

Inverse Yield Locus Identification of Sheet Metal Using a Complex Cruciform in Biaxial Tension and Digital Image Correlation [†]

Sam Coppieters ^{1,*}, Tomoyuki Hakoyama ², Dimitri Debruyne ¹, Susumu Takahashi ³ and Toshihiko Kuwabara ⁴

¹ Department of Materials Engineering, KU Leuven, 9000 Ghent, Belgium; dimitri.debruyne@kuleuven.be

² Department of Mechanical Engineering, Gifu University, Gifu 501-1193, Japan; hakoyama@gifu-u.ac.jp

³ Department of Mechanical Engineering, Nihon University, Chiba 275-8575, Japan; takahashi.susumu32@nihon-u.ac.jp

⁴ Division of Advanced Mechanical Systems Engineering, Institute of Engineering, Tokyo University of Agriculture and Technology, Tokyo 184-8588, Japan; kuwabara@cc.tuat.ac.jp

* Correspondence: sam.coppieters@kuleuven.be; Tel.: +32-9-331-6672

[†] Presented at the 18th International Conference on Experimental Mechanics, Brussels, Belgium, 1–5 July 2018.

Published: 9 May 2018

Abstract: Finite Element Model Updating (FEMU) is an intuitive inverse technique enabling to efficiently characterize plastic material behavior. Although, conclusive proof of concept for this method can be found in literature, a thorough understanding of the key FEMU-ingredients and their impact on the identification of plastic anisotropy is currently missing. In this paper, we aim at minimizing the experimental work associated with yield locus identification of sheet metal via homogeneous biaxial tensile tests. To this end, a biaxial tension apparatus with link mechanism is used to generate a heterogeneous deformation field within a perforated cruciform specimen. The experimentally measured force and displacement field are used in the FEMU procedure to identify an anisotropic yield criterion. The FEMU approach is assessed by comparing the results with experimental data acquired from state-of-the-art stress-controlled biaxial tensile test in the first quadrant of stress-space.

Keywords: anisotropic yield function; Finite Element Model Updating; digital image correlation; biaxial tensile testing

1. Introduction

State-of-the-art stress-controlled biaxial tensile experiments are conducted to determine the parameters of advanced anisotropic yield functions for sheet metal. Plastic yielding in the first quadrant of stress space can be probed using a cruciform specimen [1] and a stress-controlled biaxial tensile machine [2]. Such approach enables to characterize plastic yielding with a high resolution and accuracy. The downside, however, is the large amount of experimental effort and the required availability of dedicated test equipment. A biaxial tension apparatus with link mechanism [3] enables to reduce the equipment cost since a standard tensile machine can be used. Lecompte et al. [4] showed that the experimental work can be further reduced by resorting to the Finite Element Model Updating (FEMU) technique using a complex cruciform specimen. The basic principle of the latter approach is the generation of a heterogeneous deformation field using the biaxial tension apparatus, which is measured with digital image correlation and compared to FE simulations enabling inverse identification of the yield locus through FEMU. In this paper a biaxial tension apparatus with link mechanism [3] is used to generate an inhomogeneous deformation field within the measurement

gauge of a perforated cruciform specimen. The work hardening behavior is identified a priori by a standard tensile test in the rolling direction (RD) while the in-plane plastic anisotropy is inversely identified using FEMU. The accuracy of the identified plastic anisotropy is assessed by comparison with experimental data obtained from state-of-the-art stress-controlled biaxial tensile testing [2].

2. Methodology and Materials

The idea residing in the FEMU-approach relies on a heterogeneously deforming specimen. To this end, a perforated cruciform specimen is used in this paper. The specimen is shown in Figure 1c. An FE model assuming a von Mises material was used to investigate the stress states generated in the Area Of Interest (AOI), i.e., the region in which the strains are measured. Coppieters et al. [4] found that this perforated specimen generates stress states covering a large portion of the first quadrant of stress space and concluded that the specimen is a good candidate for inverse yield locus identification through FEMU. The experimental set up is shown in Figure 1a,b. The biaxial tension apparatus with link mechanism proposed by Nagayasu et al. [3] is used to subject the perforated specimen to biaxial tension in such a way that an equal velocity of all grips is obtained in the x - and y -directions. The mechanism is mounted in a standard uniaxial tensile machine with a load capacity of 250 kN. Stereo DIC is used to measure the displacement fields at the surface of the deforming specimen. The tensile forces in the arms of the cruciform are measured with load cells with a capacity of 20 kN and synchronized with the DIC system. Abaqus/Standard was used to build the FE model using shell elements (S4R). A low carbon steel with a nominal thickness of 1.2 mm was used in this study. The perforated cruciform specimen was produced by laser cutting. The material was characterized in the first quadrant of stress space using biaxial tensile tests and tube expansion tests (7 linear stress paths). The parameters of the Yld2000-2d yield function were calibrated using r_0 , r_{45} , r_{90} , $\dot{\epsilon}_b$, σ_0/σ_0 , σ_{45}/σ_0 , σ_{90}/σ_0 and σ_b/σ_0 , where $r_{\#}$ and $\sigma_{\#}$ are the r -value and tensile flow stress measured at an angle of $\#$ from the RD, respectively, and $\dot{\epsilon}_b$ and σ_b are the plastic strain rate ratio $d\epsilon_y^p/d\epsilon_x^p$ and the flow stress at equibiaxial tension $\sigma_x : \sigma_y = 1:1$, respectively. The exponent M of the Yld2000-2d yield function was calibrated by minimizing the root mean square error between the selected contour of plastic work and the calculated yield locus. Differential work hardening was captured by changing the parameters and the exponent of the Yld2000-2d yield criterion as a function of the reference plastic strain ϵ_0^{pl} . Figure 2 shows the evolution of the Yld2000-2d yield function as a function of different values of plastic reference strain $\epsilon_0^{pl} = 0.002, 0.05, 0.2$. The Rolling Direction (RD) and the Transverse Direction (TD) of the material are defined as the x - and y -axis, respectively. The strain hardening behavior in the RD was identified using a quasi-static standard tensile test.

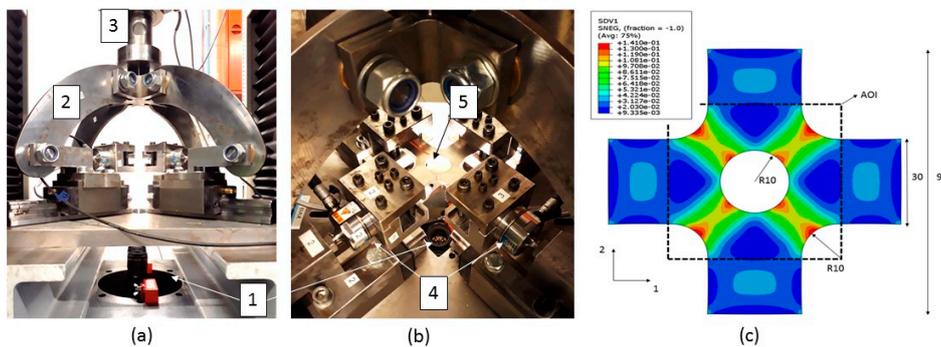


Figure 1. Experimental set up; (a) 1. Stereo DIC 2. Biaxial link mechanism 3. Cross-head uniaxial tensile machine; (b) 4. Load cells 5. Perforated cruciform specimen; (c) Perforated cruciform specimen: plastic equivalent strain.

The basic principle of FEMU is to minimise the discrepancy between the experimentally measured and numerically computed response by adapting the unknown parameters of the

anisotropic yield criterion in the FE model. In this work, the Levenberg-Marquardt minimisation algorithm is used to minimize the following cost function:

$$C(\mathbf{p}) = \sum_{i=1}^m \sum_{j=1}^{n_i} \left[\left(\frac{\varepsilon_{xx,ij}^{exp} - \varepsilon_{xx,ij}^{num}}{\varepsilon_{xx,RMS,i}^{exp}} \right)^2 + \left(\frac{\varepsilon_{yy,ij}^{exp} - \varepsilon_{yy,ij}^{num}}{\varepsilon_{yy,RMS,i}^{exp}} \right)^2 + \left(\frac{\varepsilon_{xy,ij}^{exp} - \varepsilon_{xy,ij}^{num}}{\varepsilon_{xy,RMS,i}^{exp}} \right)^2 \right] + \sum_{i=1}^m \left[n_i \left(\frac{F_i^{exp} - F_i^{num}}{F_i^{exp}} \right)^2 \right] \quad (1)$$

With \mathbf{p} the vector of unknown parameters of the anisotropic yield function, m the number of load steps ($m = 1$ in this paper) and n_i the number of data points in the DIC measurement at load step i . The subscripts exp and num indicate experimental response and numerical response, respectively. Figure 3a shows the experimentally obtained strain field at $F^{exp} = 8$ kN in the transverse direction (TD). The maximum equivalent plastic strain at this load step was about 0.2 and the average strain rate was kept below $10^{-4} \frac{1}{s}$.

3. Results and Discussion

The experimental data at $F^{exp} = 8$ kN in TD), is used to identify the plane stress Hill48 yield criterion using FEMU. The most straightforward approach is to use the measured forces in the arms of the cruciform as boundary conditions in the FE model of the perforated cruciform specimen. Coppieters et al. [5] found that this approach is liable to modelling errors in the load distribution. The latter study showed that applying displacement boundary conditions leads to more reliable results. As opposed to a force distribution, displacement components can be measured locally using DIC and directly implemented as boundary conditions in the FE model. Figure 2 shows the effect of boundary conditions on the identification of the Hill48 yield criterion. The yield locus labeled *Hill48–Force-driven FEMU* was identified by assuming a distributed shell edge load in the FE model. The yield locus *Hill48–Displacement-driven FEMU I* was identified by adopting locally measured displacement components as boundary conditions. Both yield loci were identified by solely minimizing the discrepancy between experimental and numerical strain values. It can be inferred from Figure 3 that FEMU is highly sensitive to an erroneous modelling of the boundary conditions. Figure 3b,c show the absolute error in the strain fields obtained with both identified yield loci.

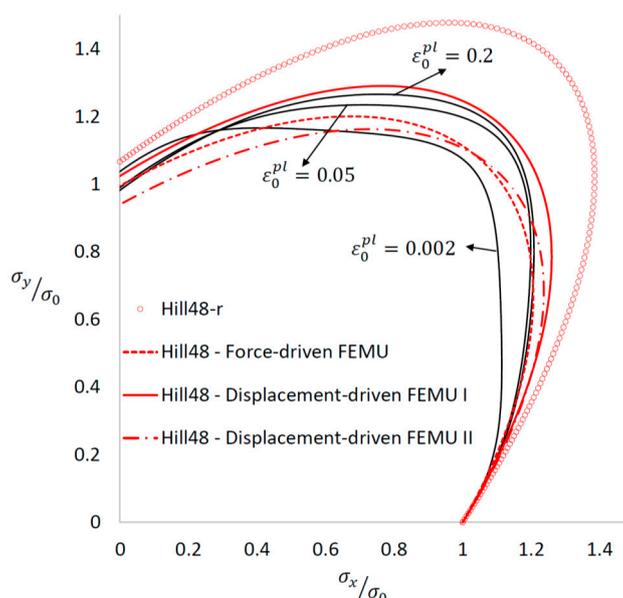


Figure 2. Normalized yield loci: Reference yield loci (Yld2000-2d) and inversely identified yield loci (Hill48).

The strain error map obtained with yield locus *Hill48–Force-driven FEMU* (Figure 3b) clearly shows that the strain error in the transition region towards the arms is larger than the results obtained with the yield locus *Hill48–Displacement-driven FEMU I*. Nevertheless, the difference in predicted strain values by both identified yield loci is deemed small. The relative error with respect to the predicted tensile force in the TD by *Hill48–Displacement-driven FEMU I*, however, is about 14%, see Table 1. The yield locus *Hill48–Displacement-driven FEMU II* shown in Figure 2 is identified by including the force (TD) in the cost function. It can be inferred that including the force significantly affects the yield locus identification. The relative error in the force prediction is in this case below 1% (see Table 1) while the strain error map (Figure 3d) is similar to the one obtained using the yield locus *Hill48–Displacement-driven FEMU I* (Figure 3c). As a consequence, it can be concluded that *Hill48–Displacement-driven FEMU II* yields the most accurate identification. In the remainder of this work, we refer to this yield locus as the inversely identified Hill48 yield function.

Table 1. Relative error in the force prediction (TD).

Yield Function	Yld2000-2d (DH)	Hill48-r	Hill48–FEMU I	Hill48–FEMU II
Force in TD (N)	8542.2	10053.8	9133.8	7924.9
Relative Error (%)	6.8	25.7	14.2	0.94

Comparison with the bench mark characterization through homogeneous biaxial tensile testing (see solid black loci in Figure 2), however, reveals a significant difference. The main reason for this is that the identified Hill48 yield criterion cannot describe the actual material behavior. Indeed, the material exhibits differential work hardening which cannot be captured by the adopted Hill48 yield function. In essence, the FEMU fits the Hill48 yield function to the available experimental data, and, consequently, merely yields an average of the actual yield behavior. Given the fact that the material exhibits differential work hardening also affects the influence of the number of load steps used in the FEMU. Here, only the final state was taken into account which means that the deformation history is ignored. Finally, it must be noted that the heterogeneous experiment generates stress states which are not present in the homogeneous biaxial tensile tests. Indeed, the experiment on a perforated specimen generates shear stresses which are absent during conventional biaxial tensile testing in the first quadrant of stress space. The predictive accuracy of the inversely identified Hill48 yield function can be compared with the accuracy of conventionally calibrated anisotropic yield functions. Figure 2 shows the Hill48 yield function (labeled *Hill48-r*) calibrated using the *r*-values ($r_0; r_{45}; r_{90}$). The black yield loci represent the actual material behavior modelled by the Yld2000-2d (DH) yield function dependable of the reference plastic strain to reproduce the experimentally observed differential work hardening of the test material during biaxial tensile testing using cruciform specimens. Both the Hill48-r and the Yld2000-2d yield functions are used to reproduce the experiment using a displacement-driven finite element simulation. The strain error maps are shown in Figure 4 and it can be inferred that the Yld2000-2d yield function predicts the strain field more accurately than the Hill48-r yield function. In addition, the force prediction using Yld2000-2d (DH) is much more accurate (relative error 6.8% versus 25.7%, see Table 1) than by using Hill48-r. The inversely identified Hill48 yield function, however, predicts a similar strain error map (Figure 3d) as the one obtained with the Yld2000-2d (DH) yield function (Figure 4b). Additionally, the force prediction of the inversely identified Hill48 yield function is in better agreement with the experiment (see Table 1). This is, however, not surprising since the Hill48 yield function was inversely identified using the same experiment. Given that the Yld2000-2d (DH) yield function was calibrated by other experiments, assessment using the perforated cruciform is valid and it can be concluded that the material modelling approach using Yld2000-2d (DH) yields accurate results. In order to assess the accuracy of both the yield functions, a tensile test in the 45-degree direction (45D) to RD can be used as this experiment was not used for calibration purposes. Figure 5 shows the experimental data along with the FE simulations of a standard tensile test in the 45D. Figure 5a shows the measurement and the prediction of the engineering stress-strain curve using both yield functions. It can be inferred that the Yld2000-2d (DH) yield function enables to reproduce the stress-strain curve much more

accurately than the inversely identified Hill48 yield criterion. Figure 5b shows the evolution of r_{45} as a function of the true strain in the tensile direction (45D). The experimental data was obtained through DIC measurements. Unlike the inversely identified Hill48 yield function, the Yld2000-2d (DH) yield function accurately reproduces the r_{45} -evolution. From this it can be concluded that the validity of the inversely identified Hill48 yield function is strictly confined to experiment used in the FEMU approach, i.e., the perforated cruciform specimen under biaxial tension.

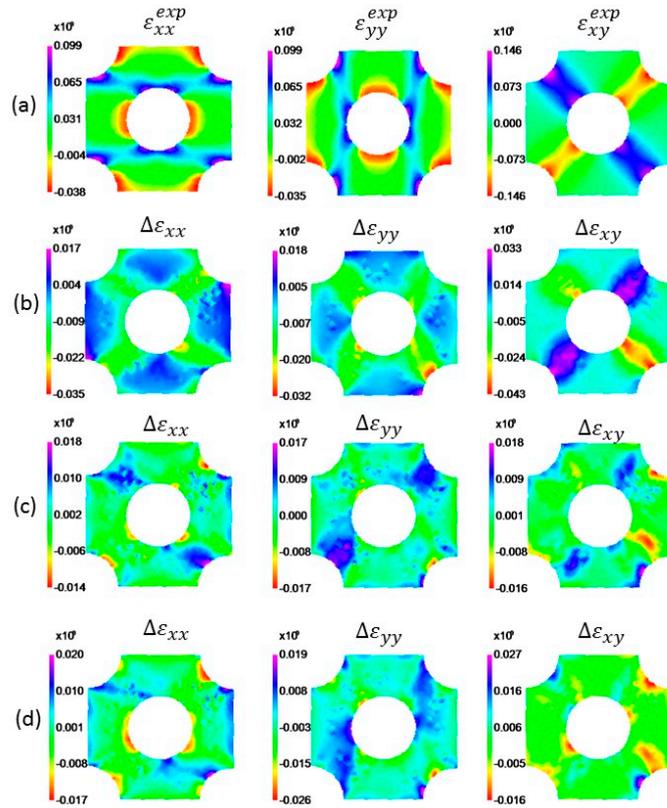


Figure 3. (a) Experimental strain field at approximately 8kN (TD); Discrepancy between experimental and numerical strain components obtained with the identified Hill48 yield criterion; (b) Force-driven FEMU (strain-based cost function); (c) Displacement-driven FEMU (strain-based cost function); (d) Displacement-driven FEMU (strain –and force-based cost function).

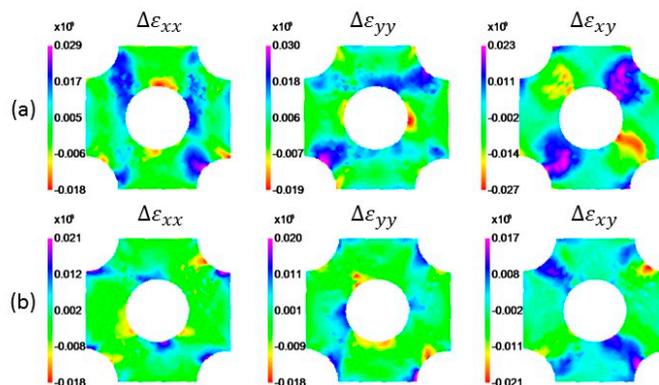


Figure 4. Discrepancy between experimental and numerical strain components at load step 8 kN (TD): (a) Hill48-r yield criterion; (b) Yld2000-2d (DH) yield criterion that reproduces the differential hardening of the test material.

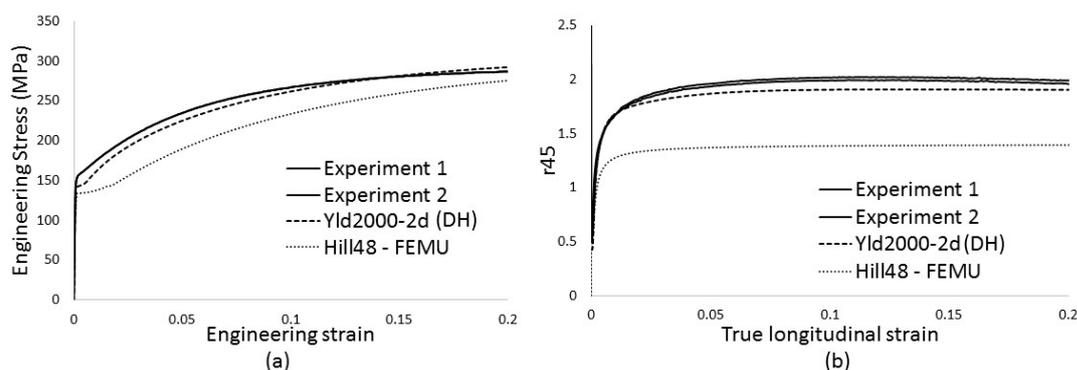


Figure 5. Assessment of the identified yield functions through a tensile test in the 45D (a) Engineering stress–engineering strain curve; (b) r_{45} evolution as a function of the true longitudinal strain.

4. Conclusions

The Finite Element Model Updating (FEMU) technique and Digital Image Correlation (DIC) are used to inversely identify the Hill48 yield function via a perforated cruciform specimen under biaxial tension. The FEMU approach is assessed by comparing the results with experimental data obtained from biaxial tensile testing using cruciform specimens. In addition, the identified anisotropic yield functions are used to simulate an independent experiment demonstrating that the validity of the inversely identified Hill48 yield function is confined to the experiment used in the FEMU procedure.

Author Contributions: S.C. conducted the experiments on the perforated cruciform specimen and performed the inverse identification. S.C. and D.D. wrote the paper. T.H. and T.K. conducted the state-of-the-art biaxial tensile tests and provided the test material. S.T. provided the biaxial tension apparatus with link mechanism.

Conflicts of Interest: The founding sponsors had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript, and in the decision to publish the results.

References

1. International Organization for Standardization. *Metallic Materials—Sheet And Strip—Biaxial Tensile Testing Method Using a Cruciform Test Piece*; ISO 16842:2014; International Organization for Standardization: Geneva, Switzerland, 2014.
2. Kuwabara, T.; Ikeda, S.; Kuroda, K. Measurement and analysis of differential work hardening in cold-rolled steel sheet under biaxial tension. *J. Mater. Process. Technol.* **1998**, *80*, 517–523.
3. Nagayasu, T.; Takahashi, S.; Kuwabara, T. Development of compact biaxial tensile testing apparatus using conventional compression testing machine and evaluation of the results. In Proceedings of the IDDRG 2010, Graz, Austria, 31 May–2 June 2010.
4. Lecompte, D.; Cooreman, S.; Coppieters, S.; Vantomme, J.; Sol, H.; Debruyne, D. Parameter identification for anisotropic plasticity model using digital image correlation. *Eur. J. Comput. Mech.* **2009**, *18*, 393–418.
5. Coppieters, S.; Hakoyama, T.; Debruyne, D.; Takahashi, S.; Kuwabara, T. Inverse yield locus identification using a biaxial tension apparatus with link mechanism. In Proceedings of the Numisheet 2018, Accepted, Tokyo, Japan, 30 July–3 August 2018.
6. Barlat, F.; Brem, J.C.; Yoon, J.W.; Chung, K.; Dick, R.E.; Lege, D.J.; Pourboghrat, F.; Choi, S.-H.; Chu, E. Plane yield stress function for aluminum alloy sheets-Part I: Theory. *Int. J. Plast.* **2003**, *19*, 1297–1319.

