

Proceeding Paper

# A Hydrometallurgical Process for Cu Recovery from Printed Circuit Boards <sup>†</sup>

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**Abstract:** The current study presents an effort to develop a sustainable hydrometallurgical process for the recovery of copper from waste printed circuit boards (PCBs) to be applied at local small to medium industrial units. The process aims to separate and recover copper from filter dust produced during the crushing of PCBs using a hammer mill in a recycling facility. Due to the high plastic content in the dust (approximately 30% *w/w*), the metal fraction was separated gravimetrically, and the material originated consisted mainly of Cu (23.8%), Fe (17.8%), Sn (12.7%), Pb (6.3%), Zn (3.4%), Al (3.3%), Mn (1.6%), and Ni (1.5%). Prior to copper recovery, the dust was leached with HCl as a pretreatment step. During this step, more than 80% of iron, zinc, and tin were leached out. The resulting solid consisted mainly of Cu (37.6%) and Fe (10.7%), leading to a copper enrichment of around 60% in the powder. The leaching of copper was conducted in a two-step process using H<sub>2</sub>SO<sub>4</sub> as a leaching agent with the addition of H<sub>2</sub>O<sub>2</sub> as an oxidizing agent. The experimental conditions had low energy requirements (no heating or agitation needed). The leaching of Cu reached 98%. Despite the pretreatment step, the concentration of other metals (Fe, Zn, Ni) in the pregnant solution was too high to proceed to electrowinning. Therefore, the organic solvent ACORGA M5640 was selected for the extraction of copper from the pregnant solution. The extraction was conducted in two stages at pH equilibrium 1.5, and the loaded organic phase was stripped with HCl in two steps. The strip liquor was suitable for electrowinning.

**Keywords:** copper; leaching; hydrometallurgy; recycling; PCBs



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## 1. Introduction

In the last decades, the amount of electric devices in the market has increased. Thus, the demand of raw materials in electric devices has also increased [1]. However, the ores used by the traditional mining industry are reaching their limits, and the struggle to reach the demands in the future will increase day by day [2].

Wasted printed circuit boards (PCBs) contain the highest concentrations of base and precious metals [3]. Hence, it is of great importance for them to be recycled. At present, the main route for the recycling of electronic scrap is based mainly on physical and pyrometallurgical methods. Although, pyrometallurgy has high metal recovery and is a well-known technology, the high energy needs and the environmental restrictions make its processes unsustainable [4]. On the other hand, hydrometallurgical methods are not energy intensive and do not produce gaseous emissions, and for these reasons they are mainly considered sustainable compared to pyrometallurgical methods [5].

The European Union's annual copper demand is around 4 million tons and rising [6]. In 2016, almost 40% of copper needed was imported [6]. Recovering copper from e-waste could decrease the amount of imports. The percentage of copper contained in PCBs

(10–20%) remains the highest among all metals, much higher than in natural ores [7]. A particular interest is expressed by e-waste recycling companies for pure metal recovery from e-wastes. Only sustainable metallurgical processes for metal recovery from e-wastes can be scaled up by local small to medium industrial units [8].

This study, part of the HYDROPCB project (Development of a hydrometallurgical process for metal recovery from Printed Circuit Boards in pilot scheme: A zero waste process), presents the results obtained in an effort to selectively recover copper from filter dust, produced during the crushing of PCBs in a hammer mill at a local recycling facility (ECORESET SA).

## 2. Materials and Methods

In the present research, a dust sample was provided by a local recycling facility.

### 2.1. Solid Characterization and Pretreatment Leaching

The characterization of the dust and the solid products was performed by dissolution after eutectic fusion at 1000 °C. The dust composition in plastic material was determined by Thermogravimetric Analysis (TGA) and Differential Scanning Calorimetry (DSC). The leaching solutions were analyzed by Atomic Absorption Spectrometry (AAS). The solids were analyzed by X-ray Diffraction (XRD) and Scanning Electron Microscopy (SEM).

The dust was subjected to treatment in a shaking table and divided in two fractions, a metallic and a non-metallic.

Prior to leaching for the extraction of copper, the metallic part of the initial dust was subjected to leaching with 6M HCl (pretreatment leaching) in order to remove other metals and enrich the fraction in copper. The resulted leached residue was the raw material for copper recovery.

### 2.2. Leaching of Copper

The copper dust was leached with H<sub>2</sub>SO<sub>4</sub>, and H<sub>2</sub>O<sub>2</sub> was used as the oxidizing agent (OA). The effect of various process factors on Cu recovery was investigated. The factors studied were the S/L ratio (0.05 g/mL, 0.1 g/mL, and 0.2 g/mL), the leaching agent concentration (1 M, 2 M, and 3 M), and the oxidizing agent concentration (1 mL<sub>O.A.</sub>/g<sub>solid</sub>, 2 mL<sub>O.A.</sub>/g<sub>solid</sub>, 4 mL<sub>O.A.</sub>/g<sub>solid</sub>, and 6 mL<sub>O.A.</sub>/g<sub>solid</sub>). The residence time for all the experiments was 4h. The optimum conditions were then determined, and a solution was prepared by leaching the copper dust at these conditions

### 2.3. Extraction and Stripping of Copper

The resulting solution was then used to study the extraction of copper using solvent extraction with ACORGA M5640. The effect of the pH on the extraction efficiency was investigated. A McCabe–Thiele extraction diagram was plotted. The loaded organic phase was stripped by HCl. The effect of the HCl concentration on the stripping efficiency was investigated. A McCabe–Thiele stripping diagram was plotted.

## 3. Results

### 3.1. Pretreatment Leaching

The chemical composition of the PCB dust and the metallic fraction after the physical separation in the shaking table are presented in Table 1. The non-metallic fraction in the initial dust was 30% *w/w*. During the pretreatment step, less than 0.3% of copper was leached. Thus, the solid was enriched in copper.

**Table 1.** Chemical composition of the dust before and after separation and the pretreatment step.

Metal	Initial Dust (% wt.)	Metallic Fraction after Separation (%wt.)	Solid Product after Pretreatment Leaching (%wt.)
Sn	5.01	12.74	1.30
Cu	5.19	23.86	37.60
Fe	8.17	17.84	10.67
Zn	1.90	3.36	1.68
Ni	0.76	1.48	1.77
Pb	1.53	6.28	7.45
Al	3.18	3.29	1.04
Total	26.50	68.85	61.51

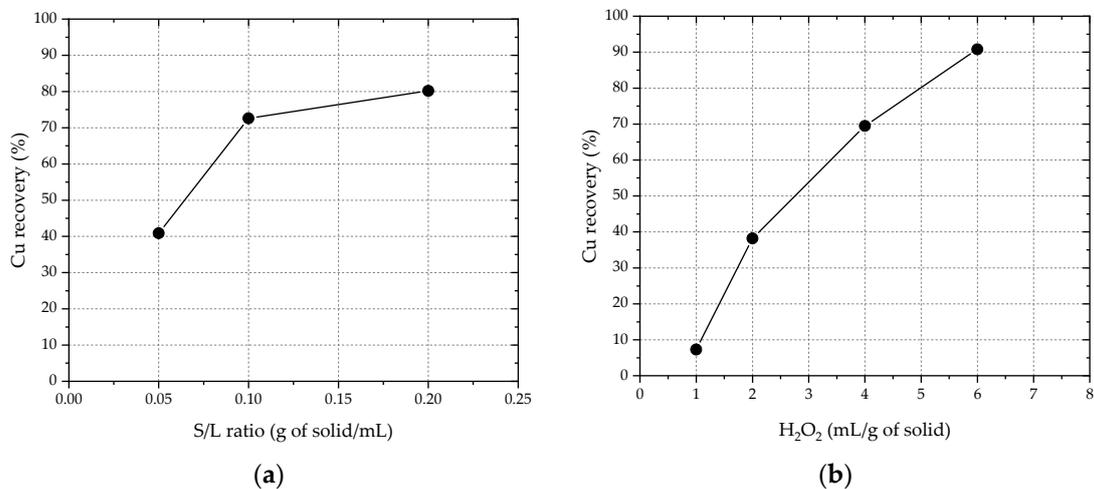
### 3.2. Leaching of Copper

The effect of the leaching agent concentration on Cu recovery is given in Table 2.

**Table 2.** Cu recovery after two-step leaching of the copper dust in 1 M, 2 M, and 4 M H<sub>2</sub>SO<sub>4</sub> in an S/L ratio of 0.1 g/mL and 1 mL H<sub>2</sub>O<sub>2</sub> (30% w/w)/g of copper dust.

H <sub>2</sub> SO <sub>4</sub> Concentration	Cu Leaching Efficiency %
1 M	62.4
2 M	66.0
4 M	45.6

It was concluded that 2 M was the optimum H<sub>2</sub>SO<sub>4</sub> concentration. The effect of the S/L ratio and the H<sub>2</sub>O<sub>2</sub> concentration on leaching efficiency at 2 M H<sub>2</sub>SO<sub>4</sub> was then studied, and the results are shown in Figure 1a and 1b, respectively.

**Figure 1.** (a) Effect of the S/L ratio on Cu recovery, using 2 M H<sub>2</sub>SO<sub>4</sub> and 1 mL H<sub>2</sub>O<sub>2</sub> (30% w/w)/g of copper dust. (b) Effect of the H<sub>2</sub>O<sub>2</sub> concentration (mL of oxidant/g of dust) on Cu recovery, using 2 M H<sub>2</sub>SO<sub>4</sub> and an S/L ratio of 0.1 g/mL.

Based on the results, the relatively optimum conditions for Cu were determined as follows:

- A total of 2 M H<sub>2</sub>SO<sub>4</sub> as leaching agent;
- A total of 3 mL/g H<sub>2</sub>O<sub>2</sub> (30% w/w) as oxidizing agent;
- An S/L ratio of 0.1 g/mL;
- Two stages;
- Residence time of 4 h;
- No agitation.

A two-stage leaching test of the copper dust was carried out at these relatively optimum conditions. The results are shown in Table 3.

**Table 3.** Cu recovery during a two-stage leaching test.

Leaching Stage	Cu Recovery %
1	34.4
2	63.7
<b>Total</b>	<b>98.1</b>

### 3.3. Extraction and Stripping of Copper

The copper solution produced at the optimum conditions of leaching was subjected to purification by chemical precipitation of the impurity metals contained in order to be further treated by solvent extraction. The purification was conducted at pH 3.0 by the addition of 5 M NaOH. Table 4 gives the analysis of the pregnant solution before and after purification.

**Table 4.** Analysis of the pregnant solution before and after purification at pH 3.0.

Metal	Concentration before Purification (g/L)	Concentration after Purification (g/L)
Cu	18.8	13.8
Fe	2.6	0.44
Zn	1.0	0.32
Ni	1.17	0.40

A number of solvent extraction tests were conducted in various pH values in order to determine the optimum extraction pH, which was determined to be 1.5. The analysis of the raffinate after solvent extraction in one stage with ACORGA M5640 (30% *v/v* in kerosene), at pH 1.5, at an A/O ratio of 1:1, and a contact time of 5 min is shown in Table 5.

**Table 5.** Analysis of the pregnant solution after solvent extraction with ACORGA M5640 in one stage.

pH	Cu (mg/L)	Fe (mg/L)	Zn (mg/L)	Ni (mg/L)
1.5	1460	405	305	375

Copper was stripped off the loaded organic phase in the stripped liquor with 2 M HCl, and its analysis is shown in Table 6.

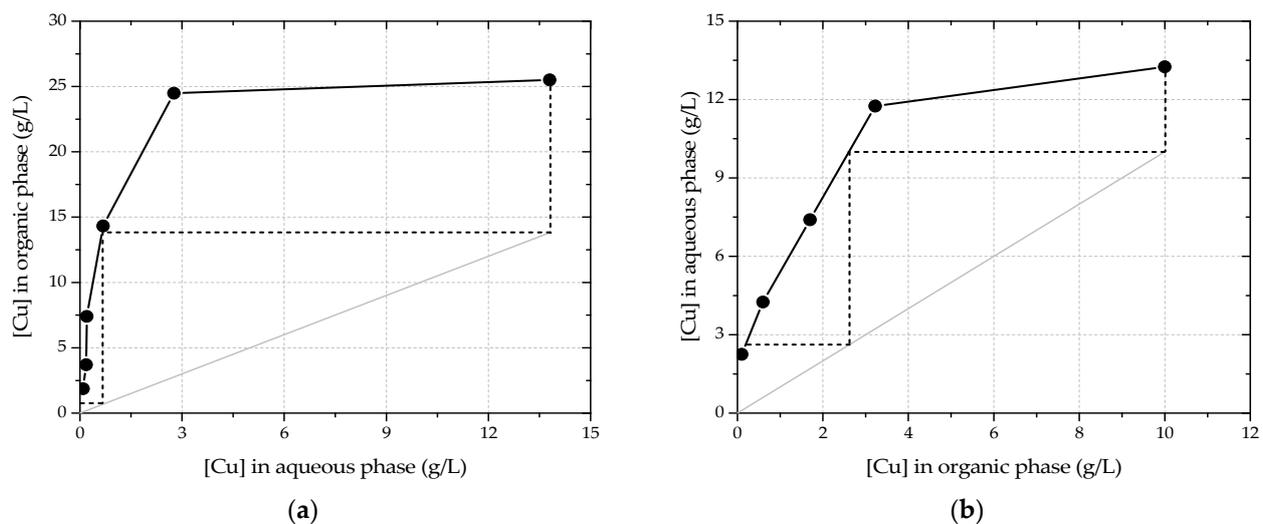
**Table 6.** Analysis of the stripped liquor in one step.

HCl (M)	Cu (mg/L)	Fe (mg/L)	Zn (mg/L)	Ni (mg/L)
2	7400	0.16	0.06	0.01

The analysis shows that the stripped liquor is suitable for electrowinning, as it contained mainly copper. All other metals had a concentration of less than 0.2 mg/L.

A McCabe–Thiele diagram for the extraction of copper from the pregnant solution was plotted for the equilibrium pH 1.5 (Figure 2a). For an A/O ratio of 1:1, copper can be extracted from the pregnant solution, quantitatively, in two stages.

A McCabe–Thiele stripping diagram was plotted for 2 M HCl as stripping solution (Figure 2b). For an A/O ratio of 1:1, copper can be stripped off the loaded organic phase, quantitatively, in two stages.



**Figure 2.** (a) McCabe–Thiele extraction diagram at equilibrium pH 1.5. The A/O ratio for the operation line is 1:1. (b) McCabe–Thiele stripping diagram with 2 M HCl. The A/O ratio for the operation line is 1:1.

#### 4. Conclusions

The conclusions of this study are:

- The PCB metallic fraction, after the removal of the plastic material, is a remarkable copper resource as its copper content exceeds 20% and can be treated hydrometallurgically.
- More than 98% of copper was recovered from the dust by oxidative leaching in two stages, using 2 M H<sub>2</sub>SO<sub>4</sub>, 3 mL H<sub>2</sub>O<sub>2</sub> (30% w/w)/g dust, and a solid/liquid ratio of 0.1 g/mL of dust.
- The optimum pH for the copper solvent extraction with ACORGA M5640 was 1.5.
- Copper was extracted quantitatively from the pregnant solution in two stages by ACORGA M5640 organic reagent at equilibrium pH 1.5 and an A/O ratio of 1:1.
- Copper was stripped off the loaded organic phase quantitatively in two stages by 2 M HCl and at an A/O ratio of 1:1.
- The concentration of copper in the stripped liquor was 7.4 g/L, with all other impurities being less than 0.2 mg/L, thus allowing copper electrowinning.

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