

MDPI

Article

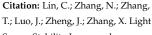
# Light Source Stability Issues and Measurements in Flux Calibrations for Space Gaze Camera

Cui Lin 1,2, Ning Zhang 1, Tianyi Zhang 1, Jing Luo 1, Jianing Zheng 1,2 and Xiaohui Zhang 1,\*

- Changchun Institute of Optics, Fine Mechanics and Physics, Chinese Academy of Sciences, Changchun 130033, China
- <sup>2</sup> University of Chinese Academy of Sciences, Beijing 100049, China
- \* Correspondence: zhangxiaohui@ciomp.ac.cn

Abstract: Flux calibration is an important test item in laboratory calibration experiments of space gaze cameras, which is the basis for obtaining high-precision scientific application data. In the flux calibration of a space gaze camera, the multi-field calibration method is adopted. The instability of the calibration light source will introduce uncertainty during the calibration process. When the spatial camera adopts the gaze imaging mode, the stability of the light source indicates the change in the total energy received by the image plane during the gaze time, which is characterized by relative uncertainty. When the luminous intensity standard lamp runs for the long-term calibration of the stability of the calibration light source, real-time performance and accuracy cannot be guaranteed. Therefore, it is proposed to use a photodetector to measure the stability of the calibration light source for long-term and real-time accurate measurements. First, the stability of the photodetector is calibrated using the light emitting diode; then, the stability of the calibration light source is measured using the photodetector; finally, the stability uncertainty of the calibration light source and the measurement uncertainty of the method is evaluated. The results of the simulation analysis and experimental verification indicate that the gaze time is 5 min and the sampling frequency of the photodetector is 15 Hz; for example, when the flux calibration time is 8 h, the stability uncertainty of the calibration source is 0.42%, and the relative measurement uncertainty is 0.01%.

**Keywords:** space gaze cameras; flux calibration; light source stability; photoelectric detectors; optoelectronic measurements



check for updates

Source Stability Issues and Measurements in Flux Calibrations for Space Gaze Camera. *Photonics* **2022**, *9*, 976. https://doi.org/ 10.3390/photonics9120976

Received: 10 November 2022 Accepted: 6 December 2022 Published: 12 December 2022

**Publisher's Note:** MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https://creativecommons.org/licenses/by/4.0/).

#### 1. Introduction

Since the 20th century, astronomical telescopes have shown two major development trends. One is to develop in the direction of a large aperture and large field of view [1–5] to obtain higher spatial resolution and resolution efficiency; the other is to develop from ground-based telescopes to space telescopes [6–8] to reduce the influence of atmospheric and other factors on the observation results. Therefore, large-aperture and large-field-of-view space telescopes are an important branches of the future development of astronomical observation equipment. However, due to the non-Lambertian reflection characteristics of the telescope observation target and the response characteristics of the telescope sensor, the information received by the telescope image detector contains radiometric aberrations. It is necessary to carry out flux calibration to obtain the radiometric properties of the target [9,10]. The high-precision flux calibration enables the telescope to measure the shape of galaxies more accurately, reduce transmission errors, and promote the upgrade of deep space exploration to quantitative and refined technology [11,12]. Therefore, it is of great significance to carry out high-precision flux calibrations for space telescopes with large apertures and large-fields.

At present, the integrating sphere method, the flat-field screen method, and the collimator method are commonly used to calibrate the flux of optical loads [13–15]. To

Photonics 2022, 9, 976 2 of 16

adapt to the working environment of a space telescope, the flux calibration method for a large-aperture space telescope based on multifield calibration (MFFC) is proposed. Based on flat-field calibration, the sub-field calibration is selected to obtain the full-field calibration information. In the process of sub-field scanning, the calibration light source will produce brightness drift after working for a long time. Therefore, it is necessary to accurately measure the stability of the light source to correct the calibration coefficient.

To improve the flux calibration accuracy, the calibration source is traced to the radiation standard. The common method is to use a luminous intensity standard lamp (SL) and a photometer to measure the luminous intensity of the calibration light source according to the equidistance method. For example, the radiometric calibration spectral source (RCSS) [16] in the James Webb Telescope and the direct illumination calibration experiment (DICE) [17] in the Sloan Digital Sky Survey project trace the stability of the light source to the national standards. However, the equidistance method of measuring the stability of the light source has the limitation that it cannot monitor the luminous intensity of the light source in real-time and the long term.

This manuscript proposes a method to measure the stability of a calibration light source using a photodetector (PD) to achieve the purpose of long-term, real-time monitoring of light source stability and, to a certain extent, improve the measurement accuracy of light source stability. The monitoring time of the stability is extended from 4 h to 8 h or more. First, a light-emitting diode (LED) is used to calibrate the stability of a PD; then, the calibrated PD is used to measure the stability of the calibrated light source; finally, the stability of the calibrated light source and the measurement uncertainty is evaluated. In the simulation analysis and experimental verification, the gaze time is 5 min, and the PD sampling frequency is 15 Hz when the flux calibration time is set to 8 h. The experimental results show that the stability uncertainty of the calibration light source was 0.42%, and the relative measurement uncertainty was 0.01%. The experimental results show that the measurement accuracy of using PD monitoring and the stability of the light source meets the calibration requirements of the space gaze camera. The method can be used to correct the coefficients in the flux calibration work of the large-aperture space telescope to obtain more accurate scientific observation results.

# 2. Light Source Stability on Flux Calibration

At present, space telescopes are developing toward large-aperture and large fields of view for deep space exploration. The commonly used flux calibration methods, such as the integrating sphere method, can no longer meet the calibration needs of space telescopes. Therefore, an MFFC device is proposed, as shown in Figure 1. Based on flat-field calibration, multiple subfields are selected for calibration to achieve the purpose of full-field flux calibration. For imaging faint targets in deep space exploration, the space telescope uses a gaze camera at the image plane. The beam-splitting device divides the emergent light of the integrating sphere source into two beams; one beam is used for calibrating the space gaze camera, and the other beam is used for monitoring the stability of the light source in real-time. A neutral density filter is used to adjust the irradiance of the PD to ensure that it is within the linear operating range of the PD.

The integrating sphere light source can be approximated as a Lambertian source. The radiant flux  $\Phi$  through the precision pinhole is:

$$\Phi = E \cdot S = \frac{\pi I d^2}{4I^2} \tag{1}$$

where E represents the irradiance at the pinhole, S represents the area of the pinhole,  $\pi$  is the PI, I represent the luminous intensity of the light source, d represents the pinhole diameter,

Photonics 2022, 9, 976 3 of 16

and l is the distance between the light source and the pinhole. Through the collimator and the space telescope, the radiant flux received by the space camera is attenuated by c (0 < c < 1), i.e.,

$$\Phi = c \cdot \frac{\pi I d^2}{4l^2} \tag{2}$$

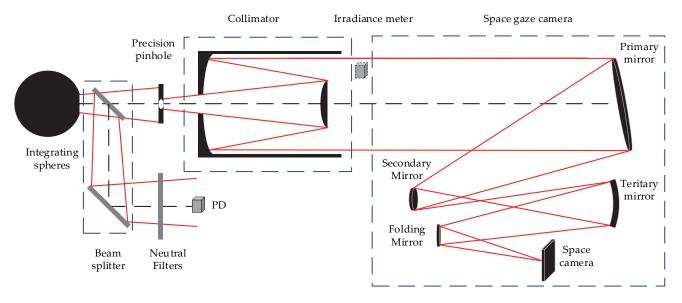


Figure 1. Schematic diagram of the flux calibration device for a large-aperture space telescope.

The output voltage V of the space camera can be calculated by the following equation [18]:

$$V = P \cdot E \cdot S \cdot R_f = P \cdot \Phi \cdot R_f \tag{3}$$

where P represents the responsivity of the image plane detector, and  $R_f$  is the gain of the detector preamplifier.

The flux calibration coefficient *R* of the space telescope can be calculated by the following equation:

$$R = \frac{V}{I} \tag{4}$$

where *L* represents the radiance at the entrance pupil of the telescope, which is measured by the luminance meter.

Space telescopes have a long gaze time to achieve the detection of faint targets in deep space. To improve the accuracy of the laboratory flux calibration, the calibration coefficient of the space camera during the gaze time should be calculated.

When the space camera is used for deep space observation, the variation in the total energy *Q* is received by the image plane during the gaze time. That is:

$$Q = \int_{t_0}^{t_0 + \tau} \Phi dt = c \cdot \frac{\pi d^2}{4l^2} \int_{t_0}^{t_0 + \tau} I dt$$
 (5)

where  $t_0$  is the start time of the single gaze imaging in the telescope and  $\tau$  is the time of the single gaze. When the luminous intensity of the calibration light source changes with time as I(t), the energy received by the image plane of the staring camera is a function of time Q(t):

$$Q(t) = c \cdot \frac{\pi d^2}{4l^2} \int_{t_0}^{t_0 + \tau} I(t)dt$$
 (6)

Photonics 2022, 9, 976 4 of 16

The flux calibration coefficient of the space telescope at this time is:

$$R = \frac{PR_f \int \Phi(t)dt}{\int L(t)dt} = c \cdot \frac{PR_f}{L\tau} \cdot \frac{\pi d^2}{4l^2} \int_{t_0}^{t_0+\tau} I(t)dt$$
 (7)

The stability of the light source has less influence on the calibration accuracy when the gaze time of the space camera is short. There is a gradual increase in the impact of light source stability on the calibration accuracy with the growth of the gaze time. In summary, the quantitative analysis of the light source stability should be performed to improve the accuracy of space telescope flux calibrations. To improve the calibration accuracy, the light source should be corrected if the stability uncertainty is larger.

## 3. Measurements of Light Source Stability

Parallel light is incident on the telescope at different field-of-view angles when using the MFFC calibration space telescope. The attenuation coefficient introduced by the space telescope becomes  $c(\theta)$ , and the received energy  $Q(\theta, t)$  on the image plane is:

$$Q(\theta, t) = c(\theta) \cdot \frac{\pi d^2}{4l^2} \int_{t_0}^{t_0 + \tau} I(t) dt$$
 (8)

The received energy at the image plane decreases with the increasing angle at which parallel light is incident. Therefore, the stability of the calibration source cannot be analyzed directly using received energy from the spatial camera image plane detector.

#### 3.1. Equidistance Method to Measure the Stability of the Light Source

The commonly used measurement method for light source stability is shown in Figure 2, which calibrates the light source stability with SL and the photometer according to the equidistance method.

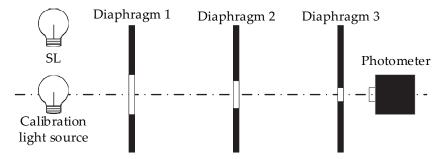


Figure 2. Equidistance method to measure light source stability.

However, the equidistance method has some limitations when measuring the stability of the light source:

- 1. The luminous intensity of the SL is used as the standard. The measurement results of luminescence intensity are transmitted using the photometer. The real-time monitoring of the calibrated light source cannot be realized.
- 2. SL was required so that the voltage change at the lamp terminal did not exceed 0.15% within 4 h of illumination. When using MFFC for the flux calibrations of space telescopes, the total calibration time is much longer than 4 h due to the large aperture and gaze imaging of the space telescope. Therefore, the equidistance method cannot achieve the long-term monitoring of the calibration light source stability.

In summary, the equidistance method cannot monitor the stability of the calibration light source in real-time and over time. The voltage fluctuations at the lamp terminal of

Photonics **2022**, *9*, 976 5 of 16

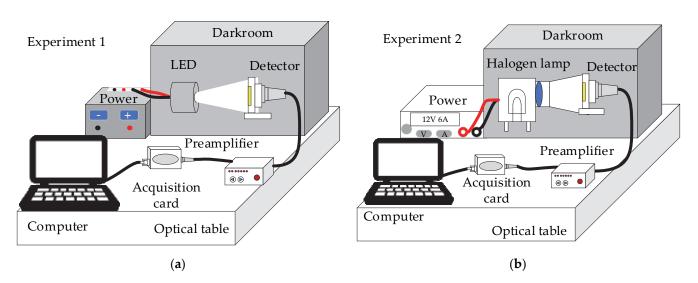
the SL are consistent with a uniform distribution. The uncertainty  $u_1$  of the equidistance method is calculated by the B class rating:

$$u_1 = \frac{0.15\%}{\sqrt{3}} \approx 0.09\% \tag{9}$$

We propose to use PD to measure the stability of the light source in order to achieve a high-precision flux calibration for large-aperture space telescopes. This will realize the real-time and long-term monitoring of light source stability, as well as improve measurement accuracy.

## 3.2. PD Measurement of the Stability of the Light Source

The device for the PD measurement of light source stability is shown in Figure 3. It consists of a light source system and a real-time monitoring system. The light source system includes an LED light source and a halogen lamp. In Experiment 1, the LED light source is used to calibrate the stability of the PD, as shown in Figure 3a; in Experiment 2, the halogen lamp is used as the calibration light source, and the stability measurement device is shown in Figure 3b. The real-time monitoring system consists of a PD, a preamplifier, an AD acquisition card, and a computer. Since the stability of the light source characterizes the relative change degree of the light source luminance over time, the influence of the spatial uniformity of the light source luminance on the measurement results is not considered.



**Figure 3.** Schematic diagram of the light source stability measurement: (a) Device for calibrating PD stability; (b) Device for measuring the stability of the light source.

The total energy Q(T) received by the PD during the gaze time is:

$$Q(T) = \int_{t_0}^{t_0 + \tau} \Phi(t)dt = \frac{1}{P \cdot R_f} \int_{t_0}^{t_0 + \tau} V(t)dt$$
 (10)

The stability of PD in Experiment 1 is characterized by the fluctuation of Q(T). The main sources of uncertainty are the stability of LED and PD. Therefore, the lamp terminal voltage of the LED light source should be monitored during the experiment. In Experiment 2, the stability of the light source is characterized by the fluctuation of Q(T). The main error source is the stability of the detector.

#### 3.3. Light Source Stability Measurement Accuracy

The factors affecting the measurement accuracy of the light source stability mainly include the following aspects:

Photonics 2022, 9, 976 6 of 16

#### 1. Stability of LED

LED stability is expressed as the stability of luminous intensity. The most important factors are the voltage fluctuation of the power supply, the ambient temperature, and the lifetime of the LED.

It is affected by the electricity consumption of the city's power supply circuit. The voltage fluctuation between the peak and trough values ranges from -7 to 10%. It is assumed that the voltage fluctuations conform to a uniform distribution. According to the class B assessment, the introduced uncertainty is:

$$u_2 = \frac{10\%}{\sqrt{3}} = 3.33\% \tag{11}$$

The introduced uncertainty is large. Voltage fluctuations are reduced by using a regulated power supply [19].

The ambient temperature is an important factor impacting the luminous intensity of LED. LED operation creates heat accumulation in the surrounding environment. LED luminous intensity decreases as the temperature increases [20]. To reduce the impact of temperature accumulation on the LED luminous intensity, a large number of heat sinks should be used to accelerate the temperature transfer.

The LED luminous intensity changes rapidly during the initial operation and then decays slowly. The lifetime of general lighting LED is 50,000~100,000 h [21]. The lifetime of high-stability LED can be shortened by 10 times. The luminous intensity decreases as the LED ages. The stability of the calibration light source has a shorter measurement time compared to the lifetime of the LED. Therefore, the impact of LED aging on measurement accuracy is not considered.

#### 2. Noise of PD

The total noise introduced during the operation of the PD is:

$$r = \sqrt{r_{shot}^2 + r_{dark}^2 + r_{VR}^2 + r_{read}^2 + r_{other}^2}$$
 (12)

where r is the total noise,  $r_{shot}$  is the scatter noise,  $r_{dark}$  is the dark noise,  $r_{VR}$  is the thermal noise,  $r_{read}$  is the readout noise, and  $r_{other}$  is the fixed noise and other noises. Among them, thermal noise has the greatest impact on PD stability, which can be represented by the following equation:

$$r_{VR} = \sqrt{4kTR\Delta f} \tag{13}$$

where k is the Boltzmann constant, T is the absolute temperature, R is the resistance, and  $\Delta f$  is the noise equivalent bandwidth. After the PD operate, the output voltage value increases with internal temperature accumulation. Dynamic stability is achieved after some time.

### 3. Uncertainty introduced by stray light

The lower irradiance of the observed target is used for deep space exploration by space telescopes. The luminous intensity of the calibration light source is low during the flux calibration in the laboratory. Straying light from the external environment has a greater impact on the stability of the light source. Therefore, the experimental setup should be placed in a dark room when using PD to measure the stability of the light source.

In summary, the measurement uncertainty of the calibration source stability mainly comes from LED stability and PD stability. The uncertainty introduced by these two factors is finally expressed as the measurement uncertainty of PD in Experiment 1.

### 3.4. Light Source Stability Algorithm

For the flux calibration of space gaze cameras, the impact of light source stability on calibration accuracy is characterized as the change in the total energy received by the image plane during the gaze time. The change in the total energy received by the image plane

Photonics **2022**, 9, 976 7 of 16

during the gaze time should be considered when using PD to measure the stability of the light source. Therefore, a light source stability metrology algorithm is proposed for the flux calibration of the gaze camera. Based on the method for measuring the stability of the light source, the algorithm is used for measuring the stability of the flux calibration light source of the space gaze camera. This realizes the real-time, long-term, and high-efficient stability monitoring of the calibration light source. Improving the flux calibration precision of the space gaze camera is essential to obtaining more accurate scientific observation results.

In the light source stability measurement device shown in Figure 3, the luminous flux received by the photosensitive surface at a single sampling of the PD can be calculated according to Equation (3):

$$\Phi = \frac{V}{PR_f} \tag{14}$$

The total energy Q(T) received by the PD during the gaze time can be calculated by:

$$Q(T) = \int_{t_0}^{t_0 + \tau} \Phi dt = \frac{\int_{t_0}^{t_0 + \tau} V dt}{PR_f} = \frac{\sum_{i=1}^{m} V}{PR_f f}$$
 (15)

where f is the PD sampling frequency (in Hz) and m is the number of PD sampled in the gaze time:

$$m = \tau/f \tag{16}$$

The uncertainty of the light source stability is evaluated using the standard deviation s:

$$s = \sqrt{\sum_{i=1}^{n} v_i^2 / (n-1)} \tag{17}$$

$$v_i = Q(T) - Q_0 \tag{18}$$

where  $v_i$  is the residual error, n is the number of gaze times in the calibration time, and  $Q_0$  is the estimate of Q(T).  $Q_0$  is the mean when Q(T) does not drift significantly; otherwise, the initial value is taken. To describe the stability of the light source more accurately, the relative uncertainty u is used to evaluate the influence of the light source stability on the calibration coefficient:

$$u = \frac{s}{O_0} \tag{19}$$

Formulas (15)–(19) are used to process the measurement results of Experiment 1 and Experiment 2, respectively. In this case, the stability uncertainty of the calibration source and the relative measurement uncertainty of the measurement method can be obtained.

## 4. Simulation Verification

Figure 4 shows the flowchart of the light source stability measurement for the flux calibration of the space gaze camera. Firstly, the stability of PD is calibrated using the LED light source, and the output voltage of PD and the terminal voltage of the LED light source are measured. When the lamp terminal voltage fluctuation can meet the PD calibration requirements, the calibrated PD is used to measure the stability of the calibration light source. The measurement result is output if the measurement uncertainty introduced by the PD stability can meet the light source stability requirements of the flux calibration of the space gaze camera.

Photonics 2022, 9, 976 8 of 16

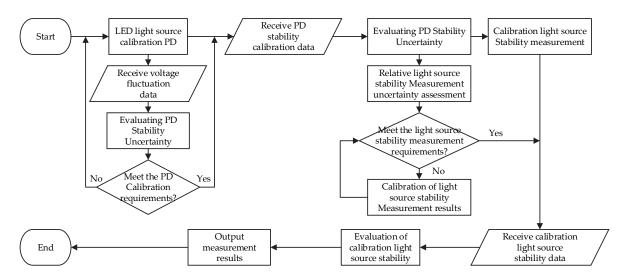
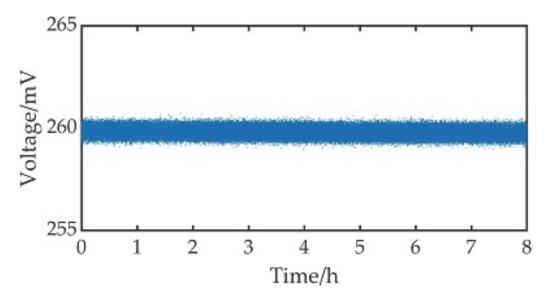


Figure 4. Flowchart of light source stability measurement for space gaze camera flux calibration.

The total calibration time of the spatial gaze camera is controlled at 8 h, and the single gaze time is 5 min. Moreover, the sampling frequency of PD is set to 15 Hz. The feasibility of the light source stability for measuring the flux calibration of the space gaze camera by PD is verified through the simulation analysis of Experiment 1 and Experiment 2.

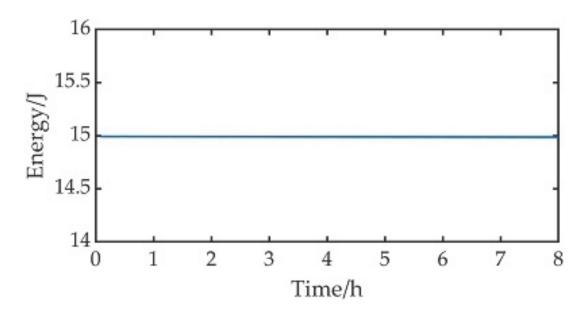
When the luminous intensity of the LED light source is set to 0.5 cd, there is a random error of 0.05%, which conforms to the uniform distribution. This produces a drift of 0.01% in the calibration process. The PD photosensitive surface area is  $100~\text{mm}^2$ , and the responsiveness is 0.52 A/W. The gain of the preamplifier circuit is  $10^4~\text{V/A}$ . Moreover, the distance between the LED and the PD is 1000~mm. There is a 0.05% random error in the PD, which conforms to the normal distribution. The PD output voltage in Experiment 1 is shown in Figure 5.



**Figure 5.** Simulation results of PD output voltage in Experiment 1.

Substitute the measured data in Figure 5 into Equation (15). The change in the total energy received by PD with time within the imaging time of a single gaze in Experiment 1 can be obtained as shown in Figure 6.

Photonics 2022, 9, 976 9 of 16



**Figure 6.** Simulation results of the total energy received by the PD in a single gaze time versus time in Experiment 1.

The statistical analysis of the results in Figure 6 shows that the relative uncertainty of PD stability was 0.01% when the gaze time was 8 h.

It is assumed that the spectral range of the space gaze camera flux calibration light source is the same as that of the LED light source. Set the luminous intensity to 1 cd, and the relative error limit is 0.05%, which conforms to the normal distribution. Moreover, the luminous intensity has a drift of 0.5% in the calibration process. The distance between the light source and the PD is 1000 mm. The output voltage of PD in Experiment 2 is shown in Figure 7.

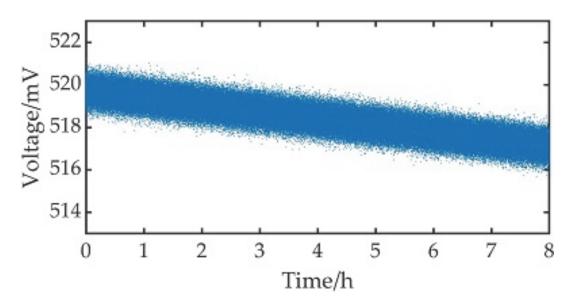


Figure 7. Simulation results of PD output voltage in Experiment 2.

Substitute the data in Figure 7 into Equation (15). The change in the total energy received by PD over time within a single gaze time in Experiment 2 can be obtained, as shown in Figure 8.

Photonics 2022, 9, 976 10 of 16

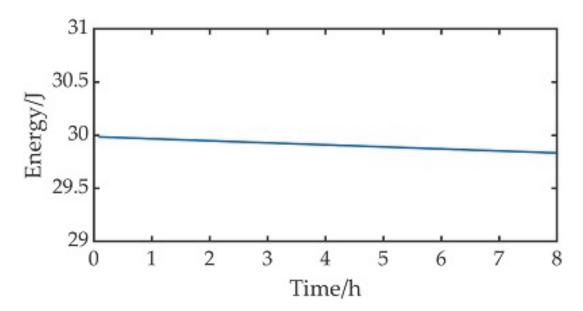


Figure 8. Simulation results of total energy received by PD over time in Experiment 2.

The statistical analysis of the data in Figure 8 can be seen in that the relative uncertainty of the calibration light source stability was 0.58% when the gaze time was 8 h.

The simulation result shows that when the gaze time is 5 min and the PD sampling frequency is 15 Hz within the 8 h flux calibration time, the stability of the calibration light source is 0.58%. The relative measurement uncertainty of this method was 0.01%. It was proved that the stability of the light source for the flux calibration of the space gaze camera using PD measurement could meet the accuracy requirement of long-time flux calibration.

# 5. Validation Experiments and Results

# 5.1. Experimental Device

The device for the real-time measurement of the calibration light source stability is shown in Figure 9 and includes the light source system and real-time monitoring system. To reduce the influence of the external environment on measurement accuracy, the experiment was carried out in a dark room. The ambient temperature was controlled to 25  $\pm$  0.5  $^{\circ}$ C.

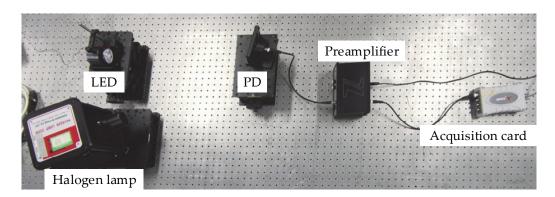


Figure 9. Device for measuring the stability of the calibration light source in real time.

In Experiment 1, a white LED was used as the light source. A heat sink was used to improve the heat dissipation efficiency of the LED and reduce the influence of temperature accumulation on the LED light source stability. In Experiment 2, a halogen lamp with a similar detection band as that of the space gaze camera was selected as the flux calibration light source.

Photonics **2022**, 9, 976 11 of 16

To reduce the impact of voltage fluctuations on the LED luminous intensity using a regulated power supply, the voltage change at the lamp terminal of the LED was monitored using a 6-1/2 digit precision multimeter to quantitatively assess the voltage fluctuation at this point.

The PD was selected from the Zolix (Beijing, China) DSi300 silicon photodetector. The structure diagram and photoelectric parameters are shown in Figure 10 and Table 1, respectively. The ZAMP-A was used for the preamplifier. The ADLINK 2405 data acquisition card was used to connect with the computer for data acquisition. This set of optoelectronic measurement equipment has the advantages of a wide detection wavelength range and low equivalent noise power. It can be used for the precision measurement of the luminous intensity of the flux-calibrated light source for space telescopes.

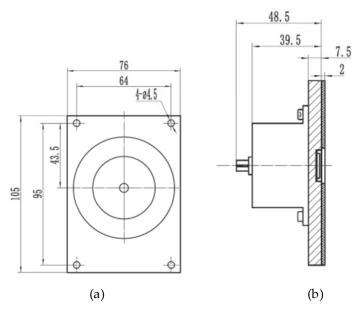


Figure 10. Structure of DSI300 silicon photodetector: (a) Main view; (b) Top view.

Table 1. Parameters of DSI300 Silicon Photodetector.

Technical Specifications	Value	
Model	DSi300	
Effective reception area (mm <sup>2</sup> )	100 (ø11.28)	
Wavelength usage range (nm)	350–1100	
Peak wavelength (nm), typical	970	
Peak wavelength responsiveness (A/W)	0.6 (>0.55)	
Typical wavelength responsiveness (A/W)	0.2 (>0.15) @410 nm	
Equivalent noise power NEP (W/ $\sqrt{\text{Hz}}$ )	$2.0 \times 10^{-13}$	

The sampling frequency in the experiment was 15 Hz. The preamplifier gain was set to  $10^4$  V/A. A neutral density filter was used to adjust the irradiance of the PD within the linear operating range.

# 5.2. Experimental Program

The PD was calibrated using LED in Experiment 1. The voltage at the lamp terminal of the LED is measured using a 6-1/2-digit precision multimeter at 1 h intervals. The number of single measurement readings was not less than three, and the mean should be taken as the single measurement result of the lamp terminal voltage. In Experiment 2, PD was used to measure the stability of the halogen lamp.

The measurement time for both experiments was 8 h. The experiments were set up with a gaze imaging of 5 min. The output voltage of PD when the luminous intensity of the

Photonics **2022**, 9, 976 12 of 16

light source was stable was selected for data processing. The relative uncertainty of the PD stability in Experiment 1 was the relative measurement uncertainty of this experiment. To ensure the accuracy of the measurement results, the stability of the calibration light source was repeatedly measured three times. The average value of the relative uncertainty was taken as the final measurement result.

## 5.3. Experimental Results and Analysis

8

9

Table 2 shows the measurement results of the terminal voltage at the LED light source in Experiment 1. The results show that the maximum relative error of the lamp terminal voltage was 0.002% when it conformed to the uniform distribution. The uncertainty introduced by the voltage fluctuation of the supply power supply  $u_3$  is:

$$u_3 = \frac{0.002\%}{\sqrt{3}} \approx 0.001\% \tag{20}$$

Number	Voltage (V)	Average (V)	Maximum Relative Deviation (%)
1	3.07245		
2	3.07238		
3	3.07238		
4	3.07237		
5	3.07232	3.07238	0.002%
6	3.07243		
7	3.07234		

**Table 2.** Voltage fluctuation of LED light source in Experiment 1.

3.07242

3.07233

Figure 11 shows the PD output voltage during the measurement time of 8 h in Experiment 1. This can be substituted into the light source stability measurement algorithm for the flux calibration of the space gaze camera. Figure 12 demonstrates the change in the total energy over time in gaze time. Statistical analysis was performed on the three-measurement data, respectively. The results of the error analysis for a single measurement are shown in Table 3.

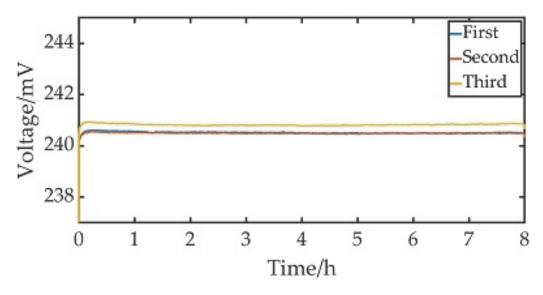


Figure 11. The output voltage of PD in Experiment 1.

Photonics 2022, 9, 976 13 of 16

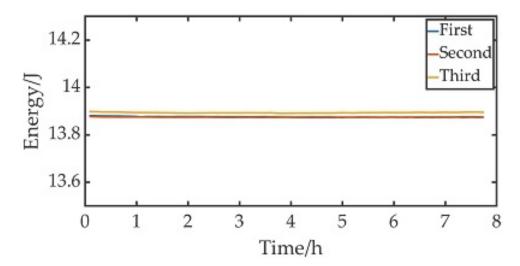


Figure 12. Variation in the total energy received with time during the PD gaze time in Experiment 1.

**Table 3.** The relative uncertainty of PD stability in Experiment 1.

Number	Estimated Value (mW)	Maximum (mW)	Minimum (mW)	Standard Deviation (mW)	Relative Uncertainty Degree (%)
1	13.8759	13.8814	13.8738	0.0017	0.012
2	13.8748	13.8777	13.8728	0.0010	0.007
3	13.8936	13.8985	13.8911	0.0016	0.012

As can be seen from the above table, the relative uncertainty of PD stability obtained by triplicate measurement was 0.012%, 0.007%, and 0.012%, respectively. The mean of 0.01% was taken as the relative uncertainty of PD stability.

The PD output voltage in Experiment 2 is shown in Figure 13. The halogen lamp light source at  $0\sim30$  min was poor in stability, so these data were omitted when analyzing the stability of the light source. The data shown in Figure 13 can be substituted into the light source stability algorithm for the flux calibration of the space gaze camera. The change in the total energy received by PD with time during a single gaze time in Experiment 2 is shown in Figure 14. The relative uncertainty of the halogen lamp stability obtained after analysis is shown in Table 4.

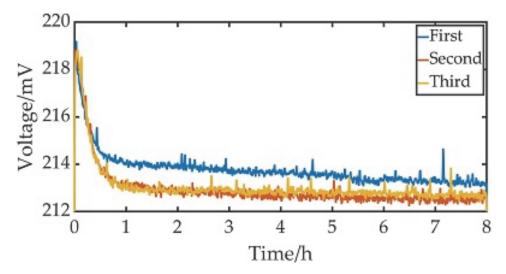


Figure 13. The output voltage of PD in Experiment 2.

Photonics **2022**, 9, 976 14 of 16

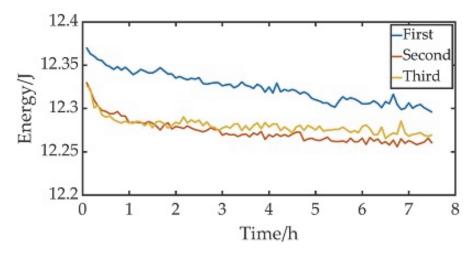


Figure 14. Variation in the total energy received with time during the PD gaze time in Experiment 2.

**Table 4.** The relative uncertainty of the stability of halogen lamp in Experiment 2.

Number	Estimated Value (mW)	Maximum (mW)	Minimum (mW)	Standard Deviation (mW)	Relative Uncertainty Degree (%)
1	12.3705	12.3705	12.2957	0.0493	0.399
2	12.3305	12.3305	12.2559	0.0589	0.478
3	12.3265	12.3265	12.2655	0.0475	0.385

From the above table, the relative uncertainty of the light source stability in the three repeated measurements was 0.399%, 0.478%, and 0.385%. The mean of 0.42% was taken as the relative measurement uncertainty of the halogen lamp light source.

#### 6. Discussion

The equidistance method has the limitation that it cannot monitor the luminous intensity in real time for a long time when measuring the stability of the light source. To improve the above issues, a method to measure the stability of the light source using PD is proposed in this manuscript. It is also combined with algorithms for light source stability in the flux calibrations of space gaze cameras. The comparison of the two methods is shown in Table 5.

**Table 5.** Comparison of light source stability measurement methods.

Parameters	<b>Equidistance Method</b>	PD Measures Light Source Stability
Measurement equipment	SL and Photometers	LED, PD, Preamplifiers, and Acquisition cards
Measurement time (h)	4	8
Real-time measurements	No	Yes
Measurement uncertainty (%)	0.09	0.01

The table shows that the PD measurement source stability improves the measurement accuracy from 0.09% to 0.01%. The measurement time was increased from a maximum of 4 h to 8 h in the validation experiment. A total of 8 h is not the limit length of the measurement. Furthermore, the PD measurement of the light source stability achieves real-time measurement of the stability of the space gaze camera flux calibration light source. It reduces the measurement uncertainty of the light source stability caused by changes in the external environment.

To reduce the impact of voltage fluctuations on the power supply of the light source stability measurement in the verification experiment, a regulated power supply is used to power the LED. The uncertainty introduced by the voltage fluctuation before using the regulated power supply was 3.33%. The uncertainty introduced by the voltage fluctuation

Photonics 2022, 9, 976 15 of 16

was changed to 0.001% after using the regulated power supply. It proves the necessity of a regulated power supply.

There are also some problems in the experimental verification of this paper, which will be improved in the future. For example:

- In this paper, a halogen lamp was selected as the light source to be measured. To
  verify the wide practicality of the method for measuring the stability of light sources
  by PD, other types of light sources, such as xenon and mercury lamps, will be selected
  for subsequent experiments.
- The time settings in the experimental validation are an estimate based on the scientific objectives of a particular model of space camera. There were differences between them and the parameter settings during the actual flux calibration.
- 3. In the experiment, the PD stability selected by many comparisons can meet the measurement accuracy of the light source stability for the space gaze camera, so the stability of the light source is not corrected. If the calibration accuracy of PD cannot meet the calibration requirements of the space gaze camera, the corresponding algorithm should be used to calibrate the PD output voltage in the experiment.

#### 7. Conclusions

The purpose of this paper is to solve the problem of measuring the stability of the space gaze camera flux calibration light source in the multi-field calibration of large-aperture and large-field space telescope flux calibration. The equidistance method cannot monitor the luminous intensity of the light source in real-time. Additionally, the long-term stability of SL cannot be guaranteed. The method of using PD to measure the stability of the calibration light source was proposed. This paper introduces the principle and algorithm of a light source stability measurement for a space gaze camera flux calibration. Moreover, the design for the simulation analysis and experimental scheme to verify the correctness of the measurement method has also been proposed. First, PD was calibrated by using an LED light source; then, this PD was used to measure the stability of a calibration light source. At this time, the main sources of measurement uncertainty in the stability of the light source are the stability uncertainty of LED and the stability uncertainty of PD. The gaze time in the validation experiment was set to 5 min, and the sampling frequency of PD was 15 Hz. When the flux calibration time was 8 h, the stability uncertainty of the calibration light source was 0.42%, and the relative measurement uncertainty was 0.01%. At this time, the uncertainty caused by power supply fluctuation was 0.001%, which had little influence on the measurement uncertainty and could be ignored. Compared to the traditional method, this enables the real-time monitoring of the luminous intensity of the light source; moreover, the measuring time is not limited by the SL. The measuring time of the light source stability was prolonged from 4 h in the traditional measuring method to 8 h or even longer. It improves the situation that the measurement accuracy cannot be guaranteed when the calibration light source runs for a long time in the traditional method. The measurement accuracy of light source stability was improved by 0.01%, which meets the requirement of the high-precision flux calibration for a large-aperture space telescope.

**Author Contributions:** Conceptualization, C.L. and X.Z.; methodology, C.L.; software, C.L.; validation, C.L., N.Z., J.Z. and T.Z.; formal analysis, C.L. and N.Z.; investigation, C.L. and T.Z.; resources, X.Z. and J.L.; data curation, C.L.; writing—original draft preparation, C.L.; writing—review and editing, C.L., N.Z., J.L. and X.Z; visualization, C.L.; supervision, X.Z.; project administration, X.Z.; funding acquisition, X.Z. All authors have read and agreed to the published version of the manuscript.

Funding: Supported by the National Natural Science Foundation of China (No. 12003033).

Data Availability Statement: Data are contained within the article.

**Acknowledgments:** The authors would like to thank the anonymous reviewers for their constructive comments.

Conflicts of Interest: The authors declare no conflict of interest.

Photonics **2022**, 9, 976 16 of 16

#### References

1. Szeto, K.; Roberts, S.; Gedig, M.; Austin, G.; Lagally, C.; Patrick, S.; Tsang, D.; MacMynowski, D.; Sirota, M.; Stepp, L.; et al. TMT Telescope Structure System: Design and Development Progress Report. In Proceedings of the Ground-Based and Airborne Telescopes II, Marseille, France, 23–28 June 2008.

- 2. Fanson, J.L.; Bernstein, R.A.; Angeli, G.Z.; Ashby, D.S.; Bigelow, B.C.; Brossus, G.P.; Bouchez, A.H.; Burgett, W.S.; Contos, A.R.; Demers, R.; et al. Overview and Status of the Giant Magellan Telescope Project. In Proceedings of the Ground-Based and Airborne Telescopes VIII, Online, 14–22 December 2020.
- 3. Gressler, W.; DeVries, J.; Hileman, E.; Neill, D.R.; Sebag, J.; Wiecha, O.; Andrew, J.; Lotz, P.; Schoening, W. LSST Telescope and Site Status. In Proceedings of the Ground-Based and Airborne Telescopes V, Montréal, QC, Canada, 22–27 June 2014.
- Lou, Z.; Liang, M.; Yao, D.; Zheng, X.; Cheng, J.; Wang, H.; Liu, W.; Qian, Y.; Zhao, H.; Yang, J. Optical Design Study of the Wide Field Survey Telescope (WFST). In Proceedings of the International Symposium on Optoelectronic Technology and Application, Beijing, China, 9–11 May 2016.
- 5. The 2.5 m Telescope of the Sloan Digital Sky Survey—IOPscience. Available online: https://iopscience.iop.org/article/10.1086/500975/meta (accessed on 19 October 2022).
- Sabelhaus, P.A.; Decker, J.E. An Overview of the James Webb Space Telescope (JWST) Project. In Proceedings of the SPIE Astronomical Telescopes and Instrumentation Symposium, Glasgow, UK, 21–25 June 2004.
- 7. Robberto, M.; Sivaramakrishnan, A.; Bacinski, J.J.; Calzetti, D.; Krist, J.E.; MacKenty, J.W.; Piquero, J.; Stiavelli, M. Performance of HST as an Infrared Telescope. In Proceedings of the 2000 SPIE-ESO Symposium on Astronomical Telescopes and Instrumentation, Munich, Germany, 27–31 March 2000.
- 8. Prusti, T.; de Bruijne, J.H.J.; Brown, A.G.A.; Vallenari, A.; Babusiaux, C.; Bailer-Jones, C.A.L.; Bastian, U.; Biermann, M.; Evans, D.W.; Eyer, L.; et al. The Gaia Mission. *Astron. Astrophys.* **2016**, *595*, A1. [CrossRef]
- 9. Sebag, J.; Gressler, W.J.; Liang, M.; Axelrod, T.; Claver, C.; Andrew, J. Calibration Systems for LSST. In Proceedings of the Ground-Based and Airborne Telescopes V, Montréal, QC, Canada, 22–27 June 2014.
- Bagnasco, G.; Ferruit, P.; Boeker, T.; Closs, M.; Dorner, B.; Gnata, X.; Koehler, J.; Kolm, M.; Kuechel, C.; Langenbach, H.; et al.
   The On-Ground Calibration of the near Infrared Spectrograph (NIRSpec) Instrument On-Board the James Webb Space Telescope (JWST). In Proceedings of the SPIE Astronomical Telescopes and Instrumentation Symposium, Marseille, France, 23–28 June 2008.
- 11. Lemieux, S.; Giese, E.; Fickler, R.; Chekhova, M.V.; Boyd, R.W. A Primary Radiation Standard Based on Quantum Nonlinear Optics. *Nat. Phys.* **2019**, *15*, 529–532. [CrossRef]
- 12. Guo, Q.; Chen, F.; Li, X.; Chen, B.; Wang, X.; Chen, G.; Wei, C. High-Accuracy Source-Independent Radiometric Calibration with Low Complexity for Infrared Photonic Sensors. *Light Sci. Appl.* **2021**, *10*, 163. [CrossRef] [PubMed]
- 13. Building a Better Flat-Field: An Instrumental Calibration Projector for the Large Synoptic Survey Telescope. Available online: https://dspace.mit.edu/handle/1721.1/65435 (accessed on 16 August 2022).
- 14. A Scheme of Flat-Fielding for LAMOST. Available online: https://www.spiedigitallibrary.org/conference-proceedings-of-spie/5493/0000/A-scheme-of-flat-fielding-for-LAMOST/10.1117/12.548014.short (accessed on 19 October 2022).
- 15. Coughlin, M.; Abbott, T.M.C.; Brannon, K.; Claver, C.; Doherty, P.; Fisher-Levine, M.; Ingraham, P.; Lupton, R.; Mondrik, N.; Stubbs, C. A Collimated Beam Projector for Precise Telescope Calibration. In Proceedings of the SPIE Astronomical Telescopes + Instrumentation, Edinburgh, UK, 26 June–1 July 2016.
- Taubert, R.D.; Monte, C.; Baltruschat, C.; Schirmacher, A.; Gutschwager, B.; Hartmann, J.; Hollandt, J.; Kochems, D.; Küchel, C.; te Plate, M. The Spectral Photon Flux of the Radiometric Calibration Spectral Source for the NIRSpec Instrument of the James Webb Space Telescope. *Metrologia* 2009, 46, S207. [CrossRef]
- 17. Regnault, N.; Guyonnet, A.; Schahmanèche, K.; Le Guillou, L.; Antilogus, P.; Astier, P.; Barrelet, E.; Betoule, M.; Bongard, S.; Cuillandre, J.-C.; et al. The DICE Calibration Project Design, Characterization, and First Results. *Astron. Astrophys.* **2015**, *581*, A45. [CrossRef]
- 18. Zhang, N.; Ye, L.; Song, Y. Design and Detection for the Photoelectric Device Used in the Point Source Transmission Testing. *Yi Qi Yi Biao Xue Bao/Chin. J. Sci. Instrum.* **2018**, *39*, 92–99. [CrossRef]
- Borecki, M.; Kruszewski, J. Laser Diode Supply for Fiber Optic Sensors. In Proceedings of the Lightguides and Their Applications, Krasnobród, Poland, 14–16 October 1999.
- 20. Bürmen, M.; Pernuš, F.; Likar, B. Smart LED Light Source Driver for Machine Vision System. In Proceedings of the Light-Emitting Diodes: Research, Manufacturing, and Applications XII, San Jose, CA, USA, 21–24 January 2008.
- 21. Narendran, N.; Gu, Y.; Freyssinier, J.P.; Yu, H.; Deng, L. Solid-State Lighting: Failure Analysis of White LEDs. *J. Cryst. Growth* **2004**, *268*, 449–456. [CrossRef]