Figure S1. Linear plots of (a) KAS; (b) FWO model; (c) SK model; and (d) EA depending on the degree of conversion

Table S1.

Expressions for $f(\alpha)$ and $g(\alpha)$ functions of reaction models to describe thermal decomposition solid state reactions (Sangaré et al. and Mumbach et al.) [18, 19].

Reaction model	$f(\alpha)$	$g(\alpha)$
Reaction order models		
R1 Mampel (first order)	$1 - \alpha$	$-\ln(1 - \alpha)$
R2 Second order	$(1 - \alpha)^2$	$(1 - \alpha)^{-1} - 1$
R3 Third order	$(1 - \alpha)^3$	$0.5[(1 - \alpha)^{-2} - 1]$
R4 One and half order	$(1 - \alpha)^{3/2}$	$[(1 - \alpha)^{-1/2} - 1]$
Rn n-order reaction	$(1 - \alpha)^n$	$[1 - (1 - \alpha)^{1-n}] / (1-n)$
Diffusion models		
D1 One dimensional	$0.5 \alpha^{-1}$	α^2
D2 Two dimensional (Valensi model)	$[-\ln(1 - \alpha)]^{-1}$	$(1 - \alpha)\ln(1 - \alpha) + \alpha$
D3 Diffusion control (Jander control)	$(1 - \alpha)^{2/3} [1 - (1 - \alpha)^{1/3}]^{-1}$	$[1 - (1 - \alpha)^{1/3}]^2$
D4 Diffusion control (Ginstling model)	$(3/2) [(1 - \alpha)^{-1/3} - 1]^{-1}$	$1 - (2/3)\alpha - (1 - \alpha)^{2/3}$
Power law nucleation models		
P1 Power law	$(2/3)\alpha^{-1/2}$	$\alpha^{3/2}$
P2 Power law	$2\alpha^{1/2}$	$\alpha^{1/2}$
P3 Power law	$3\alpha^{2/3}$	$\alpha^{1/3}$
P4 Power law	$4\alpha^{3/4}$	$\alpha^{1/4}$
Random nucleation and subsequent growth models		
A1 Avarami-Erofeev	$1.5(1 - \alpha)[- \ln(1 - \alpha)]^{1/3}$	$[- \ln(1 - \alpha)]^{2/3}$
A2 Avarami-Erofeev	$2(1 - \alpha)[- \ln(1 - \alpha)]^{1/2}$	$[- \ln(1 - \alpha)]^{1/2}$
A3 Avarami-Erofeev	$3(1 - \alpha)[- \ln(1 - \alpha)]^{2/3}$	$[- \ln(1 - \alpha)]^{1/3}$
A4 Avarami-Erofeev	$4(1 - \alpha)[- \ln(1 - \alpha)]^{3/4}$	$[- \ln(1 - \alpha)]^{1/4}$
A5 Random nucleation	$(1 - \alpha)^2$	$(1 - \alpha)^{-1}$
A6 Random nucleation	$0.5(1 - \alpha)^3$	$(1 - \alpha)^2$
Geometrical contraction models		
F2 Contracting cylinder	$2(1 - \alpha)^{1/3}$	$1 - (1 - \alpha)^{1/2}$
F3 Contracting sphere	$2(1 - \alpha)^{2/3}$	$1 - (1 - \alpha)^{1/3}$

Table S2.Apparent activation energy (E_A) of pyrolysis of BCS determined by isoconversional methods.

α	KAS		FWO		SK	
	E_A (kJ/mol)	R^2	E_A (kJ/mol)	R^2	E_A (kJ/mol)	R^2
0.10	128.3	0.98	130.4	0.98	128.6	0.98
0.15	145.8	0.98	147.3	0.98	146.1	0.98
0.20	150.6	0.97	151.9	0.97	150.8	0.97
0.25	150.8	0.96	152.4	0.97	151.1	0.96
0.30	147.9	0.96	149.8	0.96	148.1	0.96
0.35	149.6	0.96	151.6	0.96	149.9	0.96
0.40	161.7	0.97	163.2	0.97	161.9	0.97
0.45	174.4	0.98	175.4	0.98	174.6	0.98
0.50	178.9	0.98	179.8	0.99	179.2	0.98
0.55	176.7	0.99	177.8	0.99	177.0	0.99
0.60	165.9	0.99	167.5	0.99	166.1	0.99
0.65	140.9	0.98	143.9	0.98	141.2	0.98
0.70	70.6	0.96	77.3	0.97	70.9	0.96
0.75	40.8	0.92	49.4	0.95	41.2	0.92
0.80	32.8	0.89	42.6	0.94	33.3	0.89
0.85	30.7	0.88	41.5	0.94	31.2	0.88
0.90	33.4	0.90	45.2	0.95	34.0	0.90
Average	122.3	0.95	126.3	0.97	122.7	0.96