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Assessing Annual Actual Evapotranspiration Based on Climate, Topography and Soil in Natural and Agricultural Ecosystems

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Abstract: Simple formulas for estimating annual actual evapotranspiration (AET) based on annual climate data are widely used in large scale applications. Such formulas do not have distinct compartments related to topography, soil and irrigation, and for this reason may be limited in basins with high slopes, where runoff is the dominant water balance component, and in basins where irrigated agriculture is dominant. Thus, a simplistic method for assessing AET in both natural ecosystems and agricultural systems considering the aforementioned elements is proposed in this study. The method solves AET through water balance based on a set of formulas that estimate runoff and percolation. These formulas are calibrated by the results of the deterministic hydrological model GLEAMS (Groundwater Loading Effects of Agricultural Management Systems) for a reference surface. The proposed methodology is applied to the country of Greece and compared with the widely used climate-based methods of Oldekop, Coutagne and Turk. The results show that the proposed methodology agrees very well with the method of Turk for the lowland regions but presents significant differences in places where runoff is expected to be very high (sloppy areas and areas of high rainfall, especially during December–February), suggesting that the proposed method performs better due to its runoff compartment. The method can also be applied in a single application considering irrigation only for the irrigated lands to more accurately estimate AET in basins with a high percentage of irrigated agriculture.

Keywords: actual evapotranspiration; reference evapotranspiration; surface runoff; surface slope; percolation; saturated hydraulic conductivity; irrigation



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1. Introduction

Actual evapotranspiration is a crucial component of both water and energy balance, which plays a significant role in climate–soil–vegetation interactions [1,2]. It is an extremely complicated biophysical procedure since it is regulated by the combination of climate, soil, topography, vegetation type and density [3]. For this reason, its measurement is only feasible in small scale applications (e.g., by using weighing lysimeters) while it is practically and economically impossible over long periods of time in large scale applications [4]. The methods of estimating actual evapotranspiration are divided into plant physiological, micrometeorological and hydrological estimations depending on the purposes of the study [5]. In the case of large-scale applications (e.g., basin-scale and beyond), the problem of measuring evapotranspiration can be addressed by hydrological methods, which are based on various conceptual approaches such as assessing water balance components using physically-based hydrological models (e.g., SWAT, MIKE, etc.) [6,7], simplistic water balance models [3,8–11], or even more simple actual evapotranspiration formulas such as those of Oldekop [12], Coutagne [13], Turk [14], Bouchet [15,16], Budyko [17–19] or similar

that provide relationships between annual actual evapotranspiration (AET), annual average precipitation and potential evapotranspiration or temperature. The Budyko concept, which in reality is the evolution of the Oldekop concept [20], is the most widely used method, and many efforts have been made to improve its proposed framework and to understand how climate and catchment characteristics regulate the long-term average water balance [21–29].

The aforementioned simplistic formulas of annual actual evapotranspiration do not take into account the following features that may lead to significant errors: (a) Surface runoff is the dominant water balance component in sloppy areas, leading to much lower rates of annual actual evapotranspiration; (b) In main river watersheds, irrigated agriculture dominates in the lowland areas, which leads to higher actual evapotranspiration rates even when annual rainfall is low; (c) Soil permeability regulates percolation and available water storage. In the Budyko-based formula of Fu [22], all the above features were included in one empirical coefficient, which was later expressed by Sun et al. [27] as a function of saturated hydraulic conductivity, rainfall intensity and water holding capacity of the underlying surface.

In another field of research related to the analysis of water and nitrogen losses by agricultural lands, a new methodology was developed by Aschonitis et al. [30,31] for estimating water losses by runoff and percolation from a reference surface, with or without irrigation. The specific method was a hybrid method because it was developed using the results of a large number of simulations made by a physically-based hydrological model in order to calibrate regression formulas able to estimate the annual rates of runoff and percolation separately. The aim of this study was to show that the specific concept and formulas could be used in a simplistic water balance approach in large-scale applications for assessing annual actual evapotranspiration of natural ecosystems but also to assess irrigated agricultural ecosystems considering easily obtained information about climate, soil, topography and irrigation. The specific concept was applied to the country of Greece and was compared with other simplistic climate-based formulas of actual evapotranspiration that do not require calibration [12–14].

2. Materials and Methods

2.1. Derivation of Actual Evapotranspiration and Comparison with Previous Methods

The proposed methodology for estimating actual evapotranspiration is based on the losses of water (LOSW) indices [30,31] that assess the intrinsic rates of annual water losses from surface runoff (*LOSW-R*) and percolation (*LOSW-P*) of a reference surface. According to the *LOSW* concept, a reference surface was set as a uniform surface of actively dense cover with clipped perennial grass, whose rates of evapotranspiration under non-water stress conditions were equivalent to the reference crop evapotranspiration of American Society of Civil Engineers (ASCE)-standardized/Food Agriculture Organization of the United Nations (FAO)-56 concept [32,33]. The *LOSW-P* and *LOSW-R* indices were calibrated based on the inputs and outputs of simulation scenarios performed by the Groundwater Loading Effects of Agricultural Management Systems (GLEAMS) model [34]. The simulations covered: (i) Different soils with respective hydraulic characteristics of the four hydrological soil types A, B, C and D of USDA–NRCS [35]; (ii) Different topography by using different slopes of grass surfaces using the curve number vs. the slope of the grass surface relationship of Getter et al. [36]; (iii) Different climate conditions from Greece, Italy and USA; (iv) Irrigation or non-irrigation conditions. Irrigation was applied automatically by the GLEAMS model when the soil moisture was falling to 20% of available soil moisture (ASM) in order to return it to 100% ASM corresponding to field capacity conditions. All scenarios were performed for the first 30 cm of the soil profile, which included the largest percentage of the rootzone. The results were used to develop and calibrate *LOSW-P* and

LOSW-R, which describe annual percolation and surface runoff water losses, according to the following equations [29]:

$$LOSW - P = \left\{ \begin{array}{l} 0.0941\sqrt{K_s} - 0.761\sqrt{SL} + 0.4185\sqrt{P} \\ - 0.0487\sqrt{ET_o} + 0.0903\sqrt{IR} \end{array} \right\}^2 \quad (1)$$

$$LOSW - R = \left\{ \begin{array}{l} - 0.0856\sqrt{K_s} + 1.8573\sqrt{SL} + 0.9966\sqrt{P} \\ - 0.5612\sqrt{ET_o} + 0.2384\sqrt{IR} \end{array} \right\}^2 \quad (2)$$

where *LOSW-P* is intrinsic percolation water losses (mm year⁻¹), *LOSW-R* is intrinsic runoff water losses (mm year⁻¹), *K_s* is saturated hydraulic conductivity (mm day⁻¹), *SL* is soil surface slope (%), *P* is annual precipitation (mm year⁻¹), *ET_o* is the annual reference evapotranspiration (mm year⁻¹) and *IR* is the annual irrigation to cover the deficit of reference evapotranspiration (mm year⁻¹). It has to be noted that when the formulas inside the brackets of Equations (2) and (3) lead to negative values, the value of *LOSW-P* and *LOSW-R* are set equal to 0.

The above equations can be used either for *IR* = 0 or *IR* ≠ 0. For the latter case, the annual irrigation *IR* for covering the deficit of annual reference evapotranspiration is calculated as follows [30]:

$$IR = \sum_{i=1}^{12} IR_i, \text{ where } IR_i = ET_{o,i} - P_i \text{ when } ET_{o,i} > P_i \text{ else } IR_i = 0 \quad (3)$$

where *IR* is the annual irrigation required for covering the deficit of annual reference evapotranspiration (mm year⁻¹), *IR_i* is monthly irrigation for covering the deficit of reference evapotranspiration of the month *i* (mm month⁻¹), *ET_{o,i}* is monthly reference evapotranspiration (mm month⁻¹) (estimated in this study by FAO-56 method), *P_i* is monthly precipitation and *i* is the month. The use of larger *IR* values from the values of Equation (3) for over-irrigation analysis using Equations (1) and (2) is not indicated.

The main aspect of *LOSW* indices, which has not been analyzed in previous studies, is that they can be used for the estimation of the actual evapotranspiration of the reference surface, taking into consideration not only the climate but also soil and topography. Thus, a new approach for estimating actual evapotranspiration *ET_a* is built based on *LOSW* indices as follows:

$$(LOSW - ET) = TW - (LOSW - P) - (LOSW - R) \quad (4)$$

where *LOSW-ET* is the actual evapotranspiration of the reference surface (mm year⁻¹), *TW* is the total water inflow equal to *P* + *IR*, where *IR* = 0, or is equal to Equation (3). Equation (4) is built under the assumption of null annual change in soil moisture storage Δ*S* ≈ 0 among sequential years. For general applications of Equation (4) with *IR* ≠ 0 estimated by Equation (3), the use of filter (*LOSW-ET*) = *ET_o* is suggested when (*LOSW-ET*) > *ET_o*. In this study, this filter was not used in order to show the overall response of Equation (4) when *IR* ≠ 0.

In this study, the *LOSW-ET* method was compared with the widely known *ET_a* methods of Oldekop [12], Coutagne [13] and Turk [14]. The Oldekop method equation is the following:

$$ET_D = P[1 - \exp(-ET_o/P)] \quad (5)$$

where *ET_D* is the annual Oldekop actual evapotranspiration (mm year⁻¹), *P* is the annual precipitation (mm year⁻¹) and *ET_o* is the annual reference/potential evapotranspiration (mm year⁻¹).

The Coutagne method equation is the following:

$$\begin{aligned} ET_C &= P \quad \text{for } P < L/8 \\ ET_C &= P(1 - P/L) \quad \text{for } L/8 \leq P \leq L/2 \\ ET_C &= 200 + 35T \quad \text{for } P > L/2 \quad \text{where } L = 800 + 140T \end{aligned} \quad (6)$$

where ET_C is the annual Coutagne actual evapotranspiration (mm year^{-1}), P is the annual precipitation (mm year^{-1}), T is mean annual temperature ($^{\circ}\text{C}$) and L is the function of temperature (unitless).

The Turk method equation is the following:

$$ET_T = P \quad \text{for } P/L_T \leq 0.316$$

$$ET_T = P / \left[0.9 + \left(\frac{P}{L_T} \right)^2 \right]^{0.5} \quad \text{for } P/L_T > 0.316 \quad (7)$$

where $L_T = 300 + 25T + 0.05T^2$

where ET_T is the annual Turk actual evapotranspiration (mm year^{-1}), P is annual precipitation (mm year^{-1}), T is mean annual temperature ($^{\circ}\text{C}$) and L_T is the function of temperature (unitless).

The ET_o in Equations (1)–(5) was estimated using the ASCE-standardized method (former FAO-56) for short reference crop by the following function [2]:

$$ET_o = \frac{0.408\Delta(R_n - G) + \frac{\gamma u_2(e_s - e_a)C_n}{(T + 273.16)}}{\Delta + \gamma(1 + C_d u_2)} \quad (8)$$

where ET_o is the reference crop evapotranspiration (mm d^{-1}), R_n is net radiation at the crop surface ($\text{MJ m}^{-2} \text{d}^{-1}$), u_2 is mean daily wind speed at 2 m height (m s^{-1}), T is the mean daily air temperature ($^{\circ}\text{C}$), G is soil heat flux density at the soil surface ($\text{MJ m}^{-2} \text{d}^{-1}$), e_s is the mean daily vapor pressure (kPa), e_a is the mean daily actual vapor pressure (kPa), Δ is the slope of the saturation vapor pressure–temperature curve ($\text{kPa } ^{\circ}\text{C}^{-1}$), γ is the psychrometric constant ($\text{kPa } ^{\circ}\text{C}^{-1}$) and C_n and C_d are constants of 900 and 0.34, respectively.

2.2. Study Area and Data

The LOSW-ET methodology for estimating actual evapotranspiration and the comparison with the other methods of Oldekop, Coutagne and Turk was employed for the case of Greece. The analysis was based on climatic data, which were obtained from the following four databases:

- The database of Hijmans et al. [36] provides gridded data of mean monthly precipitation P and mean monthly temperature T for the period 1950–2000 (WorldClim version 1.2) at 30 arc-sec ($\sim 1 \times 1 \text{ km}$) spatial resolution. Their mean annual values are given in Figure 1a,b, respectively, and their frequency histograms in Figure 2a,b, respectively.
- The database of Aschonitis et al. [37] (10.1594/PANGAEA.868808) provides gridded data of mean monthly reference evapotranspiration ET_o (Equation (8)) of the period 1950–2000 at 30 arc-sec ($\sim 1 \times 1 \text{ km}$) spatial resolution (Figure 1c) (this database is built using temperatures from the WorldClim version 1.2 database). Using the ET_o (Figure 1c) and precipitation (Figure 1a) from the previous database, the irrigation map of the reference crop IR is built according to Equation (3) (Figure 1d). The frequency histograms of ET_o and IR are given in Figure 2c,d, respectively.
- The surface slope (Figure 1e) is obtained by the digital elevation model of GTOPO30 (pixel analysis of 30 arc-sec, $\sim 1 \times 1 \text{ km}$) as it is given by the USGS (United States Geological Survey). The frequency histogram of the slope is given in Figure 2e.
- The European Soil Database (ESDB) provided by the European Commission Joint Research Centre [38,39] provides soil data (% sand, % silt, % clay, % gravel, % organic carbon) with spatial analysis ($\sim 1 \times 1 \text{ km}$). These data are used to estimate the saturated hydraulic conductivity K_s according to the respective pedotransfer function (PTF) of Saxton and Rawls [40], taking into account the gravel and organic matter effect (Figure 1f). The frequency histogram of K_s is given in Figure 2f.

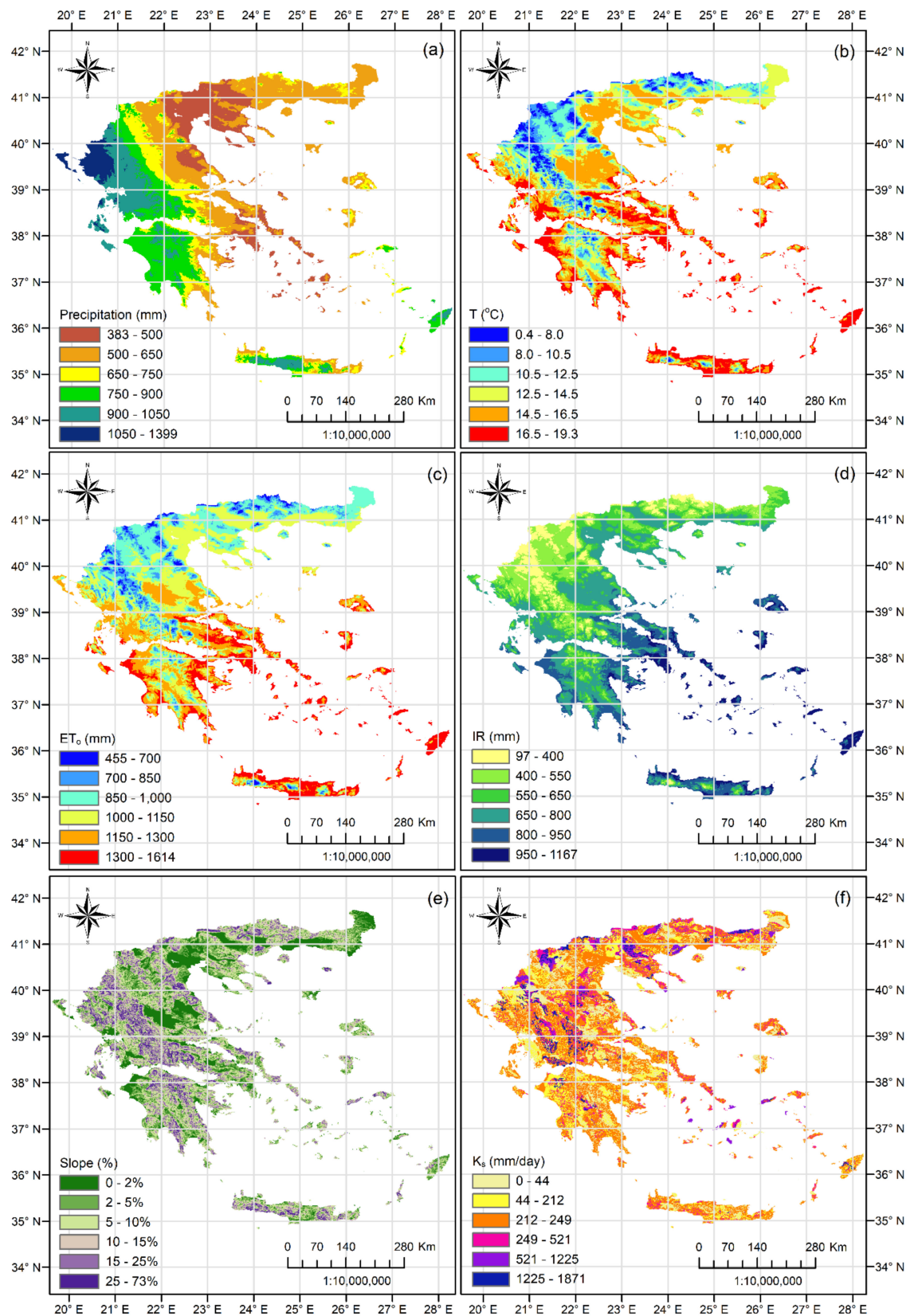


Figure 1. Mean annual values of (a) precipitation, (b) temperature, (c) reference evapotranspiration according to ASCE-standardized for short reference crops, (d) irrigation required for covering the deficit of annual reference evapotranspiration for the period 1950–2000, (e) surface slope and (f) saturated hydraulic conductivity in Greece.

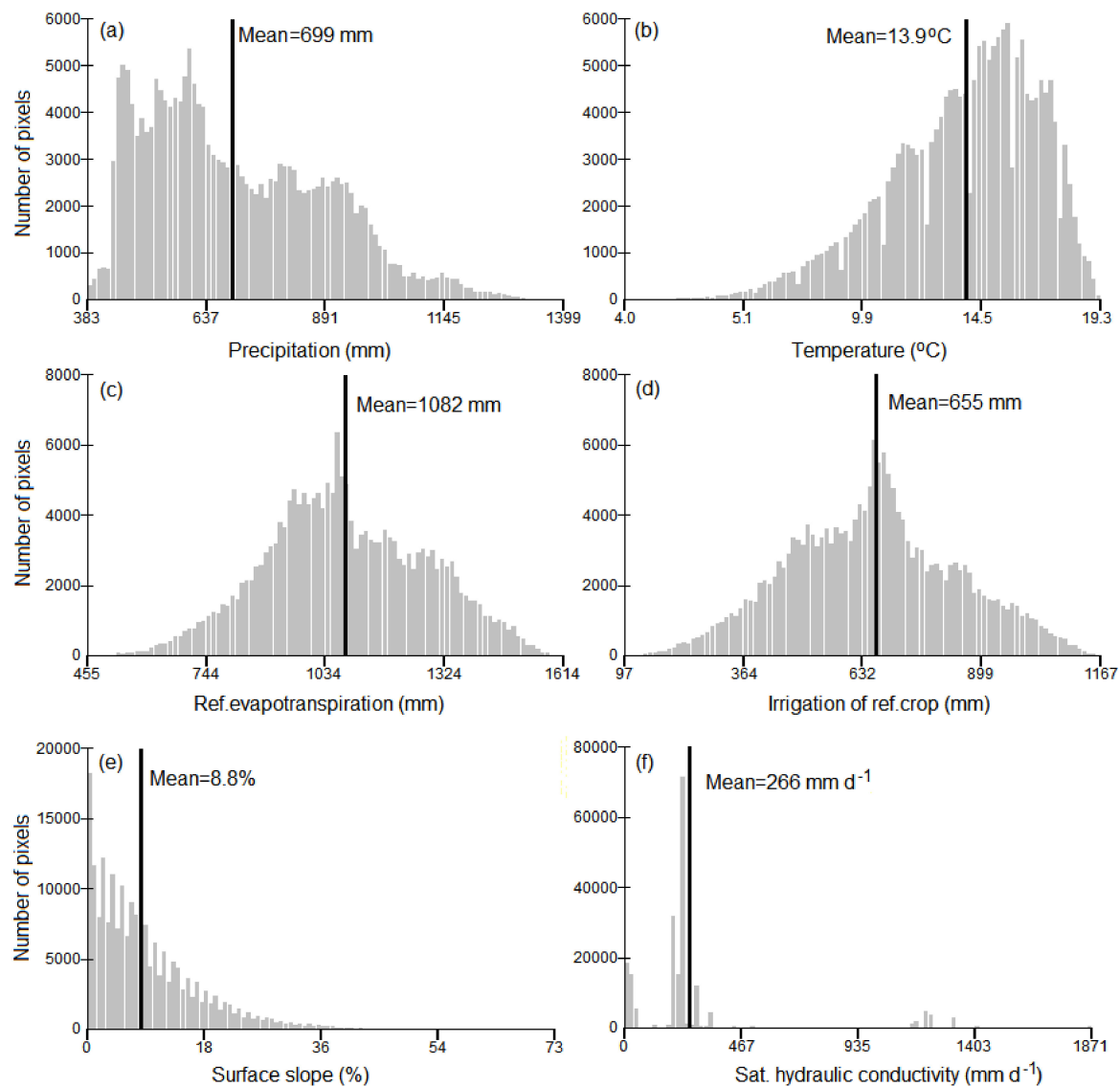


Figure 2. Histograms of mean annual values of (a) precipitation, (b) temperature, (c) reference evapotranspiration according to ASCE-standardized for short reference crops, (d) irrigation required for covering the deficit of annual reference evapotranspiration for the period 1950–2000, (e) surface slope and (f) saturated hydraulic conductivity based on the pixel values of the respective raster datasets of Figure 1.

3. Results

Taking into account Equation (4) (for $IR \neq 0$ and $IR = 0$), and Equations (5)–(7), the mean annual values of actual evapotranspiration based on $LOS\text{-}ET(IR \neq 0)$, $LOS\text{-}ET(IR = 0)$, ET_D , ET_C , and ET_T were estimated for the period 1950–2000 for the whole country of Greece (Figure 3a–e). The frequency histograms of their respective raster values are given in Figure 4a–e.

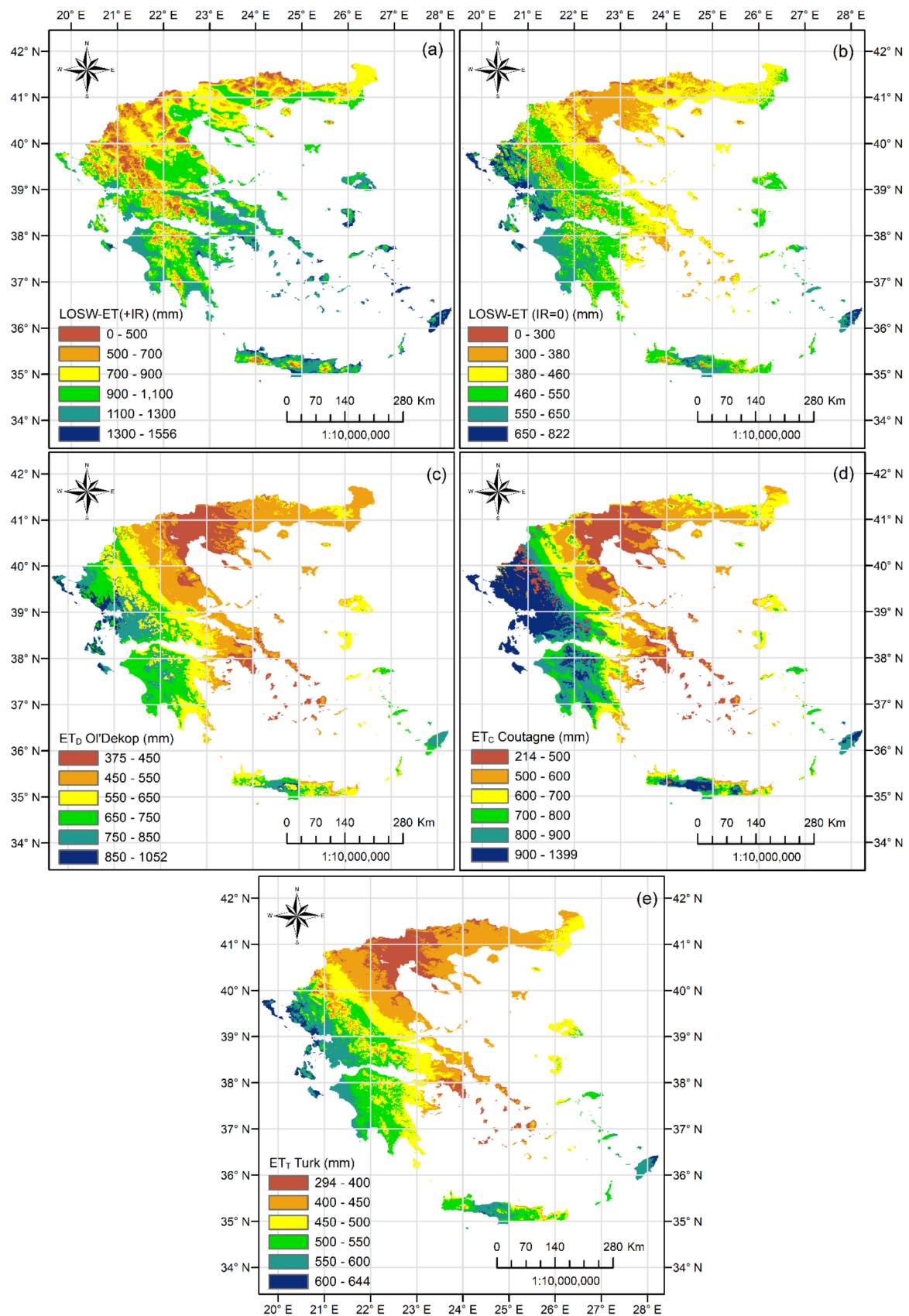


Figure 3. Mean annual actual evapotranspiration of (a) LOSW-ET with $IR \neq 0$, (b) LOSW-ET with $IR = 0$, (c) ET_D Oldekop, (d) ET_C Coutagne and (e) ET_T Turk for the period 1950–2000.

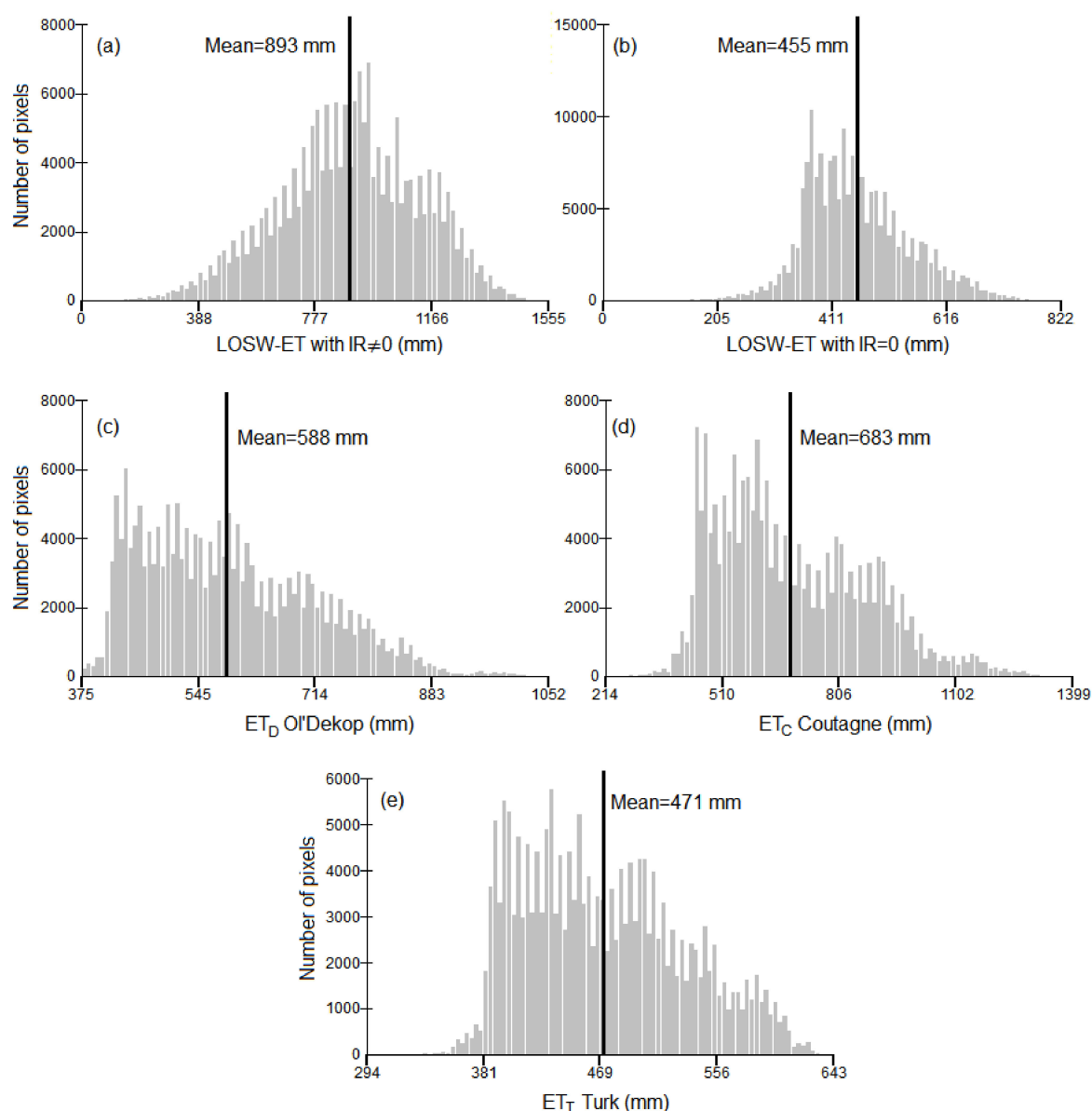


Figure 4. Frequency histograms of mean annual actual evapotranspiration of (a) *LOSW-ET* with $IR \neq 0$, (b) *LOSW-ET* with $IR = 0$, (c) ET_D Oldekop, (d) ET_C Coutagne, and (e) ET_T Turk for the period 1950–2000 based on the pixel values of the respective raster datasets of Figure 3.

As ET_D , ET_C and ET_T do not consider irrigation, they were compared with *LOSW-ET*($IR = 0$) using pedotransfer. The comparison was made in two ways. The first way was based on 1:1 plots (Figure 5a–c) between *LOSW-ET*($IR = 0$) vs. ET_D , ET_C and ET_T , respectively. The 1:1 plots were built using 15% of all pixels after random selection and exclusion of those with $K_s = 0$ (rocky areas). Linear trend lines and Spearman rank correlations were also determined (the given in the respective 1:1 plots). The second way was based on calculating the D difference in mm per year between the raster values of *LOSW-ET*($IR = 0$) and ET_D , ET_C and ET_T , respectively. The D difference of ET_D , ET_C and ET_T from *LOSW-ET*($IR = 0$) is given in the maps of Figure 6a–c, respectively. The respective frequency histograms of D raster values are given in Figure 7a–c. In the maps of Figure 6, the class of $-50 \text{ mm} < D < 50 \text{ mm}$ in the legends is considered the class where *LOSW-ET*($IR = 0$) is in good agreement with the ET_D , ET_C and ET_T methods because their mean annual difference is in the range of $\sim \pm 10\%$.

Taking into account the results of the 1:1 plots (Figure 5), D maps (Figure 6) and their histograms (Figure 7), it was observed that the actual evapotranspiration of Oldekop ET_D and Coutagne ET_C showed significantly higher values using $LOSW-ET(IR = 0)$. ET_D provided 29% greater values, while ET_C provided almost 50% greater values from $LOSW-ET(IR = 0)$ at the country level.

On the other hand, the comparison between $LOSW-ET(IR = 0)$ and the ET_T of Turk showed not only a good agreement at the country level based on their mean values ($\sim 3.5\%$ difference according to Figure 4b,e), but also a much better trend line and Spearman correlation (Figure 5c) compared to ET_D and ET_C . Further investigation of Figure 6c showed that 73% of the total country coverage had D values inside the range of ± 50 mm that corresponded to $\sim \pm 10\%$ mean annual difference. This is an extremely important finding since it shows that at least one of the three older actual evapotranspiration methods (ET_D , ET_C , ET_T) is in accordance with $LOSW-ET(IR = 0)$. Combining the results of Figure 6c with the maps given in Figure 1, it can be observed that D deviates from the range of ± 50 mm in regions where the surface slope is $> 10\%$ and in regions where annual ET_o is > 1200 mm with $P/L_T \geq 1$.

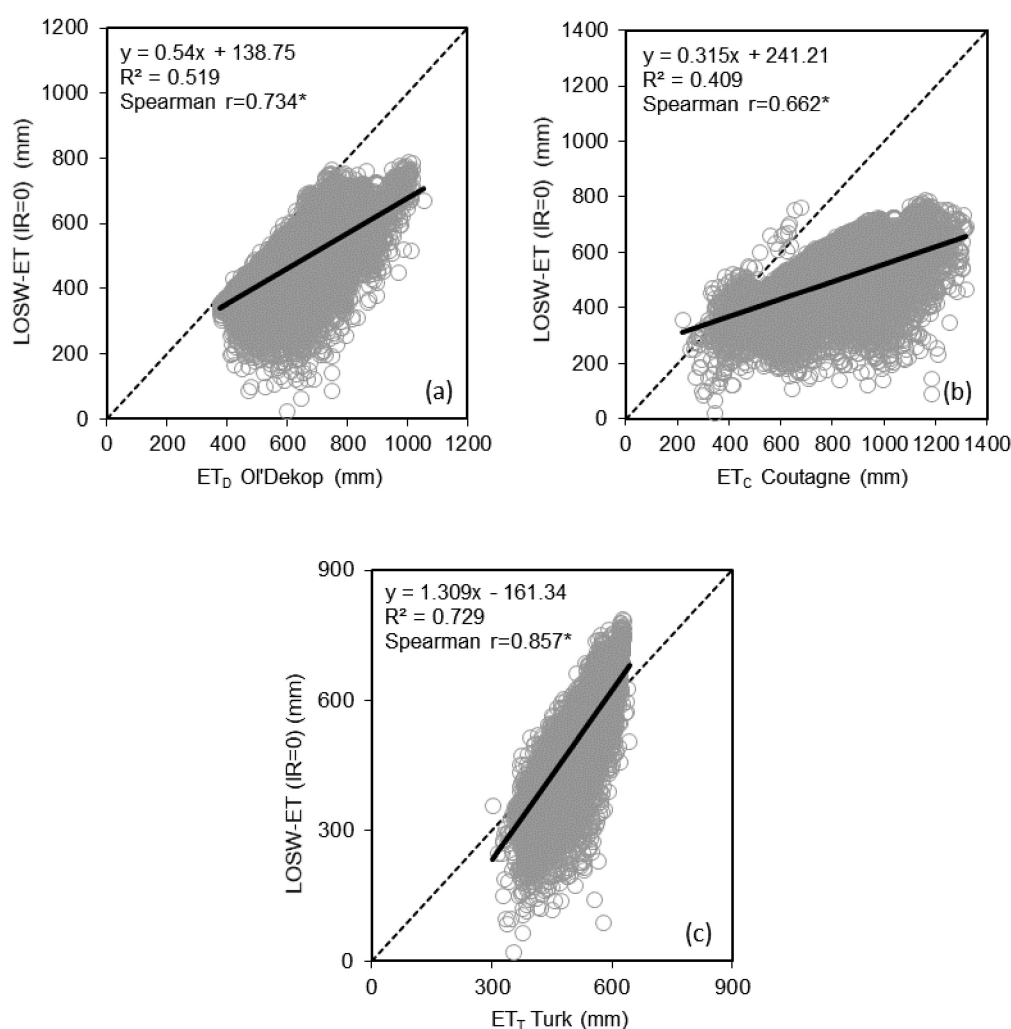


Figure 5. 1:1 plots between mean annual actual evapotranspiration of $LOSW-ET(IR = 0)$ versus (a) ET_D Oldekop, (b) ET_C Coutagne and (c) ET_T Turk for the period 1950–2000 (15% of random data selection and exclusion of regions with $K_s = 0$).

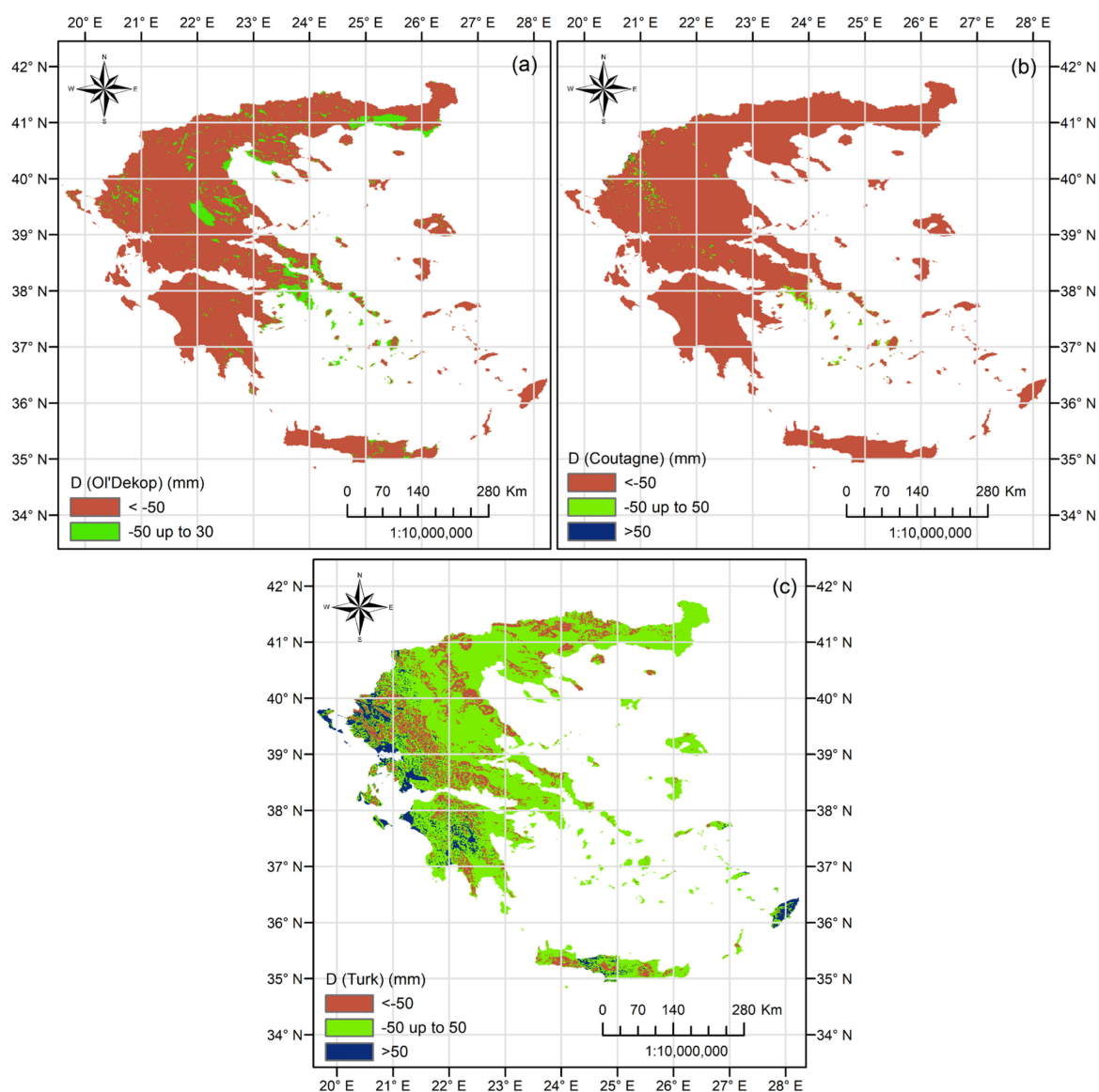


Figure 6. Mean annual difference D between $LOSW-ET(IR = 0)$ and (a) ET_D Oldekop, (b) ET_C Coutagne and (c) ET_T Turk for the period 1950–2000.

$LOSW-ET(IR \neq 0)$ can only be compared with ET_o as it describes the irrigated reference crop evapotranspiration, including the effect of soil, topography and soil moisture reduction between irrigation intervals (the last effect is embodied in the $LOSW-ET$ formula through its calibration with GLEAMS results). The 1:1 plot between $LOSW-ET(IR \neq 0)$ and ET_o is given in Figure 8. According to Figure 8, ET_o is always larger using $LOSW-ET(IR \neq 0)$ (21% larger at country level based on Figures 4a and 2c). The trend line and the Spearman correlation show a good correspondence between ET_o and $LOSW-ET(IR \neq 0)$. The smaller values of $LOSW-ET(IR \neq 0)$ compared to ET_o are absolutely justified by the effect of soil moisture reduction between the irrigation intervals used in GLEAMS model simulations (automated irrigation is applied when soil moisture reaches 20% of available water). This option of automatic irrigation is selected on purpose since it gives a more realistic reflection of the actual evapotranspiration of a reference crop under actual irrigated conditions and not theoretical conditions of constant soil moisture at field capacity. Thus, $LOSW-ET(IR \neq 0)$ is expected to always be lower than ET_o because it does not consider constant soil moisture conditions at field capacity.

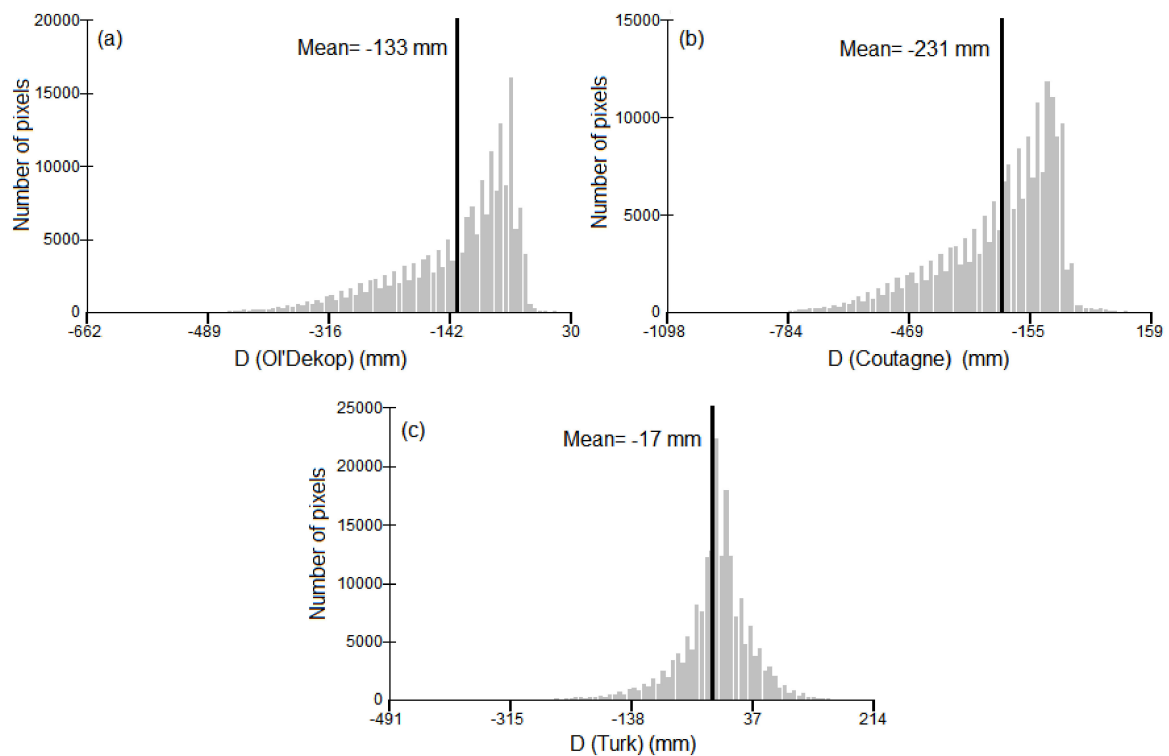


Figure 7. Frequency histograms of mean annual difference D between $LOSW-ET(IR = 0)$ and (a) ET_D Oldekop, (b) ET_C Coutagne and (c) ET_T Turk for the period 1950–2000.

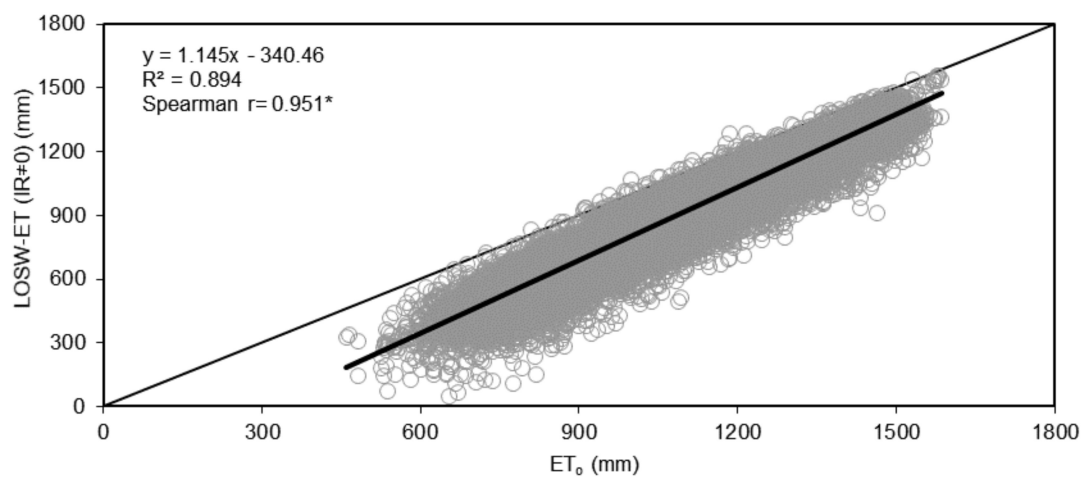


Figure 8. 1:1 plot between mean annual actual evapotranspiration of $LOSW-ET(IR \neq 0)$ versus ET_o for the period 1950–2000 (15% of random data selection and exclusion of regions with $K_s = 0$).

4. Discussion

4.1. Differences between Actual Evapotranspiration Methods

As shown in Figures 3–7, different methods of determining actual ET for $IR = 0$ can lead to extremely different results, which in many cases may seem unjustifiable. Before judging the validity of each method, it is crucial to understand that these differences may be the result of inevitable factors associated with the creator and the user, such as:

- (a) The creators used calibration data from different regions with extreme hydroclimatic differences that led to coefficients describing different attributes of hydroclimatic conditions.
- (b) Many of the methods were extremely old, and the accuracy and representativity of the data used for calibration were completely different when they were developed compared to the respective data provided nowadays. For example, the method of Oldekop is more than a century old, while most of the important methods, including Coutagne and Turk, are more than 50 years old.
- (c) The user may not apply the methods in the same way proposed by the creators. For example, the user may estimate the potential/reference evapotranspiration using a different method from the one used by the developer. For example, old methods had available data only for rainfall and temperature. Thus, potential evapotranspiration was mainly estimated using a temperature-based formula, e.g., the Thornthwaite method [41]. Nowadays, there is a vast amount of methods for estimating potential/reference evapotranspiration with limited or full data requirements depending on the data availability. This may be convenient but can also lead to differences not only between actual ET methods but also to differences between the results of the same actual ET method due to the use of a different ET_o method.

The above may justify the observed differences between actual ET methods in this study, but it is also crucial to note that even similar results between two ET methods may be the result of a counterbalanced effect of the aforementioned factors.

Regarding the comparison between $LOSW-ET(IR = 0)$ and ET_T , it was observed that D deviated from the range of ± 50 mm in regions where surface slope was $>10\%$, regions where annual ET_o was >1200 mm and $P/L_T \geq 1$ (Figure 6c). The negative values of $D < -50$ mm (i.e., $LOSW-ET(IR = 0) < ET_T$) were mostly observed in sloppy regions, which was probably due to the runoff compartment $Losw-R$ (Equation (2)) that pulled down actual evapotranspiration estimation by increasing runoff in higher slopes. The K_s parameter was not found to be a responsible driver of D deviation outside the range of ± 50 mm, apart from cases where $K_s \approx 0$ in very sloppy rocky areas where the high slope effect coincided with the K_s effect. The regions with positive D ($LOSW-ET(IR = 0) > ET_T$) greater than 50 mm (Figure 6c) were regions that had the common characteristics of $ET_o > 1200$ mm with $P/L_T \geq 1$, where almost half of annual precipitation and more than 10% of ET_o occurred during December–February according to the cluster maps [42–44] that were developed using the same datasets. Thus, these regions tended to present higher actual evapotranspiration during winter compared to other regions in Greece due to higher P and ET_o . If we assume that $LOSW-ET(IR = 0)$ is more correct from ET_T , then ET_T will probably require an additional module for environments with $P/L_T \geq 1$; otherwise, $LOSW-ET(IR = 0)$ needs improvements through recalibration with stations from the specific regions.

4.2. Inclusion or Noninclusion of Irrigation in Actual Evapotranspiration Methods

The application of the older actual evapotranspiration methods ET_D , ET_C and ET_T raises concerns about their use in regions/basins with a large percentage coverage by irrigated crops since they do not consider irrigation. In this case, the concept of $LOSW-ET$ provides the solution of the mixed model with the use of $LOSW-ET(IR = 0)$ for natural areas and nonirrigated agricultural lands and the use of $LOSW-ET(IR \neq 0)$ for irrigated lands. The only additional input, which is required for the mixed $LOSW-ET$ application, is a land cover map that can be obtained from various databases. An example of the mixed model use is given in Figure 9, where CORINE Land Cover 2018 was used to separate irrigated from nonirrigated lands in Greece (Figure 9a). Irrigated lands were considered in the LC (Land Cover) codes (212: permanently irrigated lands, 213: rice fields, 221: vineyards, 222: fruit trees and berry plantations), accounting for $\sim 9.6\%$ of the total country coverage. Other classes were not considered (e.g. 223: olive groves) because the irrigated portion was unknown. This was the same for the irrigated portion of vineyards (221). For this reason, the specific mixed model analysis is given as an example to stress the effect of a

large proportion of irrigated lands on actual evapotranspiration. The pixels of irrigated lands obtained the values of $LOS\text{-}ET(IR \neq 0)$ (Figure 3a), while the pixels of nonirrigated and natural lands obtained the values of $LOS\text{-}ET(IR = 0)$ (Figure 3b) in order to develop the final actual evapotranspiration map of the mixed $LOS\text{-}ET$ method (Figure 9b). The frequency histogram of mixed $LOS\text{-}ET$ raster values is given in Figure 9c. The mean annual value of the mixed $LOS\text{-}ET$ at the country level (Figure 9c) is about 10.7% larger than the respective $LOS\text{-}ET(IR = 0)$ (Figure 4b), highlighting a possible error in the calculation of actual evapotranspiration analogous to the portion of irrigated lands. If we consider that most of the applications are usually restricted in watersheds of significant rivers, which are hotspots of human presence and irrigated agriculture, then the expected errors of methods that do not consider the effect of irrigation is expected to be significant.

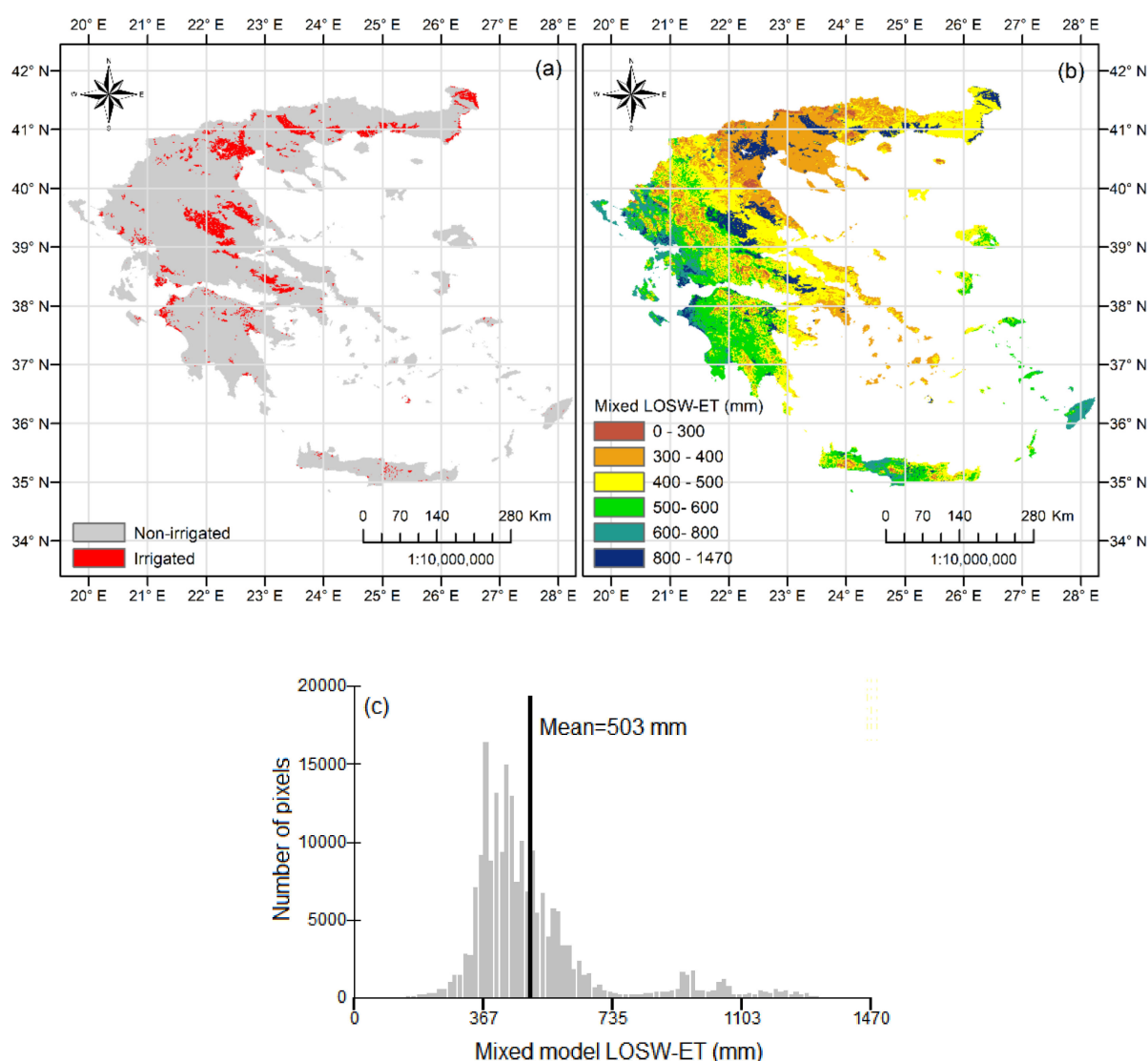


Figure 9. (a) Irrigated and nonirrigated lands in Greece according to CORINE 2018; (b) Mean annual actual evapotranspiration in Greece for the period 1950–2000 according to the mixed $LOS\text{-}ET$ concept; (c) Frequency histograms of mean annual actual evapotranspiration of mixed $LOS\text{-}ET$ based on the pixel values of the respective raster dataset of Figure 9b.

The use or non-use of the IR term in Equations (1) and (2) is regulated by the objectives of the user (e.g., for irrigated arable land or for nonirrigated land, and of course, for natural ecosystems). For the case of irrigated lands, $LOS\text{-}ET(IR \neq 0)$ could further be adapted in order to improve the estimation of actual evapotranspiration. For example, if the types of irrigated crops in a region and their irrigation period is known, then IR can be calculated

by Equation (3) only for the months of irrigation and also considering crop factors if they are available for the specific crops [45].

4.3. Possible Solutions for Validation

A basic limitation of the current study is the lack of validation of *LOSW-ET* with actual data. Since *LOSW-ET* is a method for estimating actual evapotranspiration, the most appropriate procedure would be to use actual evapotranspiration data. This option covering the full approach of *LOSW-ET* for various slopes and soil hydraulic properties under irrigation or no irrigation conditions is almost impossible from an experimental point of view since actual evapotranspiration is one of the most challenging parameters to measure, even with simple lysimeter conditions. An alternative way of validation would be to compare *LOSW-ET* results with the results of a distributed hydrological model (e.g., MIKE or SWAT) for a basin after being calibrated with actual values of runoff and if it is possible with additional values of percolation indirectly estimated by measurements of groundwater table variation.

5. Conclusions

The method of *LOSW-ET* extends the concept of actual evapotranspiration by including various dimensions of natural ecosystems such as soil and topography but also the dimension of irrigation in agricultural lands. The case of *LOSW-ET* ($IR \neq 0$) also extends the concept of reference crop evapotranspiration ET_o , which is basically a climatic parameter providing a more realistic estimation of the maximum evapotranspiration that can be achieved by taking the soil-topographic characteristics and the effect of soil moisture variation between realistic irrigations into consideration.

The overall approach, and especially in the case of mixed *LOSW-ET*, seems promising since it can reduce the possible errors of simplistic formulas of actual evapotranspiration when they are used in basins where irrigated agriculture is dominant. Future studies could focus on evaluating the individual or mixed *LOSW-ET* approaches at basin scale using a deterministic distributed or semidistributed hydrological model.

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1. <https://www.worldclim.org/>
2. <https://doi.pangaea.de/10.1594/PANGAEA.868808>
3. <https://earthexplorer.usgs.gov/>
4. <https://esdac.jrc.ec.europa.eu/content/european-soil-database-derived-data>

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