

Review



# A Review and Experimental Revisit of Alternative Catalysts for Selective Oxidation of Methanol to Formaldehyde

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**Abstract:** The selective oxidation of methanol to formaldehyde is a growing million-dollar industry, and has been commercial for close to a century. The Formox process, which is the largest production process today, utilizes an iron molybdate catalyst, which is highly selective, but has a short lifetime of 6 months due to volatilization of the active molybdenum oxide. Improvements of the process's lifetime is, thus, desirable. This paper provides an overview of the efforts reported in the scientific literature to find alternative catalysts for the Formox process and critically assess these alternatives for their industrial potential. The catalysts can be grouped into three main categories: Mo containing, V containing, and those not containing Mo or V. Furthermore, selected interesting catalysts were synthesized, tested for their performance in the title reaction, and the results critically compared with previously published results. Lastly, an outlook on the progress for finding new catalytic materials is provided as well as suggestions for the future focus of Formox catalyst research.

Keywords: formaldehyde; Formox; selective oxidation; methanol; molybdenum

# 1. Introduction

Formaldehyde (FA), H<sub>2</sub>CO, is the lightest of the aliphatic aldehydes and is present in low concentrations in nature since it is an important product in the metabolism of plants and animals. Furthermore, FA is formed from organic material by photochemical processes in the atmosphere, as well as by incomplete combustion [1].

FA is the most commercially important aldehyde as it is an irreplaceable  $C_1$  building block for higher-valued products due to its high reactivity [2].

The high reactivity means that pure anhydrous FA polymerizes to solid paraformaldehyde when the gas temperature is below 100 °C. The polymerization is accelerated by traces of polar compounds. FA is, therefore, commercially sold as an aqueous solution called formalin (typically 37 wt%). In this solution, monomeric FA may react with water to form a hydrate, which reacts further with FA to form solid polyoxymethylenes; thus methanol (MeOH) and other stabilizers are added to concentrated formalin solutions (37–57 wt%) [1].

The main usage of FA and its polymers is the production of resins such as ureaformaldehyde, phenol-formaldehyde, and melamine-formaldehyde resins, which are used in wood products applied in the construction industry (e.g., plywood) [3], as well as adhesives [2] and plastics [4]. Lastly, FA plays an integral role in various other industries such as automotive, aviation, textile, and energy as well as being an indispensable antibacterial agent in various personal hygiene consumer products [4].

FA was first synthesized in 1859 by Butlerov [1], with commercial production from MeOH in Germany starting in 1889 [1,5]. Global production has grown to more than 50 million metric tons formalin per year with an expected production of more than 60 million metric tons per year in the late 2020s [6]. Its global market value is expected to grow with about 6% per year [7].



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**Copyright:** © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). As mentioned above, FA has been produced commercially since 1889 [1,5]. Today there are three different processes used industrially, i.e., the silver process, the BASF process, and the Formox process. The first two utilize Ag catalysts, and the last utilizes a metal oxide catalyst. In addition to the industrial processes, other reaction pathways such as photocatalytic oxidation of MeOH [8], partial oxidation of MeOH in supercritical CO<sub>2</sub> [9], liquid phase partial oxidation of MeOH [10], hydroboration of CO<sub>2</sub> to FA [11], selective homogeneous one-step reduction of CO<sub>2</sub> to FA [12], oxidation of methane to MeOH and FA [13], selective oxidation of methanol using N<sub>2</sub>O as oxidant [14], and partial oxidation of S containing volatile organic compounds [15] have also received research interest.

The Ag catalyst processes usually operate at ambient pressure, with temperatures of 600-720 °C and excess MeOH. The conversion of MeOH to FA occurs through three main reactions (Reactions (1)–(3)) [1].

$$\begin{array}{l} \mathrm{CH}_{3}\mathrm{OH}(\mathrm{g}) \end{array} \rightleftharpoons \mathrm{CH}_{2}\mathrm{O}(\mathrm{g}) + \mathrm{H}_{2}(\mathrm{g}) \\ \Delta H^{\mathrm{o}}_{298 \mathrm{\ K}} = 84 \frac{\mathrm{kJ}}{\mathrm{mol}} \end{array} \tag{1}$$

$$H_2(g) + \frac{1}{2}O_2(g) \rightleftharpoons H_2O(g)$$

$$\Delta H_{298 K}^o = -243 \frac{kJ}{mol}$$
(2)

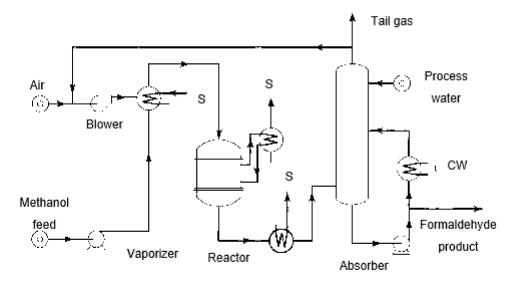
$$CH_{3}OH(g) + \frac{1}{2}O_{2}(g) \rightleftharpoons CH_{2}O(g) + H_{2}O(g)$$

$$\Delta H_{298 \text{ K}}^{o} = -159 \frac{\text{kJ}}{\text{mol}}$$
(3)

Depending on the process, the operating temperature may be 650–720 °C with a conversion of 97–98% with no MeOH recovery (BASF process) or 600–650 °C and 77–87% single pass conversion with MeOH recovery through a distillation unit. The yields of the processes are 86.5–90.5% and 87–92%, respectively [1,16].

The metal oxide process (Formox) utilizes an iron molybdate catalyst (FeMo). In contrast to the Ag processes, where the formation of MeOH can happen by endothermic dehydrogenation (Reaction (1)), the formation of FA in the Formox process only occurs by oxidative dehydrogenation (Reaction (3)). The Formox process runs under ambient pressure, temperatures of 250-400 °C, excess of air, and MeOH conversions above 99%, with a yield between 88 and 92% [1,16]. In a typical Formox plant (Figure 1), MeOH is added to air and recycled product gas in an evaporator before it is fed to the reactor. The product stream is then cooled, and FA is absorbed in H<sub>2</sub>O in an absorber yielding the FA product, typically 37 wt% FA in H<sub>2</sub>O (formalin), but it can be up to 55 wt% FA and less than 1 wt.% MeOH in the bottom where a fraction of it is cooled and recycled back into the absorber. The product is fed through an anion-exchange column in order to reduce the amount of HCOOH. The tail gas leaves the top of the tower, and part of it is recycled and mixed with the air feed before entering the evaporator. The feed composition is kept on the MeOH lean side of the explosive limit. Recycling tail gas decreases O<sub>2</sub> content in the feed gas to around 10 mol% and adds H<sub>2</sub>O from the absorber [16]. The MeOH concentration in the feed has increased from 6.5 mol% in the 1960s to around 10 mol% after various process improvements [17]. The reactor is a multi-tube reactor, which is cooled by a fluid (typically oil) with a high boiling point, which produces steam in a heat exchanger to condense heat-transfer fluid. The reactor tubes are between 1 and 1.5 m long, and the outer shell diameter of the multi-tube reactor is >2.5 m [16].

The choice of process depends on various factors such as operating and capital cost, but it also depends on plant capacity, type of operation, and end product usage [1,16]. However, due to the increase in MeOH price from 125 euro/tonnes in January 2002, to 330 euro/tonnes in October 2017, with peak prices as high as 525 euro/tonnes [18], the market share has moved towards the Formox process due to its higher selectivity and yield. Thus, the global share of the produced FA from the Formox process is now around two thirds [19].



**Figure 1.** Process diagram of typical Formox process plant. S = steam; CW = cooling water. Copyright © (2013) by John Wiley & Sons, Inc. [16].

#### 2. Literature Survey

In 1921, the oxidation of MeOH to FA was first patented on a metal oxide (V oxide) and later in 1933 on Fe-Mo oxide, where the first commercial plant using FeMo was in operation by 1952. Since then, FeMo has become the most used catalyst in the Formox process. The main disadvantage for the Formox process stems from the deactivation of the FeMo catalyst, where Mo vaporizes in the front-end of the bed and deposits further down resulting in increasing pressure drop and an expensive change of catalyst every 6–18 months [20].

Before looking into possible methods for solving/remedying the problem, an understanding of the FeMo catalyst as well as knowledge about the reaction conditions and mechanism is needed, which is provided in the following section.

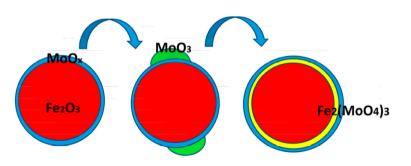
#### 2.1. Iron-Molybdenum Catalysts

# 2.1.1. Structure

The industrial catalyst consists of iron (ferric) molybdate  $Fe_2(MoO_4)_3$  with a surplus of MoO<sub>3</sub>. Thus, the main component of the catalyst is the bulk stoichiometric  $Fe_2(MoO_4)_3$ . A study by Abaulina et al. [21] on an industrial catalyst found the structure of the catalyst to be an Fe deficient  $Fe_2(MoO_4)_3$  structure with MoO<sub>3</sub> in the voids.

To understand the surface of the FeMo catalyst, a number of studies have been performed on catalysts with excess Fe<sub>2</sub>O<sub>3</sub>. Chapman et al. [22] studied a core-shell type  $MoO_x/Fe_2O_3$  (MoO<sub>x</sub> shell and Fe<sub>2</sub>O<sub>3</sub> core) catalyst doped and not doped with Al. The catalysts were investigated by X-ray photoelectron spectroscopy (XPS), which showed surface Mo enrichment for both samples. An amorphous surface layer of  $MoO_3$  was found by X-ray absorption near edge spectroscopy (XANES) on a Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> sublayer, which increased with Mo impregnation in the investigated range (1–6 monolayers (ML)). This was confirmed by using other techniques such as Raman, extended X-ray absorption fine structure spectroscopy (EXAFS), attenuated total reflectance infrared spectroscopy (ATR-IR) and X-ray diffraction (XRD) spectroscopy [22]. Brookes et al. [23–25] similarly found that octahedral Mo units, different from the tetrahedral MoO<sub>4</sub> sub-units of bulk Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, were at the surface at all times. Moreover, characterization by Uhlrich et al. [26] of Mo deposited onto  $Fe_2O_3$  thin films (app. 5 ML of  $Fe_2O_3$ ) on Pt(111) showed Mo concentration to be larger in the surface layers compared to the lower crystal layers (unless annealed at >627 °C). At low temperatures, the iron oxide film was covered by Mo=O terminated Mo oxide nano-particles. If the thin films were oxidized at temperatures above 627 °C, the Mo migrated into the surface layers of the iron oxide but retains iron oxide

structure [26]. House et al. [27] also observed the segregation of Mo to the surface by scanning transmission electron microscopy (STEM) on a stoichiometric FeMo catalyst prepared by co-precipitation. A simplified schematic of the structure of the catalyst was proposed by Brookes et al. [28], summing up the findings in the literature, as a function of annealing temperature (Figure 2). The schematic was in agreement with the other findings regarding the structure of the catalysts with excess Fe<sub>2</sub>O<sub>3</sub> mentioned above. However, the industrial catalyst has MoO<sub>3</sub> in excess.



**Figure 2.** Evolution of the surface structure of 3 ML MoO<sub>3</sub> deposited on Fe<sub>2</sub>O<sub>3</sub> catalyst as function of the annealing temperature. Left: Structure at 120 °C. Middle: Structure at 400 °C. Right: Structure at 500 °C. (red) Fe<sub>2</sub>O<sub>3</sub>; (blue) amorphous layer of MoO<sub>x</sub>; (green) MoO<sub>3</sub> nano-crystallites; (yellow) Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> [28]. Reproduced from [28] Copyright 2016, MDPI.

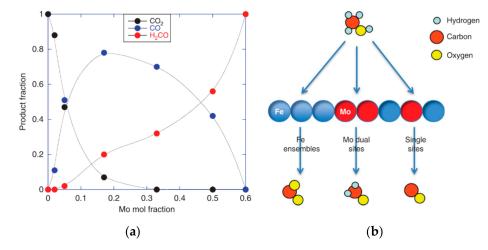
Routray et al. [29] investigated the synergistic effect between MoO<sub>3</sub> and Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> on the catalytic oxidation of MeOH to FA and found, using low-energy ion scattering (LEIS), it to arise from excess MoO<sub>3</sub> forming a surface MoO<sub>x</sub> layer covering all the originally exposed Fe sites present in the surface layer of stoichiometric bulk Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>. When the Mo/Fe ratio increased further, an increase in the amount of observed crystalline MoO<sub>3</sub> phase was observed in addition to the surface layer [29]. The structure starting from Fe<sub>2</sub>O<sub>3</sub> in excess had a core of Fe<sub>2</sub>O<sub>3</sub> with a layer of Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> around it, with an amorphous layer of MoO<sub>3</sub> on top. When the Mo/Fe ratio increased, the core of Fe<sub>2</sub>O<sub>3</sub> decreased while the layer of Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> increased in thickness until Mo/Fe = 1.5, where the core Fe<sub>2</sub>O<sub>3</sub> disappeared and only Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> with the amorphous MoO<sub>3</sub> on top remained. When the Mo/Fe ratio further increased, the formation of crystalline MoO<sub>3</sub> increased. These observations are supported by Bowker et al. [30].

## 2.1.2. The Active Site

Bowker et al. [31] determined the changes in the FA selectivity by the addition of Mo to  $Fe_2O_3$  so that catalysts with a Mo/Fe < 1.5 were synthesized. The selectivity changed from pure  $CO_2$  as product over  $Fe_2O_3$  at low Mo loadings, to CO as the main product at intermediate Mo loadings, and to FA at high Mo loadings (Figure 3a). These observations, taken together with the evolution of Fe ensembles, Mo dual sites, and Mo single sites, resulted in the proposal of Mo dual sites being responsible for the formation of FA while Fe ensembles made  $CO_2$  and Mo single sites CO (Figure 3b).

The effects of surface Mo was further investigated by Bowker et al. [32] by addition of Mo oxide to  $Fe_2O_3$  and performing diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS) during temperature programmed oxidation/reduction (TPO/TPR) experiments. On the pure  $Fe_2O_3$ , MeOH adsorbed as methoxy groups and was oxidized to formate at around 200 °C, which then desorbed as  $CO_2$ . When a ML of molybdena had been formed on the hematite, the formate formation was blocked and formaldehyde became the main gas phase product from temperature programmed desorption (TPD) after MeOH adsorption [32]. This was supported by the earlier work by Bowker et al. [33] measuring the activity of the FeMo component oxides. The dual Mo sites for the FA formation was in agreement with previous studies [34–37]. Bowker et al. [38,39] also established the importance of the surface Mo being in the +6 oxidation state as they found MoO<sub>2</sub>

and surface reduced  $MoO_3$  to be most selective towards CO, whereas  $MoO_3$  and surface oxidized bulk  $MoO_2$  ( $MoO_3$  surface layer) primarily yielded FA. It was furthermore stated by Trifiró et al. [40] that the Mo needed to have octahedral coordination to be active and selective, where both octahedral and tetrahedral coordination is possible for +6 oxidation state depending on the compound.



**Figure 3.** (a) Yields of CO, CO<sub>2</sub>, and FA from MeOH oxidation observed in TPD vs. Mo fraction in the catalyst (Mo mole fraction of 0.6 corresponds to  $Fe_2(MoO_4)_3$ ) [31]. (b) Model of the active sites on Fe-Mo oxide materials showing the variation in products from different site ensembles proposed by Bowker et al. [31]. Reproduced from [31] Copyright 2015, with permission from Taylor and Francis.

Dias et al. [41] investigated the role of suprastoichiometric Mo in the FeMo catalyst during MeOH oxidation to FA by the addition of surface Mo to  $Fe_2(MoO_4)_3$  until a maximum of five MLs of MoO<sub>3</sub>. Crystalline MoO<sub>3</sub> was not observed for any of the samples. All the samples showed a surface enrichment of Mo, and the addition of surface Mo was claimed to promote surface aggregation of Mo species, which was already observed for the stoichiometric molybdate before Mo addition. A higher yield of FA was achieved with loadings higher than 0.5 ML. Catalytic performance was concluded to be a cooperative effect between the high selectivity but low activity of MoO<sub>3</sub> and the high activity of  $Fe_2(MoO_4)_3$  [41].

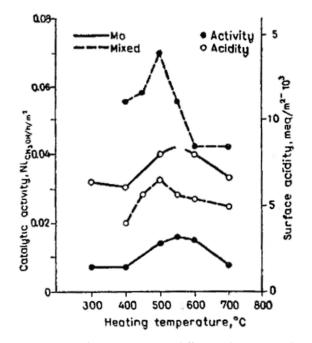
Hummadi et al. [42] proposed Fe to be an activity promoter, where the important feature in the Fe(III) molybdate catalysts was the presence of -O-Mo-O-Fe-O-Mo-O- groups, which were found in Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, and Fe<sup>3+</sup> finely dispersed in MoO<sub>3</sub>. This was in opposition to the work conducted by Bowker et al. [31], who found two Mo side by side to be the important feature. For higher Fe(III) concentrations, Hummadi et al. [42] found that patches of iron oxide or particles result in selectivity loss due to iron oxide catalyzing the total combustion of MeOH [42].

Taking these considerations together, the excess of Mo compared to Fe is important for ensuring that there is an amorphous overlayer of  $MoO_x$  on the surface. The overlayer ensures firstly that there are no Fe ensembles at the surface, which makes  $CO_2$ , and secondly that the surfaces are covered by Mo–Mo sites, which are selective for oxidation to formaldehyde. Fe acts as an activity promoter. This is in agreement with work conducted by the authors of [43], who found FA selectivity to stay high even when most of the Mo was gone, as there was still a surface layer of  $MoO_x$ .

#### 2.1.3. Influence of Catalyst Acidity/Basicity on Reaction Pathways

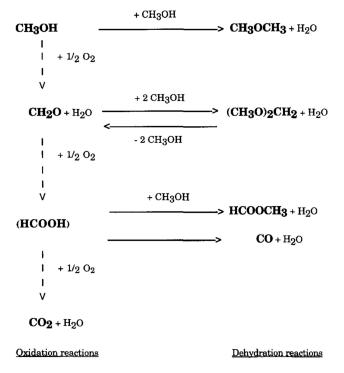
Pernicone et al. [44] found a correlation between the surface acidity and the activity for  $MoO_3$  and  $MoO_3$ -Fe<sub>2</sub>( $MoO_4$ )<sub>3</sub> (Figure 4). They proposed the surface acidity to be of the Brønsted type and suggested that an active catalyst needed to be Fe defective (have a small

excess of Mo), as they observed a steep decline in catalyst activity with Mo/Fe < 1.7, or that  $Fe_2(MoO_4)_3$  had a promoting effect on MoO<sub>3</sub> [44].



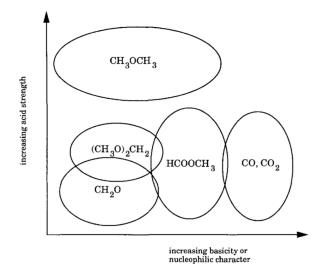
**Figure 4.** Catalytic activity in a differential reactor and surface acidity of pure  $MoO_3$  and mixed 2.5: 1  $MoO_3$ -Fe<sub>2</sub>( $MoO_4$ )<sub>3</sub> catalysts versus calcination temperature [44]. Reproduced from [44] copyright (1968) with permission from copyright holder.

The formation of FA comes from MeOH oxidation. However, FA is not the only possible product from MeOH and  $O_2$  over a catalyst. Tatibouët [45] proposed a scheme of the reaction pathways for MeOH oxidation/dehydration (Figure 5) [45].



**Figure 5.** Scheme showing the reaction pathways for MeOH conversion via either oxidation or dehydration reactions. Reprinted from [45] Copyright © 1997 with permission from Elsevier.

Part of the challenge is to stop oxidation after the first oxidative step and to prevent forming any of the dehydration products. Additionally, Tatibouët [45] mapped the products with respect to the catalyst's acid-base properties, which provided a simplified scheme as shown in Figure 6.



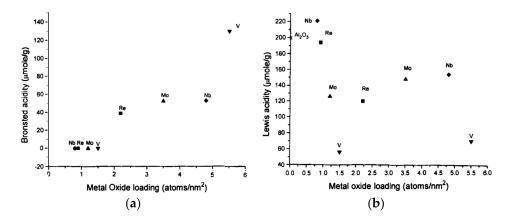
**Figure 6.** Rough sketch of the main reaction products as function of the acid-base character of the catalyst. Reprinted from [45] Copyright © (1997) with permission from Elsevier.

Ivanov and Dimitrov [46] published an extension to the reaction scheme proposed by Tatibouët [45]. They found that independent oxidation reactions of DME took place on an industrial FeMo catalyst, producing FA, CO, and CO<sub>2</sub> (which they stated were not an oxidation product from FA), and that CO could not be oxidized to CO<sub>2</sub> in the relevant temperature range by the FeMo catalyst.

The influence of the catalyst's acid-base properties on MeOH oxidation in vapor-phase was investigated by Ai [47] over a series of composite oxide catalysts such as MoO<sub>3</sub>-TiO<sub>2</sub>, MoO<sub>3</sub>-Fe<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub>-SnO<sub>2</sub>, MoO<sub>3</sub>-P<sub>2</sub>O<sub>5</sub>, MoO<sub>3</sub>-Bi<sub>2</sub>O<sub>3</sub>-P<sub>2</sub>O<sub>5</sub>, V<sub>2</sub>O<sub>5</sub>-MoO<sub>3</sub>, WO<sub>3</sub>-based and U<sub>3</sub>O<sub>8</sub>-based oxides, SnO<sub>2</sub>-K<sub>2</sub>O, Co<sub>3</sub>O<sub>4</sub>-K<sub>2</sub>O, and Bi<sub>2</sub>O<sub>3</sub>-X<sub>n</sub>O<sub>m</sub> where X = P, Mo, W, V, and S. FA was obtained from acidic oxides such as MoO<sub>3</sub>, WO<sub>3</sub>, V<sub>2</sub>O<sub>5</sub>, and U<sub>3</sub>O<sub>8</sub>. However, from more basic oxides such as TiO<sub>2</sub>, Fe<sub>2</sub>O<sub>3</sub>, SnO<sub>2</sub>, Bi<sub>2</sub>O<sub>3</sub>, ZnO, and Co<sub>3</sub>O<sub>4</sub>, FA was not obtained, and selectivity was towards full oxidation to CO<sub>2</sub>. In general, selectivity decreased for FA and increased for CO<sub>2</sub> with an increase in basicity. A more or less linear correlation between acidity and activity for FA formation was found for V<sub>2</sub>O<sub>5</sub> and MoO<sub>3</sub> containing catalysts with only small amounts of by-products, with the exception of MoO<sub>3</sub>/SnO<sub>2</sub>, which had high production of by-products [47].

Nikolenko et al. [48] recently investigated the adsorption of organic compounds (1-napthylamine; *N*,*N*-dimethylaniline; m-toluidine; pyridine-3-aldehyde; aniline; 2,8-dimethylquinoline; pyridine; 2-picoline) on Fe<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub>, and Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> and found that they were adsorbed by surface hydrogen bonds. The adsorption propensity of organic bases was linearly correlated with the effective charge on nitrogen atoms giving the order Fe<sub>2</sub>O<sub>3</sub> > MoO<sub>3</sub> > Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>. This resulted in the proposal stating that methanol and formaldehyde were adsorbed by oxygen atoms to Lewis acid sites or that the atoms in the C-H bonds interacted with the Lewis basic centers for MeOH oxidation reactions. The good selectivity of the FeMo catalyst was concluded to arise from low adsorption of intermediate products in MeOH oxidation [48].

The dependence of active metal loading on an  $Al_2O_3$  carrier on Brønsted and Lewis acidity was described by Wachs [49]. Brønsted acidity increased with metal loading on the surface (Figure 7a). For Lewis acidity, no apparent trend with metal loading was visible (Figure 7b) [49]. The acidity did not seem to be related to the coordination of the surface metal, as Re possessed 4-fold coordination at all coverages and had both 4-fold and 6-fold coordination at high coverages [49].



**Figure 7.** Dependence of (**a**) Brønsted and (**b**) Lewis acidity on metal loading on Al<sub>2</sub>O<sub>3</sub> support. Reprinted from [49] Copyright © (1996) with permission from Elsevier.

The knowledge of the influence of acidity and basicity may be used as a tool to direct preparation if a catalyst is not sufficiently selective, since the by-products may be able to inform the direction in which the acid-base properties of the catalyst should be modified.

### 2.1.4. Reaction Mechanism and Kinetics

As discussed in the Introduction, the formation of FA over the FeMo catalyst occurs by an overall oxidative dehydrogenation reaction, Reaction (4).

$$CH_{3}OH(g) + \frac{1}{2}O_{2}(g) \leftrightarrows CH_{2}O(g) + H_{2}O(g)$$

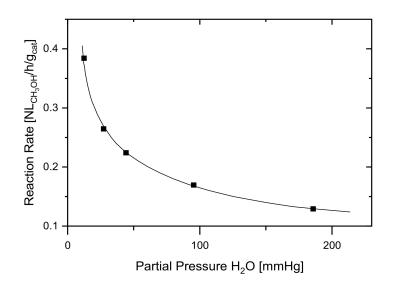
$$\Delta H_{298 K}^{o} = -159 \frac{kJ}{mol}$$
(4)

This section describes the reaction kinetics and reaction mechanism of the FA formation. The effect of H<sub>2</sub>O on the formation of FA from MeOH was investigated by Pernicone et al. [50]. H<sub>2</sub>O strongly inhibited the reaction rate of MeOH formation (Figure 8). The effect was explained by the authors to arise from competitive adsorption between H<sub>2</sub>O and MeOH on the catalyst [50]. It should be noted that this study was conducted at a rather low temperature (232 °C), and the inhibiting effect of water is expected to be lower at higher and industrially relevant temperature.

The reaction kinetics and mechanisms were further investigated by Pernicone et al. [51] in the temperature range of 180–280  $^{\circ}$ C. The reaction was inhibited by H<sub>2</sub>O and by FA (although not as much), which was in agreement with their conclusion that reaction product desorption was the rate determining step at these temperatures. Under industrial conditions, the inhibition from formaldehyde desorption is, thus, very low in agreement with the selectivity towards FA being very high. Recent density functional theory (DFT) calculations showed that FA does not adsorb strongly [52]. Furthermore, the reaction rate was independent of reactant partial pressures (zero order kinetics) above 100 mmHg for both methanol and oxygen, when the other reactant (MeOH and O<sub>2</sub>, respectively) was kept constant at 180 mmHg. The results showed first order kinetics in both MeOH and O<sub>2</sub> below 100 mmHg. The catalyst formed the same reaction products with and without  $O_2$  in the feed. This indicates that the reaction is of the Mars van Krevelen type where the catalyst supply lattice oxygen for the reaction and is subsequently re-oxidized by gaseous O<sub>2</sub> [51]. Those findings were further supported by the same group with work in a pulse micro-reactor [53]. The effect of H<sub>2</sub>O vapor on the kinetics of MeOH oxidation was also investigated by Holstein and Machiels [54] in a continuous flow reactor with external recycling at temperatures between 200 and 300  $^{\circ}$ C. Here, the kinetics were found to be well described by a power rate law expression as in Equation (5):

$$r = k P_{\text{MeOH}}^{x} P_{\text{O}_{2}}^{y} P_{\text{H}_{2}\text{O}}^{z}$$
(5)

where  $x = 0.94 \pm 0.06$ ,  $y = 0.10 \pm 0.05$ , and  $z = -0.45 \pm 0.07$ . H<sub>2</sub>O was suggested to inhibit the reaction by kinetic coupling, meaning that H<sub>2</sub>O adsorbs dissociatively as surface OH\* groups, which is in competition with the dissociative adsorption of MeOH to hydroxy and methoxy groups. Site blocking by non-dissociative H<sub>2</sub>O adsorption was dismissed at temperatures above 200 °C, as the adsorption energy was too low to compete with MeOH; however, it should be taken into consideration at lower temperatures. The reaction rate was found to be independent of FA partial pressure [54]. This was in contrast with Pernicone et al. [51] who found FA to inhibit the reaction rate, however, at lower temperatures. Drăgan and Kulic [55] also reported FA to significantly lower than MeOH oxidation rate; however, they added FA by bubbling an air stream through a 38% FA solution and did not comment on H<sub>2</sub>O inhibition nor on the removal of H<sub>2</sub>O from the feed when adding FA; hence, the measured inhibition was most likely from H<sub>2</sub>O.



**Figure 8.** Influence of H<sub>2</sub>O partial pressure on the rate of MeOH oxidation. T = 232 °C;  $P_{tot} = 920 \text{ mmHg}$ ;  $P_{O_2} = 180 \text{ mmHg}$ ;  $P_{CH_3OH} = 180 \text{ mmHg}$ . Reproduced from [50] Copyright © (1968) with permission from Elsevier.

A non-exhaustive summary of rate expressions found in the literature is provided in Table 1.

| Authors                                                           | Year           | Expression                                                                                                                                                                                                                                                                      | Comments                                                                                      |
|-------------------------------------------------------------------|----------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------|
| Pernicone et al. [51]<br>(Bhattacharyya et al. [56]) <sup>a</sup> | 1969<br>(1967) | $r = \frac{2k_1k_2P_{O_2}^m P_{MeOH}^n}{k_1P_{MeOH}^n + 2k_2P_{O_2}^m}$                                                                                                                                                                                                         | m = n = 0.5<br>( $m = n = 1$ )                                                                |
| Bibin and Popov [57]                                              | 1969           | $r = \frac{k_1 C_{\text{MeOH}}}{1 + \alpha_1 C_{\text{MeOH}} + \alpha_2 C_{\text{H}_2\text{O}}}$                                                                                                                                                                                |                                                                                               |
| Evemenenko and<br>Gorokhovatskii [58]                             | 1968           | $r = \frac{kC_{\rm MeOH}}{1 + b_1 C_{\rm MeOH} + b_3 C_{\rm H_2O}} \frac{C_{\rm O_2}}{1 + b_2 C_{\rm O_2}}$                                                                                                                                                                     |                                                                                               |
| Santacesaria et al. [59]                                          | 1981           | $r = \frac{k_1 k_2 P_{\text{MeOH}} P_{O_2}^{\frac{1}{2}}}{k_1 P_{\text{MeOH}} + k_2 P_{O_2}^{\frac{1}{2}}} \frac{1}{1 + K_{\text{H}_2 \text{O}} P_{\text{H}_2 \text{O}}}$                                                                                                       |                                                                                               |
| Holstein and Machiels [54]                                        | 1996           | $r = k P_{\rm MeOH}^x P_{\rm O_2}^y P_{\rm H_2O}^z$                                                                                                                                                                                                                             | $\begin{array}{l} x = 0.94 \pm 0.06, \\ y = 0.10 \pm 0.05, \\ z = -0.45 \pm 0.07 \end{array}$ |
| Deshmukh et al. [60]                                              | 2005           | $r = \frac{k_{\text{MeOH}\to\text{CH}_2\text{O}}K_{\text{MeOH}}P_{\text{MeOH}}K_{\text{O}_2}P_{\text{O}_2}^{\frac{1}{2}}}{\left(1+K_{\text{MeOH}}P_{\text{MeOH}}+K_{\text{H}_2\text{O}}P_{\text{H}_2\text{O}}\right)\left(1+K_{\text{O}_2}P_{\text{O}_2}^{\frac{1}{2}}\right)}$ |                                                                                               |
| Ulukardeslar et al. [61]                                          | 2010           | $\frac{r}{\left(1+K_{O_2}P_{O_2}+K_{MeOH}P_{MeOH}+K_{H_2O}P_{H_2O}+K_{CH_2O}P_{CH_2O}\right)^2}$                                                                                                                                                                                |                                                                                               |

Table 1. Proposed rate expressions in literature for the oxidation of MeOH to FA.

<sup>a</sup> The work by Bhattacharyya et al. [56] was on  $V_2O_5$ .

Deshmukh et al. [60] performed kinetic investigations to derive a model for all the relevant reactions on a Perstorp industrial FeMo catalyst in a differential reactor. The oxidation of MeOH to FA was found to have a Langmuir–Hinshelwood (LH) type dependence on both  $O_2$  and MeOH concentrations (plateauing at >5 vol.%). For the further oxidation of FA to CO, the rate was first order in CH<sub>2</sub>O with identical LH behavior in  $O_2$  as for the MeOH oxidation, indicating that the same oxygen sites participate in further oxidation. DME formation was first order in MeOH feed concentration, and DMM formation was first order in both MeOH and FA concentrations. The formation of FA from DME showed first order LH contributions from both DME and  $O_2$ . H<sub>2</sub>O was found to have a large inhibiting effect on the MeOH oxidation, which reached a plateau at low H<sub>2</sub>O vapor concentrations. This was incorporated as LH competitive adsorption, giving the rate expressions (6)–(10) [60].

$$r_{\rm MeOH\to CH_2O} = \frac{k_{\rm MeOH\to CH_2O} K_{\rm MeOH} P_{\rm MeOH} K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}}{\left(1 + K_{\rm MeOH} P_{\rm MeOH} + K_{\rm H_2O} P_{\rm H_2O}\right) \left(1 + K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}\right)}$$
(6)

$$r_{\rm CH_2O\to CO} = \frac{k_{\rm CH_2O\to CO} P_{\rm CH_2O} K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}}{1 + K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}}$$
(7)

$$r_{\rm DME} = k_{\rm DME} P_{\rm MeOH} - \frac{k_{\rm DME}}{K_{\rm DME}^{eq}} \frac{P_{\rm DME} P_{\rm H_2O}}{P_{\rm MeOH}}$$
(8)

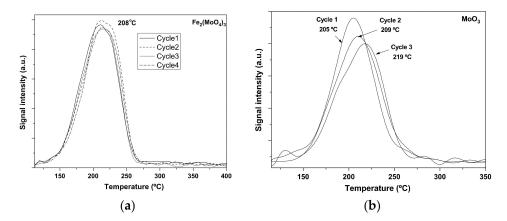
$$r_{\rm DME \to CH_2O} = \frac{k_{\rm DME \to CH_2O} K_{\rm DME} P_{\rm DME} K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}}{(1 + K_{\rm DME} P_{\rm DME}) \left(1 + K_{\rm O_2} P_{\rm O_2}^{\frac{1}{2}}\right)}$$
(9)

$$r_{\rm DMM} = k_{\rm DMM} P_{\rm CH_2O} P_{\rm MeOH} - \frac{k_{\rm DMM}}{K_{\rm DMM}^{eq}} \frac{P_{\rm DMM} P_{\rm H_2O}}{P_{\rm MeOH}}$$
(10)

This reconciled the differences in whether the rate was zero or first order as it depended on the regime because the LH type behavior will be approximately first order at low concentrations and approximately zero order at high concentrations. This is the same case for O<sub>2</sub>, MeOH, and H<sub>2</sub>O inhibition, although the definition of high concentrations differ due to different adsorption equilibrium constants (at 250 °C:  $K_{MeOH} = 124 \text{ atm}^{-1}$ ;  $K_{O_2} = 15.4 \text{ atm}^{-1}$ ;  $K_{H_2O} = 245 \text{ atm}^{-1}$ ). Tesser et al. [62] found that they could accurately simulate the axial temperature profile in their experiments in a fixed bed reactor with only rates for MeOH oxidation to FA (including H<sub>2</sub>O inhibition) and the oxidation of FA to CO.

An investigation of the kinetic isotope effect on  $MoO_3$ ,  $MoO_3/Fe_2(MoO_4)_3$ ,  $Fe_2(MoO_4)_3$ , and  $FeMoO_4$  was performed by Machiels and Sleight [63,64] with the use of CH<sub>3</sub>OD and CD<sub>3</sub>OD. It was found unambiguously that the rate limiting step on the catalyst was the abstraction of H from the methyl group [63], which was supported by Yang and Lunsford [65].

An investigation of  $MoO_3/Fe_2(MoO_4)_3$  by use of CH<sub>3</sub>OH-temperature programmed surface reaction (TPSR) performed by Routray et al. [29], looked into the roles of the catalyst components w.r.t. the Mars-van Krevelen (MvK) mechanism. In the experiment [66], a 2000 ppm CH<sub>3</sub>OH in He stream was fed over the catalyst sample for 30 min at 100  $^{\circ}$ C, flushed with He at 110 °C for 60 min. The temperature was then ramped to 490 °C with 10 °C/min with tracking of possible released surface species. The sample was then cooled to 100 °C concluding one cycle. The  $Fe_2(MoO_4)_3$  catalyst stayed fully oxidized at the surface since the FA signal did not change between the cycles (Figure 9a). This meant that the catalyst supplied lattice oxygen to the surface for the reaction, since no  $O_2$  was fed between the cycles. Thus, Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> strongly facilitated a MvK mechanism by supplying oxygen from the bulk structure. On the other hand  $MoO_3$  alone did not facilitate the MvK mechanism as efficiently (Figure 9b), as the FA signal changed peak temperature  $(T_p)$  and shape, which meant the lattice oxygen diffusion from the bulk to the surface was not high enough to fully keep the surface oxidized [29], which however may not be a problem with oxygen in the feed. This was supported by work in a temporal analysis of products (TAP) reactor study by Lafyatis et al. [67]. The lattice oxygen contribution was also supported by an investigation by electrical conductivity methods [68]. O'brien et al. [69] clearly observed MvK type oxygen transport in MoO<sub>3</sub> by in situ measurements during anaerobic dehydrogenation, but this may not be as fast as for the FeMo catalyst. Bowker et al. [70] observed that a temperature of at least 250  $^{\circ}$ C was needed for oxygen lattice transport to the surface in anaerobic pulse MeOH reduction experiments and at 300 °C the surface was kept oxidized as Mo(VI) from lattice oxygen [39].



**Figure 9.** Cyclic CH<sub>2</sub>O/CH<sub>3</sub>OH-TPSR spectra with no oxidation between TPSR experiments for (**a**) bulk  $Fe_2(MoO_4)_3$  catalyst Mo/Fe = 1.5 and (**b**) bulk MoO<sub>3</sub> catalyst. Reprinted from [29] Copyright © (2010) with permission from Elsevier.

In the study by Routray et al. [29], it was measured by IR that both surface  $CH_3OH^*$ and  $CH_3O^*$  could be converted directly to FA. This resulted in the suggestion of the following reaction mechanism (Reactions (11)–(18)) for the oxidation of MeOH to FA on a  $MoO_3/Fe_2(MoO_4)_3$  [29].

$$CH_3OH + * \rightleftharpoons CH_3OH^*$$
 (11)

$$CH_3OH + O^* + * \rightleftharpoons CH_3O^* + OH^*$$
(12)

$$CH_3OH^* + O^* \rightarrow CH_2O + H_2O + 2*$$
(13)

$$CH_3O^* + O^* \rightarrow CH_2O + HO^* + *$$
(14)

$$CH_3O^* + HO^* \rightleftharpoons CH_3OH + O^* + *$$
(15)

$$HO^* + OH^* \rightleftharpoons H_2O + O^* + *$$
(16)

$$O^*_{\text{bulk lattice}} \rightleftharpoons O^*$$
 (17)

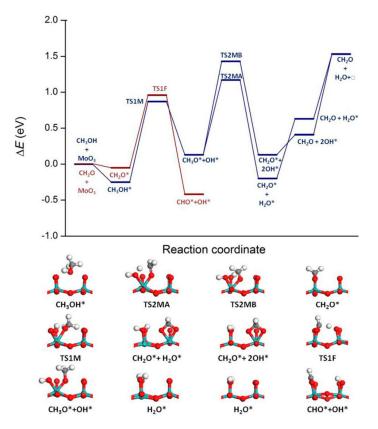
$$O_2 + 2* \rightleftharpoons 2O_{\text{bulk lattice}}^*$$
 (18)

Reactions (13) and (14) were suggested as rate limiting steps. Reactions (12) and (15) look very similar, with the difference in the notation indicating that OH may bind with the O-atom (Reaction (15)) or the H-atom (Reaction (12)), which does not seem realistic. The mechanism had both LH and Eley-Rideal kinetics. The authors suggested the catalytic active phase to be the  $Fe_2(MoO_4)_3$  and that the  $MoO_x$  on the surface was the active sites in bulk FeMo catalysts, with the role of the excess  $MoO_3$  to keep the Fe sites covered when mobile Mo-CH<sub>3</sub>O species leave the catalyst, which will be discussed further in Section 2.1.5 [29].

The mechanism has also been investigated by Rellán-Piñeiro and López [52] by using DFT calculations on  $\alpha$ -MoO<sub>3</sub>(010) (Figure 10), as well as other Mo oxide surfaces. The reaction mechanism was similar to Reactions (11)–(18) proposed by Routray et al. [29], but with no direct reaction of molecularly adsorbed MeOH to form FA. FA adsorbs very weakly on the  $\alpha$ -MoO<sub>3</sub>(010) surface. The decomposition pathway from FA was not investigated further than to CHO<sup>\*</sup> + OH<sup>\*</sup> since the energy barrier over TS1F was stated by the authors to be too large compared to the desorption energy barrier, i.e., FA desorbs rather than oxidize further.

Rellán-Piñeiro and López [52] concluded from their work that the energy of oxygen vacancy formation was the major factor regarding activity and selectivity. They proposed that Fe contributed as an electron donor, rendering vacancy formation easier [52]. Choksi and Greeley [71] also investigated the MoO<sub>3</sub>(010) facets by DFT and microkinetic modelling for MeOH oxidation, where they found a CH<sub>3</sub>O\* pathway, a CH<sub>2</sub>OH\* pathway, and a crossover pathway. They concluded that the CH<sub>3</sub>O\* pathway was the kinetically and thermodynamically preferred route in agreement with Rellán-Piñeiro and López [52]. As the C-H cleavage of CH<sub>2</sub>O\* to CHO\* was very slow compared to FA desorption, the selectivity to FA was very high. CH<sub>2</sub>O formation was stated to have three kinetically important steps: C-H cleavage of CH<sub>3</sub>O\*, recombination of OH\* to form H<sub>2</sub>O\*, and oxidation of the reduced surface by gas phase O<sub>2</sub>, each of them being possible rate determining steps depending on the O<sub>2</sub> pressure (proceeding from high to low pressure) [71].

Peyrovi et al. [72] concluded that the most important aspect of FA production was the presence of  $Fe_2(MoO_4)_3$ , and deactivation was due to the degradation of  $Fe_2(MoO_4)_3$  to a smaller particle size, although this seems unlikely from the authors's views. They stated that there were no changes to the MoO<sub>3</sub> phase after the reaction [72], which was in direct contrast to the other studies summarized above and seems unlikely. Peyrovi et al. [72] stated the reaction to be structure sensitive as they observed higher activity for a coprecipitated FeMo/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst with Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> particles of 29 nm compared to 16 nm achieved by impregnation.

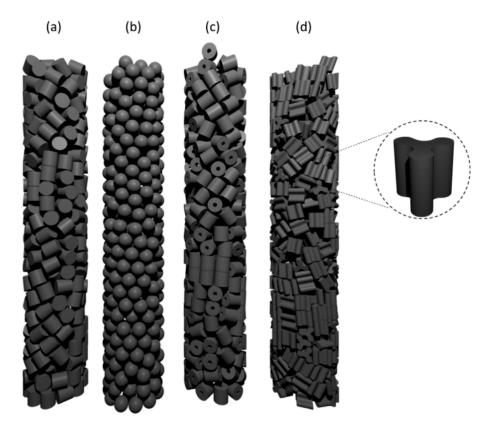


**Figure 10.** Reaction energy profile calculated by DFT for the oxidation of MeOH to FA via two different routes (blue lines) and FA decomposition (red line) on a  $\alpha$ -MoO<sub>3</sub>(010) surface. Newly formed vacancies are marked by  $\Box$ . Beneath the reaction energy profile, the structures for the different reaction coordinates are shown, where TS1F means that it was transition state 1 starting from FA, and TS1M was transition state 1 starting from methanol. For the structures, the colors are as follows: red: O; cyan: Mo; dark grey: C; white: H. © 2015 Wiley-VCH Verlag GmbH & Co. KGaA, Weinheim [52].

# 2.1.5. Reaction Engineering

Later, Ivanov et al. [73] performed an operating parameter investigation in a "pseudoisothermal" reactor with up 60 cm of NEOCHIM SA industrial FeMo catalyst rings. More precisely, it seemed to be a reactor with an unknown degree of cooling, but it was not close to isothermal. An increase in the MeOH feed concentration drastically changed the catalyst's temperature profile with markedly higher hot-spot temperature and resulted in different product distributions as side reactions became more significant. Increasing space velocity produced the same kind of change in temperature profile and product distribution, although less drastically. O<sub>2</sub> should have similar or higher concentrations with respect to MeOH and not have too large dehydration relative to DME and a displacement in the hot spot. Two to three percent of H<sub>2</sub>O in the feed increased process selectivity. Changes in the inlet temperature either resulted in low conversion if the temperature became too low or decreasing selectivity due to high inlet temperature. Using an adiabatic layer after the main reactor produced, in all cases, a loss of FA to CO, but the oxidation of the remaining MeOH and the DME to FA, if controlled well, was a cheap method of optimizing formalin quality [73].

The kinetic models developed by Deshmukh et al. [60] were incorporated into a particle resolved CFD model for a fixed bed reactor by Partopur and Dixon [74] simulating beds with a length of 0.1 m for four different kinds of pellets generated numerically (Figure 11). The simulations included local and overall conversion, selectivity, pressure drop, voidage, velocity profiles, and heat transfer. The trilobes had the lowest pressure drop due to increased voidage, but the rings showed the highest overall conversion (~20%) and selectivity due to the best overall performance on the parameters. A mixture of rings with trilobes was simulated for a bed of 0.19 m and showed the possibility of a slight improvement in performance.



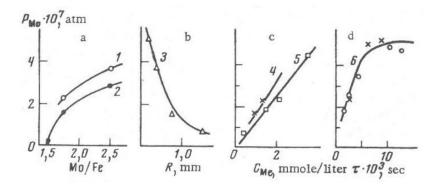
**Figure 11.** Four fixed bed models/packings investigated by CFD (tube wall invisible). Tube length: 0.1 m; diameter: 0.021 m; tube to particle diameter ratio: 4.7. (**a**) Cylinders, (**b**) spheres, (**c**) rings, and (**d**) trilobes. © 2019 American Institute of Chemical Engineers [74].

#### 2.1.6. Deactivation

Earlier, it became apparent that Mo becomes volatile and that this was the main problem with the industrial catalyst. The volatility of the Mo was investigated specifically by Popov et al. [75] already in 1976 by collecting Mo volatile species formed at 350 °C in a trap inserted in a loop reactor system.

During investigations of industrial type FeMo catalysts with Mo/Fe ratios of 1.75 and 2.5, the partial pressure of the volatile Mo species ( $P_{Mo}$ ) remained approximately constant when the activity of the catalyst remained constant. When the initial Mo/Fe ratio increased, the initial  $P_{Mo}$  increased as well (Figure 12).

Under the reported conditions, pure MoO<sub>3</sub> was found to have  $P_{Mo}$  of  $6 \cdot 10^{-6}$  atm. This was 40 times  $P_{Mo}$  of Mo/Fe ratio of 1.75.  $P_{Mo}$  decreased with increasing catalyst grain size and was directly proportional to MeOH concentration when the other parameters were kept constant. This suggested a first order reaction in MeOH in the formation of the volatile Mo-species. Volatility increased only initially with increasing contact time after which it became constant indicating that the gas phase was saturated by the volatile Mo-species. For a sample with Mo/Fe of 1.75, a grain size of  $3 \times 3$  mm (exact geometry not given) and a contact time ( $\tau$ ) of  $11 \cdot 10^{-3}$  s  $P_{Mo}$  in the reactor outlet could be estimated with Equation (19) [75].



**Figure 12.** Dependence of the partial pressure for volatile Mo species in FeMo catalysts with respect to (**a**) Mo/Fe ratio, (**b**) diameter of catalyst grains, (**c**) MeOH concentration, and (**d**) contact time [75].

$$P_{\rm Mo} \simeq 6.9 \cdot 10^{-4} P_{\rm CH_3OH} \exp\left(-\frac{6500}{RT}\right)$$
 (19)

Lastly, when the formation of the volatile Mo species was assumed to be first order in MeOH and decomposition was assumed to be first order in volatile species, the rate constants were found to be  $14 \text{ s}^{-1}$  and  $304 \text{ s}^{-1}$  for the formation and decomposition of volatile Mo-MeOH species, respectively [75]. Moreover, Carbucicchio et al. [76] observed increased Mo volatilization with increasing MeOH pressure. In an industrial reactor after 150 days, Popov and Skomorokhova [77] observed a decreasing surface area along the catalyst bed due to MoO<sub>3</sub> migration and deposition as needle-like crystals. The Mo volatilization was highest at the hot spot, where temperature and concentration of MeOH were both high. At the inlet, the volatilization was lower as the temperature was still low, and after the hot spot, the MeOH concentration decreased producing lower Mo volatilization [77]. This was in agreement with a previous study by Burriesci et al. [78]. Ma and Kmiotek [79] found that the decrease in specific activity for MeOH oxidation to FA could be correlated with the loss of reaction sites at the ferric molybdate surface due to Mo volatilization.

The exact mechanism of volatilization of the Mo is still debated. Smith and Rohrer [80] succeeded in studying the blue deposit formed in the reactor outlet from MoO<sub>3</sub> treated with MeOH/air mixtures at 300 °C with scanning electron microscopy energy dispersive X-ray analysis (SEM-EDX) and XRD and found the deposit to be Mo<sub>2</sub>O<sub>5</sub>(OCH<sub>3</sub>)<sub>2</sub>. They suggested two routes of formation. The volatilization of Mo oxide-hydroxide which then reacted with MeOH to form Mo<sub>2</sub>O<sub>5</sub>(OCH<sub>3</sub>)<sub>2</sub> either in the gas phase or after deposition or desorption of a Mo oxy-methoxide which upon condensation formed Mo<sub>2</sub>O<sub>5</sub>(OCH<sub>3</sub>)<sub>2</sub>. As no Mo evaporation was observed without MeOH in the feed, the second mechanism was considered the most plausible [80]. Mo<sub>2</sub>O<sub>5</sub>(OCH<sub>3</sub>)<sub>2</sub> could be formed by reaction of MoO<sub>3</sub>·2H<sub>2</sub>O with MeOH. Upon thermal decomposition MeOH, DME, FA, and H<sub>2</sub>O were detected [81].

Catalyst deactivation was investigated in a Perstorp Formox plant using FeMo catalysts by Andersson et al. [20]. The plant was operating with a MeOH concentration of 10.2 vol.% at the inlet. There were two consecutive catalyst layers. In the first layer, the KH44L catalyst  $(4.5 \text{ m}^2/\text{g}, \text{Mo/Fe} = 2.43)$  was mixed with inert rings while the second layer consisted of pure KH26 catalyst  $(5.4 \text{ m}^2/\text{g}, \text{Mo/Fe} = 2.29)$ . The catalysts were investigated fresh, after half expected lifetime and after full lifetime. After operation, the KH44L catalyst in the mixed layer had an increase in surface area, which decreased when proceeding down the bed, while the KH26 catalyst in the second layer had a decrease in surface area in the top of the layer and no change further down. At the same time, an increase in pore volume was observed for the first layer at both half and full expected catalyst lifetime. This decreased down the bed. KH26 in the second layer showed a decrease in pore volume at half expected lifetime but an increase in pore volume for the first half of the second layer and a larger decrease in pore volume of the second part at full expected lifetime.

By Atomic Absorption Spectroscopy (AAS), it was measured that the Mo/Fe ratio after termination was approximately 1.5 in the mixed oxide top layer after initially being 2.4, while the ratio had increased for the second (pure KH26) layer. It was measurable by XRD, Raman spectroscopy, and elemental analysis that Mo migrated from the inlet towards the outlet of the reactor. The migration of Mo was suggested mainly to result from the formation of volatile Mo methoxy species since the effect was moving from the top and downwards, from high to low MeOH concentration. If  $H_2O$  was the main cause, the effect should have increased down the reactor. The Mo deposited as the MeOH concentration and temperature decreased, resulting in decreased surface area and pore volume and giving rise to an increased pressure drop, which ultimately, together with falling selectivity, resulted in shut down and change of the catalyst [20]. Andersson et al. [20] concluded a surplus of MoO<sub>3</sub> was needed to maintain the active phase in the catalyst according to the redox reactions (Reactions (20)–(22)) [20].

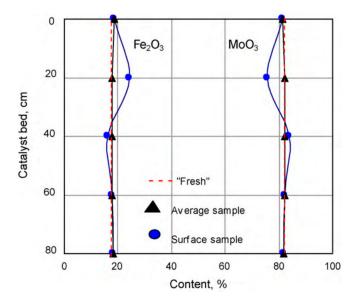
$$CH_3OH + Fe_2(MoO_4)_3 \rightarrow CH_2O + H_2O + 2FeMoO_4 + MoO_3$$
(20)

2 FeMoO<sub>4</sub> + MoO<sub>3</sub> + 
$$\frac{1}{2}$$
 O<sub>2</sub>  $\rightarrow$  Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> (21)

$$3 \text{ FeMoO}_4 + \frac{3}{4}\text{O}_2 \rightarrow \text{Fe}_2(\text{MoO}_4)_3 + \text{Fe}_2\text{O}_3$$
 (22)

Reaction (20) was the main reaction, Reaction (21) was the reoxidation with  $MoO_3$  in excess, and Reaction (22) was the reoxidation with depletion of Mo, which resulted in the formation of an unselective  $Fe_2O_3$  catalyst surface [20].

Catalyst deactivation phenomena found under FA production was studied on an industrial Neochim PLC-Dimitrovgrad FeMo catalyst by Ivanov and Dimitrov [82] over a period of 15 months with 6.2 vol.% MeOH in the feed over two reactors, which had either good or bad heat transfer. This gave the reactors different temperature profiles, but the inlet and outlet temperatures were the same. In the reactor with bad heat transfer, a large region with temperatures between 300 °C and 335 °C existed, whereas the temperature in the reactor with good heat transfer never exceeded 290 °C. In the hot reactor, the top catalyst layer had a distinct reddish-brown coloration when discharged. This was due to the formation of Fe<sub>2</sub>O<sub>3</sub> under reoxidation of FeMoO<sub>4</sub> according to Reaction (22) also found by Anderson et al. [20]. For the low temperature reactor, the catalyst composition at different positions in the bed was measured by ICP giving the profile shown in Figure 13.



**Figure 13.** Catalyst composition measured by ICP along the catalyst bed in reactor with good heat transfer. Reprinted from [82] Copyright © (2010) with permission from Elsevier.

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There was a shift of MoO<sub>3</sub> content down in the reactor from the process intense zone (determined from the temperature profile), which produced a partly MoO<sub>3</sub> depleted catalyst outer layer in the process intense zone (Reaction (23)) and deposition of MoO<sub>3</sub> further down in the catalyst bed. It was claimed by Ivanov and Dimitrov [82] that the sublimation and, thus, the deactivation of the catalyst were driven by H<sub>2</sub>O according to Reactions (23) and (24) because no reddish-brown coloration from FeMoO<sub>4</sub> oxidized to Fe<sub>2</sub>O<sub>3</sub> was observed at low temperatures [82].

$$MoO_4^{2-} + 2H_2O \to MoO_2(OH)_2 + 2OH^-$$
 (23)

$$MoO_2(OH)_2 \rightarrow MoO_3 + H_2O$$
 (24)

However, if excess  $MoO_3$  was still present, Mo can be volatilized without formation of  $Fe_2O_3$ , and the concentration of water is the highest in the outlet; thus, a larger degree of Mo volatilization in the last half the reactor should be significant for this to be probable.

The results by Andersson [20] and Ivanov and Dimitrov [82] were very similar, although the conclusions/suggestions for the deactivation mechanism differed. The major difference in the results was that the reactor with good heat transfer in the study by Ivanov and Dimitrov [82] did not deactivate from the top but a bit lower in the reactor (also observed by Popov and Skomorokhova [77]). However, this might arise from the temperature being too low in the inlet and the heating being too slow, so the temperature was not high enough for the deactivation to begin at the top as it did for the reactor with bad heat transfer. Thus, the difference in the deactivation profile may be explained from the temperature profile. Spatiotemporal imaging performed by O'Brien et al. [83] on  $MoO_3$  with MeOH in N<sub>2</sub> supported that the evaporation came from an Mo-methoxy species. However, a study by Soares et al. [84,85] found  $H_2O$  was strongly promoting the deactivation as adding 2 vol.% H<sub>2</sub>O in the feed drastically increased the rate of deactivation, and they proposed this effect to come from inhibition of the reoxidation of the surface. However, as discussed above, H<sub>2</sub>O inhibits the oxidation of MeOH to FA. A more likely cause of the accelerated deactivation is, thus, the higher concentration of MeOH, which promotes the volatilization of Mo. Furthermore, Soares et al. [86] proposed excess Mo to increase surface reoxidability [86].

The findings of Ivanov and Dimitrov [82] and Andersson [20] were also substantiated in the studies by Raun et al. [43,87,88] utilizing Raman spectroscopy, XRD, XPS, SEM, and STEM on powder samples used at 384–416 °C for up to 600 h on stream. Excess MoO<sub>3</sub> evaporated (within 10 h), then Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> was reduced to the Mo depleted phases FeMoO<sub>4</sub> (10-250 h on stream) and Fe<sub>2</sub>O<sub>3</sub> (observed after 600 h on stream) due to the loss of Mo during operation. The catalyst could be reactivated by thermal treatment. The reactivation was believed to stem from re-establishing the Mo rich surface from crystalline  $MoO_3$  in the first phase and then later from the bulk  $Fe_2(MoO_4)_3$  phase [43,87,88]. The deactivation was further investigated by Gaur et al. [89] by operando XAS/XRD and in situ Raman spectroscopy, finding similarly that  $\alpha$ -MoO<sub>3</sub> evaporated. The evaporation rate (at 300 °C) was found to increase with increasing MeOH concentration (increasing from 5 vol.% to 9.5 vol.% increased the rate by a factor of two), decreasing  $O_2$  concentration (increased by 67% for  $O_2$  concentration going from 10% to 5%), and increasing temperature (three times higher at 350 °C compared to 300 °C). The volatilization rate was also observed to be highly affected by the particle size [89]. Furthermore, in situ measurements during redox cycling on a FeMo catalyst showed phase reduction and segregation into MoO<sub>2</sub> and FeMoO<sub>4</sub>, which needed to be oxidized at 500 °C in order to fully regenerate (not including the volatilized Mo) [90]. Other studies [70,91–95] show similar trends and results for deactivation and phase reduction. Raun et al. [96] developed a dynamic one-dimensional single particle model for Mo volatilization involving diffusion and reaction of MeOH to FA, formation and diffusion of a volatile Mo species, and the local change in Mo content in the pellet. Only the loss of free Mo was included-not the transformation to less oxidized FeMo. The model was compared to experimentally measured Mo loss in an industrial FeMo

pellet. The pellets were subjected to different reaction conditions such as 1.6–4.5 vol.% MeOH, 2.5–10 vol.% O<sub>2</sub>, and 0–10.2 vol.% H<sub>2</sub>O in N<sub>2</sub> at temperatures of 250, 300, and 350 °C. Mo was shown by SEM-EDX to volatilize from the surface of the pellet, giving a sharp front of  $Fe_2(MoO_4)_3$  depleted from excess MoO<sub>3</sub>, which moved inwards with increasing TOS. The sharp front indicated that Mo volatilization was equilibrium limited. The measured mass losses under the varying conditions were used to fit the kinetics of Mo depletion in the model, which was then verified against the placement movement of the depletion front showing good agreement. The model showed that increasing the pellet volume by 100% with the same dimensional ratios would decrease the volatilization by 20% over 400 h on stream [96]. The single particle model was then implemented into a dynamic model for Mo transport and pressure drop in a single tube fixed bed reactor (FBR) [97]. The FBR was modelled as a series of CSTRs and had fixed axial profiles of temperature and concentrations of MeOH and H<sub>2</sub>O as input from a pilot plant reactor. The model was fitted to experimental data for the hydraulic diameter of the cylindrical catalyst pellets and porosity of the deposited MoO<sub>3</sub> from the pilot plant reactor. In agreement with Burriesci et al. [78] and Ivanov and Dimitrov [82], the simulations showed that not all the  $MoO_3$  was depleted from the inlet of the reactor even after 2 years because the temperature was too low. The study suggested that by having solid cylinders instead of rings for the first 21 cm of a 100 cm bed, the pressure drop over the bed could be decreased by 16% after 2 years, although the initial pressure drop would be 22% higher. Using pellets with no excess  $MoO_3$  for the first 21 cm was calculated to decrease pressure drop by 49% after 2 years; however, such pellets may have low mechanical stability. Thus, both strategies could decrease the pressure drop and, thus, increase process lifetime. The model should be further developed as the changes in activity and selectivity and, thus, temperature profile over time and from the catalyst modifications were not included in the model [97].

A patent for in situ regeneration of metal molybdate catalysts was taken by Wachs and Briand [98], where redispersion should happen in a stream of MeOH and inert gas. This may shortly regenerate/re-disperse Mo; however, the effect might be very short lived as the mechanism of regeneration was the same as the deactivation mechanism. It will likely be difficult to re-deposit Mo into the pores of the catalyst and obtain the distribution of Mo as in the fresh catalyst.

Overall, the findings indicate that the most important factors for the deactivation and Mo volatilization include increases with high temperature, high methanol concentration, and low oxygen concentration. From these findings, the most straight forward optimization when using a FeMo catalyst may be to modify operating conditions [43,87–89] and optimizing pellet size and shape [96,97].

## 2.2. Alternative Catalysts

An overview of the benefits and challenges of the currently applied industrial catalyst has been provided above. There are various methods to go about the problem of Mo volatilization, such as finding an alternative process or to change the existing process and/or catalyst. Only the latter would be applicable to the existing FA plants. Looking at the catalyst, there are two main routes. The first is to start with the existing FeMo catalyst and to try to find other preparation methods, conditions, or promoters to increase the stability of the catalyst without a significant loss of activity and selectivity. The other route is to look for a different catalyst that is more stable than the FeMo catalyst without sacrificing high selectivity. Such a catalyst does not need to be as active as the FeMo catalyst as long as it is sufficiently active, stable under reaction conditions, and possesses high selectivity, since a solution could be to have two layers of catalyst consisting of a stable, less active catalyst at the top and the FeMo catalyst beneath where the MeOH concentration is lower. The scope of the remaining part of this review is to provide an overview of the reported results, the problems to be aware of, and the progress made within finding an alternative catalyst for the Formox process. Furthermore, some results of the authors' own screening studies will be included for comparison. Full details are shown in the Supplementary Materials.

2.2.1. Overview of Catalysts Reported in the Literature

The open literature was thoroughly searched for catalysts reported for selective oxidation of methanol to FA. Figures 14 and 15 summarize the identified catalyst compositions.



**Figure 14.** Solar plot for Mo and V containing catalysts showing main components (inner circle), secondary component or support material (middle circle), and tertiary component or support material (outer circle). Oxygen may be present without it being specified.

Most catalysts investigated contain either Mo or V in some form. Detailed descriptions of the reported results will be given in the following sections, roughly divided after the active catalyst component, with a section at the end presenting the results available on catalysts' stability and the volatility of active components.

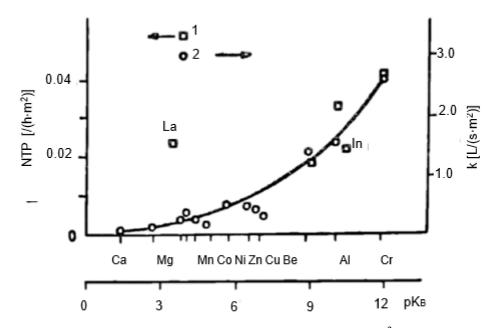
## 2.2.2. Mo Containing Catalysts

Pernicone et al. [44] investigated various trivalent metal molybdates mixed with excess Mo oxide (MoO<sub>3</sub>-Me(MoO<sub>4</sub>)<sub>3</sub>) as catalysts, Me = Al, Cr, Fe, In, and La, in a pulse microreactor and a differential reactor at 232 °C, 1.25 bar, and N<sub>2</sub>/O<sub>2</sub>/MeOH = 70/20/10 mol%. The catalysts were prepared with a Mo/Me ratio of six. The catalyst surface acidities were found to have no significant deviation to that of pure MoO<sub>3</sub> in contrast to prior publications attributing formaldehyde selectivity to acidity. The catalyst activities were ranked as follows: MoO<sub>3</sub> < 9 MoO<sub>3</sub> + Al<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> < 9 MoO<sub>3</sub> + In<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> < 9 MoO<sub>3</sub> + La<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> < 9 MoO<sub>3</sub> + Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> < 9 MoO<sub>3</sub> + Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>. Pernicone et al. [44] found pure Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> and Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> (prepared by sublimation of MoO<sub>3</sub> from the mixtures at 700 °C) to be without activity and surface acidity. This was probably a result of the preparation method. This was in contrast with the findings mentioned in Section 2.1.5 by Andersson et al. [20] and may be due to the very low surface area resulting from high temperature treatment. The addition of MoO<sub>3</sub> to Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> achieving Mo/Cr = 2 produced a catalyst three times as active as pure MoO<sub>3</sub>. Catalysts with Me<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> mixed with  $Me_2O_3$  having a Mo/Me ratio of 1 were prepared for Me = Cr and Al. They had no surface acidity nor any measurable activity. The Cr and Fe samples were proposed to be more active due to the nature of Fe<sup>3+</sup> and Cr<sup>3+</sup> ions. Due to differences in the rate observed in the differential reactor and pulse microreactor, the effect was proposed to come from an increased product desorption rate, as the catalyst surface was mostly product free in the pulse microreactor. This was questioned by Vichterlova et al. [44] who stated that an active catalyst must contain acidic sites to chemisorb MeOH and possess adequate reducibility, as acidic non-reducible catalysts had no activity [44]. In the discussion of [44] at the Fourth International Congress on Catalysis, Yu. I. Ermakov stated that in order for catalyst reduction to be the rate determining step, the rate of transition of the Me element from the highest to the lowest oxidation state determines the rate. The activity increased as the stability of the lower oxidation state increased, measurable by increased reducibility of the catalyst. He found the data by Kolovertnov [44] and Pernicone et al. [44] showed growing catalytic activity for MeOH oxidation with increasing electronegativity of the cation based on  $pK_B$  for the hydroxyl compounds of the cations (Figure 16) showing the same curve.



**Figure 15.** Solar plot for catalysts not containing V or Mo showing main components (inner circle), secondary component or support material (middle circle), and tertiary component or support material (outer circle). Oxygen may be present without it being specified.





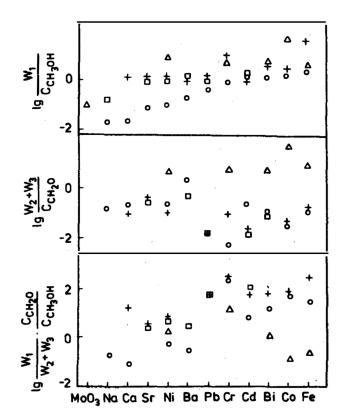
**Figure 16.** Activity vs. reducibility: (1) Pernicone's data ( $\Box$ ) [NL/h/m<sup>2</sup>]; (2) Kolovertnov's data (o), k [mL/s/m<sup>2</sup>], [44]. Reproduced from [44] copyright (1968) with permission from copyright holder.

Lanthanum molybdate/hydroxide did not fit the curve due to anomalously high alkaline properties of the hydroxide. Other minor deviations were believed to stem from impurities in the prepared molybdates. Catalytic activity was shown to be a function of Mo-O bond ionicity, and it was stated to be largely independent of, e.g., cation valence, presence of d-electrons and Mo coordination with oxygen [44]. Cu and Ni molybdates were stated to be less active than Al molybdate [44]. A similar dependence of catalytic activity on electronegativity was observed by Kolovertnov for ortho-vanadates [44]. A similar relationship was reported by Burcham et al. [99,100] between the electronegativity of the ligand cation (Mo-O-X) and turnover frequency. This was reported to be similar for both the supported molybdena and the bulk molybdates Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, NiMoO<sub>4</sub>, MnMoO<sub>4</sub>, CoMoO<sub>4</sub>, ZnMoO<sub>4</sub>, Al<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, Ce(MoO<sub>4</sub>)<sub>2</sub>, Bi<sub>2</sub>Mo<sub>3</sub>O<sub>12</sub>, and Zr(MoO<sub>4</sub>)<sub>2</sub>.

In 1976, Popov et al. [101] tested the effect of excess  $MoO_3$  on molybdates of Na, Ca, Sr, Ni, Ba, Pb, Cr, Cd, Bi, Co, and Fe with respect to selectivity to  $CH_2O$  and activity to  $CH_2O$  and  $CO_x$  (Figure 17).

The selectivity and activity to FA from MeOH were greatly enhanced by the addition of 10 mol% excess MoO<sub>3</sub>, while further addition only produced slight variations [101]. Although Figure 17 does not provide any accurate numbers for selectivity and activity, it does indicate the relative performances. The FeMo showed the best results in terms of both activity and selectivity, but several other molybdates may be of some interest.

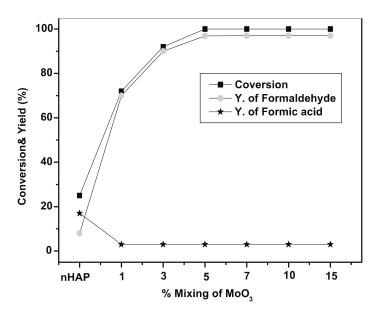
The same group later studied Cd-Mo oxide catalysts (Mo/Cd = 1.0 and Mo/Cd = 1.2) for the oxidation of MeOH (3.0–3.7 vol.% MeOH in the feed) [102]. The stoichiometric molybdate was active in the dehydrogenation of MeOH to CO<sub>2</sub> and H<sub>2</sub>, and at 350 °C, conversions to CH<sub>2</sub>O, CO<sub>2</sub>, CO, and H<sub>2</sub> were 7%, 55%, 2%, and 59%, respectively. The selectivity to FA changed with the addition of excess MoO<sub>3</sub> to above 85% at ~75% conversion. The oxidation of both MeOH and FA was reported to be first order. The CO<sub>2</sub> formation over CdMoO<sub>4</sub> was reported to come from oxidation of CH<sub>2</sub>O, as the selectivity towards CH<sub>2</sub>O was 100% when the degree of conversion was close to zero [102]. They also performed semiempirical investigations (INDO method) of MeOH interaction with Ga<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, which they stated had similar performance with respect to MeOH oxidation as Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> [103,104].



**Figure 17.** Presentation of the effect of excess MoO<sub>3</sub> on the activity to FA  $\left(\ln \frac{W_1}{C_{CH_3OH}}\right)$ , activity to CO<sub>x</sub>  $\left(\ln \frac{W_2+W_3}{C_{CH_2O}}\right)$ , and the selectivity to CH<sub>2</sub>O  $\left(\ln \frac{W_1}{W_2+W_3}, \frac{C_{CH_2O}}{C_{CH_3OH}}\right)$ .  $\Delta$  oxides;  $\bigcirc$  normal molybdates;  $\square$  molybdates with approximately 10 mol% excess MoO<sub>3</sub>; + molybdates with approximately 20 mol% excess MoO<sub>3</sub>. Reprinted by permission from [101] Springer, Reaction kinetics and catalysis, Copyright © (1969).

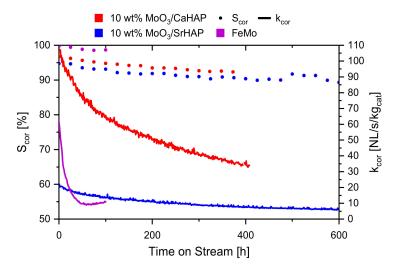
Popov et al. [105] investigated the effect on selectivity to FA of the excess of MoO<sub>3</sub> on calcium molybdate at 350 °C. At stoichiometric ratios of Mo/Ca = 1.0, the selectivity to FA was 18.5%. When the ratio was increased to 1.01, the selectivity increased to 94% and the reaction rate doubled. Upon further increasing the ratio to 1.2, selectivity stabilized at 96% to FA [105]. Malka and Tatibouët [106] reported selectivity to FA to be 48% on unsupported stoichiometric CaMoO<sub>4</sub>. They found that highly dispersed CaMoO<sub>x</sub> (formed with excess of Mo) on SiO<sub>2</sub> was very active but with methyl formate as the main product [106]. Thrane et al. [107] prepared molybdates of alkali earth metals (MgMoO<sub>4</sub>, CaMoO<sub>4</sub>, SrMoO<sub>4</sub>, and BaMoO<sub>4</sub>). In agreement with Popov et al. [101,105], excesses of Mo were found to be important for activity and selectivity towards FA, as the stoichiometric CaMoO<sub>4</sub> and MgMoO<sub>4</sub> had relatively low activities and considerably lower selectivity than the samples with excess Mo. The stoichiometric alkali earth metal molybdates showed very good catalytic stability, while excess Mo quickly evaporated [107].

The possibility of using hydroxyapatite (HAP and  $Ca_5(OH)(PO_4)_3$ ) as a support for Mo oxide was investigated by Said et al. [108] (2014–2016), where the catalyst was prepared by a sol-gel method. A selectivity and yield of 97% was achieved for the 5 wt% MoO<sub>3</sub>/HAP catalyst at 400 °C, with an initial MeOH concentration of 1.6% (Figure 18) for the dehydrogenation of MeOH (although it was stated to be oxidation in the article, there was no O<sub>2</sub> in the feed).



**Figure 18.** Conversion of MeOH and FA yield as function of MoO<sub>3</sub> loading on HAP. Reprinted by permission from [108] Springer, Catalysis Letters, Copyright © (2015).

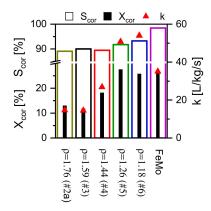
The catalyst was reported stable for 90 h (the catalyst particle size was not reported). The active sites were concluded to be  $Mo^{6+}$ , which produced Lewis and Brønsted acid sites of weak and intermediate strength [108]. The active phase of the catalyst was suggested to be calcium molybdate formed under calcination [108,109]. Thrane et al. [110] investigated MoO<sub>3</sub> supported on hydroxyapatite and the Sr analogue in a feed of 150 NmL/min, 5 vol.% MeOH, and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. MoO<sub>3</sub>/CaHAP and MoO<sub>3</sub>/SrHAP were found to be more stable than an industrial reference FeMo catalyst when measured as powder catalysts for up to 600 h on stream at 350 °C (Figure 19). Additionally, the selectivity was found to be as high as 96% at 95% conversion, which is in agreement with Said et al. [108].



**Figure 19.** Reversible byproducts corrected selectivity towards FA and corrected activity at 350 °C measured on 25 mg catalyst sample (150–250  $\mu$ m) in 150 mg of SiC dilutant in a flow of 150 NmL/min consisting of 5 vol.% MeOH and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. Reprinted from [110] with permission from Wiley-VCH GmbH Copyright © (2021).

The active phase was proposed to be amorphous  $MoO_x$  on the surface of the HAP support, which was observed with STEM, substantiated by XAS (XANES and EXAFS) and X-ray PDF, as previous studies found stoichiometric CaMoO<sub>4</sub> by itself was not very active or selective. The phosphate was proposed to decrease selectivity towards CO and CO<sub>2</sub>

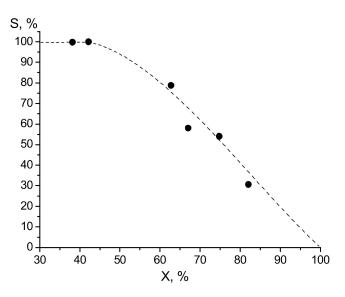
compared to stoichiometric CaMoO<sub>4</sub> and SrMoO<sub>4</sub> [110,111]. Thrane et al. [112] further investigated samples of 10 wt% MoO<sub>3</sub>/HAP pressed as industrial sized Mo/HAP pellets with different pellet densities, measuring the catalytic performance in a single pellet reactor with 300 NmL/min, 5 vol.% MeOH, and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. Both selectivity and activity increased with decreased pellet density (Figure 20). The difference between the selectivity of Mo/HAP pellets and FeMo pellets was larger than the difference observed between Mo/HAP powder and FeMo powder.



**Figure 20.** Observed first order rate constant and reversible byproduct corrected conversion and selectivities on single pellets of Mo/HAP with different densities and a FeMo pellet at 350 °C in 300 NmL/min, 5 vol.% MeOH, and 10 vol.%  $O_2$  in  $N_2$ . Reproduced from [112] with permission from the Royal Society of Chemistry.

In contrast to the powder results, the pellets of Mo/HAP and FeMo were found to have similar catalytic stability [112], highlighting the challenges in proceeding from powder screenings and upscaling to industrially relevant catalysts.

Stabilization of the FeMo catalyst by CaO has been investigated by Kostynyuk and Nikolenko [113]. The catalyst was tested at 300 °C with 5.9 vol.% MeOH in the feed. The catalyst had 100% selectivity until 45% conversion after which it decreased dramatically (Figure 21) [113].



**Figure 21.** Selectivity of  $Fe_2(MoO_4)/MoO_3/CaO = 1/0.7/0.3$  towards  $CH_2O$  from  $CH_3OH$  at varying conversions at 300 °C. Reprinted with permission from [113].

The very sudden decrease in selectivity was different from the expectations, which would be a more gradual decrease in selectivity.

Na containing compounds was shown by Popov et al. [114] to have a significant impact on the activity of FeMo catalysts as 0.4 wt% Na added as Na<sub>2</sub>MoO<sub>4</sub>, NaCl, or NaNO<sub>3</sub> decreased activity with a factor of 10 and 12 for Mo/Fe = 2.5 and 1.5 catalysts, respectively. For samples supported on SiO<sub>2</sub>, a decrease in selectivity was also observed. The sample activity decreased exponentially with Na content in the sample. NaCl produced an even higher decrease in activity, and this was explained by the formation of molybdenum dioxychloride by Reaction (25), which was very volatile and evaporates at 400 °C, thus, decreasing the Mo content [114].

$$2NaCl + MoO_3 \rightarrow Na_2MoO_4 + MoO_2Cl_2$$
(25)

The catalytic properties of Cr-Mo oxide catalysts with Mo/Cr ratios of 0.4–6.5 were investigated by Popov et al. [115,116] who found maximum activity and selectivity at Mo/Cr = 1.6-1.9, similarly to what they observed for FeMo catalysts. With 6.5 vol.% MeOH in the feed at 300 °C, they achieved 96.9% and 96.2% selectivity at 85.4% and 87% conversion for the Mo/Cr = 1.6 and 1.9 catalysts, respectively, and >99.5% selectivity at <21.2% conversion. This was similarly to the FeMo catalysts, which had 96.6% and 97.5% selectivity at 83% conversion and 99.7% and 99.8% selectivity at 20% conversion for Mo/Fe = 1.75 and 2.5. Mo/Cr = 1.9 with particle size 0.25–0.5 mm losing 25% of its activity over 50 h at 300 °C with 2.2 mmol/L MeOH. The Mo/Fe = 1.75 catalyst with similar particle size lost 80% of its activity. Chromium molybdate was, thus, more stable [115]; however, as Cr is highly poisonous, it is not fully viable to use chromium molybdates. The oxidation of MeOH with air and its kinetics on a Cr-Mo oxide (Cr/Mo ~ 3) catalyst supported on porous  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> were further investigated by the same group [117] at 300–350 °C. The kinetics behaved similarly to the FeMo, with decreasing selectivity at higher temperatures. The activation energy for FA oxidation was determined to be lower than for MeOH oxidation, thus implying an optimum temperature where the catalyst was most selective. There was no significant inhibition from  $H_2O$  nor FA. The extent of oxidation of FA to  $CO/CO_2$  was reported to be 150% larger with no MeOH present in the gas [117]. The effect of Na on the activity was investigated by Ivanov et al. [118], who found that less than 0.2 wt% of Na from the precipitation did not have a large influence, but larger quantities from the precipitation or even small quantities by impregnation significantly reduced the activity. The formation of Na<sub>2</sub>O·Cr<sub>2</sub>O<sub>3</sub>·3MoO<sub>3</sub> was observed by XRD [118]. Similar trends for the addition of Na to  $Fe_2(MoO_4)_3$  were reported in [119]. A study on alkali salts showed them to be active for the dehydrogenation of MeOH to anhydrous FA with a maximum of 75% selectivity for NaCO<sub>3</sub> [120].

The preparation of Fe-Cr-Mo was studied by Del Arco et al. [121], who found the Mo content to be only dependent on Fe in the precipitation solutions; however, Cr content was very low in comparison and may, thus, have an influence that was not detected. A Fe-Cr-Mo oxide catalyst (Mo/(Fe+Cr) = 2.5/(0.5+0.5)) was investigated and compared with an industrial FeMo catalyst by Klissurski et al. [122]. They achieved a yield of above 80% at 275 °C. The Fe-Cr-Mo catalyst (0.3–0.6 mm) was tested at 400–420 °C with a MeOH concentration of 4%, where it had a constant activity for 100 h on stream in comparison to the industrial FeMo catalyst, which deactivated at about 20%. The catalysts were shown to be partly reduced under reaction conditions [122]. A catalyst prepared similarly and pure  $Fe_2(MoO_4)_3$  and  $Cr_2(MoO_4)_3$  were investigated for stability in MeOH reduction by Pesheva et al. [123].  $Cr_2(MoO_4)_3$  was much more stable than  $Fe_2(MoO_4)_3$ as XPS detected no changes after 2 h at 320 °C for Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>. A 45% reduction of Fe<sup>3+</sup> to  $Fe^{2+}$  was measured for  $Fe_2(MoO_4)_3$ , with only 30% reduction in the mixed FeCrMo sample. No reduction of  $Cr^{3+}$  nor  $Mo^{6+}$  was measured. Surface enrichment with  $Cr^{3+}$  was observed during reduction but was reversible upon oxidation. The Mo/(Fe+Cr) ratio was permanently decreased by the reduction experiment, implying volatilization of Mo. Cr3+ was concluded to have a promoting effect on the reduction stability of Fe<sup>3+</sup> in addition to its own higher stability [123]. A TAP reactor study of an Fe-Cr-Mo catalyst was performed by Lafyatis et al. [67]. The only products in significant quantity were H<sub>2</sub>O and FA [67].

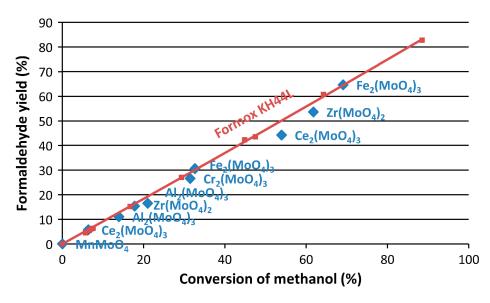
Popov and Bibin [124] investigated  $Bi_2O_3$  and  $Bi_2(MoO_4)_3$  at 250–350 °C. The  $Bi_2O_3$ mostly made CO<sub>2</sub> (selectivity towards CH<sub>2</sub>O was less than 3.2%), but Bi<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> had 85% selectivity to FA at 75% conversion at 300 °C, which, however, was lower than the 90% and 95% selectivity on  $Fe_2(MoO_4)_3$  and  $MoO_3$ , respectively. The activation energies were found to be similar (~75 kJ/mol) for  $Bi_2(MoO_4)_3$ ,  $Fe_2(MoO_4)_3$ , and  $MoO_3$  at 250–300 °C, but Bi<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> had an  $E_a$  of ~25 kJ/mol at higher temperatures, implying different reaction mechanisms at low and high temperatures as the same behavior was observed for  $B_2O_3$ at otherwise different rates, and it is lower than the  $E_{a,app}=E_a/2$  observed from diffusion limitations [124]. Arora et al. [125] investigated various Bi containing metal-oxide catalysts for FA formation by using a feed of 6 vol.% MeOH and 11 vol.% O<sub>2</sub> at 280 °C at less than 10% conversion. The best catalyst reported was a  $MoO_3/Bi_2O_3$ , calcined to yield  $\beta$ -Bi<sub>2</sub>Mo<sub>2</sub>O<sub>9</sub>, giving 97.2% selectivity towards FA, with the main by-product being DME. For MoO<sub>3</sub>/CeO<sub>2</sub>/Bi<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub>/Pr<sub>2</sub>O<sub>3</sub>/Bi<sub>2</sub>O<sub>3</sub>, and MoO<sub>3</sub>/La<sub>2</sub>O<sub>3</sub>/Bi<sub>2</sub>O<sub>3</sub>, selectivities of 94.5%, 93%, and 70% were achieved, respectively. For low loading  $MoO_3$  supported on  $Bi_2O_3$  and calcined at 300 °C, a selectivity of 95.2% was achieved, similarly to  $MoO_x$  on Fe<sub>2</sub>O<sub>3</sub> core-shell catalysts [29].

Mann and Hahn [126,127] investigated a system of 20 wt% MnO<sub>2</sub> on MoO<sub>3</sub>. They found that with increasing temperature, the selectivity was approximately 100% until 365 °C, where a conversion of 84% was achieved with an O<sub>2</sub>/MeOH ratio of 2.42. At 460 °C, the conversion increased to 100%, but the selectivity towards FA decreased to approximately 10% [126,127]. Ivanov et al. [128–130] also investigated the manganese oxide system and found MnMoO<sub>4</sub> with a small excess of Mo to be the most active and selective (>94% selectivity at up to 95% conversion at 300–350 °C) with a higher thermal stability than the FeMo catalyst [128–130]. Manganese(II) molybdates were found by researchers at Topsøe to have reasonable activity and selectivity, but the stability was not good enough [131].

More recently, an investigation of the molybdates  $Al_2(MoO_4)_3$ ,  $Ce_2(MoO_4)_3$ ,  $Cr_2(MoO_4)_3$ ,  $Fe_2(MoO_4)_3$ ,  $MnMoO_4$ , and  $Zr(MoO_4)_2$  was performed by Andersson et al. [6] and was compared to the Formox KH44L commercial catalyst at 300 °C with 10 vol.% MeOH and 10 vol.% O<sub>2</sub> in the feed. None of the alternative molybdates performed as well as the Formox KH44L or pure  $Fe_2(MoO_4)_3$ . Especially at conversions above 50%, the selectivity of, e.g.,  $Zr(MoO_4)_2$  and  $Ce_2(MoO_4)_2$  was 76–87% compared to 93–95% for Formox KH44L and  $Fe_2(MoO_4)_3$  (Figure 22). In general, they found the performance of the alternative catalysts worse than previously reported, in agreement with there being no examples of industrial implementations.

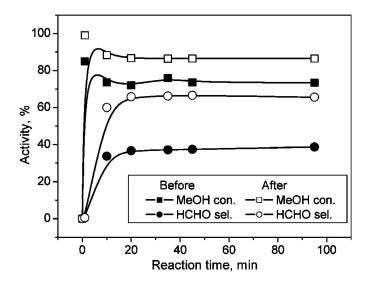
MoO<sub>3</sub>-WO<sub>3</sub> mixtures were investigated by Mann et al. [132] who achieved 95% selectivity at 95.6% conversion at 480 °C,  $W/F = 48.0 \text{ g}_{cat} \cdot h/\text{mol}$ , and 10 vol.% MeOH in the feed. They fitted the kinetics to a two stage redox mechanism [132]. The WO<sub>3</sub> was reported to be essentially inactive by Machiels et al. [133] as the activity reported per surface Mo was unchanged with changing Mo/W ratios.

Ivanov et al. [119,134] investigated the effect of incorporation of up to 15.9 wt% WO<sub>3</sub> into Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, where the formation of a mixed Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>-Fe<sub>2</sub>(WO<sub>3</sub>)<sub>3</sub>-MoO<sub>3</sub> oxide was observed by XRD and Mössbauer spectroscopy. An optimum in the activity and selectivity was found at 4.9 wt% WO<sub>3</sub> with 96.3% selectivity and 97% conversion at 350 °C with the major byproducts being CO and DME [134]. The Topsøe group found FeMo with WO<sub>3</sub> instead of excess MoO<sub>3</sub> showed loss of MoO<sub>3</sub> from Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> and formation of Fe<sub>2</sub>(WO<sub>4</sub>)<sub>3</sub> [131].



**Figure 22.** Comparison of catalyst performance of various molybdates to the Formox KH44L commercial catalyst showed as yield vs. conversion. T = 300 °C. Feed: 6 vol.% MeOH and 11 vol.% O<sub>2</sub> in inert gas. Flow: 227–277 mL/min. Catalyst loading: 25–1000 mg catalyst (surface area of catalyst 0.1–3 m<sup>2</sup>). Particle size: 0.215–0.425 mm. Reprinted with permission from [6] Springer, Topics in catalysis, Copyright © (2016).

A Mo based mixed oxide catalyst with composition  $Mo_{0.65}V_{0.25}W_{0.10}$  was investigated for FA production by Ramachandra et al. [135]. Thermal treatment at 540 °C for 2 h in pure N<sub>2</sub> increased the activity and selectivity substantially; however, it was still not higher than 65% selectivity for FA at nearly 90% conversion of MeOH (Figure 23) [135].



**Figure 23.** Activity of a  $Mo_{0.65}V_{0.25}W_{0.10}$  mixed oxide catalyst as function of reaction time at 350 °C before and after heat treatment at 540 °C for 2 h in N<sub>2</sub>. Feed:  $O_2/CH_3OH = 1.47$ . Reprinted with permission from [135] Springer, Catalysis Letters, Copyright © (1969).

Three multicomponent catalysts (K1:  $Mo_{12}Ni_{4.5}Co_4FeBiO_x$ , K2:  $Mo_{12}Ni_{4.5}Co_4FeBiTl_{0.3}P_{0.08}$ O<sub>x</sub>, and K3:  $Mo_{12}Ni_{4.5}Co_4FeBiTl_{0.3}P_{0.08}O_x/SiO_2$ ) with a particle size of 0.3–0.6 mm, 250 mg cat, and 240 mL/min were investigated by Klissurski et al. [136] at 270–420 °C inlet temperature and 3.5 vol.% MeOH in air. The catalysts were prepared by simultaneous evaporation of an aqueous solution of ammonium paramolybdate and corresponding metal nitrates, with subsequent addition of phosphoric acid and Tl nitrate for K2. For all the catalysts, high selectivities were achieved (>97% for 360, 370, and 390 °C). During extended measurements, the deactivation was 30% within 80 h for K1, while for K2 and K3 it was around 5–10% in 60 days, at conversions of 50–60% [136].

Klissurski et al. [137] further investigated  $MoO_3$  supported on montmorillo Al-type pillared clays from 320–440 °C for selective oxidation of MeOH to FA. The catalysts did not show great selectivity towards FA.

Mann and Dosi [138] investigated catalysts of mixed  $V_2O_5$ -MoO<sub>3</sub>. They found an optimum of 20%  $V_2O_5$  to provide 100% selectivity at more than 99% conversion at 466 °C with a feed space velocity of 31.7 g<sub>cat</sub>/h/mol and 8 vol.% MeOH in air in the feed. Increasing V content further increased the conversion but decreased selectivity, where until 20%  $V_2O_5$  only an increase in selectivity was observed [138].

Molybdena was supported on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (6.9–58.5 wt% MoO<sub>3</sub>), TiO<sub>2</sub> (anatase and rutile) (1–25 wt% MoO<sub>3</sub>), ZrO<sub>2</sub> (1–25 wt% MoO<sub>3</sub>), and CeO<sub>2</sub> (5–25 wt% MoO<sub>3</sub>), and their activity for MeOH oxidation to FA was investigated by Matsuoka et al. [139] with 3.4 vol.% MeOH in the feed at 225 °C. The TOF of the oxides were in the order of ZrO<sub>2</sub> > TiO<sub>2</sub> > CeO<sub>2</sub> > Al<sub>2</sub>O<sub>3</sub>, with the order of the selectivities towards FA for the most selective samples being ZrO<sub>2</sub> > CeO<sub>2</sub> > TiO<sub>2</sub> > Al<sub>2</sub>O<sub>3</sub> with selectivities of 89%, 88%, 83%, and 66%, respectively, and the major byproducts being DME, MF, and DMM with small amounts of CO<sub>2</sub> and CO [139]. In our studies (see Supplementary Materials, Section 2.2.3, Figure S6, and Table S6) on MoO<sub>3</sub> supported on  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, the selectivity of 6.2 wt% MoO<sub>3</sub>/ $\alpha$ -Al<sub>2</sub>O<sub>3</sub> towards FA was very high (>93%) with DME being the main byproduct. With only 1 wt% MoO<sub>3</sub>, the CO<sub>2</sub> and CO

Burcham et al. [140] investigated the ligand effect of Fe, Al<sub>2</sub>O<sub>3</sub>, and TiO<sub>2</sub> on MoO<sub>3</sub> with 2000 ppm MeOH in the feed at differential conversions. The highest oxidation selectivity was obtained for MoO<sub>3</sub>/TiO<sub>2</sub> with 89.9% towards FA and CO<sub>x</sub> combined (reporting these combined makes it difficult to evaluate the usefulness of the catalyst), with 9% to MF and 1.4% to DME. Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> and MoO<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> only achieved 83% and 68% combined FA and CO<sub>x</sub> selectivity, respectively, but with DME selectivity of 17% and 32% making it the only side product [140]. The FA selectivity of the Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub> catalyst was unexpectedly low in this study; however, it might have been better with higher conversion (due to conversion of reversible by-products such as DME to FA at high conversion) and/or feed concentration of MeOH.

A series of  $MoO_3/SiO_2$  prepared by different researchers with different silicas and preparation methods was studied by in situ Raman spectroscopy and X-ray photo electron spectroscopy by Bañares et al. [141]. The surface Mo species were assigned to be isolated, highly distorted octahedral mono-oxo Mo structure. The Mo coverage was found to be the only relevant factor with respect to the catalytic properties for MeOH oxidation. All loadings above 0.1 Mo/nm<sup>2</sup> were found to be unstable due to transformation and aggregation into  $\beta$ -MoO<sub>3</sub>. The decrease in activity was found to be proportional with the decrease in the number of exposed Mo sites due to agglomeration.

In an investigation by Inokawa et al. [142] was conducted on group 6B elements supported on CeO<sub>2</sub>-ZrO<sub>2</sub>, among those which include MoO<sub>3</sub>, which produced the best selectivity of the investigated samples. A FA selectivity of 60% was found at 50% conversion at 375 °C. This was the best result in the investigated temperature interval of 275–450 °C [142]. Overall, a rather low selectivity was observed.

Niwa et al. [143] measured the ESR signal for Mo in a SnO<sub>2</sub>-MoO<sub>3</sub> catalyst under MeOH oxidation. Pure SnO<sub>2</sub> made CO<sub>2</sub>, but together with MoO<sub>3</sub> the catalyst showed selective activity from 180 °C. The SnO<sub>2</sub>-MoO<sub>3</sub> system was stated to have higher activity than compared to MoO<sub>3</sub>-TiO<sub>2</sub> (1/1), Fe<sub>2</sub>O<sub>3</sub>-MoO<sub>3</sub> (1/1), and Co<sub>3</sub>O<sub>5</sub>-MoO<sub>3</sub> (1/1). They concluded from following the Mo<sup>5+</sup> signal that the activity came from a Mo<sup>5+</sup>  $\Rightarrow$  Mo<sup>4+</sup> redox cycle, as no hysteresis behavior was observed upon changing the MeOH partial pressure, resulting in the belief that Mo<sup>5+</sup> was reduced to Mo<sup>4+</sup>, but Mo<sup>6+</sup> was not reduced [143]. Only little change in the activity and selectivity was found as the Mo/Sn ratio was changed from 9/1 to 3/7 [144]. In a later study, they stated that the Mo<sup>6+</sup> reduction rate was much smaller than that of  $Mo^{5+}$ ; thus,  $Mo^{5+}$  was a much more reactive oxidation site [145]. At 20% conversion, the selectivity towards other products than FA (mainly DME and MF) was stated to be negligible with 80% ML coverage of  $MoO_x$  on the  $SnO_2$  (a full ML coverage was reported not achievable, even with addition of more four times the theoretical amount of Mo for full surface coverage). Adsorption of MeOH on Brønsted acid sites on  $MoO_3$  instead of on  $SnO_2$  was found important for the selectivity in their studies [146–148]. Narishige and Niwa [149] exchanged  $SnO_2$  with  $ZrO_2$  and performed MeOH TPD experiments and found again that FA was formed on the surface of  $MoO_3$  and desorbed during the temperature ramp, while  $ZrO_2$  adsorbed MeOH strongly as dioxymethylene and carbonates as an intermediate to full oxidation [149]. The partial oxidation of MeOH on a coprecipitated mixed Sn-Mo oxide catalyst was investigated by Valente et al. [150], with the best selectivity towards FA being 43%; however, in most samples, the highest selectivity was towards methyl formate [150] in contrast to the reports by Niwa et al. [143–148]. However, the difference may be a result of comparing a mixed Sn-Mo oxide [150] with MoO<sub>3</sub> supported on SnO<sub>2</sub> [143–148].

The oxidation of MeOH to FA over a Sb-Mo oxide catalyst ( $Sb_2O_4/MoO_3$ ) prepared by impregnation was investigated by Mann and Diaz-Real [151] at 350 °C to 425 °C and 6 vol.% MeOH in air. A maximum in conversion and selectivity of 82% and 100%, respectively, was achieved at 400 °C and with a Sb<sub>2</sub>O<sub>4</sub>/MoO<sub>3</sub> ratio of two. The conversion was observed to increase with temperature, with no apparent decrease in selectivity [151]. Later, an investigation of the catalytic abilities of a mechanical mixture of  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> and  $MoO_3$  was conducted by Castillo et al. [152]. Even with only a mechanical mixture, a promoting effect of  $Sb_2O_4$  on MoO<sub>3</sub> was observed. The selectivity of the mixture was >99% at 350–450 °C, with 94% conversion at 450 °C. The selectivity was stated to be equal to or surpassing those of commercial FeMo catalysts. The promotional effect was suggested to be a result of remote spillover of oxygen from  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> increasing the rate of reoxidation of  $MoO_3$  [152]. Similar results have been proposed by Xiong et al. [153–155] for the oxidation of isobutene to methacrolein and ethanol to acetaldehyde at 420 and 450  $^\circ C$ by  $Fe_2(MoO_4)_3$  and  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> and  $Fe_2(MoO_4)_3$  mixed in n-pentane, agitated for 10 min by ultra-sonication, and then evaporated and dried. A-Sb<sub>2</sub>O<sub>4</sub> stabilized ethanol oxidation so that the conversion decreased less for the mixture than for pure FeMo. Furthermore, XRD showed less reduction of  $Fe_2(MoO_4)_3$  to  $FeMoO_4$  and  $MoO_2$  in the presence of  $\alpha$ - $Sb_2O_4$  [155]. This is in opposition with our own investigations of a mixed Mo-Sb oxide from co-precipitation (see Supplementary Materials, Section 2.2.3, Figure S6, and Table S6), which lost 58% of its activity within 8 h at 400 °C compared to 36% for 6.2 wt%  $MoO_3/\alpha$ -Al<sub>2</sub>O<sub>3</sub>. In our study (see Supplementary Materials, Section 2.2.3, Figure S6, and Table S6), a mixed Mo-Sb oxide was co-precipitated. Selectivity was found to be >98%, but a maximum conversion of 12.5% was achieved as the activity was low.

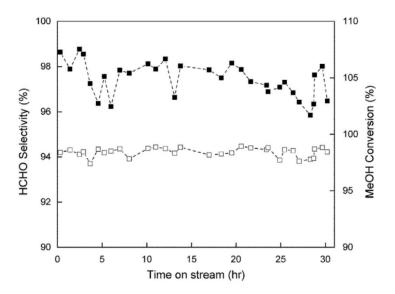
The oxidation of MeOH to FA over heteropolyacids (probably Keggin structure,  $H_{x-8}[XM_{12}O_{40}]^{x-8}$ , X = P, Si, As, Ge, etc.; M = Mo, W, V, and Co) and their salts has also been investigated [156]. The selectivity in the presence of the salts was higher than on the heteropolyacids because of their lower acidity. At 260 °C, with a contact time of 0.6 s, the selectivity towards FA from MeOH was 82% on CuPMo/SiO<sub>2</sub> with a conversion of 70%. The byproducts were DME and CO [156].

The catalytic properties of Mo phosphate,  $(MoO_2)_2P_2O_7$  promoted with V, was investigated by Whiting et al. [157] in the temperature range of 200–480 °C in a feed containing 5 vol.% MeOH. For pure Mo phosphate, the selectivity was 100%, 91.4%, and 89.5% at conversions of 5.3%, 50.8%, and 95.8% obtained at 200, 400, and 480 °C, respectively. The conversion increased when doping with V at all temperatures, and this was also the case for the selectivity at 400 °C, while it decreased slightly at 200 °C and a bit more at 480 °C. The promotion was concluded to stem from the formation of vanadium or vanadyl phosphate phases, which increased the reducibility of the catalyst [157].

At Haldor Topsøe, various alternative catalysts have been investigated [131].  $Li_{2.8}Fe_2Mo_{3.2}$  showed promising activity, selectivity, and stability in a sieve fraction of 150–300 µm at 450 °C

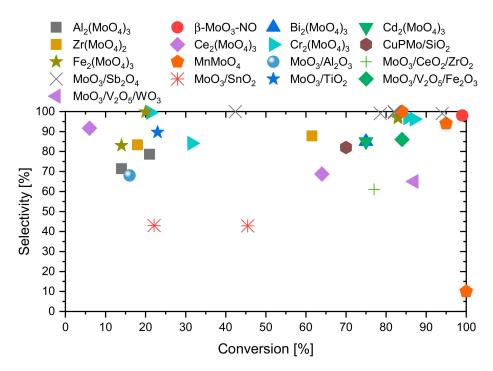
and 5 vol.% MeOH and 5 vol.%  $O_2$  in the feed. The investigation, however, was stopped since full conversion was difficult to obtain over the activated catalyst, and the activity and selectivity were found to be insufficient when the catalyst was tested as whole pellets. Furthermore, the pellets were found to be fragile and suffered from  $MoO_3$  evaporation [131]. The Topsøe group found that  $FeCr(MoO_4)_3$  was more stable towards  $MoO_3$  loss than  $Fe_2(MoO_4)_3$ . When investigating pure  $Cr_2(MoO_4)_3$ , the stability of the system was good; however, selectivity was only approximately 90%. For  $Al_2(MoO_4)_3$ , the selectivity was not satisfying, and the catalyst deactivated quickly and became even less selective. This also showed that there are other important factors than the molybdate ion and crystal structure, as Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, Al<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, and  $Fe_2(MoO_4)_3$  are isostructural [158]. Upon incorporation of Al into hematite with subsequent addition of 1 to 3 ML of Mo to the surface, an increase in surface area was not only achieved but also increased CO and  $CO_2$  formation [159]. Bi molybdates were investigated and were discarded due to too low selectivity for FA over Bi<sub>2</sub>MoO<sub>6</sub> (87–89%) and too low activity for FA over  $Bi_2(MoO_4)_3$ , which, however, showed high selectivity (97%). CoMoO\_4 and CuMoO\_4 had too low activity, while NiMoO<sub>4</sub> had too low selectivity. FeMo in a mechanical mixture with Sb<sub>2</sub>O<sub>4</sub> and no excess MoO<sub>3</sub> showed "surprisingly" fast deactivation. Lastly,  $\alpha$ -FeMoO<sub>4</sub>,  $\beta$ -FeMoO<sub>4</sub>, Cs<sub>3</sub>Pmo<sub>12</sub>O<sub>40</sub>, and Fe[Pmo<sub>12</sub>O<sub>40</sub>] have been tested. A-FeMoO<sub>4</sub> (low temperature structure [160]) had very low activity but good selectivity (>95%). B-FeMoO<sub>4</sub> (high temperature structure, formed at >400  $^{\circ}$ C [160]) had low selectivity (<81%) and low activity. Both of the  $[Pmo_{12}O_{40}]^{2-}$  salts had too low activity [131].

A study of nitric oxide (NO)-doped  $\beta$ -MoO<sub>3</sub> was performed by Pham et al. [161] at 260–350 °C achieving 99% conversion of MeOH with a selectivity of ~98% to FA at 320 °C at a catalyst to feed ratio of 28 g<sub>cat</sub>/h/mol. The NO-doped  $\beta$ -MoO<sub>3</sub> had a surface area trice that of their industrial reference. The NO-doping was inferred but not proven to have increased oxygen mobility. A stability test at 300 °C for 30 h was conducted with  $W/F = 70 \text{ g}_{cat}/h/mol$  (Figure 24), where the selectivity and conversion were both 98% for the test period [161]. Unfortunately, it is not possible to evaluate catalyst stability at such high conversion.



**Figure 24.** MeOH conversion ( $\Box$ ) and FA selectivity ( $\blacksquare$ ) over NO-doped  $\beta$ -MoO<sub>3</sub> at 300 °C *W*/*F* = 70 g<sub>cat</sub>/h/mol. Reprinted from [161] Copyright © (2016), with permission from Elsevier.

Most of the results reported in the literature for the Mo containing catalysts are summarized as selectivity as a function of conversion in Figure 25 (when possible). Interesting catalysts are found in the upper right corner of the figure, and relevant catalysts should show >95% conversion at high conversion such as the FeMo catalyst. High selectivity was reported for many molybdates, e.g., chromium, bismuth, and manganese molybdate, but molybdenum based catalysts with a reducible second component (e.g., Ce and Zr) and supported molybdenum oxide in general showed lower selectivity, with the antimony based catalysts as exception. One should be cautious when the conversion is reported to be "100%", as the selectivity is then influenced (negatively) by the residence time in the reactor near full conversion.



**Figure 25.** Summary of catalytic test results for Mo containing catalysts in the literature shown as selectivity vs. conversion [108,113,125,135,139,140,150–152,156,157].

#### 2.2.3. V Containing Catalysts

V oxides have been reported in the literature for a number of different selective oxidation reactions. Depending on the preparation method, it can have a number of different structural configurations. As a supported catalyst, it can yield isolated  $VO_x$  ions, dimeric or polymeric species, two-dimensional over-layers, three dimensional over-layers, mixed metal oxide surfaces, or a mixture of it all [162]. In addition, bulk vanadium oxide, mixed metal vanadates, and vanadyl phosphates are also tested as catalysts for selective oxidation reactions, including MeOH to FA.

**Vanadium phosphates.** In the late 1990s the catalytic activity of V-Ti aluminophosphate molecular sieve with MFI structure was investigated by Kapoor and Raj [163] in 20 vol.% MeOH and 10 vol.%  $O_2$  at 200 °C. A maximum selectivity of 79.2% was achieved with 5.73% conversion with CO being the largest byproduct and without Ti in the catalyst. The performance became worse when Ti was introduced to the structure [163].

Vanadyl phosphate catalysts were tested for MeOH oxidation by Whiting et al. [157]. For VOHPO<sub>4</sub>·0.5H<sub>2</sub>O and VOPO<sub>4</sub>·2H<sub>2</sub>O, the selectivities were 100%, 74.8%, 29%, and 100%, 98.6%, 78.4% at 200, 400, and 480 °C, respectively [157]. The use of V phosphates as catalysts for selective MeOH oxidation was investigated by Behera et al. [164,165]. They investigated the promotional effect of Al [164] and tungstate [165] in V phosphate, with a feed of 5 vol.% MeOH and 10 vol.% O<sub>2</sub>. It was found for Al promotion that 5% Al performed better than the other Al doped samples. One hundred percent selectivity was observed at 200 and 250 °C with conversions less than 30%. Selectivity decreased drastically with increasing temperature to 62% at 350 °C with 94% conversion [164]. For tungstate promotion, the catalyst containing 25 wt% WO<sub>3</sub> performed the best, with a selectivity of 98.9% at 200 °C, which decreased to 95.8% at 300 °C where full conversion was achieved. The yield of FA was 89.9% or better at 250–350 °C, which was the same as the industrial process but at lower temperatures. The promotional effect of WO<sub>3</sub> was thought to stem

from a combination of enhanced Brønsted acidity from  $WO_3$  and good redox properties of V phosphate [165]. The high selectivity of the V phosphates was confirmed in our study (see the Supplementary Materials, Section 2.2.2, Figure S8, and Table S8) by the synthesis methods by Behera et al. [164,165]. However, the activities were only moderate.

The Topsøe group [131] investigated a V oxide promoted with W, P, and Cs on TiO2, with a final composition of 3.9% V, 3.1% W, 0.79% P, and <0.22% Cs. The sample was found to have almost 100% selectivity at conversions of nearly 90% at a temperature of 330 °C. Above 330 °C, the selectivity decreased as CO and CO<sub>2</sub> formation increased. A study of V phosphate promoted by K and supported on TiO2 and SiO<sub>2</sub> was also conducted. The particle sizes were 300–500  $\mu$ m, gas feed of 5 vol.% MeOH, 5 vol.% O<sub>2</sub>, and 3 vol.% H<sub>2</sub>O in N<sub>2</sub>. Selectivities were high (>90%) at temperatures below 375 °C for all samples using TiO<sub>2</sub>, where the sample with 0.61 wt% V, 0.82 wt% K, and 1.05 wt% P had selectivities of 98% at 300 and 325 °C, 96% at 350 °C, 94% at 375 °C, and 91% at 400 °C. This was later investigated in a pilot plant where the temperature showed runaway behavior with a feed temperature of 250 °C, 8.4 vol.% MeOH, 10 vol.% O<sub>2</sub>, and 4 vol.% H<sub>2</sub>O in N<sub>2</sub>. This was also found for a similar catalyst with lower V content (0.6 wt% V, 0.9 wt% P, and 0.3 wt% K) when the MeOH concentration in the feed became too high (7%) with an inlet temperature of 280 °C. The same V, P, and K loadings were tested on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and also without K and with only V. In all cases, the DME and CO<sub>x</sub> selectivities were unacceptably high [131].

The results reported in the literature for vanadyl phosphate catalysts are summarized in Figure 26 as formaldehyde selectivity against conversion (when possible). The phosphates with high amounts of Al generally had lower selectivity (V-Ti-AlPO and V-AlPO), but lower amounts of Al (VPO-Al) was also detrimental for selectivity at higher conversions. VOHPO<sub>4</sub>·0.5H<sub>2</sub>O had too low selectivity as it was below 80%. VOPO<sub>4</sub>·2H<sub>2</sub>O had good selectivity (>95%) at low conversion, but it lost its selectivity near 100% conversion. MoPO-V had selectivity that was too low in general to be of real interest (~90%). In general, the vanadyl phosphates showed good selectivity at low conversions. The most promising vanadyl phosphate was the VPO-WO<sub>3</sub>, which had >95% selectivity at 100% conversion.

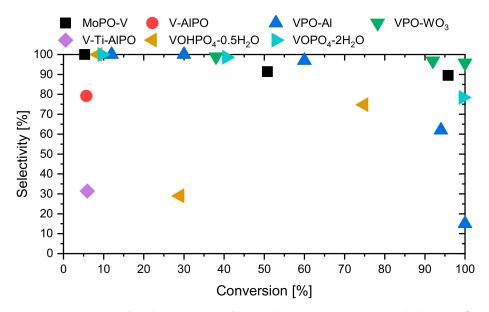


Figure 26. Summary of catalytic test results for vanadyl phosphate catalysts in the literature [157,163–165].

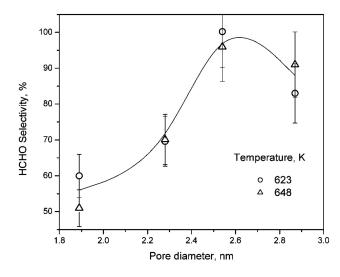
Vanadium mixed metal oxides and supported catalysts. In an investigation conducted by Klissurski and Pesheva [166], the temperature dependence of pure vanadia was investigated. The selectivity went from 100% at 250 °C to approximately 70% at 430 °C with 3.8 vol.% MeOH in the feed (O<sub>2</sub> concentration not specified) [86].

Smith et al. [167] investigated vanadia supported on SBA-15 at temperatures of 300-400 °C with 4 vol.% MeOH and 10 vol.% O<sub>2</sub> in the feed. The selectivity to FA was

never higher than 75%. It was reported that the surface roughness of SBA-15 represented by the surface fractal dimension ( $D_f$ ), calculated from the fractal-FHH equation (Frenkel–Halsey-Hill equation for multilayer adsorption)[168] as a measure of the micro porosity, was important for the selectivity at 300 °C, since the selectivity was 20% higher on rough surfaces than on smooth surfaces at the same conversion. The effect was observed to decrease at higher temperatures and conversions [167].

A study of a nanostructured VO<sub>x</sub>/SBA-15 model catalyst was performed by Hess [169] with 3 vol.% MeOH and 7 vol.% O<sub>2</sub> in the feed. At 350 °C, a selectivity of 94% was achieved with 15.7% conversion. It was stated that FA and the byproducts of MF and DMM were formed over redox sites, while DME and CO<sub>x</sub> were formed over acidic and basic sites, respectively [169]. This is in agreement with Figure 6.

An investigation of a V-MCM-41 catalyst (V incorporated in the crystal structure) with respect to the effect of pore diameter on the oxidation of MeOH to FA was performed by Yang et al. [170] with 3 vol.% of both MeOH and  $O_2$  in the feed. The study was motivated by reports of highly porous materials with large surface areas having positive influences on selectivity and activity for other reactions as well as on apparent acidic strength. Selectivity increased from approximately 60% at a pore diameter of 1.9 nm to 99% at 20% conversion at 350 °C at the optimum pore diameter of approximately 2.5 nm, which then decreased to below 85% selectivity at approximately 2.9 nm in pore diameter and 350 °C [170] (Figure 27).



**Figure 27.** Selectivity of MeOH oxidation to FA as function of pore diameter in V-MCM-41 catalyst at 350 °C and 375 °C in a feed of 3 vol.% MeOH and 3 vol.%  $O_2$  in He. Reprinted from [170] Copyright © (2005), with permission from Elsevier.

Such high influence from such small changes in the pore radius seems unlikely and may well be from the changes in the other synthesis parameters needed to change the pore size [171].

Mechanistic studies of V oxide supported on MCM-48 was performed by Bronkema and Bell [172,173]. The oxidized V was in the form of isolated VO<sub>4</sub> units (no evidence of V-O-V bonds was found). When adsorbing MeOH on the surface, V-OCH<sub>3</sub>/Si-OH or V-OH/Si-OCH<sub>3</sub> were formed in roughly equal amounts. FA was exclusively formed from the V-OCH<sub>3</sub> specie and was believed to happen by H-abstraction. The Si-OCH<sub>3</sub> was found to contribute to the formation of CO and CO<sub>2</sub>, which was especially observed at higher temperatures [172,173].

Guido Busca [35] made a FT-IR study of adsorption of MeOH, FA, and HCOOH on  $V_2O_5$  and  $V_2O_5/SiO_2$ . MeOH adsorbed as methoxy groups and was oxidized to dioxymethylene, which desorbed at 177 °C as dimethoxymethane. Dioxymethylene and polyoxymethylene species were observed to desorb near room temperature after adsorp-

tion of FA, leaving a clean surface. The results show that dioxymethylene is a common product on adsorption. No formate groups were found from adsorbing MeOH nor FA [35]. Kortewille et al. [8] showed isolated VO<sub>4</sub> species on SiO<sub>2</sub> being able to convert methoxy species to FA by following C-H vibrational bands in DRIFTS under a TPD procedure [8].

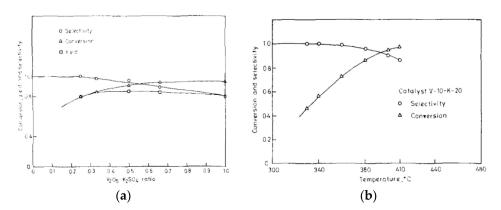
A DFT study on V oxide supported on SiO<sub>2</sub> by Döbler et al. [174] proposed the oxidation of MeOH to FA to occur through a two-step redox mechanism, dissociative adsorption of MeOH forming a methoxy group, and the rate-limiting H abstraction step from the methoxy group. They studied  $O=V(OCH_3)_3$ ,  $(O=V(OCH_3)_3)_2$ , and  $O=V(OCH_3)_3^{\bullet+}$  as model molecules in addition to the  $V=Si_7O_{12}H_7$  molecule, as the catalysts for the selective oxidation. A proposal of the support effect arising from the strength of adsorption was made as the energy barrier for the H abstraction was found to be very similar [174].

The influence of preparation pH and V surface species was evaluated by Trejda et al. [175] for V<sub>x</sub>SiBeta catalysts with x = 0.25–4.0 wt% V with 40 mg of catalyst in a flow of 40 mL/min consisting of Ar/O<sub>2</sub>/MeOH = 88/8/4 mol% at 250 °C. At low V loading and pH = 2.5, V was incorporated into the Beta framework evidenced by (SiO)<sub>2</sub>(HO)V=O vibrations in FT-IR increasing with increasing V content. For pH = 6, the incorporation only happened at higher loadings, and then only a fraction of the V was incorporated. The MeOH conversion was 5% and 2% before the incorporation of V, respectively. This increased to 16% and 5% with 4.0 wt% V, while DME selectivity decreased from 100 to 32% and 37%, FA selectivity increased to 44% and 45% and total partial oxidation selectivity increased to 67% and 65%, respectively [175] (not taking into account that DMM and MF are also reversible products from dehydration reactions). The pseudo-tetrahedral hydroxylated (SiO)<sub>2</sub>(HO)V=O species were concluded to be responsible for the selectivity towards FA and the activity, acting as either redox or acidic and basic centers [175].

The redox dynamics of V impregnated into 3D Ferrierite and 2D ITQ-6 siliceous supports with 1–10 wt% V were investigated by Vieira et al. [176], who found that dispersion and stabilization of V oxides were improved by isolated silanol groups on the surface before impregnation. XRD, XAS, and DR-UV-Vis spectroscopy identified V to be highly dispersed at 1 wt% and 5 wt% V in Si-ITQ-6 with monomeric and polymeric species or oxide clusters while 10 wt% in Si-ITQ-6 and Si-FER showed formation V<sub>2</sub>O<sub>5</sub> clusters on the surface. EXAFS and XANES showed complete reduction of V<sup>5+</sup> to V<sup>4+</sup> and back by isothermal periods of non-oxidizing atmosphere followed by regeneration with O<sub>2</sub>. All V species were concluded to be active in the oxidation of MeOH albeit with different rates due to differences in the V<sup>5+</sup>/V<sup>4+</sup> equilibrium under oxidant conditions as reoxidation was limited [176]. In a study by Zhang et al. [177] on co-electrospun VtiO<sub>x</sub> hollow nanofibers, a yield of 90% MF was reached at 150 °C and was attributed to a high surface content of V<sup>4+</sup> [177].

A catalyst consisting of 10% V<sub>2</sub>O<sub>5</sub>, 20% K<sub>2</sub>SO<sub>4</sub>, and 70% SiO<sub>2</sub> gel was chosen as an optimum composition for the vanadia-potassium sulfate system and subjected to MeOH oxidation at 330–410 °C (Figure 28a) by Agarwal et al. [178]. It showed 100% selectivity below 340 °C and 55% conversion, which decreased to ~85% at 410 °C and 95% conversion (Figure 28b). The improved selectivity from K<sub>2</sub>SO<sub>4</sub> promotion was proposed to be a result of the weakening strength of the V=O bond [178].

In the 1980s, investigations of MLs of V on support oxides picked up speed with the investigation by Roozeboom et al. [179] of a ML V on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub>, TiO<sub>2</sub>, and ZrO<sub>2</sub> as catalyst for MeOH oxidation at temperatures between 100 and 400 °C with 4 vol.% MeOH in the feed. The order of selectivity was V<sub>2</sub>O<sub>5</sub> > V<sub>2</sub>O<sub>5</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> > V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> > V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub> > V<sub>2</sub>O<sub>5</sub>/ZrO<sub>2</sub> at the temperatures, which gave 50% conversion with a fixed loading of 0.2 g catalyst and a feed flow of 40 NmL/min. The order of the selectivities was the reverse of the reducibility of the catalysts, except for V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> being more reducible than V<sub>2</sub>O<sub>5</sub>/CeO<sub>2</sub>. Basic oxides such as ZrO<sub>2</sub> and CeO<sub>2</sub> yielded CO<sub>2</sub> already at 200–250 °C [179]. This is in accordance with Figure 6.

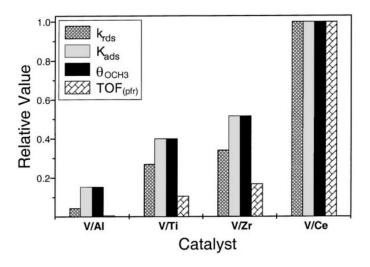


**Figure 28.** (a) Effect of catalyst composition on conversion, yield, and selectivity:  $W/F = 42.0 \text{ g}\cdot\text{h/mol}$ ,  $T = 410 \,^{\circ}\text{C}$ , and 10 vol.% MeOH in air. (b) Effect of temperature on conversion and selectivity for  $W/F = 41 \text{g}\cdot\text{h/mol}$  and 10 vol.% MeOH in air. Reprinted from [178] Copyright © (1978), with permission from Elsevier.

The catalytic activity ranking of vanadia supported on oxides was investigated by Deo and Wachs [180] for SiO<sub>2</sub>, ZrO<sub>2</sub>, TiO<sub>2</sub>, Nb<sub>2</sub>O<sub>3</sub>, and Al<sub>2</sub>O<sub>3</sub>. At 230 °C and 6 vol.% MeOH in the feed, the TOFs were ranked  $SiO_2 < Al_2O_3 < Nb_2O_5 < TiO_2 < ZrO_2$ , while selectivity was ranked  $Al_2O_3 < SiO_2 < ZrO_2 < Nb_2O_5 < TiO_2$ , where the by-products was mostly DME. Deo and Wachs [180] found the same tendency for reducibility as Roozeboom et al. [179], although the measured values differed significantly due to differences in conditions and setup. The pre-exponential factors were found to depend on the support [180]. Activity ranking was supported by Fievez et al. [181] and by later work in the Wachs group [100]. Kaichev at al. [182] investigated the catalytic properties for V oxide on SiO<sub>2</sub>,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>,  $ZrO_2$ , and  $TiO_2$  at 100–250 °C, where at low temperature and conversion, all samples had selectivities towards DMM > 80% and mostly MF at higher temperatures. Crystalline  $V_2O_5$ species were formed on SiO<sub>2</sub> and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, which were less active than the monomeric  $VO_x$  species formed on  $ZrO_2$  and  $TiO_2$ , which were less active than the polymeric  $(VO_x)_n$ species on TiO<sub>2</sub> [182]. In another study, the  $V_2O_5$  crystals were reported to be formed on  $ZrO_2$  regardless of V content, whereas  $V_2O_5$  crystallites only formed above the amount for an ideal ML on TiO<sub>2</sub> [183].

The origin of the support effect of metal oxides was investigated by Burcham and Wachs [184] regarding the TOF values on vanadia supported on CeO<sub>2</sub>, ZrO<sub>2</sub>, TiO<sub>2</sub>, and Al<sub>2</sub>O<sub>3</sub>. The surface steady-state concentration of methoxy exhibited the same tendency as the TOF values in a fixed bed reactor ( $V_2O_5/CeO_2 > V_2O_5/ZrO_2 > V_2O_5/TiO_2 > V_2O_5/Al_2O_3$ ), arising from changes in desorption and adsorption constants (Figure 29) [184].

This was further investigated by Burcham et al. [140]. However, in the presentation of the results, there was no distinction between FA and  $CO_x$ , which renders the selectivities difficult to interpret. The ligand effect was concluded to come from the electronegativity of the support cation. The electropositive (basic) supports (CeO<sub>2</sub> and TiO<sub>2</sub>) always have higher TOFs than the electronegative (acidic) supports (SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>) [140]. Kim and Wachs [185] prepared a series of supported V<sub>2</sub>O<sub>5</sub> (1–27%) on Al<sub>2</sub>O<sub>3</sub>. They found that, above ML coverage, the activity decreased because crystalline V<sub>2</sub>O<sub>5</sub> covered the active [VO<sub>4</sub>] redox surface sites. They found no correlation between activity and surface acidity nor reducibility measured by H<sub>2</sub>-TPR.



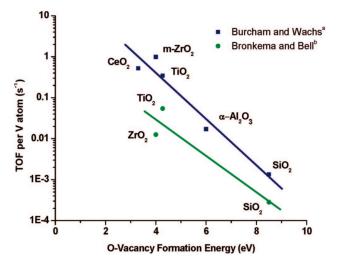
**Figure 29.** Relative changes in kinetic parameters, methoxy coverage, and TOF as function of support at 225 °C. Reprinted from [184] Copyright © (1999), with permission from Elsevier.

Khaliullin and Bell [186] investigated the oxidation of MeOH to FA by DFT calculations of VO<sub>4</sub> isolated surface units on SiO<sub>2</sub>, ZrO<sub>2</sub>, and TiO<sub>2</sub> by using the B3LYP/6–31G\* functional, finding good geometric agreement with experimental investigations. However, they found  $E_a$  of MeOH oxidation to FA to be independent of the support and higher than the experimental values. It was proposed that the methoxy group broke the V-O-M bond upon adsorption and that the abstraction of H from the methoxy group adsorbed to V=O could be by transfer of H to an adjacent VO<sub>4</sub> unit or dimer unit (V<sub>2</sub>O<sub>7</sub>) [186]. The dimer units have been reported on TiO<sub>2</sub> and ZrO<sub>2</sub> but not on SiO<sub>2</sub> [182]. This would explain why the theoretical investigation could not reproduce the difference in rate observed by experiments [186]. This conclusion/proposal was questioned by Zhanpeisov [187] as he strongly disagreed with Zr and Ti having tetrahedral VO<sub>4</sub> surface units but octahedral instead. He stated that breaking of the V-O-M bond was not necessary and that with proper use of the cluster models (tetrahedral vs. octahedral), the difference in TOF was readily described with the B3LYP/6–31G\* functionals without the need of adjacent VO<sub>4</sub> units or dimers [187].

The industrial V<sub>2</sub>O<sub>5</sub>-TiO<sub>2</sub> catalyst for oxidation of o-xylene was tested for MeOH oxidation by Makedonski et al. [188] with 3.5 vol.% MeOH in the feed and a conversion of 20%. The catalysts were found to have high selectivity to FA at low temperatures of 200–330 °C, but selectivity decreased with increasing temperature [188].

A mechanistic study of isolated vanadate sites supported on high surface area anatase utilizing temperature programmed experiments, IR, Raman, and XANES performed by Bronkema et al. [173] showed V to be in VO<sub>4</sub> units after calcination. At 50 °C, MeOH adsorbed in three different ways: (1) molecularly, (2) Ti-OCH<sub>3</sub>/Ti-OH, and (3) V-OCH<sub>3</sub>/Ti-OH. Upon heating, TiO<sub>2</sub> produced small amounts of FA; however, small additions of V greatly improved the rate of FA formation. It was believed to stem from reverse spillover of methoxy species from Ti to V.  $E_{a,app}$  was found to be at 67 kJ/mol. Most of the difference in activity for V on SiO<sub>2</sub> and TiO<sub>2</sub> comes from the difference in  $E_a$  (96 kJ/mol when supported on SiO<sub>2</sub>) [173]. Similar adsorption species were found when ZrO<sub>2</sub> was used as support with an  $E_a$  of 75 kJ/mol [189].

A theoretical investigation of isolated vanadate species on TiO<sub>2</sub> was conducted by Goodrow and Bell [190] in order to understand why VO<sub>x</sub>/TiO<sub>2</sub> was three orders of magnitude more active than VO<sub>x</sub>/SiO<sub>2</sub>. The difference did not arise from intrinsic electronic effects on the active site of the support but from the difference in O-vacancy formation next to the active site where the concentration is larger for TiO<sub>2</sub> but Ti<sup>4+</sup> also becomes Ti<sup>3+</sup> and increases lattice Ti–Ti distance, where the lattice distance becomes smaller in SiO<sub>2</sub>. The calculations showed  $E_a$  to proceed from 95.4 to 66.5 kJ/mol when introducing an O-vacancy in TiO<sub>2</sub> next to a vanadate site. A correlation between TOF per V atom and the O-vacancy formation energy was also presented with experimental data from other work (Figure 30) [190].



**Figure 30.** TOF per V atom for MeOH oxidation as function of the O-vacancy formation energy. <sup>a</sup> [184]; <sup>b</sup> [172,173,189]. Reprinted from [190] Copyright © (2008) American Chemical Society.

The reaction mechanism and kinetics of MeOH oxidation to FA of vanadia supported on TiO<sub>2</sub> have been investigated by González-Navarrete et al. [191] by utilizing DFT calculations using the B3LYP functional. The most stable intermediate was methoxy on tetrahedral VO<sub>4</sub>, with the rate-limiting step being the abstraction of H from methoxy.  $E_a$ was 100 kJ/mol [191].

In a study by Busca et al. [192] on  $V_2O_5/TiO_2$ , the selectivity towards FA decreased drastically with increased temperature with an observed increase in selectivity towards MF first and CO later and CO<sub>2</sub> already at 200 °C with a ratio of 0.9 between CH<sub>3</sub>OH and O<sub>2</sub> [192].

The difference between isolated V, Mo, and Cr clusters supported on rutile  $TiO_2(110)$  was investigated by Kim et al. [193] by utilizing DFT calculations. By analyzing three different dehydration paths, the schemes were exoergic for the VO<sub>3</sub> cluster, while they were endoergic for MoO<sub>3</sub>. CrO<sub>3</sub> had one exoergic scheme and two endoergic schemes. The supported VO<sub>3</sub> cluster was concluded to be the better catalyst in terms of activity by far from having a much lower  $E_a$  than MoO<sub>3</sub> and CrO<sub>3</sub> [193].

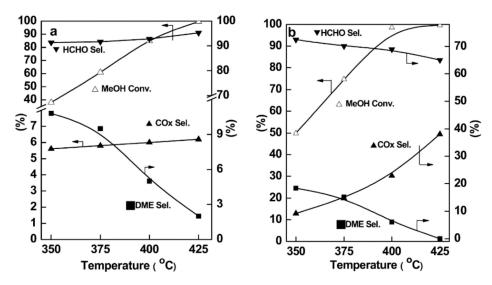
The role of CeO<sub>2</sub> in the oxidative dehydrogenation of MeOH on supported vanadia catalysts was investigated by Ganduglia-Pirovano et al. [194] by using  $VO_x/CeO_2(111)$ model catalysts. TPD measurements showed product desorption at much lower temperatures than for pure CeO<sub>2</sub> or vanadia supported on SiO<sub>2</sub>. Calculations using DFT also predicted increased reactivity of the vanadia/ CeO<sub>2</sub> from the hydrogenation and oxygen vacancy energies. The support effect was concluded to stem from CeO<sub>2</sub> stabilizing reduced states [194]. Oxidative dehydrogenation of MeOH on CeO<sub>2</sub> supported vanadia oligomers was investigated by using simulations by Kropp et al. [195] after an initial investigation on monomeric vanadia species [196]. The trimeric  $VO_x$  specie  $V_3O_6$  was the most thermodynamically stable species under slightly reducing conditions. The trimers were stated to bind MeOH less strongly than the monomers (VO<sub>2</sub> in VO<sub>4</sub> geometry with the surface O's in  $CeO_2$ ). This seemed to be only partly true from the trimers showing FA desorption at 227 °C, while the monomer showed desorption at 97 °C and 257 °C. The intrinsic barriers for MeOH oxidation were stated to be similar for  $V_3O_6$  and  $CeO_2$  (111), but they have pre-exponential factors differing by two orders of magnitude, making the V trimer more active [195].

A TPD study of CeO<sub>2</sub> supported V oxide was conducted by Feng and Vohs [197]. The primary desorption species of adsorbed MeOH on CeO<sub>2</sub> were MeOH and CO. Small

H-abstraction reaction, thus producing a higher  $E_a$  and lower reaction rate [197]. The structure and activity of VO<sub>x</sub>/SiO<sub>2</sub> and VO<sub>x</sub>/CeO<sub>2</sub>/SiO<sub>2</sub> catalysts were investigated by Vining et al. [198]. TOF was nearly two orders of magnitude larger for VO<sub>x</sub>/CeO<sub>2</sub>/SiO<sub>2</sub> compared to VO<sub>x</sub>/SiO<sub>2</sub> at 270 °C. In both cases, the vanadia existed as pseudo-tetrahedral vanadate species bonded to either SiO<sub>2</sub> or CeO<sub>2</sub>. The increase in activity was explained by a decrease in activation energy of the rate determining step of H-abstraction from methoxy bound to a V-O-Ce site compared to V-O-Si site [198].

and the lower oxidation states were concluded to destabilize the transition state of the

An investigation by Zhang et al. [199] examined utilizing SiO<sub>2</sub> supported Sb-V mixed oxide catalysts for MeOH conversion to FA. For a feed containing 1 vol.% MeOH, a one-pass yield of 91% was achieved on a VSbO<sub>x</sub>/SiO<sub>2</sub> catalyst at 425 °C. The mixed oxide catalyst had increasing selectivity to FA (due to increasing conversion of reversible by-products and no significant increase in overoxidation) with increasing temperature, whereas the selectivity decreased with increasing temperature if there was no Sb (Figure 31).

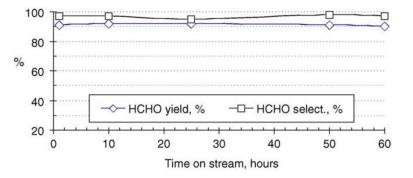


**Figure 31.** Catalytic conversion and selectivity of (**a**) 5.3 wt%  $V_2O_{5-}19.5$  wt%  $Sb_2O_5/SiO_2$  and (**b**) 5.4 wt%  $V_2O_5/SiO_2$  catalysts as function of temperature. Reprinted from [199] Copyright © (2008), with permission from Elsevier.

The active phase of the mixed oxide catalyst was found to be monomeric VO<sub>x</sub> species stabilized in the mixed oxide phase. The oxidation state of V could be influenced by the Sb/V ratio between the +5 and +4 state, where +5 was most active but +4 was most selective towards FA [199]. Guerrero-Pérez et al. [200] found that antimonates promoted the surface redox sites of V oxides. In our investigations of a V oxide supported on Sb oxide, a selectivity of 98.9% at 22.6% conversion at 400 °C was achieved (see Supplementary Materials, Section 2.2.2, Figure S8, and Table S8); thus, the selectivity was good, but the activity was too low compared to the industrial FeMo catalyst (selectivity of 98% at 97% conversion).

An investigation of the oxidative dehydrogenation of MeOH on a V-Mg-O catalysts was conducted by Isaguliants and Belomestnykh [201]. A 12 wt%  $V_2O_5$  catalyst calcined at 550 °C had above 97% selectivity in the range of 250–450 °C with a conversion of 95% at 450 °C with 17 vol.% MeOH in air in the feed. The catalyst contained pyrovanadate species, with  $V^{5+}$  and  $V^{4+}$  ions in octahedral and tetrahedral coordination. Over 60 h, the average

FA yield and selectivity were 91% and 97%, respectively, with no visible change in activity (Figure 32) [201]. However, it is difficult to observe any deactivation when the conversion is very high in the stability test.



**Figure 32.** Oxidative dehydrogenation of MeOH over V-Mg-O catalyst at 420 °C, LHSV of 1.5 h<sup>-1</sup>, and CH<sub>3</sub>OH/O<sub>2</sub> of 1/1. Reprinted from [201] Copyright © (2005), with permission from Elsevier.

Whether MgO may turn into MgCO<sub>3</sub> over time would have to be tested since experience has showed this carbonate to be rather stable [202]. The Topsøe group [131] has investigated  $V_2O_5/TiO_2$  and  $V_2O_5/MgO$ . Both catalysts were found to have high selectivity relative to FA until a certain temperature at which the non-selective oxidation to CO and CO<sub>2</sub> dominated, and the total consumption of MeOH was reached [131].

Experiments on vanadia supported on phosphate modified  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was conducted by Lakshmi et al. [203] at 175 °C with 4 vol.% MeOH in the feed. The highest conversion was 30.5%, and the total selectivity towards FA and DME was approximately 98% for the investigated catalyst loadings, with increasing conversion and selectivity to FA (decreasing towards DME) with higher vanadia loadings; thus, FA selectivity was 83.5% with 20 wt% vanadia [203].

In the 1980s, a V<sub>2</sub>O<sub>5</sub>-MoO<sub>3</sub>-TeO<sub>2</sub> catalyst was investigated by Bliznakov et al. [204] at 390–400 °C with 3.5 vol.% MeOH in the feed gas. When the catalyst loading of TeO<sub>2</sub> was 5–15 wt%, the reported selectivity was 100% relative to FA but only 94% with no TeO<sub>2</sub>. The distribution of V<sup>5+</sup> vs. V<sup>4+</sup> was measured ex situ. In all samples, more than 80% of the samples were in the 5+ state. Mo was present as Mo<sup>6+</sup> in the samples, and Te was present as Te<sup>4+</sup> at the surface [204]. Pesheva et al. [205] also investigated the mixed vanadia and molybdena supported on montmorillonite and compared to vanadia on montmorillonite. The Mo containing sample had higher selectivity but lower activity in the temperature range of 300–475 °C.

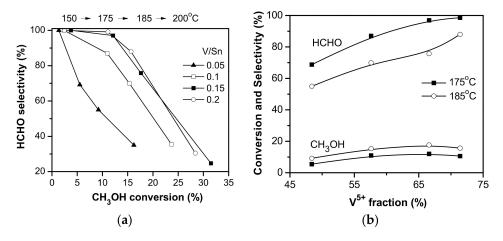
Arora et al. [125] investigated various Bi containing metal-oxide catalysts for MeOH oxidation in 6 vol.% MeOH and 11 vol.%  $O_2$  at 280 °C and less than 10% conversion. For  $V_2O_5/Bi_2O_3$ , a FA selectivity of 83.5% was achieved after calcination at 500 °C.

A mechanistic study of MeOH partial oxidation on  $V_2O_5(001)/Au(111)$  was conducted by Sturm et al. [206]. By STM, MeOH was found to form methoxy groups over the vanadyl oxygen vacancies and produce FA in the temperature range of 127–277 °C under temperature-programmed desorption, whereas MeOH only adsorbed molecularly on non-reduced surfaces; thus, no FA was formed [206].

The reactivity of V oxide supported on Sn oxide was investigated by Reddy [207] at 175 °C, with 4 vol.% MeOH in the feed. With 4.3%  $V_2O_5$  in the catalyst, selectivities of 97.6% and 2% towards FA and DME were achieved [207], which were quite good but also far from industrial reaction conditions.

The catalytic activity of V-Sn oxide catalysts was studied by Wang et al. [208] in 2.1 vol.% MeOH. The selectivity was found to be best at low temperatures and conversions and higher V loadings (Figure 33a). XPS showed that the V<sup>5+</sup> fraction increased with increased loading; thus, a correlation between selectivity, conversion, and V oxidation state

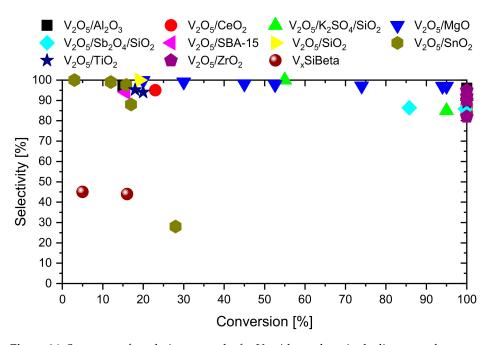
was found, which indicated  $V^{5+}$  to facilitate the chemisorption and partial oxidation of MeOH to FA Figure 33b).



**Figure 33.** (a) V-Sn catalyst activity and selectivity for MeOH oxidation to FA at temperatures 150–200 °C [208]. (b) MeOH conversion and selectivity towards  $CH_2O$  as function of  $V^{5+}$  fraction measured by XPS at the reaction temperatures 175 °C and 185 °C. Reprinted with permission from [208] © 2011 The American Ceramic Society.

Three wt% and five wt% V<sub>2</sub>O<sub>5</sub>/HAP were investigated by our group (see Supplementary Materials, Section 2.2.2, Tables S8 and S9, and Figures S8 and S9) and were found to be highly active with a selectivity of 94% at 77% conversion at 300 °C for the 5 wt% sample. The selectivity towards CO and CO<sub>2</sub>, however, increased drastically when proceeding close to full conversion. Similarly, it was found for 1 wt% V<sub>2</sub>O<sub>5</sub>/ $\alpha$ -Al<sub>2</sub>O<sub>3</sub> (see Supplementary Materials, Section 2.2.2, Tables S8 and S9, and Figures S8 and S9).

The results reported in the literature for vanadium oxide catalysts are summarized in Figure 34 as formaldehyde selectivity vs. conversion (when possible). From Figure 34, the danger with selectivities at full conversion is also exemplified, as there was more than 15% variation in the reported selectivity of  $V_2O_5/ZrO_2$ .

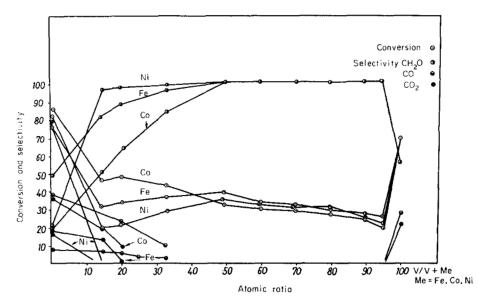


**Figure 34.** Summary of catalytic test results for V oxide catalysts in the literature shown as selectivity vs. conversion [125,140,166,169,179,180,188,199,201,203,204,207,208].

A general trend observed is the high activity of catalysts with a reducible support, e.g.,  $SnO_2$  and  $CeO_2$  [184,208], which, however, also had a tendency to over oxidize the MeOH to  $CO/CO_2$  at higher temperatures and result in conversions producing lower formaldehyde selectivities (Figure 34) [208]. Moreover, catalysts with basic supports such as  $ZrO_2$ ,  $TiO_2$ , and Bi oxides had, in general, high activity and good selectivity if the temperatures were low (points in Figure 34) [100,125,131]; however, at industrially relevant temperatures, they catalyzed full oxidation to CO and  $CO_2$  [125,131]. Vanadia supported on the more acidic  $Al_2O_3$  and  $SiO_2$  supports had higher selectivity towards dehydration products [100,199,203] and were generally less active than the basic and reducible supports [100,179,184].

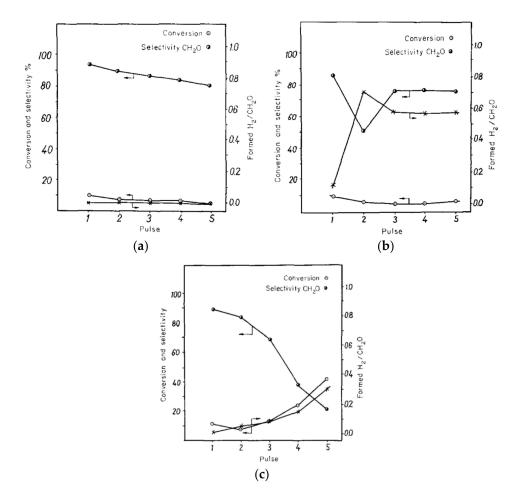
Many supported/mixed vanadium oxides have been investigated; however, most of them seem to have too low selectivity at the temperatures observed in the hot-spot under the industrial process (350 °C to 400 °C) and are, thus, of limited interest. The most promising candidate reported was the V<sub>2</sub>O<sub>5</sub>/MgO catalyst, which has been reported to have 97% selectivity also at high temperatures and conversion (~95%), although Topsøe [131] reported it to catalyze the total oxidation to CO and CO<sub>2</sub> in agreement with MgO being basic. In any case, a stability test sufficiently far from full conversion would be needed to assess applicability.

**Bulk vanadates and spinel-type catalysts.** Ni, Fe, and Co vanadates were investigated in the 1970s with V/(V+Me) ratios from 0 to 1 by Malinski et al. [209] (Figure 35) with an optimum at V/(V+Me) = 0.5 in conversion and V/(V+Me) = 0.5-0.95 for selectivity.



**Figure 35.** Effect of V to Fe, Co, and Ni ratio in vanadate catalysts after 1 h at a reaction temperature of 310 °C,  $W/F = 3.78 \text{ g}\cdot\text{h/mol}$ , 44 vol.% MeOH, and mole ratio MeOH/O<sub>2</sub> = 2.2 [209]. Reproduced from [209] Copyright 1976, with permission from Elsevier.

Pure V<sub>2</sub>O<sub>5</sub>, Fe<sub>2</sub>O<sub>3</sub>, NiO, and Co<sub>3</sub>O<sub>4</sub> all had higher activity and lower selectivity than the mixed oxides. The nickel vanadate was the most selective of the three vanadates reaching close to 100% selectivity already with V/Ni = 0.3. The three vanadates were also investigated by a MeOH pulsing experiment with no O<sub>2</sub> (Figure 36). The selectivity relative to FA over the Ni and Co vanadate decreased monotonically with number of pulses (Co much faster than Ni), whereas FeVO<sub>4</sub> had constant selectivity but interestingly had a much higher formation of H<sub>2</sub>, which for the NiVO<sub>4</sub> was very low and was increasing drastically for CoVO<sub>4</sub> with the number of pulses. In addition, the V=O bond disappeared in the cobalt vanadate but remained in the Ni and Fe vanadate [209]. The disappearance of the V=O bond in CoVO<sub>4</sub>, thus, seems linked to increasing hydrogen formation.



**Figure 36.** Overall conversion and selectivity in pulse reactions without  $O_2$  at 340 °C for (**a**) V/Ni = 1, (**b**) V/Fe = 1, and (**c**) V/Co = 1 [209]. Reproduced from [209] Copyright 1976, with permission from Elsevier.

The NiVO<sub>4</sub> system was further investigated as supported catalysts [210], which gave higher activity per surface area but lower selectivity. Furthermore, the V=O bond of the NiVO<sub>4</sub> was reported to be weaker than for  $V_2O_5$  and was given as an explanation for the increased selectivity of this phase [210].

The functionality of hexagonal orthovanadates ( $Sr_{3-x}La_{2x/3}(VO_4)_2$ , x=0.3-1.5) as catalysts for the oxidation of MeOH to FA was tested by Salagre and Sueiras [211] at 300 °C with 10 vol.% MeOH and 15 vol. O<sub>2</sub> in the feed. Seventy-eight percent selectivity was obtained for x = 1.1 and a MeOH conversion of 12%, which was significantly better than  $Sr_3(VO_4)_2$  and LaVO<sub>4</sub>, which had 0 and 3% selectivity, respectively [211].

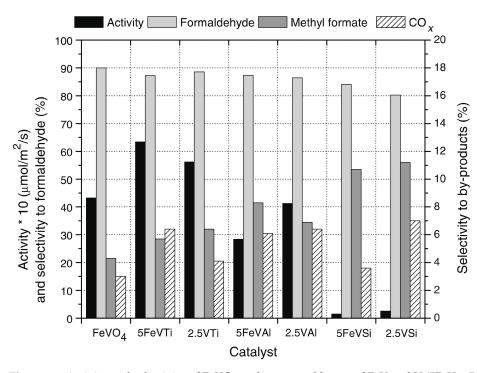
Arora et al. [125] achieved 93.1% selectivity relative to FA on Bi vanadates in a feed of 6 vol.% MeOH and 11 vol.%  $O_2$  at 280 °C at less than 10% conversion.

The Andersson group in Lund had performed investigations of V containing spineltype structures. Häggblad et al. [212] investigated a series of  $Fe_{1-x}Al_xVO_4$  with 6 vol.% MeOH in the feed at 350 °C. The selectivity increased for the first 16 h for all the samples, indicating structural rearrangements in the catalyst, snf they stabilized at approximately 90% selectivity towards FA after with less than 2% DME by-product formation when the conversion was between 95% and 98%. The activity was lower than for the reference pure V<sub>2</sub>O<sub>5</sub> catalyst; however, selectivity was better. The structure went from triclinic  $Fe_{1-x}Al_xVO_4$  phases to amorphous cation vacant spinel-type  $Fe_{1.5}V_{1.5}O_4$  on top of the stable bulk AlVO<sub>4</sub>, which was supported by HRTEM [212].

Häggblad et al. [213] then investigated the activity of cation vacant  $Fe_{3-x-y}V_x \Box_y O_4$  spinel phase catalyst ( $\Box$  denotes cation vacancies) at 300 °C and 10 vol.% MeOH in the

feed. The best selectivity was for a Fe/V ratio 2.8/0.2 (91%), and the second best was from 1/1 (90%). The specific activity was found to decrease with Fe content [213].

The Fe<sub>3-x-y</sub>V<sub>x</sub> $\Box_y$ O<sub>4</sub> catalyst was further investigated by Massa et al. [214] and compared to "theoretical" Fe-V-oxide layers (one theoretical layer was in this case defined as 12 µmol cations/m<sup>2</sup> surface area of the support) on TiO<sub>2</sub>,  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub> supports at the same conditions but with 80% conversion. None of the investigated supported samples had better selectivity than FeVO<sub>4</sub> ranging from 80–88%; however, the surface area specific activity was higher for the TiO<sub>2</sub> supported Fe-V-oxide and much lower for the SiO<sub>2</sub> supported catalysts (Figure 37). It was possible to stabilize FeVO<sub>4</sub> by pre-oxidizing the samples into a spinel-like structure with the same selectivity [214].

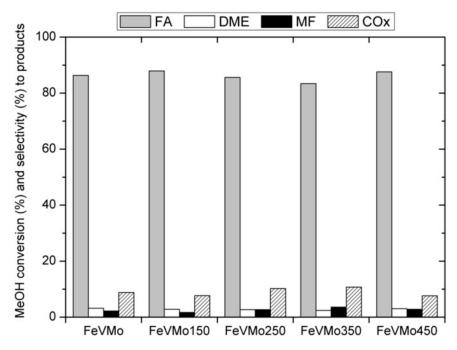


**Figure 37.** Activity and selectivity of FeVO<sub>4</sub> and supported layers of FeV and V (5FeV = 5 theoretical layers of FeV; 2.5V = 2.5 theoretical layers) on TiO<sub>2</sub>,  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub>. *T* = 300 °C. Composition: 10 vol.% MeOH and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. Conversion of 80%. Activities were measured at low conversions. Reprinted with permission from [214] Springer Science+Bussiness Media. Copyright © (2011).

A spinel-type catalyst of Fe, V, and Mo was investigated by Massa et al. [215] at 300 °C by using a mixture of 10 vol.% MeOH and 10 vol.%  $O_2$  in  $N_2$ . All the samples had selectivities of around 86% at 82–88% conversion, regardless of temperature-programmed pre-oxidation (Figure 38).

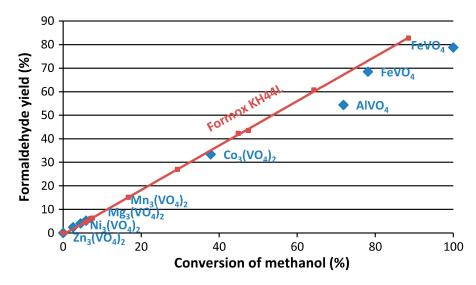
XANES and XPS showed that the surface metal ions were primarily in their highest oxidation state. The  $Fe_{2.5}V_{0.2}Mo_{0.5}O_y$  catalyst was less selective than the commercial type FeMo catalyst, producing 93% FA selectivity [215].

The selectivity of approximately 90% for FeVO<sub>4</sub> towards CH<sub>2</sub>O was reproduced by our group (see Supplementary Materials, Section 2.2.2, Tables S8 and S9, and Figures S8 and S9), with the main byproduct being CO. FeVO<sub>4</sub> was by far the most active sample in our tests. By impregnation with 1 wt% NH<sub>4</sub>Cl, the selectivity towards FA was significantly improved by suppressing CO formation. Thus, the selectivity was 97.5% instead of 88.2% at 300 °C.



**Figure 38.** Selectivities to formaldehyde (FA), dimethyl ether (DME), methyl formate (MF), and carbon oxides over Fe-V-Mo-O spinel-type catalyst preoxidized up to different temperatures in the temperature programmed oxidation. The selectivities are taken after 16 h at a steady-state at 300 °C with a feed flow of 100 mL/min of 10 vol.% MeOH and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. The conversions were in the range of 82–88%. Reprinted from [215] Copyright © (2011), with permission from Elsevier.

Different vanadates (AlVO<sub>4</sub>, Co<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>, FeVO<sub>4</sub>, Mg<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>, Mn<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>, Ni<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>, and Zn<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>) were investigated by Andersson et al. [6] and compared against the commercial Formox KH44L catalyst at 300 °C with 6 vol.% MeOH and 11 vol.% O<sub>2</sub> in inert gas (Figure 39).

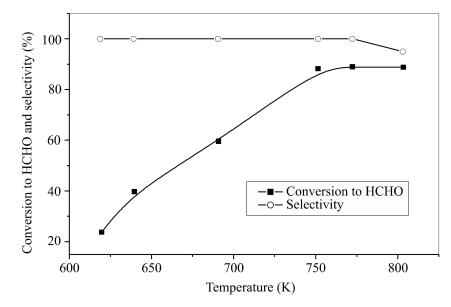


**Figure 39.** Comparison of catalytic performance of various vanadates to the Formox KH44L commercial catalyst shown as yield vs. conversion. T = 300 °C. Feed: 6 vol.% MeOH and 11 vol.% O<sub>2</sub> in inert gas. Flow: 227–277 mL/min. Catalyst loading: 25–1000 mg catalyst (surface area of catalyst 0.1–3 m<sup>2</sup>). Particle size: 0.215–0.425 mm. Reprinted with permission from [6] Springer, Topics in catalysis, Copyright © (2016).

The selectivities of  $AIVO_4$  and  $FeVO_4$  were between 76% and 87% when the conversion was above 50% [6]. All the other vanadates must be assumed to have had low activity, but

since no information on the amount or surface area of the samples in the reactor was given, this is unclear.

Selective oxidation of MeOH on FeVO<sub>4</sub> catalysts was investigated by Klissurski et al. [216]. The catalyst consisted of a single-phase Fe(III) vanadate. Mössbauer spectroscopy showed Fe(III) to be in a high spin state at various crystallographic sites.  $V^{5+}$  was partially reduced to  $V^{4+}$  on the surface during reaction, as measured by XPS. An increase in V content at the surface was also observed. The selectivity relative to FA was 100% at temperatures of 500 °C and below, while selectivity fell to 93% at 530 °C with 6.5 vol.% MeOH in the feed (Figure 40) [216], thus reporting better selectivity results than the Andersson group [6,212].



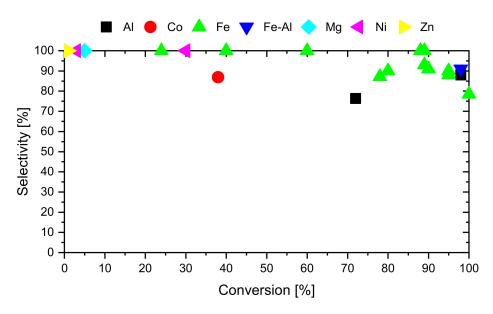
**Figure 40.** Temperature dependence of MeOH conversion and selectivity towards FA for FeVO<sub>4</sub> catalyst at flow rate of 4 mL/min, 6.5 vol.% MeOH in the feed, and 0.6 g catalyst in the reactor. Reprinted from [216] with permission from copyright holder.

The structure of FeVO<sub>4</sub> was investigated by Routray et al. [217] under MeOH oxidation reaction conditions. The surface of the bulk FeVO<sub>4</sub> was enriched with VO<sub>x</sub>. This was similar to what was described for the commercial FeMo catalyst in Section 2.1.1 and to the measurements on 4% V<sub>2</sub>O<sub>5</sub>/Fe<sub>2</sub>O<sub>3</sub>. In both cases, there was a predominance of V-OCH<sub>3</sub> and V-CH<sub>3</sub>OH intermediates on the surface and absence of distinct peaks for Fe-OCH<sub>3</sub> and Fe-CH<sub>3</sub>OH peaks measured by IR. This taken together with minimal DME and DMM formation was stated by the authors to hint at the low concentration of acidic FeO<sub>x</sub> sites at the surface, since they were covered by the VO<sub>x</sub> ML [217]. It was further concluded in another work by Wachs and Routray [218] that there likely will be an enrichment of one component at the surface in every bulk mixed oxide catalyst [218].

A study by Hellier et al. [219] showed the formation of FeVO<sub>4</sub>, VO<sub>x</sub>, and Fe<sub>2</sub>O<sub>3</sub> upon the impregnation of Fe<sub>2</sub>O<sub>3</sub> with NH<sub>4</sub>VO<sub>3</sub>, analogous to what was described for the FeMo catalyst (Section 2.1.1). Hellier et al. [220] prepared samples of Fe<sub>2</sub>O<sub>3</sub> with 1 ML VO<sub>x</sub> and 3 ML VO<sub>x</sub> finding that 1 ML VO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> was selective to FA albeit less than the corresponding 1 ML MoO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> and that the selectivity dropped as T<sub>50</sub> (230 °C) was reached for the pulses of MeOH into 10 vol.% O<sub>2</sub> in He. At higher temperatures, CO and CO<sub>2</sub> were produced in high amounts. Neither FeVO<sub>4</sub> nor V<sub>2</sub>O<sub>5</sub> were detectable by Raman spectroscopy for the 1 ML VO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> sample, but FeVO<sub>4</sub> was observed for the 3 ML VO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> sample [220].

Malmusi et al. [221] investigated ethanol oxidation over FeVO<sub>4</sub> and V<sub>2</sub>O<sub>5</sub>. This is a similar reaction as the MeOH oxidation. Both showed the primary product to be acetaldehyde. FeVO<sub>4</sub> reduced to a spinel compound containing V<sup>3+</sup> and Fe<sup>2+</sup>/Fe<sup>3+</sup> ions, which had similar catalytic performance as V<sub>2</sub>O<sub>5</sub>, but it was more stable [221].

The results reported in the literature for bulk vanadates and spinel-type catalysts are summarized in Figure 41 as formaldehyde selectivity against conversion (when possible). Among those, FeVO<sub>4</sub> showed high selectivities also at higher temperatures and high levels of conversion but also with some spreading in the results (our results for the iron vanadate were in the low end of the reported selectivities). The tendencies observed for the molybdenum based catalysts and the supported vanadium oxides were also observed for the bulk vanadates such that the Al vanadate performed poorly. The Co, Zn, and Ni vanadates also had poor activity.

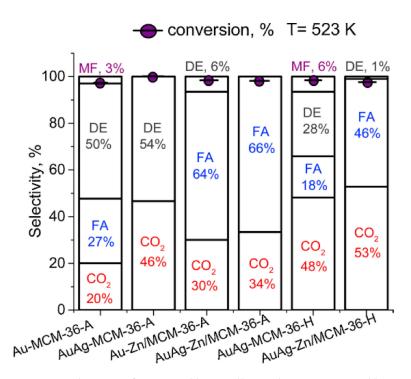


**Figure 41.** Summary of catalytic test results for vanadates and spinel-type catalysts in the literature [125,211–216].

### 2.3. Other Types of Catalysts

The surface and catalytic properties of Au and CeO<sub>2</sub> containing catalysts supported on SBA-15 and the promotion with Cu and Zr species were investigated by Kaminski and Ziolek [222] with 4 vol.% MeOH in the feed and an excess of O<sub>2</sub>. CeO<sub>2</sub> on SBA-15 had a selectivity of 50% towards FA at 13% conversion at 350 °C, while the Zr containing supports had lower selectivity but higher conversion. None of the investigated catalysts had a selectivity higher than 39% towards FA at 250 °C. Zr loading produced an increase in Brønsted acidity and selectivity towards DME, and Cu increased Lewis acidity and selectivity towards MF. Au and Ce catalyzed the total oxidation of MeOH [222]. Another investigation of Au supported on modified aluminosilicates found that Ce and Zr increased selectivity relative to FA. However, this was investigated under the conditions of the BASF (silver catalyst) process, with selectivities of 80–90% [223]. Au, Ag, Zn, and Au-Ag alloys effect on MeOH oxidation was studied by Kaskow et al. [224] on MCM-36 supports at 100-250 °C in a 23.4/3.2/2.5 mL/min Ar/O<sub>2</sub>/MeOH flow on 0.04 g of catalyst. The catalysts were found to reach high conversions already at 150 °C, but all of the samples had a large over-oxidation selectivity to  $CO_2$  at 250 °C (Figure 42). Zn improved the FA selectivity of Au, while Ag promoted combustion to  $CO_2$  [224].

FA had 95% selectivity relative to the main product from MeOH oxidation during a TPRS study at 307 °C on a thin ZnO film over Au(111). This finding was supported by DFT studies [225].



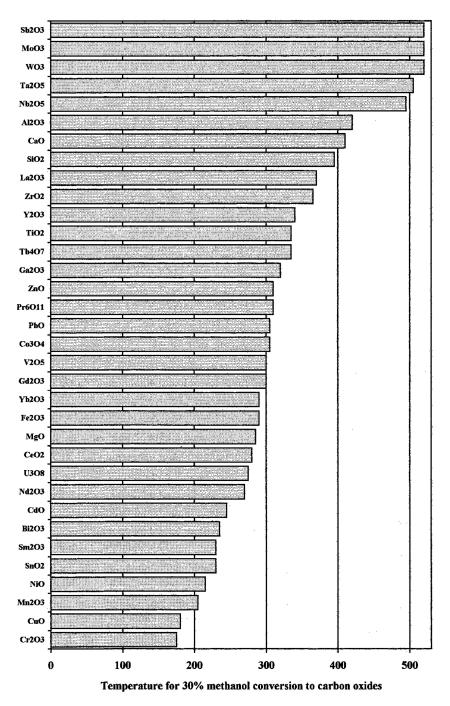
**Figure 42.** Selectivity of mono and bi-metallic catalysts investigated by Kaskow et al. [224] for the MeOH oxidation at close to 100% conversion and 250 °C. FA = Formaldehyde; DE = dimethyl ether; MF = methyl formate. Feed:  $23.4/3.2/2.5 \text{ mL/min of } Ar/O_2/MeOH$ . Reprinted from [224] Copyright © (2020), with permision from Elsevier.

The catalytic properties of nanosized Fe<sub>2</sub>O<sub>3</sub>/MgO were investigated by El-Molla and Mahmoud [226]. The catalysts had 100% selectivity at 300 °C. The MeOH concentration was not mentioned. Selectivities above 97.9% towards FA were reported at 400 °C [226]. This high selectivity was surprising as Fe<sub>2</sub>O<sub>3</sub> is known to oxidize MeOH relative to CO<sub>2</sub>, and MgO is basic and would, thus, be expected to form CO<sub>2</sub> as well (Figure 7). By following the synthesis method reported in [222], samples with 8.2 and 15.2 wt% Fe<sub>2</sub>O<sub>3</sub>/MgO were synthesized (see Supplementary Materials, Section 2.2.3, Figures S10 and S11, and Tables S10 and S11). These catalysts showed very different catalytic properties than those reported by El-Molla and Mahmoud [226]. Full combustion of MeOH was achieved at 400 °C, and selectivity was also significantly lower at 250–350 °C. Selectivity close to 100% relative to FA seemed implausible from these results, which is in better agreement with the expectations for this catalyst.

An investigation of Sb-Re-oxide catalysts for DMM production from MeOH was investigated by Yuan et al. [227]. The selectivity at 300 °C for  $Re_2O_7/Sb_2O_3$  was 49.8% to FA, 42.7% to DME, and only 7.4% to DMM with 2.5% conversion of a 4 vol.% MeOH feed.  $Sb_2O_5$  was found to possess selectivity of 55.5% to FA, 26.4% to DME, and 18% to  $CO_2$  under the same conditions with 1.3% conversion [227].

The activity of Re oxide supported on  $Al_2O_3$  and  $TiO_2$  was investigated by Burcham et al. [140] at 200 °C with 2000 ppm MeOH in the feed, where  $Re_2O_7/Al_2O_3$  and  $Re_2O_7/TiO_2$  produced 72% and 90% selectivity towards FA and  $CO_x$  combined and 28% and 2% selectivity towards DME, respectively [140].

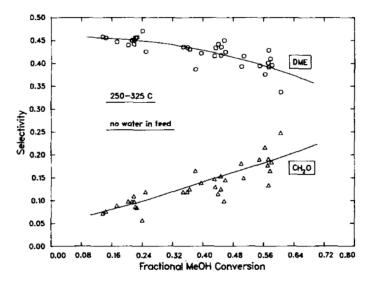
Hutchings and Taylor [228] presented an approach to the design of oxidation catalysts, exemplified by the oxidation of methane to MeOH. As a part of this, an investigation of the stability of MeOH on different oxides was conducted, where it was measured at what temperature 30% of the fed MeOH, in a feed composition of MeOH/O<sub>2</sub>/He = 1/4/12, was converted to carbon oxides (Figure 43). In particular, Sb<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub>, WO<sub>3</sub>, Ta<sub>2</sub>O<sub>5</sub>, and Nb<sub>2</sub>O<sub>5</sub> performed well with respect to MeOH stability in their investigations. Moreover, all of them were observed to have high selectivities towards FA [228].



**Figure 43.** MeOH stability based on the temperature at which 30% conversion of the fed MeOH was converted to carbon oxides. MeOH/ $O_2$ /He = 1/4/12, 12000 h<sup>-1</sup>. Reprinted from [228] Copyright © (1999), with permision from Elsevier.

Harrison et al. [229] investigated the tungstate analogue to the FeMo (Fe<sub>2</sub>(WO<sub>3</sub>)<sub>3</sub>) at 200–350 °C. The O<sub>2</sub> to MeOH ratio varied from 0.2 to 35, H<sub>2</sub>O to MeOH from 0.2 to 2, and MeOH conversion from 10% to 60%. The investigations were carried out on 3 g of catalyst with over 1 week on stream. No losses in activity, visible change, or difference in X-ray diffractograms were observed. The reaction kinetics were reported to be very similar to that of Fe<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, 0.5–1st-order in MeOH, zero order in O<sub>2</sub>, and -0.5th-order in H<sub>2</sub>O. Product distribution was different as the main product was DME and the secondary product FA (Figure 44). The addition of H<sub>2</sub>O improved selectivity towards FA. The Fe<sub>2</sub>(WO<sub>3</sub>)<sub>3</sub> catalyst had only 14% of the activity per surface area of the FeMo [229]. According to Harrison et al. [229], Popov et al. had performed studies in the 1960s on WO<sub>3</sub>

and tungstates with Fe(II), Mn, Co, Ni, Cu, and Zn claiming all to be selective catalysts, with Fe(II) being the most selective. It was not possible to procure the referenced material.



**Figure 44.** DME and FA selectivity as function of MeOH conversion over  $Fe_2(WO_3)_3$ . Reprinted from [229] Copyright © (1985), with permision from Elsevier.

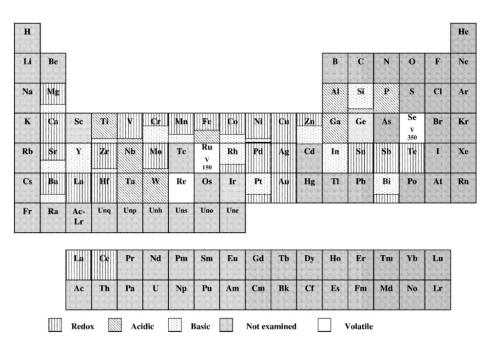
A study by Wachs et al. [230] on bulk mixed oxide catalysts ( $Mo_{0.6}V_{1.5}O_x$ ,  $Mo_{1.0}V_{0.5}Te_{0.16}O_x$ , and  $Mo_{1.0}V_{0.5}Te_{0.16}Nb_{0.12}O_x$ ) using CH<sub>3</sub>OH-TPSR investigated the activities of the surface sites found in the catalysts. The most active sites were the fully oxidized cations. Selectivity decreased upon reduction. V<sup>5+</sup> was more active than Mo<sup>6+</sup>, and they were both significantly more active than Nb<sup>5+</sup> and Te<sup>4+</sup>. V<sup>5+</sup>, Mo<sup>6+</sup>, and Te<sup>4+</sup> were stated to behave as redox sites, while Nb<sup>5+</sup> was a Lewis site [230].

Badlani and Wachs [231] investigated the products from MeOH oxidation on pure metal oxide catalysts at low conversions in order to quantify the number of surface redox sites (FA, MF, and DMM as products), acidic sites (DME), and basic sites (CO<sub>2</sub>) (Figure 45).

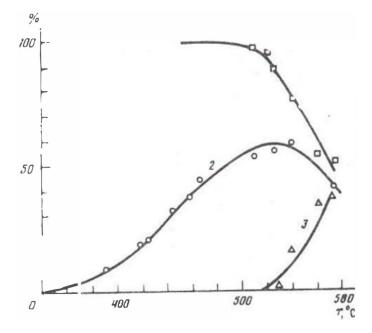
In the investigation of group 6b oxides on CeO<sub>2</sub>-ZrO<sub>2</sub> by Inokawa et al. [142], WO<sub>3</sub> and Cr<sub>2</sub>O<sub>3</sub> were investigated in the temperature range of 275–450 °C. It was found over the entire range that selectivity and yield was poor, although the conversions were above 60% for both Cr<sub>2</sub>O<sub>3</sub> and WO<sub>3</sub> at 450 °C with the best selectivities being approximately 40% for both Cr<sub>2</sub>O<sub>3</sub> and WO<sub>3</sub> at 275 and 450 °C, respectively [142].

Tungsten-titanium mixed oxide bronzes were investigated for MeOH transformation by Delgado et al. [232] at 200–400 °C with 100 mL/min of 6/13/81 vol.% MeOH/O<sub>2</sub>/N<sub>2</sub> on 0.10 g of catalyst (0.25–0.4 mm). For all the samples, the major product was DME, which is in good agreement with the measured acidity. For the Ti-free sample, the selectivity reached 20% for FA at 80% conversion with above 90% conversion to DME. For the Ti containing samples, the redox activity was much lower, with less than 5% selectivity relative to FA in all cases. The redox properties were believed to come from W<sup>5+</sup>, which was present in the Ti-free sample, whereas the Ti containing samples only had W<sup>6+</sup> at the surface [232].

In the 1980s, the catalytic activity of pure  $Sb_2O_4$  was investigated by Abadzhieva and Klissurski [233] at temperatures of 360–580 °C. The formation of CO was observed only above 500 °C, and selectivity relative to FA decreased strongly from 100% at 500 °C with increasing temperature (see Figure 46). Our tests of Sb oxide on SiO<sub>2</sub> found it to have very low activity even though it had the largest surface area of the prepared samples (see Supplementary Materials, Sections 2.1.2 and 2.2.3).



**Figure 45.** MeOH oxidation selectivity over the pure oxide catalysts. Redox = FA, MF, and DMM; Acidic = DME; basic = CO<sub>2</sub>. Reprinted by permission from [231] Plenum Publishing Corporation, Catalysis Letters, Copyright © (2001).

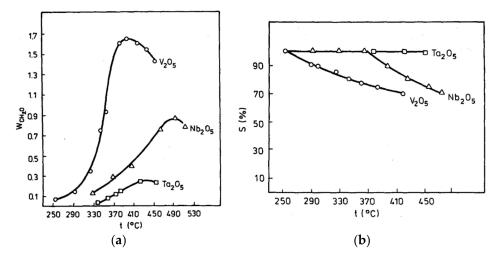


**Figure 46.** Catalytic performance of  $Sb_2O_4$  for MeOH oxidation as function of temperature. 1: Selectivity towards FA; 2: Yield of FA; 3: Yield of CO. Feed: 4.1 vol.% MeOH, 0.15 mL reaction mixture/(m<sup>2</sup>s) [233].

The specific activity was reported to be an order of magnitude lower than for  $MoO_3$  and several orders of magnitude lower than for  $V_2O_5$ .  $E_a$  of the reaction was determined to be 71 kJ/mol [233]. In good agreement, Guerrero-Pérez et al. [200] found both bulk and  $Al_2O_3$  supported antimonates had almost no acidic nor redox sites.

In the same decade, the group five transition metal oxide activities for FA production were investigated by Klissurski and Pesheva (Figure 47) [166]. The selectivity order of the oxides was  $Ta_2O_5>Nb_2O_5>V_2O_5$ . This was in contrast to the Nb containing catalysts

in our investigation (see Supplementary Materials, Section 2.2.3, Tables S10 and S11, and Figures S10 and S11), which primarily made DME, whereas V containing catalysts mostly made FA. This may well arise from the difference in distribution between acidic and redox sites, as demonstrated by Wachs et al. [231] (Figure 45), but a better NbO<sub>x</sub> surface layer may also have been achieved at higher calcination temperature according to Bowker et al. as the Tamman temperature for Nb<sub>2</sub>O<sub>5</sub> is 620 °C.



**Figure 47.** Dependence of activity (**a**) and selectivity (**b**) in MeOH oxidation of the group 5 metal oxides on temperature. Reprinted by permission from [166] Springer nature, Reaction Kinetics and Catalysis Letters, Copyright (1986).

The apparent activation energies of V<sub>2</sub>O<sub>5</sub>, Nb<sub>2</sub>O<sub>5</sub>, and Ta<sub>2</sub>O<sub>5</sub> were 50, 59, and 92 kJ/mol, respectively [166]. Chen et al. [234] reported ML Ta oxide supported on Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, and ZrO<sub>2</sub> to only have acidic surface sites and yielding only DME as the product of MeOH oxidation, whereas TaO<sub>x</sub> on SiO<sub>2</sub> had redox characteristics yielding CH<sub>2</sub>O and CO<sub>2</sub> at low coverage and MF at 5% Ta<sub>2</sub>O<sub>5</sub>/SiO<sub>2</sub>. Chen and Wachs [235] also investigated Ta oxide as a support for 1% CrO<sub>3</sub>, MoO<sub>3</sub>, Nb<sub>2</sub>O<sub>5</sub>, Re<sub>2</sub>O<sub>7</sub>, V<sub>2</sub>O<sub>5</sub>, and WO<sub>3</sub> at 230 °C. Cr, Mo, Re, and V showed redox products with main selectivity towards FA. Nb, W, and pure Ta oxide only yielded DME. Thus, the investigations by Chen et al. [234,235] did not find the same tendency with respect to selectivity as Klissurski and Pesheva [166], but they did agree on the order of the activity.

In the previously mentioned study by Arora et al. [125] with Bi containing catalysts,  $Nb_2O_5/Bi_2O_3$  and  $WO_3/Bi_2O_3$  as well as pure  $Bi_2O_3$  were investigated. Pure Bi oxide was reported not to possess selectivity above 18%, while  $Nb_2O_5/Bi_2O_3$  achieved 46.9% selectivity and  $WO_3/Bi_2O_3$  achieved 85.6% selectivity [125].  $Nb_2O_5/SiO_2$  and Nb-MCM-41 were compared by Gao et al. [236] who found dispersed NbO<sub>4</sub> species to be the active redox sites in both catalysts, which exhibited similar activity and selectivity, with up to 60% selectivity relative to FA, over 20% to MF, and the rest relative to DMM and DME [236].

Hellier et al. [220] tried, as for the VO<sub>x</sub> and MoO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub>, to prepare 1 ML and 3 ML NbO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts. In contrast to the corresponding VO<sub>x</sub> and MoO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> samples, 1 ML NbO<sub>x</sub>/Fe<sub>2</sub>O<sub>3</sub> primarily showed selectivity towards DME at lower temperatures, which were then superseded by selectivity towards CO<sub>2</sub> at ~300 °C. It was proposed that the NbO<sub>x</sub> layer was not properly formed as the calcination temperature (500 °C) was below the Tamman temperature for Nb<sub>2</sub>O<sub>5</sub> (620 °C) and high enough mobility to properly disperse may not have been achieved. The incomplete coverage of the hematite core was supported by the low temperature onset of MeOH combustion and the absence of a distinctive Nb = O peak in Raman spectroscopy after calcination [220].

Davies and Taylor [237] studied the use of niobium phosphates. The selectivity was maintained at above 80% with conversions over 90%, and it was stated to be in contrast with many niobium oxide based catalysts [237], which mainly oxidize to  $CO_x$  at above 300 °C [238]. The temperature dependence of the selectivity of niobium oxide phosphates

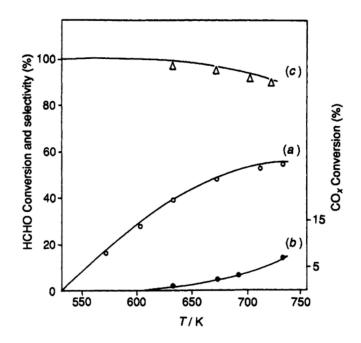
towards FA was investigated for the phosphates prepared either from pyro-phosphoric or ortho-phosphoric acid. The selectivity was 100% at temperatures below 400 °C. The selectivity at 400 °C for the niobium oxide phosphate from pyro-phosphoric acid had slightly higher selectivity than from ortho-phosphoric acid. The niobium oxide phosphate from ortho-phosphoric acid had much higher conversion when calcined at 500 °C but lower conversion when calcined at 400 °C or 600 °C compared to the niobium oxide phosphate from pyro-phosphoric acid [238].

The Nb<sub>2</sub>O<sub>5</sub> and niobium phosphate samples prepared for this study were not very active (see Supplementary Materials, Section 2.2.3, Tables S10 and S11, and Figures S10 and S11), had primarily activity towards DME, and were, thus, not suitable as catalysts for the selective oxidation of MeOH to FA. When Nb<sub>2</sub>O<sub>5</sub> was supported on HAP or  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, the selectivity towards DME was a little lower, but larger CO<sub>2</sub> selectivity was observed.

The properties of  $Al_2O_3$ , intercalated into montmorillonite, were investigated by Hashimoto et al. [239] as a catalyst for conversion of MeOH to DME or FA in a feed with 11 vol.% MeOH and 18 vol.%  $O_2$ . At 260–340 °C, a maximum selectivity of 12% towards FA was achieved, with the rest almost exclusively being DME, thus being far from ideal as an alternative to the industrial FeMo catalyst [239].

The support materials  $SiO_2$  and  $Al_2O_3$  were tested for their properties with respect to catalytic selective oxidation of MeOH in a fluid bed reactor for 60 h at 340 °C with 5.5 vol.% MeOH in air by [240]. The main products were found to be CO and CO<sub>2</sub> followed by MF. Small amounts of FA were also observed. The addition of Na and Mg to SiO<sub>2</sub> decreased CO and CO<sub>2</sub> yields [240].

The use of Zr phosphates, CuX zeolite, and their mixtures was investigated for MeOH transformations by Gryaznova et al. [241] at temperatures up to 240 °C. None of the mixtures were selective towards FA [241]. An investigation of FePO<sub>4</sub> by Klissurski et al. [242] in comparison reported high selectivity towards FA (Figure 48).



**Figure 48.** MeOH conversion (line a), FA selectivity (line b), and CO<sub>2</sub> selectivity (line c) on Fe(III) phosphate as function of temperature in 240 mL/min 4 vol.% MeOH in air. Reproduced from [242] with permission from the Royal Society of Chemistry.

High selectivity was stated to be anticipated due to the similar relative electronegativity of  $P^{5+}$  (67.9) and Mo<sup>6+</sup>(66.6) and ionicity (I) of the  $P^{5+}$ -O (27.5%) and Mo<sup>6+</sup>-O (28.9%) bonds, resulting in the belief that they should have similar catalytic behavior [242]. This resulted in the investigation of BiPO<sub>4</sub> by the same group [243] with 3.5 vol.% MeOH in air, 480 mL/min over 0.5 g of 0.3–0.5 mm particles with a BET surface area of 6 m<sup>2</sup>/g, which achieved ~42% conversion at 400 °C with no registered byproducts. At higher temperatures, CO<sub>2</sub> was measured [243]. The  $E_a$  on BiPO<sub>4</sub> (67.2 kJ/mol) [243] and on FePO<sub>4</sub> (56.6 kJ/mol) [242] were rather close to that reported on industrial FeMo catalysts (64 kJ/mol) [244].

Sulfated-TiO<sub>2</sub> binary metal oxide catalysts were investigated by Zhao et al. [245] for partial MeOH oxidation at 120–250 °C. The Cr, Mn, Mo, and V oxide containing catalysts showed low selectivities (<42%) towards FA, at 150 °C and 190 °C, whereas the Fe and Co containing catalysts showed no selectivity towards FA. The main products were DME and DMM [245].

The  $CeO_2$  surfaces (100) and (111) were investigated by using DFT calculations (using a dispersion-corrected PBE+U model) for MeOH oxidation by Kropp and Paier [246]. The (100) facet was found to have an intrinsic barrier of 91 kJ/mol while the (111) facet had 119 kJ/mol. The lower barrier inferred a lower FA desorption temperature, which was in agreement with TPD studies. The higher activity of the (100) facet was in agreement with lower oxygen defect formation energies for the (100) facet compared to the (111) facet, which was concluded to be a good reactivity descriptor for MvK mechanisms. FA was found to either desorb or form bridging dioxymethylene but adsorbed more exothermally on the (100) surface, implying a higher level of deep oxidation than on the (111) facet [246]. The C-H bond breaking on CeO<sub>2</sub>(111) was probed by Sutton et al. [247] by a simulated temperature programmed reaction study by DFT and Kinetic Monte Carlo for MeOH oxidation compared with an experimental TPR study. The simulation showed formation and desorption of FA already below room temperature [247]. The effects of Zr, Hf, and Th as dopants on the  $CeO_2(111)$  surface were described as part of a descriptor analysis by Capdevila-Cortada and López [248] using DFT. Zr-doped and Hf-doped systems together with expanded lattice  $CeO_2$  had a decreased  $E_a$  for the C-H cleavage making the conversion of CH<sub>2</sub>O to CO more favorable. The desorption was stated to be controlled by geometric and acid-base factors, while the C-H cleavage was governed by the acid-base and redox factors [248].

Pt supported on SiO<sub>2</sub>, Co<sub>3</sub>O<sub>4</sub>, MnO<sub>2</sub>, Fe<sub>2</sub>O<sub>3</sub>, NiO, and CeO<sub>2</sub> was investigated by Wang et al. [249] at 60 °C. No significant difference was observed in the selectivities towards CO<sub>2</sub>, CH<sub>2</sub>O, and MF among the different supports, with the exception of the MnO<sub>2</sub> supported sample, which showed larger CH<sub>2</sub>O selectivity (app. 60%) compared to the others (25–40%) but also orders of magnitude lower activity [249]. Pt-Bi bimetallic catalysts on activated carbon were investigated at 70–120 °C with 6 vol.% MeOH and 1.5 vol.% O<sub>2</sub> in N<sub>2</sub> by Xiao et al. [250]. The best performing catalyst was the 1 wt% Pt and 0.5 wt% Bi catalyst, which had CH<sub>2</sub>O selectivity above 70% for all temperatures at up to 17% conversion with 0.02 g catalyst in 100 mL/min of feed. It demonstrated 98% selectivity and 8.1% conversion at 70 °C [250]. This was, however, unlikely to be usable in the Formox plants.

An YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7-x</sub> perovskite catalyst was investigated by Sun and Lee [251]. At low conversions, the selectivity relative to FA was 100%. However, it decreased to 80% when the conversion increased to 40% at 300 °C with 8.8 vol.% MeOH in the feed [251].

The catalytic performance of Cu and Zn incorporated in MCM-41 was investigated by Velu et al. [252] at 200–300 °C with MeOH/O<sub>2</sub> = 2 as the feed to the reactor. Selectivities of above 90% was achieved in the entire temperature interval with the exception of the high-loading (4.2 wt% Cu) Cu-MCM-41, where the selectivity decreased drastically with increasing temperature [252].

The effect of Pd on the La-transitions metal perovskites for MeOH partial oxidation with 11 vol.% MeOH and 5 vol.%  $O_2$  in the feed was investigated by Li et al. [253,254] at 220–380 °C. The addition of 5 mol% Pd(II) cations greatly improved the activity and the selectivity of LaMnO<sub>3</sub>, LaFeO<sub>3</sub>, and LaCoO<sub>3</sub> so that the selectivity towards FA was approximately 90% for LaMnO<sub>3</sub> and LaCoO<sub>3</sub> and 85% for LaFeO<sub>3</sub>. No temperature dependence of selectivity was observed within the investigated temperature range [253].

The influence of Pd loading on LaMnO<sub>3</sub> was investigated with 1%, 3%, and 7% of the Mn ions exchanged with Pd. Selectivity increased with increasing Pd loading; however, the same temperature independence was not found [254].

The Topsøe group [131] has investigated the W based heteropolyanions  $[PW_{12}O_{40}]^3$ salts of Cs and Fe(III), both with very poor results. Moreover, FePO<sub>4</sub> and MnPO<sub>4</sub> were investigated by the Topsøe group, and both phosphates were found to have very low catalytic activity in contrast to the reports by [242,243]. Stoichiometric MgFe<sub>2</sub>O<sub>4</sub> showed ignition behavior (large sudden change in activity) and increase in selectivity to CO and CO<sub>2</sub> between 350 and 375 °C and was, thus, deemed not to be interesting. Fe<sub>2</sub>(WO<sub>3</sub>)<sub>3</sub> has also been tested and rejected due to too low selectivity [131].

A study of the influence of supports has been conducted in the Topsøe group [131]. High (56 m<sup>2</sup>/g) and low (33 m<sup>2</sup>/g) surface area anatase TiO<sub>2</sub> were tested in a pilot scale reactor.  $TiO_2$  showed high activity with low selectivity towards FA and high selectivity towards full oxidation at above 280 °C for the high area anatase and above 290 °C for the low area anatase and was, thus, disqualified as a carrier since it may negatively influence selectivity towards FA. Anatase impregnated with P was also tested. It had lower activity and decreasing selectivity towards FA with time at 300 °C. ZrO<sub>2</sub> was tested as a carrier for MeOH oxidation activity, but it was found to be even more active towards the full oxidation of MeOH than anatase TiO<sub>2</sub>, and a runaway reaction occurred.  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> showed no runaway reaction, and the  $CO_x$  selectivity was acceptable, but there was high selectivity towards DME. However, when  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was tested for FA oxidation by first having a layer of the commercial catalyst to convert MeOH to FA, it converted the major part of the FA to CO and was, thus, discarded as carrier since it may convert the FA at high conversions.  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> was tested for MeOH oxidation and was found to have negligible activity for MeOH oxidation and converted a significantly smaller fraction of FA to CO and CO<sub>2</sub>. The  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> was, thus, a possible support, which we have used with Mo and V, with good selectivities but quick loss of Mo and V (see Supplementary Materials, Sections 2.2.2 and 2.2.3). Lastly, a MgAl<sub>2</sub>O<sub>4</sub> carrier, prepared by hot impregnation of 8 wt% Mg on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, was tested. It was found to behave similarly to  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> with high activity towards DME [131].

The results reported in the literature for the catalysts not containing Mo or V are summarized in Figure 49 as formaldehyde selectivity against conversion. Some of the same trends observed for the V and Mo based catalysts are again visible. Thus, catalysts with  $CeO_2$  and  $ZrO_2$  account for the six points with the lowest selectivity.  $Re_2O_7$  based catalysts reached a maximum selectivity of 90% at 14% conversion and are, thus, without promise as it, in addition, is a very expensive metal. The perovskites (YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7-x</sub> and  $Pd/La(Co/Fe/Mn)O_3$ ) and Cu(Zn)/MCM-41 had too low selectivity at high conversion and is likely to oxidize to  $CO/CO_2$  as Cu is the main component in methanol synthesis and, thus, likely to catalyze the decomposition to  $CO/CO_2$  and  $H_2$  from the principle of micro kinetic reversibility. The Fe<sub>2</sub>O<sub>3</sub>/MgO catalyst had reported high selectivities and would, thus, have been very interesting, as there were no components that could be believed to become volatile during reaction exposure; however, our results for the Fe-Mg-O system could not reproduce promising results and showed poor selectivities to FA. The NbPO catalyst and the CrO<sub>3</sub>/Cr<sub>2</sub>O<sub>5</sub> catalysts both had significantly lower reported selectivities than the VPO and  $MoO_3$  counterparts (Figures 25 and 26). Generally, these catalyst systems show too low selectivity and/or activity to be of interest as replacement catalysts for the Formox process.

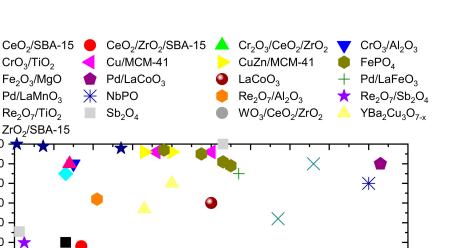


Figure 49. Summary of catalytic test results in the literature shown as selectivity vs. conversion for catalysts not containing V or Mo shown [125,140,166,222,223,226,227,233,237,241,251-254].

60

70

80

90

100

50

Conversion [%]

40

## Volatility of the Active Phase

10

0

20

30

CrO<sub>3</sub>/TiO<sub>2</sub>

Fe<sub>2</sub>O<sub>3</sub>/MgO

Pd/LaMnO<sub>3</sub>

Re<sub>2</sub>O<sub>7</sub>/TiO<sub>2</sub>

100 90

80

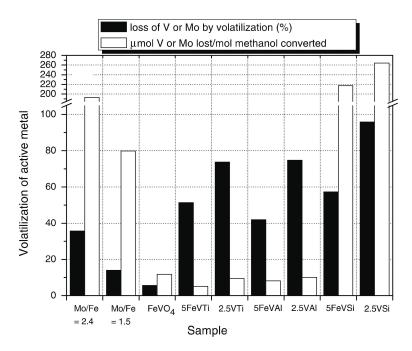
70

Selectivity [%]

ZrO<sub>2</sub>/SBA-15

Reaction induced spreading of  $MoO_3$  and  $V_2O_5$  was investigated with in situ Raman spectroscopy under MeOH oxidation reaction conditions by Cai et al. [255]. For a 4 wt%  $MoO_3/TiO_2$  physical mixture, it was suggested that  $MoO_3$  was dispersed at 230 °C as only a small amount of crystalline  $MoO_3$  could be observed. If the reaction temperature was increased to 300  $^{\circ}$ C, all crystalline MoO<sub>3</sub> had disappeared. The same behavior was observable on 0.5–1% MoO<sub>3</sub>/SnO<sub>2</sub> physical mixtures. Comparably, if the spreading was performed by thermal treatment (whether in inert or oxidative atmosphere was not reported), 400 °C produced significant spreading, while 500 °C produced almost complete dispersion. For 4 wt%  $V_2O_5/TiO_2$ , the  $V_2O_5$  crystalline phase disappeared completely at 230 °C under reaction conditions and showed only surface vanadia species. In contrast to  $MoO_3/TiO_2$ , there was no spreading observed for the vanadia on TiO<sub>2</sub> at 400–500 °C without methanol in the feed. O2-free experiments were later performed and showed that spreading was not related to  $O_2$ . It was suggested that the spreading came from MeOH strongly binding with Mo and V in the crystalline  $MoO_3$  and  $V_2O_5$  to form volatile  $Mo(OCH_3)_n$  and  $V(OCH_3)_n$ . The alkoxy complexes of vanadia and molybdena are stated by Cai et al. [255] to be well known and to be liquids at room temperatures with high vapor pressures. However, no chemical formulas were given, and properties of Mo and V alkoxides were not reported.

In the  $Fe_{1-x}Al_xVO_4$  spinel-type catalyst, the V/(Fe+Al) atomic ratio was stable as measured by XPS except for a small depletion of Fe, when comparing fresh and spent samples after 16 h [212]. The stability of the cation vacant Fe<sub>3-x-u</sub>V<sub>x</sub> $\Box_{\nu}O_4$  spinel-type catalyst was evaluated by ICP after 5 days on stream and compared to the fresh catalyst. A small increase in Fe/V ratio was observed for the 1:1 catalyst, while a small decrease was observed for the 2:1 ratio catalyst. For the remaining three investigated samples, no difference was measured with ICP within the time frame of 5 days [213]. The same was observed by Massa et al. [214]. The volatility of FeVO<sub>4</sub>, commercial type  $Fe_2(MoO_4)_3/MoO_3$ catalysts, and Fe-V-oxide layers supported on TiO<sub>2</sub>,  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, and SiO<sub>2</sub> was investigated by Massa et al. [214]. There was a stabilizing effect of Fe on V on all the supports (Figure 50).



**Figure 50.** A comparison of the loss of V or Mo from the catalysts by volatilization during MeOH oxidation for 5 days, at 300 °C feeding 10 vol.% MeOH and 10 vol.% O<sub>2</sub> in N<sub>2</sub>. 5FeV = five theoretical layers with V:Fe of 1:1 on support; 2.5 V = 2.5 theoretical layer of vanadia on support. Al =  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>; Ti = TiO<sub>2</sub>; Si = SiO<sub>2</sub>. Reprinted with permission from [214] Springer Science+Bussiness Media. Copyright © (2011).

TiO<sub>2</sub> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> have a stabilizing effect on the volatility of V, since the absolute amount of V or Mo lost/mol MeOH converted decreased (Figure 50). However, the content of vanadia was so low in the supported catalysts that the relative decrease in vanadia content became very large. Supported Fe-V-oxides were concluded not suitable for industrial purposes since low V content made it very sensitive to volatilization and shortens the catalyst lifespan even though the volatilization rate may be lower with a support [214]. The Fe<sub>2.5</sub>V<sub>0.2</sub>Mo<sub>0.5</sub>O<sub>y</sub> catalyst was tested with the same method, and there were no signs of volatility from ICP [215].

The volatility of various molybdates and vanadates was investigated by Andersson et al. [6] during 96 h of MeOH oxidation experiments at the conditions used for the comparisons of the molybdates and vanadates with the Formox KH44L (Table 2).

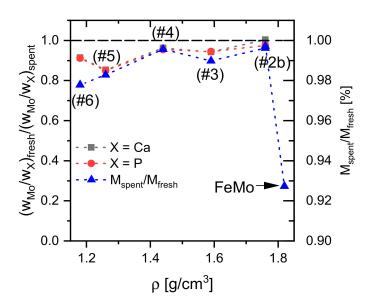
**Table 2.** Volatilization of Mo and V measured in the decrease in their surface areas from different molybdates and vanadates, respectively, under 96 h of MeOH oxidation. T = 300 °C. Feed: 6 vol.% CH<sub>3</sub>OH and 11 vol.% O<sub>2</sub> in inert gas. Flow: 277 mL/min; loading: 30 mg catalyst; particle size: 0.250–0.425 mm. Reprinted with permission from [6] Springer, Topics in catalysis, Copyright © (2016).

| Catalyst                                                           | Mo- and V-Loss<br>(%/m <sup>2</sup> Surface Area) |
|--------------------------------------------------------------------|---------------------------------------------------|
| MoO <sub>3</sub> /Fe <sub>2</sub> (MoO <sub>4</sub> ) <sub>3</sub> | 9.3                                               |
| $Fe_2(MoO_4)_3$                                                    | 2.3                                               |
| $Cr_2(MoO_4)_3$                                                    | 6.2                                               |
| $Zr(MoO_4)_3$                                                      | 9.7                                               |
| FeVO <sub>4</sub>                                                  | 1.9                                               |
| AlVO <sub>4</sub>                                                  | 4.8                                               |
| $Mn_3(VO_4)_2$                                                     | 2.9                                               |

Exactly how the surface area was correlated with component loss was not clear, but the paper states it was found by XPS. It was believed that the surface area should be

understood as the part of the total surface area of the sample, which was covered with Mo or V. The FeMo catalyst with excess  $MoO_3$  lost Mo fast and faster than the FeMo with no surplus of Mo oxide. However, the consequence was lower selectivity when there was no surplus of Mo. It can also be observed that with respect to keeping the active component,  $FeVO_4$  was the most stable of the investigated samples, but it had still lost 1.9% of its vanadate surface area within 96 h of operation [6].

Excess crystalline MoO<sub>3</sub> was found by Thrane et al. [107] to quickly volatilize from alkali earth metal molybdates at 400 °C as also observed on the FeMo catalyst. However, no Mo volatilization past the point of stoichiometry for the bulk alkali earth metal molybdates was observed by Raman spectroscopy [107]. However, in the later study of  $MoO_3$  supported on HAP and the Sr analogue, Thrane et al. [110] found that the amount of CaMoO<sub>4</sub> and  $SrMoO_4$  quantified by XRD decreased with TOS for samples with nominal loadings of 10 and 15 wt% MoO<sub>3</sub>. Thus, CaMoO<sub>4</sub> loading went from 8.1 to 3.1 wt% after 408 h on stream for the 10 wt% MoO<sub>3</sub>/HAP. From exposure to reaction conditions, weight loss from 10 wt% MoO<sub>3</sub>/HAP pellets and FeMo pellets were measured after 118.5 h on stream at 350 °C, 3 NL/min with 4 pellets (60 to 90 mg each pellet) in the reactor, 5 vol.% MeOH, and 10 vol.%  $O_2$  in  $N_2$ . Weight loss was found to increase with decreasing pellet density (increasing porosity) (Figure 51) and correlated well with the Mo loss found by ICP. The Mo loss from the Mo/HAP pellets was 70% lower than from the FeMo pellet based on the mass loss. As the catalyst showed similar activities but MoO<sub>3</sub>/HAP slightly lower selectivity, it was reported to be of potential interest for utilization in the front-end of the bed in the Formox process [112].



**Figure 51.** Ratio of Mo to Ca and P (three pellets combined and measured for each sample) and measured mass loss (four pellets combined and measured for each sample) after 118.5 h at 350 °C, 3000 NmL/min, 5 vol.% MeOH, and 10 vol.% O<sub>2</sub> in N<sub>2</sub> (<15% conversion estimated) compared to the fresh samples. Reproduced from [112] with permission from the Royal Society of Chemistry.

During a mechanistic investigation of isolated vanadate species on MCM-48 by Bronkema and Bell [172], it was found from an in situ XANES experiment, under 4 vol.% MeOH in He at 100 °C, that the main edge and pre-edge features decreased with time. Calculations from the lost intensity showed 68% of the V was lost during 28 min exposure to MeOH. In a separate experiment, the sample was exposed to 9 vol.% MeOH in He at 100 °C, where the V content fell from 5.2% to 0.9% during 12 h with a green deposit forming at the reactor outlet. The loss of V was believed to stem from volatile V methoxide species [172]. From in situ spectroscopic investigations of the molecular structures of vanadia on SiO<sub>2</sub> by Gao et al. [256], it was found that alcoholysis of the V-O-Si bonds in the catalyst destabilizes the V oxide species, which results in the aggregation of surface V oxide species. Furthermore, it also resulted in the production of some volatile V-methoxy species under MeOH oxidation at higher temperatures [256].

In an investigation of the reactivity of vanadia on different supports, there were deposits at the outlet of the reactor due to volatilization of the V oxide in the MeOH oxidation environment for all investigated  $V_2O_5/SiO_2$  samples [180].

In an investigation of the structure of the V-MCM-41 catalyst by Yang et al. [170] using Raman spectroscopy, it was observed that V was incorporated atomically into the MCM-41 framework. It was stated that they would not migrate to the surface under reaction conditions of MeOH oxidation even though the V-OCH<sub>3</sub> intermediate was quite volatile [170].

These results indicate that V oxide containing catalysts cannot solve the volatility problem encountered from Mo based catalysts, since it might be even more volatile than the Mo oxide. However, V incorporated into the crystal structure of the support may be another matter.

The dynamic state of SiO<sub>2</sub> supported metal oxide (V, Nb, Cr, Mo, W, and Re) catalysts during MeOH oxidation was investigated by Jehng et al. [257] by using in situ Raman spectroscopy. The reaction conditions were 230  $^\circ\text{C}$  , with 4 vol.% MeOH in He/O\_2 ratio of 11/6. Among those, only the  $V_2O_5/SiO_2$  had stable surface M-OCH<sub>3</sub> species. For  $V_2O_5/SiO_2$ , the initial Raman spectra was obtained after reoxidation at 350 °C with a flow of O<sub>2</sub>. The Raman intensity of dehydrated Nb<sub>2</sub>O<sub>5</sub>/SiO<sub>2</sub> decreased in the MeOH oxidation environment, and was not fully recovered after reoxidation. MoO<sub>3</sub>/SiO<sub>2</sub> was found to form an amorphous MoO<sub>3</sub> overlayer on the SiO<sub>2</sub> support since the Raman features of crystalline  $\alpha$ -MoO<sub>3</sub> disappeared under the MeOH oxidation conditions. After reoxidation, it was transformed into microcrystalline  $\beta$ -MoO<sub>3</sub> particles [257]. Similar results were found by Bañares et al. [141] during MeOH oxidation over MoO<sub>3</sub>/SiO<sub>2</sub>, where MoO<sub>3</sub> was reported to be volatile at higher loadings [141]. Jehng et al. [257] observed that the  $WO_3$  surface species could not be totally restored after reoxidation. For Re<sub>2</sub>O<sub>7</sub>/SiO<sub>2</sub>, there were no Raman features of Re at all after reoxidation even at higher temperatures, showing that the surface Re oxide species had become volatile at reaction conditions. The CrO<sub>3</sub> species were partly reduced, which produced fluorescence in the Raman spectra [257].

In our investigation of Sb oxide on  $SiO_2$  (see Supplementary Materials, Section 2.2.3), a visible deposit was observed at the reactor outlet after an 8 h test with no Mo loaded into the reactor. Thus, Sb oxide seemed to also be volatile under MeOH oxidation conditions and requires further studies before a conclusion can be drawn on whether it could be applicable as a stabilizer.

Wachs et al. [230] found  $\text{TeO}_x$  to be volatile under MeOH oxidation conditions of 230 °C, with 6 vol.% MeOH and 13 vol.% O<sub>2</sub> [230].

Studies of methoxides of Li, Mg, and La showed them to remain unchanged when kept at 360 °C for 18 h [258]. Methoxides of Al and Zr were sublimated at 240 °C and 280 °C, respectively, in a vacuum. For the physical properties of alkoxides, it was stated that they depend largely on the size and shape on the alkyl group (methoxy in this case), valence, atomic radius, stereochemistry, and coordination number of the metal. The alkoxide shift gradually from nonvolatile ionic alkoxides formed by some of the alkali metals to volatile covalent alkoxides of metals with valences of three, four, five, or six. It was stated that it was probable that most alkoxides of metals with valences of four and higher would be covalent, where the properties of the alkoxide would then be dependent on the tendency of the metal to increase its valence by intermolecular bonding with oxygen, providing relatively nonvolatile compounds. The other tendency was the steric effect of the alkyl group and its effect to block intermolecular bonding and keeping the alkoxide monomeric [258]. However, this should be the same in all cases since the alkyl group is a methoxy group in all cases. Interestingly the volatility of monomeric alkoxides with the same alkyl group increases with increasing molecular weight ( $P_{\text{Hf}} > P_{Zr} > P_{\text{Ti}}$ ) [258]. Thus, a heavier metal as the active center in the same group, e.g., Nb instead of V, and W instead of Mo may not increase the stability of the catalyst.

Summing up on the volatility, Mo in many (if not all) Mo oxide-based catalysts are volatile in the presence of MeOH. This has also been found for V in various vanadia systems, as well as for Te and Re. Thus, exchanging Mo with V may only exchange one volatility problem with another and decrease selectivity at the same time. FeVO<sub>4</sub> has been reported to be more stable towards volatilization than the FeMo catalysts. In addition, the spinel-type catalysts (reduced vanadates) have been reported to be stable under reaction conditions. Most of the catalytic systems reported in the literature were not investigated for the stability of the catalyst, and some of those that were investigated were performed under conditions unsuitable for stability measurements (i.e., overloaded reactor with full conversion). Thus, some of the most promising catalytic systems may be highly unstable at industrial reaction conditions. From the volatility of methoxides, Al and Zr based supports may not be suitable due to a risk of volatility issues; however, from  $Al_2O_3$  being part of the commercial type methanol synthesis catalyst, it seems unlikely to be a problem. A general thought would also be that Cr should be less volatile than Mo, and Nb should be less volatile than V due to the higher molecular weight, but mentioning the use of Cr in modern catalysis is undesired. However, it should be kept in mind that the volatility may actually very well increase with increasing molecular weight instead of decreasing. Thus, there is a number of considerations to keep in mind under the search for alternative catalysts for the selective oxidation of methanol.

# 3. Summary of the Experimental Reproductions of the Most Interesting Alternative Catalysts

There have been attempts to reproduce a number of the most interesting catalysts from the literature as well as some analogues. Thus, in the Supplementary Materials, results for the following types of catalysts can be found:  $Fe_2O_3/MgO$ , VPO,  $MoO_3/\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $V_2O_5/\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $Nb_2O_5/\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>),  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>),  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $V_2O_5/(\alpha$ -Al<sub>2</sub>O<sub>3</sub>),  $V_2O_5/(\alpha$ 

The main conclusions from the experimental screening of alternative catalyst were that the molybdenum containing catalysts were in general selective with FA selectivities that were not that far from the FeMo catalyst (>92% selectivity) with DME as a significant byproduct. However, significant deactivations were visible even within 8 h on stream at 400 °C for these catalysts. The vanadium containing catalysts were generally more active than the molybdenum containing catalysts, and several of them were more active than the FeMo catalyst, but the selectivity was lower than for the molybdenum containing catalysts, especially at higher temperatures and conversion. DME was only a minor byproduct with CO and CO<sub>2</sub> being the most significant byproducts. The VPO catalysts were more selective towards formaldehyde and DME but also had significantly lower activity than the other V based catalysts. For catalysts with neither molybdenum nor vanadium, the DME corrected selectivity to FA was low in general, and they were also less active than the molybdenum or vanadium containing catalysts, with the exception of the Fe<sub>2</sub>O<sub>3</sub>/MgO catalysts, which over oxidized to CO and CO<sub>2</sub>. Nb based catalysts made significant amounts of DME, and over oxidation resulted primarily in CO<sub>2</sub>.

#### 4. Concluding Remarks

Despite the fact that the industrial FeMo catalyst is active and very selective for the oxidation of methanol to formaldehyde, mainly due to the low adsorption energy of FA, it is not a perfect catalyst. This review has summarized the FeMo catalysts' main problem of forming volatile Mo species with MeOH. This results in the depletion of Mo at the top of the reactor/hot spot and the formation of deposits of Mo oxides further down in the reactor, resulting in an increase in pressure drop, decrease in selectivity, and finally shut down of the plant in order to exchange the catalyst.

This has motivated the search for alternative and more stable catalysts with similar activity and equally high selectivity. These efforts were also reviewed and several classes of alternative catalysts were identified from the open literature and some patents. Most of the investigated catalysts contain either Mo or V in some form, especially for the catalysts showing promising selectivity and conversion. A number of the studies reporting good performances of alternative materials are many decades old; thus, the lack of implementation in industry could indicate that they did not pass the test if they were tested industrially.

Mo based catalysts were the most selective catalysts for the oxidation of MeOH to FA. V based catalysts were rather selective, but mostly they were not as selective as the Mo based catalysts but more active. The catalysts without Mo and V were mostly lacking in either activity, selectivity, or both. V based catalysts have mostly been investigated as an alternative to Mo based catalysts; however, V also becomes volatile with MeOH in the feed and may, thus, only exchange one volatile component with another.

The operating temperature and pressure in the industrial Formox plants of 250–380  $^{\circ}$ C and ~0.5 barg [6] have in general led the conditions of the investigations of alternative catalysts (~150–500  $^{\circ}$ C and ~1 atm) as an alternative catalyst optimally should be applicable at a similar temperature and pressure in order to be of relevance in the existing Formox plants.

At this point, no catalyst that has the potential to fully exchange the FeMo catalyst in the industrial (Formox) process has been reported. However, some catalysts showed higher stability/lower molybdenum loss and similar activity and reasonable, but slightly lower, selectivity compared to the FeMo catalyst, including a recently developed  $MoO_3/HAP$  catalyst [110,112]. Such catalysts could possibly be used in the inlet section of the reactor, providing moderate conversion over this alternative catalyst, where selectivity is rather high. Moreover, FeMo catalyst is exposed to decreasing MeOH concentration at the downstream, thus prolonging its lifetime without significantly losing FA to over oxidation products.

Supplementary Materials: The following are available at https://www.mdpi.com/article/10.3390/ catal11111329/s1, experimental procedures and results for the revisitation on the literature. Figure S1: XRD diffractograms measured for the catalyst samples supported on the commercial hydroxy-apatite (HAP), Figure S2: XRD diffractograms measured for the catalyst samples supported on  $\alpha$ -Al2O3, Figure S3: XRD diffractograms measured for the antimony containing samples, Figure S4: XRD diffractogram measured for the vanadyl phosphate samples. VPO (a) was when the VOPO4 2H2O sample, obtained after the first reflux, was calcined. VPO (b) was when the VOHPO4.0.5H2O sample, obtained after additional refluxes in isobutanol and water, was calcined, Figure S5: XRD diffractograms for NbPO, FeVO4 and Fe2O3/MgO samples, Figure S6: Screening results for molybdenum containing catalysts. FeMo included for comparison. 50 mg of catalyst in a feed of 3-5% MeOH in 127.5 NmL/min N2 and 15 NmL/min O2. (a) Scor vs. temperature, (b) Xcor vs. temperature and (c) Scor vs. Xcor, Figure S7: Arrhenius plot for molybdenum containing catalysts, Figure S8: Screening results for vanadium containing catalysts. FeMo included for comparison. 50 mg of catalyst (except for the FeVO4 samples, here it was 7.5 mg) in a feed of 3–5% MeOH in 127.5 NmL/min N2 and 15 NmL/min O2. (a) Scor vs. temperature, (b) Xcor vs. temperature and (c) Scor vs. Xcor, Figure S9: Arrhenius plot for vanadium containing catalysts, Figure S10: Screening results for alternative catalysts not containing molybdenum or vanadium. FeMo included for comparison. 50 mg of catalyst in a feed of 3–5% MeOH in 127.5 NmL/min N2 and 15 NmL/min O2. (a) Scor vs. temperature, (b) Xcor vs. temperature and (c) Scor vs. Xcor, Figure S11: Arrhenius plot for catalysts not containing molybdenum or vanadium, Table S1: Overview of catalyst systems which were revisited, Table S2: Amounts of chemicals used for the preparation of HAP supported samples, Table S3: Amounts of chemicals used for the preparation of  $\alpha$ -Al2O3 supported samples, Table S4: Overview of BET surface areas measured on the catalysts tested, Table S5: Results of elemental analysis for catalysts samples, which were filtered during the preparation, Table S6: Selectivities at 250–400 °C, conversion and reaction rate constants for the fresh molybdenum con-taining catalysts with 50 mg of catalyst, in a feed flow of 15 NmL/min O2, 127.5 NmL/min N2 and 3-5% CH3OH, Table S7: Pre-exponential factor (k0) and activation energy (Ea) of molybdenum containing catalysts, Table S8: Selectivities at 250–400 °C, conversion and reaction rate constants for the vanadium containing catalysts with 50 mg of catalyst (except FeVO4 and FeVO4-Cl which were tested with 7.5 mg), in a feed flow

of 15 NmL/min O2, 127.5 NmL/min N2 and 3–5% CH3OH, Table S9: Pre-exponential factor (k0) and activation energy (Ea) of vanadium containing catalysts, Table S10: Specific selectivities at 250–400 °C, conversion and reaction rate constants for the catalysts not containing molybdenum or vanadium with 50 mg of catalyst, in a feed flow of 15 NmL/min O2, 127.5 NmL/min N2 and 3–5% CH3OH, Table S11: Pre-exponential factor (k0) and activation energy (Ea) of catalysts not containing molybdenum or vanadium.

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**Data Availability Statement:** In this section, please provide details regarding where data supporting reported results can be found, including links to publicly archived datasets analyzed or generated during the study. Please refer to suggested Data Availability Statements in section "MDPI Research Data Policies" at https://www.mdpi.com/ethics. You might choose to exclude this statement if the study did not report any data.

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