

Supplementary information

Ozone based AOPs for primidone removal in water using simulated solar radiation and TiO₂ or WO₃ as photocatalyst

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Absolute method for the determination of ozone-Primidone reaction rate constant

Experimental procedure: A mixture of primidone ($C_{PRM,0} 2.3 \times 10^{-5} \text{ M}$) and tert-butyl alcohol ($C_{TBA,0} 2.5 \times 10^{-3} \text{ M}$) in ultrapure water was ozonized ($C_{O_3g,inlet} = 10 \text{ mg L}^{-1}$; $Q_{O_2-O_3} = 20 \text{ L h}^{-1}$) at pH 2 and $20 \text{ }^\circ\text{C}$, and the evolution with time of PRM and dissolved ozone concentrations analyzed. At these conditions, degradation of PRM takes place only through its direct reaction with molecular ozone.

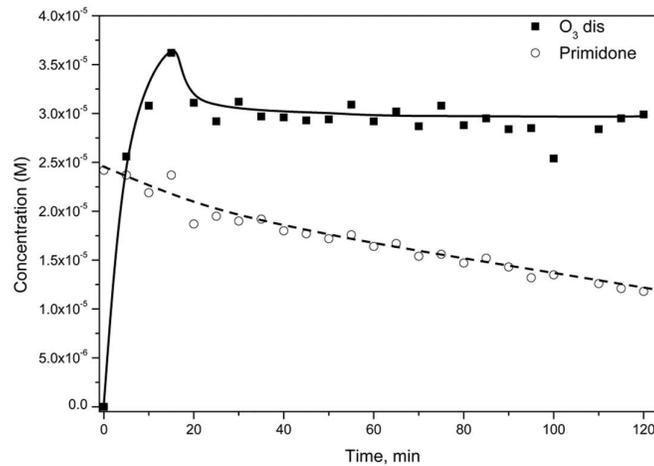


Figure S1: Evolution of PRM and dissolved O_3 concentrations with time during the ozonation of PRM in presence of TBA (two replicates). Experimental conditions: $C_{PRM,0} = 2 \times 10^{-5} \text{ M}$; $C_{TBA,0} = 2.3 \times 10^{-3} \text{ M}$; $\text{pH} = 2$; $T = 20 \text{ }^\circ\text{C}$; $C_{O_3g,inlet} = 10 \text{ mg L}^{-1}$; $Q_{O_2-O_3} = \text{L h}^{-1}$.

Calculus: In the semibatch perfectly mixed reactor used in this work, at the conditions tested and assuming a second-order kinetics for the reaction between ozone and PRM, PRM mass balance can be expressed as follows:

$$-\frac{dC_{PRM}}{dt} = k_D C_{PRM} C_{O_3} \quad (\text{S1})$$

As observed in Figure S1 dissolved ozone concentration in solution (C_{O_3}) reached a stationary state (C_{O_3ss}) after 25 minutes (t_{ss}). Hence, for higher reaction times a pseudo first order kinetic model can be assumed:

$$-\frac{dC_{PRM}}{dt} = k'_D C_{PRM} \quad (S2)$$

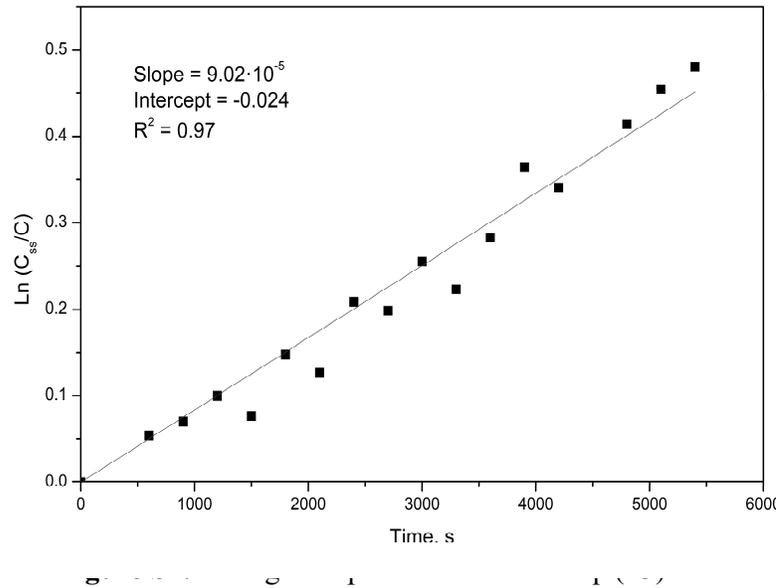
where $k'_D = k_D C_{O_3ss}$, being $C_{O_3ss} = 2.9 \times 10^{-5}$ M (see Fig S1).

The integration of equation (S2) leads to equation (S3):

$$\ln \frac{C_{PRMss}}{C_{PRM}} = k'_D (t - t_{ss}) \quad (S3)$$

where C_{PRMss} is the concentration of PRM at t_{ss} .

Thus, k'_D value can be obtained by fitting experimental data to eq. (S3) as shown in Figure S2. From least squares analysis of the straight line shown in this figure k'_D resulted to be $9.02 \cdot 10^{-5} \text{ s}^{-1}$ ($R^2=0.97$). Therefore, the second-order rate constant of the reaction between PRM and O_3 is $k_D = 3.08 \text{ M}^{-1}\text{s}^{-1}$.



Once the rate constant was obtained the slow kinetic regime of ozone absorption was verified determining the Hatta number by equation S4 [1]). In eq. S4 D_{O_3} is the diffusivity of ozone in water ($1.76 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$; [2]) and k_L the individual liquid-side mass transfer coefficient calculated as $3.74 \times 10^{-4} \text{ m s}^{-1}$ from Calderbank's equation [3]. For slow kinetic

regime Ha is < 0.3 [1].

$$Ha = \frac{\sqrt{k_D C_{PRM} D_{O_3}}}{k_L} \quad (S4)$$

According to S4 from the estimated k_D and the experimental C_{PRM} data, Ha resulted to be < 0.3 which validates the value of k_D obtained.

Concentration of hydrogen peroxide during photocatalytic oxidation processes studied in this work

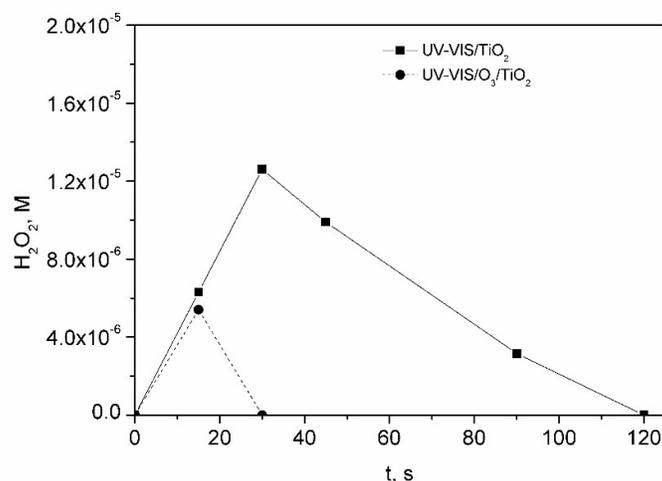


Figure S3. Changes of hydrogen peroxide concentration with time during PRM oxidation with UV-Vis/TiO₂ and UV-Vis/TiO₂/O₃ systems. Experimental conditions: Ultrapure water; [PRM]₀ = 5 mg L⁻¹; pH₀ ~ 6 (natural pH); [TiO₂] = 0.25 g L⁻¹; Q_{m,O₃} = 3.3 mg min⁻¹; T = 20-30 °C; IUV-Vis = 8.2 × 10⁻⁵ Einstein L⁻¹ s⁻¹.

References

- [1] J.C. Charpentier, Mass-transfer rates in gas-liquid absorbers and reactors, Adv. Chem. Eng. 11 (1981) 1–133. doi:10.1016/S0065-2377(08)60025-3.
- [2] P.N. Johnson, R.A. Davis, Diffusivity of ozone in water, J. Chem. Eng. Data. 41 (1996) 1485–1487. doi:10.1021/jc9602125.
- [3] G.F. Froment, K.B. Bischoff, J. De Wilde, Chemical Reactor Analysis and Design, 3rd edition, John Wiley & Sons, Inc., USA, 2011.