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The Fabrication of High-Hardness and Transparent PMMA-Based Composites by an Interface Engineering Strategy

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Abstract: The high-hardness and transparent PMMA-based composites play a significant role in modern optical devices. However, a well-known paradox is that conventional PMMA-based composites with high loadings of nanoparticles usually possess high surface hardness at the cost of poor transparency and toughness due to the aggregation of nanoparticles. In this work, ideal optical materials (SiO₂/PMMA composites) with high transparency and high surface hardness are successfully fabricated through the introduction of the flow modifier Si-DPF by conventional melt blending. Si-DPF with low surface energy and high transparency, which is located at the SiO₂/PMMA interface, and nano-SiO₂ particles are homogeneously dispersed in the PMMA matrix. As an example, the sample **SiO₂/PMMA/Si-DPF (30/65/5)** shows outstanding transparency (>87.2% transmittance), high surface hardness (462.2 MPa), and notched impact strength (1.18 kJ/m²). Moreover, **SiO₂/PMMA/Si-DPF (30/65/5)** also presents a low torque value of composite melt (21.7 N·m). This work paves a new possibility for the industrial preparation of polymer-based composites with excellent transparency, surface hardness, processability, and toughness.

Keywords: PMMA-based composites; dispersion; transparent; surface hardness



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1. Introduction

Poly (methyl methacrylate) (PMMA) has been widely used as an optical material for its high transparency, light weight, and low cost. Especially in recent years, PMMA has been used as display screens, lenses, and LED encapsulation materials [1–3]. PMMA has a high surface hardness and still needs to be improved by incorporating sufficient nanoparticles (i.e., SiO_2 [4–9], TiO_2 [9], ZrO_2 [10], Al_2O_3 [11], and ZnO [12]) for wider applications. For instance, Tseng and coworkers [6] prepared the SiO_2 /PMMA composites (50/50 by weight) and the surface hardness reached 314 MPa, which was much higher than that of PMMA (196 MPa). Obviously, the high loading of nanoparticles is necessary to attain a high surface hardness of the composites.

However, the nanoparticles are easily packed together and inevitably form a large number of agglomerates in the PMMA matrix, which seriously deteriorates the properties of the composites, especially transparency [13,14]. Tadano et al. [7] introduced 9 wt% nano-SiO₂ particles into PMMA to prepare the SiO₂/PMMA hybrid films, and the transmittance of the samples was decreased from 91% to 72% due to the formation of SiO₂ agglomerates. That is to say, the improvement in surface hardness of the PMMA-based composites by incorporating nanoparticles is achieved at the expense of reduced transparency. Moreover, the serious agglomeration of fillers generally results in poor processability and toughness of the composites, which is still urgently needed to be solved. Hence, incorporating nanoparticles into the PMMA matrix does not guarantee the fabrication of PMMA-based composites with high transparency and high surface hardness [15]. Only when nanoparticles do not aggregate and are uniformly dispersed in the PMMA matrix could high transparency and

high surface hardness of the composites be simultaneously achieved [16]. In addition, achieving homogeneous dispersion of nanofillers in the polymer matrix is one of the hot research topics in modern material science [17].

PMMA-based composites are generally prepared by techniques including in-suit polymerization, modified polymerization, hot compression, and solution blending. It has been proven to be effective to introduce nanoparticles into PMMA by in-suit polymerization, forming a homogeneous dispersion of nanoparticles. A SiO₂/PMMA composite (50/50) was synthesized via in-suit polymerization of methyl methacrylate and 2-(methacryloyloxy) ethyl isocyanate-modified SiO₂ nanoparticles, and the composite simultaneously possessed a high surface hardness (363 MPa) and high transparency (>89% transmittance) [6]. Unfortunately, the application of the aforementioned method in the industry is difficult due to its complexity [18]. If the homogeneous dispersion of nanoparticles in the PMMA matrix is easy to be realized by melt blending, it is very convenient to fabricate ideal optical materials in an industry [19].

Our previous work demonstrated that the silicone/fluorine-functionalized flow modifier (Si-DPF) with low surface energy was located at the two-phase interface in the magnesium hydroxide/linear low-density polyethylene (MH/LLDPE) composites (80/20), and evidently improved the dispersion of MH particles [20]. In this work, the proposed flow modifier Si-DPF is applied to the production of SiO₂/PMMA composites by a conventional melt processing technique, aiming to fabricate the SiO₂/PMMA composites with high transparency, high surface hardness, excellent processability, and toughness. Herein, a small amount of Si-DPF (5 wt%) is introduced into SiO₂/PMMA composites (the weight ratio of nano-SiO₂ to PMMA is 10:90, 20:80, and 30:70, respectively). It is expected that the introduction of Si-DPF is conducive to the uniform dispersion of nano-SiO₂ particles in the PMMA matrix, and the transparency of SiO₂/PMMA composites is retained while the surface hardness is improved. Moreover, the dispersion and toughening mechanisms are explored. The present work provides a strategy for the development of transparent polymer-based nanocomposites for industrial production.

2. Results and Discussion

2.1. Phase Morphology

Improving the dispersion of nano-SiO₂ particles in the PMMA matrix is a key to fabricating transparent SiO₂/PMMA composites [21–23]. As we know, the more the nano-SiO₂ particles are loaded, the more serious the SiO₂ agglomeration. To display the effect of Si-DPF on the dispersion of highly filled nano-SiO₂ particles, the morphology of nano-SiO₂ particles in the samples **SiO₂/PMMA (30/70)** and **SiO₂/PMMA/Si-DPF (30/65/5)** is observed by SEM. Obviously, Si-DPF changes the dispersion of nano-SiO₂ particles. There is a large amount of SiO₂ agglomerates in the sample **SiO₂/PMMA (30/70)** (Figure 1(a_1,a_2)), whereas nano-SiO₂ particles are uniformly dispersed in the PMMA matrix for **SiO₂/PMMA/Si-DPF (30/65/5)** (Figure 1(b_1,b_2)), indicating that Si-DPF plays an important role in the dispersion of highly filled nano-SiO₂ particles.

Furthermore, to obtain the size and dispersion mechanism of nano-SiO₂ particles, TEM tests are carried out on SiO₂/PMMA composites, as shown in Figure 2.

Clearly, for the samples without Si-DPF, there exists a large amount of SiO₂ agglomerates in the PMMA matrix (Figure $2(a_1-a_3)$), where the average size of SiO₂ agglomerates is about 430 nm, 450 nm, and 480 nm, respectively. By contrast, for the SiO₂/PMMA composites with 5 wt% Si-DPF, the nano-SiO₂ particles exhibit a homogeneous dispersion in the PMMA matrix and almost retain their original size of 20–40 nm without aggregation (Figure $2(b_1-b_3)$,c). Figure $2(d_1)$ provides a TEM image of the sample **SiO₂/PMMA/Si-DPF (30/65/5)**, in which a relatively thinner interface between the nano-SiO₂ particles and PMMA matrix is observed. The elemental mapping image (EMI) analysis is performed and the results are shown in Figure $2(d_1-d_3)$. Si signals are observed in the nano-SiO₂ particles, and F signals are observed in the interface, indicating that Si-DPF tends to be located at the interface between the SiO_2 particles and the PMMA matrix. Both SEM and TEM tests indicate that Si-DPF is able to effectively prevent nano-SiO₂ particles from aggregating.



Figure 1. SEM images of SiO₂/PMMA (30/70) (**a**₁,**a**₂) and SiO₂/PMMA/Si-DPF (30/65/5) (**b**₁,**b**₂).



Figure 2. TEM images of SiO₂/PMMA composites. (a_1) SiO₂/PMMA (10/90), (a_2) SiO₂/PMMA (20/80), (a_3) SiO₂/PMMA (30/70), (b_1) SiO₂/PMMA/Si-DPF (10/85/5), (b_2) SiO₂/PMMA/Si-DPF (20/75/5), and (b_3 , d_1) SiO₂/PMMA/Si-DPF (30/65/5). (c) SiO₂ particle size of SiO₂/PMMA composites. (d_2 , d_3) Elemental mapping images of Si and F.

2.2. Surface Hardness

The surface hardness of SiO₂/PMMA composites is evaluated by the nanoindentation tests [24]. Figure 3a shows that the PMMA matrix has a surface hardness of 236.4 MPa. The surface hardness of the samples is increased as the loading of nano-SiO₂ particles, and the surface hardness is increased to 284.2 MPa for SiO₂/PMMA (10/90), 355.8 MPa for SiO₂/PMMA (20/80), and 491.2 MPa for SiO₂/PMMA (30/70). As expected, the surface hardness is slightly decreased for the samples with Si-DPF. The results show that the long molecular chains of silicone in Si-DPF endow the samples with flexibility and reduce their hardness. Figure 3b shows the load-displacement curves by the nano-indenter. The harder sample requires more loading force for the tip to penetrate the same depth of 500 nm from the surface to the interior of the samples. The results in Figure 3a,b demonstrate that the surface hardness of SiO₂/PMMA composites is obviously increased with the loading of nano-SiO₂ particles and is easy to be adjusted.



Figure 3. Surface hardness of the PMMA matrix and SiO₂/PMMA composites. (**a**) Hardness. (**b**) Load-displacement curves.

2.3. Optical Properties

The transparency of SiO_2 /PMMA composites is crucial for their application as optical materials [25,26]. Figure 4a shows the transmittance spectra of the PMMA matrix, Si-DPF, and SiO_2 /PMMA samples, and the thickness of the samples is 1 mm. As seen, both PMMA and Si-DPF exhibit excellent transparency, which have a 91.1% and 86.8% transmittance at a wavelength of 760 nm, respectively. The transparency of SiO₂/PMMA samples is decreased as the loading of nano-SiO₂ particles, which originated from SiO₂ agglomeration in the PMMA matrix. The aggregation of nanoparticles in a polymer matrix increases the refraction of light and leads to a decrease in transparency. The transmittance is decreased to 80.4% for SiO₂/PMMA (10/90), 78.6% for SiO₂/PMMA (20/80), and 77.3% for SiO₂/PMMA (30/70) at a wavelength of 760 nm. The dispersion of nano-SiO₂ particles is improved by the introduction of Si-DPF and the transparency of SiO₂/PMMA samples is obviously increased. The transmittance is increased to 86.5% for SiO₂/PMMA/Si-DPF (10/85/5), 86.6% for SiO₂/PMMA/Si-DPF (20/75/5), and 87.2% for SiO₂/PMMA/Si-DPF (30/65/5) at a wavelength of 760 nm, indicating that Si-DPF has an obvious advantage in improving the transparency of SiO_2 /PMMA composites. The transparency of the composites could also be observed with the naked eye. The images of SiO₂/PMMA samples, as well as the PMMA matrix and Si-DPF, are displayed in Figure $4(b_1-b_8)$, which is unable to be distinguished by sight.

SIO2/PMMA (20/80) SIO2/PMMA/SI-DPF (20/75/5) SIO2/PMMA (30/70) SIO2/PMMA/SI-DPF (30/65/5)

Figure 4. (a) Transmittance spectra of PMMA matrix, Si-DPF, and SiO₂/PMMA samples with a thickness of 1 mm. (b) Images of PMMA matrix (b_1), Si-DPF (b_2), and SiO₂/PMMA samples (b_3-b_8). (c) The haze value of the PMMA matrix and SiO₂/PMMA samples.

Moreover, the haze (*H*) is also used to evaluate the optical property of the composites, which is given by the ratio of the light diffusely scattered (T_d) to the total light transmitted [27].

$$T_{\rm t}) \left[H \,(\%) = T_{\rm d} / T_{\rm t} \times 100\% \right] \tag{1}$$

In Figure 4c, PMMA shows that the haze value is 20.01%. For SiO₂/PMMA (10/90), when light passes through the interface, light-scattering would happen due to the different refractive index between the nano-SiO₂ particles and the PMMA matrix, showing a higher haze value (37.27%). However, to our surprise, the haze value is decreased as the increase of nano-SiO₂ particles loading, and the corresponding values are decreased to 27.04% for SiO₂/PMMA (20/80) and 17.66% for SiO₂/PMMA (30/70). This is attributed to the more serious agglomeration of SiO₂ particles at the higher loading. The average size of SiO₂ agglomerates increased and the total area of the interface between the PMMA matrix and SiO₂ particles decreased. Consequently, the light-scattering is weakened and the haze values of the samples present a downward trend [28–30]. With the addition of Si-DPF, the nano-SiO₂ particles exhibit a homogeneous dispersion in the PMMA matrix, and the total area of the interface between the PMMA matrix and SiO₂ particles is obviously increased. The haze values are increased to 57.10% for SiO₂/PMMA/Si-DPF (10/85/5), 38.35% for SiO₂/PMMA/Si-DPF (20/75/5), and 34.26% for SiO₂/PMMA/Si-DPF (30/65/5), respectively. The results further confirm that the Si-DPF is effective in improving the dispersion of nano-SiO₂ particles in the PMMA matrix.

Table 1 summarizes the reported transparency and surface hardness enhancement for PMMA-based composites with various nanoparticles. As seen, few studies on PMMAbased composites have focused on transparency and surface hardness simultaneously. It is noted that the PMMA-based composites with higher nano-SiO₂ particle contents in this work show higher transparency and higher surface hardness enhancement. This work

Surface Hardness Samples Strategy Filler Loading [wt%] Transmittance [%, 760 nm] Year [Ref] Enhancement [%] SiO₂/PMMA 37.5 90 80.0 2005 [4] 78 SiO₂/PMMA 4 5 2005 [5] In situ ZnO/PMMA 65 2018 [12] polymerization SiO₂/PMMA ≈ 3 88 2020 [9] TiO₂/PMMA ≈ 3 87 2020 [9] 50 89.5 SiO₂/PMMA 2006 [6] Modified 85.2 2019 [8] SiO₂/PMMA 13.5 90 polymerization ZrO₂/PMMA 1.5 -12.3 2011 [10] Hot compression Al₂O₃/PMMA 3 29.8 2020 [11] SiO₂/PMMA 9.1 72 Solution blending 2014 [7] SiO₂/PMMA Melt blending 30 87.2 95.5 This work

provides a relatively more efficient and facile method to improve the transparency and surface hardness of PMMA-based composites.

Table 1. A comparison of the transmittance and surface hardness enhancement in PMMA-based composites with various nanoparticles.

2.4. Processability

The processability of the composites is critical for engineering applications, which is evaluated by the torque rheology test. Figure 5 shows the torque vs. time curves for SiO₂/PMMA composites. As seen, the equilibrium torque of composite melt is increased as the loading of nano-SiO₂ particles and Si-DPF can decrease the melt torque. For samples SiO₂/PMMA (10/90), SiO₂/PMMA (20/80), and SiO₂/PMMA (30/70), the stable torque values are 19.0 N·m, 23.1 N·m, and 26.3 N·m, respectively. With the addition of Si-DPF, the torque values of the samples are decreased, and the corresponding ones are decreased to 15.0 N·m for SiO₂/PMMA/Si-DPF (10/85/5), 17.1 N·m for SiO₂/PMMA/Si-DPF (20/75/5), and 21.7 N·m for SiO₂/PMMA/Si-DPF (30/65/5), respectively, indicating an improvement in processability. The complex viscosity η^* is also used to evaluate the processability of composites, and Figure 5b shows the curves of complex viscosity (η^*) vs. frequency (ω) for the samples. As seen, the η^* of samples are obviously increased with the loading of nano-SiO₂ particles, and the viscosity values of SiO_2 /PMMA samples are decreased with the addition of Si-DPF. This result is ascribed to the improvement in the dispersion of nano-SiO₂ particles; that is, Si-DPF tends to be located at the interface, which prevents nano-SiO₂ particles from aggregation and results in a decrease in the melt viscosity [20].

Figure 5. (a) Torque rheological analysis of SiO₂/PMMA composites. (b) Complex viscosity versus frequency of samples. Temperature: $180 \degree$ C.

2.5. Toughness

Usually, the toughness of high-filled PMMA is decreased. To assess the toughness of $SiO_2/PMMA$ composites with and without Si-DPF, the notched impact test of the PMMA matrix and the $SiO_2/PMMA$ composites is conducted, and the results are shown in Figure 6. As seen, the PMMA matrix presents an impact strength of 1.12 kJ/m². Undoubtedly, the

notched impact strength of SiO₂/PMMA samples is decreased, as the loading of nano-SiO₂ particles and the strengths are decreased to 1.04 kJ/m^2 for SiO₂/PMMA (10/90), 0.99 kJ/m^2 for SiO₂/PMMA (20/80), and 0.96 kJ/m^2 for SiO₂/PMMA (30/70). The decrease in strength originated from the SiO₂ agglomerates in the PMMA matrix. By contrast, the notched impact strength of SiO₂/PMMA/Si-DPF (10/85/5), SiO₂/PMMA/Si-DPF (20/75/5), and SiO₂/PMMA/Si-DPF (30/65/5) are 1.17 kJ/m^2 , 1.21 kJ/m^2 , and 1.18 kJ/m^2 , respectively. These samples exhibit a higher notched impact strength and better toughness compared to the PMMA matrix, showing that Si-DPF has a positive effect on improving the toughness of SiO₂/PMMA composites. Si-DPF with low surface energy tends to be located at the phase interface, which not only plays the role of dispersing nano-SiO₂ particles but also transfers the energy. When the samples are impacted by the external force, the energy is transferred to the small aggregates, which act as a stress concentration point to dissipate energy; thus, the toughness is improved.

Figure 6. Impact strengths of the PMMA matrix and SiO₂/PMMA composites.

Nano-SiO₂ particles aggregate easily due to the high surface energy. Therefore, weakening the interaction between nano-SiO₂ particles is critical for improving the dispersion of nano-SiO₂ particles. Si-DPF with low surface energy prefers to locate at the SiO₂/PMMA interface, forming a protective layer on the SiO₂ particles, and reducing the SiO₂ agglomeration. For the highly filled SiO₂/PMMA composites, the uniformly dispersed particles could help to improve the transparency of the composites while maintaining high surface hardness. As a protective layer, Si-DPF contributes to the relative sliding of nano-SiO₂ particles under an applied stress during the melt blending stage, reducing the melt viscosity of the samples and thus improving processability.

3. Experimental

3.1. Main Materials

The commercially available poly (methyl methacrylate) (PMMA, CM-211) was purchased from Chimei Taiwan Co., Ltd., with a melt flow rate of 7 g/10 min (Tainan, Taiwan, China). Silica (nano-SiO₂, A-200, 2.2 g/cm³) was supplied by Shandong Dongyue Silicone Material Co., Ltd., with a specific area of 180–220 m²/g and a mean diameter of 10–40 nm (Zibo, Shandong, China). The synthesis of the silicone/fluorine-functionalized flow modifier (Si-DPF) referred to our previous work (CST. 2021, 214, and 108994) [20].

3.2. Fabrication of SiO₂/PMMA Composites

PMMA was dried in a vacuum oven at 80 °C for 12 h. SiO₂/PMMA composites were prepared by melt blending in a twin-screw extruder at a screw speed of 150 rpm. The extruder was configured with ten heating zones, and the extrusion was carried out at zone temperatures of 165 °C, 170 °C, 170 °C, 175 °C, 175 °C, 175 °C, 180 °C, 180 °C, 185 °C, and 185 °C, respectively. After being granulated and dried, the pellets were injection-molded on an injection-molding machine to obtain different specimens. The temperatures of the injection-molding machine were set in a range from 175 °C to 195 °C. The formulation of SiO_2 /PMMA samples is listed in Table 2.

Samples	SiO ₂ (g)	PMMA (g)	Si-DPF (g)
SiO ₂ /PMMA (10/90)	10	90	-
SiO ₂ /PMMA/Si-DPF (10/85/5)	10	85	5
SiO ₂ /PMMA (20/80)	20	80	-
SiO ₂ /PMMA/Si-DPF (20/75/5)	20	75	5
SiO ₂ /PMMA (30/70)	30	70	-
SiO ₂ /PMMA/Si-DPF (30/65/5)	30	65	5

Table 2. Formulation of various SiO₂/PMMA samples.

3.3. Analysis and Characterization

Scanning electron microscopy (SEM) images were obtained with a Nova NanoSEM430 scanning electron microscope (FEI, Hillsboro, OR, USA) operating at 20 kV. Samples were fractured in liquid nitrogen and the fracture surfaces were coated with gold before observation. Transmission electron microscopy (TEM) images were obtained with a JEM 2100F transmission electron micrograph (JEOL, Tokyo, Japan) operating at 100 kV. Samples were prepared by cutting the blends into approximately 50 nm slices with an RMC PowerTome. Transmittance spectra of the samples were recorded on a Hitachi U-3900H spectrometer (Hitachi, Tokyo, Japan) in a range from 500 to 800 nm. The haze of the samples was measured by an SGW-820 haze meter (Shanghai INESA Physico-Optical Instrument, Shanghai, China) under standard illuminant D65 and in compliance with ASTM D1003. The surface hardness of the samples was measured on a TTX-NHT³ nanoindentation instrument (Anton Paar, Graz, Austria) with a Berkovich diamond tip at room temperature. The test speed was constant at 5 mN/min and the maximum depth was 500 nm. The processability of the samples was measured on a Haake XSS-300 torque rheometer (Haake, Vreden, Germany) at a rotation rate of 50 rpm at 180 °C for 10 min. The complex viscosity of the samples (the sample disks with 25 mm diameter and 1 mm thickness) was carried out on a stresscontrolled rheometer (AR-G2, TA Instruments, NC, USA) in a dynamic frequency sweep from 0.1 to 628 rad s⁻¹ at a strain of 1% within the linear viscoelastic range at 180 °C. According to the ISO 179-1:2000 standards, the impact strength of the samples was tested on a Zwick5113 impact pendulum machine (ZwickRoell, Ulm, Germany). At least five specimens were tested for each measurement and the average results were reported.

4. Conclusions

We successfully achieved the properties of high transparency, high surface hardness, excellent processability, and toughness in high-performance SiO₂/PMMA composites by using the conventional melt mixing technique, solving the well-known problem that high loading of nano-SiO₂ particles is easy to aggregate and the problem of SiO₂ agglomerates deteriorating the transparency and toughness of the composites. The 30 wt% nano-SiO₂ particles, uniformly dispersed in the PMMA matrix with the help of Si-DPF located at the phase interface, facilitated the building of a perfect composite with high transparency and high surface hardness, compared with SiO₂/PMMA composites also presented excellent toughness and processability. This work provides a quick and effective strategy for improving the production efficiency of commercially available polymer-based composites with high transparency and high surface hardness, which pave a way for their application as ideal optical materials, such as display screens, lenses, and LED lighting.

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