



Article Development of Bio-Sourced Epoxies for Bio-Composites

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Abstract: In the air and ground transportation sectors, new environmental regulations and societal concerns have triggered a search for new products and processes that complement resources and the environment. To address these issues, this article reports on current R&D efforts to develop bio-sourced materials by an international joint project. Novel bio-sourced epoxies and biocomposites were developed, characterized, modified and evaluated in terms of the mechanical property levels. Quasi-structural composite parts were finally trial-manufactured and demonstrated.

Keywords: rosin acid; itaconic acid; bio-sourced epoxy; bio-composites

1. Introduction

With the present state of composite technological development, biocomposites are understood as composites that consist of biopolymer matrices, i.e., bio-sourced resins and/or natural fiber reinforcements, e.g., plant fibers (PF) [1,2]. Besides existing applications in automobiles [3], this new member of the material family may provide an economical and environmentally-friendly alternative to glass-fiber-reinforced composites for quasi-structural applications in aircraft. The present paper provides an overview on the current development of biocomposite materials by an international joint project, ECO-COMPASS (Ecological and Multifunctional Composites for Application in Aircraft Interior and Secondary Structures, 2016–2019) [4], which is co-funded by the Chinese Ministry of Industry and Information Technology (MIIT) and the European Union, but with a special emphasis on bio-sourced epoxies and biocomposites. Quasi-structural composite parts were finally trial-manufactured and demonstrated using the epoxies as matrix resins.

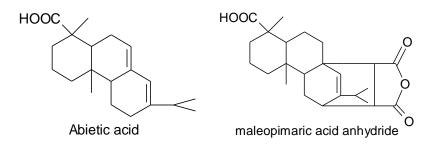
2. Rosin-Sourced Epoxy as a Matrix Resin

Rosin is an abundantly available natural product, it is nontoxic and odorless, and contains various isomerized acids (>90%) and some neutral substances [5]. Reactive double bonds and carboxyl groups of rosin acids render them suitable for the Diels–Alder reaction, esterification and condensation reaction usage. Therefore, rosin acid has received increasing attention as a bio-sourced form of renewable feedstock in polymer science.

Anhydride is one of the curing agents for epoxies (EPs). Owing to their characteristic bulky hydrogenated phenanthrene ring structure, rosin acids are analogous to many aromatic compounds in rigidity. However, their curing temperature is generally high, about 200–250 °C, and the curing time is long, which limits the use of the anhydride in some products and apparatus. The complex reactions

of epoxy/anhydride curing include the carboxyl group reaction with an epoxy ring in the catalyzed action of accelerator, alternate ring-opening copolymerization of epoxy, and anhydride catalyzed by amine and polyetherification at high temperatures, initiated by amine and catalyzed by hydroxyl groups [6]. These processes occur when an amine is added as the catalyst. An excellent reference [6] on this issue can be found in the literature.

In this study [7,8], an anhydride-type epoxy curing agent, maleopimaric (Scheme 1), was synthesized as a hardener from rosin acid (Scheme 1). This was supplied by the Ningbo Institute of Materials and Technology Engineering. A resin mixed with an E51-type epoxy and a solid phenolic epoxy was then prepared as the main component, together with an accelerator mixed of two amino imidazole salts as the thermally latent curing agent and also as the catalyst for the anhydride. The experimental details can also be find in reference [7]. Figure 1 exhibits the glass transition behavior of the formulated resin system. As shown, the curing degree increased with the curing temperature for a constant curing time of 3 h, as well as the glass transition temperature. The formulated matrix resin was finally designated as AGMP3600, with a bio-content of about 30%.



Scheme 1. Structure formula of abietic acid and maleopimaric acid anhydride.

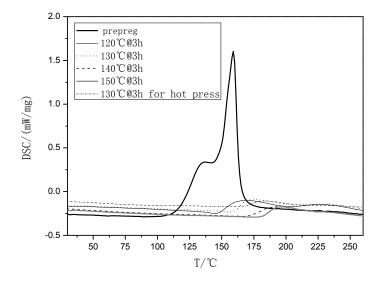


Figure 1. Differential Scanning Calorimetry (DSC) curves of the rosin-sourced epoxy resin system designated as AGMP3600 at different temperature conditions.

Figure 2 shows the typical viscosity behavior of the trial product AGMP3600. It behaved well in the film manufacturing and subsequent prepreg production. The process condition for the prepreg using AGMP3600 as the matrix in the autoclave is shown in Figure 3.

The mechanical properties of AGMP 3600 laminates reinforced with different kinds of fibers and weaves were determined and are listed in Tables 1–4 in some cases compared with the state-of-the-art counterparts as reference.

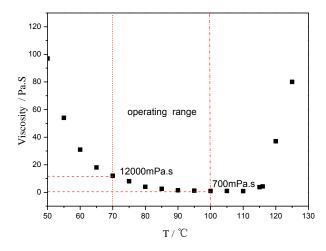


Figure 2. Viscosity vs. temperature of AGMP3600, a rosin-sourced epoxy resin system.

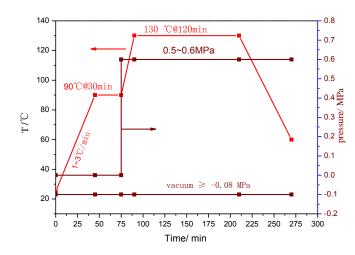


Figure 3. Process parameters for the curing of AGMP3600 prepreg in an autoclave.

Table 1. Mechanical properties of AGMP3600/EW250F (glass fabric, 8 satin, 47 vol %), a rosin-sourced epoxy laminates, and of 3233B/EW250F, a standard intermediate-temperature epoxy laminate for reference and comparison.

Properties	UNIT	3233B/EW250F	AGMP3600/EW250F
Ply thickness	mm	0.241	0.237
Bending strength	MPa	696	674
Bending modulus	GPa	19.9	21.1
Short beam shear strength	MPa	45	60.9
Tensile strength	MPa	470	540
Tensile modulus	GPa	22.5	25.3
Compression strength	MPa	474	483
Compression modulus	GPa	23.9	27

In parallel, a 180 °C/2 h cured-rosin epoxy was also developed, designated as AGMP5600, with a higher bio-content of about 40%. It is particularly interesting to note that the glass transition temperature of AGMP5600 matrix composite reinforced with EW250F glass weave was about 220 °C. Table 4 lists the mechanical properties of the laminated composite. The temperature-dependent mechanical properties were also studied, as well as those after the hot/wet exposure (1000 h/70 °C/85% r.H.)

Property and Test Condition U		Unit	Reference ¹	Test Result	Standard
Tensile strength warp	RT/dry	MPa	≥500	707	
Tensile modulus warp	RT/dry	GPa	65 ± 8	62.3	
Tensile strength weft	RT/dry	MPa	\geq 500	557	ASTM D3039
Tensile modulus weft	RT/dry	GPa	65 ± 8	60.9	
Compression strength warp	RT/dry	MPa	≥300	509	
Compression modulus Warp	RT/dry	GPa	58 ± 8	61.2	
Compression strength Weft	RT/dry	MPa	≥ 280	362	ASTM D6641
Compression modulus weft	RT/dry	GPa	57 ± 8	57.7	
Bending strength warp	RT/dry	MPa	≥650	883	
Bending modulus warp	RT/dry	GPa	58 ± 8	56.8	ASTM D790
Short bean shear strength	RT/dry	MPa	\geq 50	55.7	ASTM D2344
In plane shear strength	RT/dry	MPa	≥ 45	72.6	
In plane shear modulus	RT/dry	GPa	3.5 ± 1	3.84	ASTM D3518

Table 2. Mechanical properties of AGMP3600/CW3011 (carbon fiber plain weave, 200 g/m², 57 vol %),a rosin-epoxy laminate, and a corresponding reference laminate for comparison.

¹ A commercial product.

Table 3. Mechanical properties of AGMP3600/A38 (carbon fiber, twill fabric, 200 g/m², 42 vol %),a rosin-epoxy laminate, under a hydrothermal condition of 1000 h/70 °C/85% r.H.

Properties	Unit	Humidity	Temperature	e/°CReference ¹	AGMP3600/A3	8 Standard
ply thickness	mm		_	0.26	0.265	
			-55	_	949	
Flexural	MPa	dry	RT	_	947	
strength warp	IVII ⁻ a		70	_	903	
		70 °C/wet 85%	70	—	826	ASTMD 790-03
			-55	_	50.9	110 11112 770 00
Flexural	GPa	dry	RT	—	51.4	
modulus warp	Gra		70	—	58.7	
		70 °C/wet 85%	70	_	51.8	
Interlaminar			-55	65	62.4	
shear strength	MD	dry	RT	60	74.8	ASTMD
0	MPa		70	40	65.3	2344/D2344M-00(2006)
warp		70 °C/wet 85%	70	19	46.4	
			-55	500	618	
Tensile strength		dry	RT	625	667	
warp	MPa		70	590	714	
_		70 °C/wet 85%	70	560	674	ASTMD
			-55	52 ± 6	55.25	3039/D3039M-e1
Tensile modulus	CP	dry	RT	52 ± 6	54.6	
warp	GPa		70	52 ± 6	53	
_		70 °C/wet 85%	70	52 ± 6	49	
Poisson ratio	-	dry	RT	0.05 ± 0.005	0.052	
			-55	600	758	
Compression		dry	RT	535	651	
strength warp		2	70	430	630	
		70 °C/wet 85%	70	310	605	ASTMD
			-55	46 ± 6	52.5	6641/D6641M-14
Compression	CD	dry	RT	46 ± 6	53	
modulus warp	dulus warp GPa		70	46 ± 6	52.5	
1		70 °C/wet 85%	70	46 ± 6	55	
			-55	100	136	
In plane shear	M	MPa dry	RT	95	114	
strength	MPa		70	80	96.8	
~		70 °C/wet 85%	70	60	89	ASTMD
			-55	4.5 ± 0.35	4.74	3518/D3518M-94
In plane shear	CP	dry	RT	3.65 ± 0.35	4.21	
modulus	CPa	2	70	3.5 ± 0.35	2.63	
		70 °C/wet 85%	70	1.25 ± 0.35	2.75	

Properties	Unit	Humidity	Temperature/	°CReference ¹	AGMP3600/A3	8 Standard
CAI (lay up (+/0/-/90)2 s, energy 25 J	MPa	dry	RT	180	185	ASTMD 7136/7137
Filled hole tension strength	MPa	dry	RT	180	317	ASTMD3518
Filled hole compression strength	MPa	dry	RT	250	no destroy, displacement 4 mm	ASTMD6742

Table 3. Cont.

¹ A commercial product.

Table 4. Mechanical properties of AGMP5600/EW250F (glass fabric, 8 satin, 47 vol %), a 180 °C cure rosin-sourced epoxy laminate, under different hydrothermal conditions.

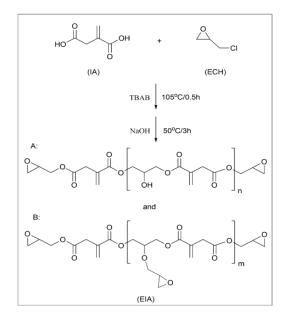
Mechanical Properties	Unit	Test Condition	Reference ¹	AGMP5600/EW250F
ply thickness	mm	—	0.26	0.265
		-55	_	864
Elevanel strongth ware	MD	RT	_	687
Flexural strength warp	MPa	70	_	650
		70 °C/wet 85%	_	431
		-55	_	21.4
Flexural modulus warp	GPa	RT	—	23.4
Hexural modulus warp	GFa	70	—	22
		70 °C/wet 85%	_	22.2
		-55	88	74.6
Interlaminar shear strength warp	MPa	RT	68	59.1
internaminal shear strength warp	MPa	70	59	49
		70 °C/wet 85%	39.6	48.3
		-55	500	573
Tensile strength warp	MPa	RT	410	510
tensne strengtit warp	MPa	70	330	460
		70 °C/wet 85%	315	—
		-55	27 ± 6	23.9
Tensile modulus warp	GPa	RT	24 ± 6	24.4
Tensne modulus warp		70	24 ± 6	22.3
		70 °C/wet 85%	24 ± 6	—
	MPa	-55	800	589
Compression strength warp		RT	660	456
Compression strength warp		70	550	397
		70 °C/wet 85%	470	384
		-55	26 ± 3	26.7
Compression modulus warp	CD	RT	25 ± 3	25.8
Compression modulus warp	GPa	70	25 ± 3	24
		70 °C/wet 85%	25 ± 3	24.7
		-55	110	113
In plane chear strongth	MD-	RT	85	90
In plane shear strength	MPa	70	88	71
		70 °C/wet 85%	77	56.4
		-55	5.7 ± 1	4.8
In plane shear modulus	CD	RT	4.8 ± 1	3.26
In plane shear modulus	GPa	70	3.9 ± 1	3.1
		70 °C/wet 85%	3.5 ± 1	3.13
	1.			

¹ A commercial product.

3. Epoxy Resins Based on Itaconic Acid

Itaconic acid, which is also referred to as methylenesuccinic acid, is typically produced through the fermentation of carbohydrates such as glucose or starch using Aspergillus terreus. Given its strong capacity to replace petrochemicals in the chemical industry, it has been selected as one of the top 12 potential bio-based platform chemicals by the U.S. Department of Energy [9]. To the best of our knowledge, it has been widely used in the production of styrene–butadiene–acrylonitrile and acrylate latex in the paper and coating sectors.

Epoxy (EP) resin derived from itaconic acid, designated in the paper as EIA, can be synthesized following the synthetic route shown in Scheme 2. To evaluate its properties, EIA and commercial DGEBA (diglycidyl ether of bisphenol A, epoxide equivalent weight of 182–192 g/eq.) were cured with methyl hexahydrophthalic anhydride (MHHPA), respectively. The results show that EIA presented higher epoxide (0.625) and higher reactivity values than DGEBA. Relative to DGEBA, the cured EIA showed comparable or higher tensile strength (87.5 MPa), elongation at break (7.1%), flexural strength (152.4 MPa) and modulus (3430.8 MPa), and glass transition temperature (Tg = 130 °C). In addition, after co-monomers such as divinyl benzene (DVB) and acrylated epoxidized soybean oil (AESO) were introduced into the EIA/MHHPA system, dual-curing systems were formed, and the rigidity and toughness could be manipulated further via the various contents of rigid DVB or soft AESO, as shown in Figure 4, compared with data from reference published [10].



Scheme 2. Synthetic route and chemical structures of itaconic-acid-based epoxy resin (EIA).

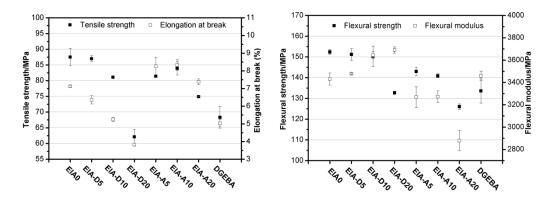
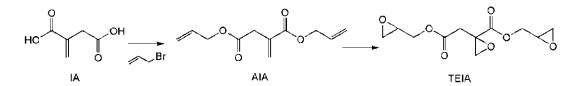


Figure 4. Mechanical properties of the cured EP resins. EIA0 and DGEBA refer to the cured samples without comonomers; D and A denote the DVB (divinyl benzene) and AESO (acrylated epoxidized soybean oil) co-monomers, respectively.

As shown in Scheme 3, direct reactions between itaconic acid and epichlorohydrin generate resin EIA, which is a mixture of different oligomers of varying molecular weights. To make the best use of the

carboxyl groups and itaconic acid double bond, a trifunctional EP monomer (TEIA) was designed and synthesized (Figure 4), and it generated an extremely high epoxide value of 1.16 and a low viscosity of 0.92 Pa s at 25 °C. It is well known that low resin viscosities are beneficial for manufacturing. The lower viscosities in TEIA render it easier to process than DGEBA. In Table 5, the flexural properties of TEIA cured by different curing agents are listed. When flexible poly(propylene glycol) bis(2-aminopropyl ether) (D230) is used as the curing agent, the TEIA/D230 system shows higher flexural modulus, higher strain at break and comparable flexural strength to DGEBA/D230. When rigid MHHPA was employed as the curing agent, the flexural strength, modulus and elongation at break of the TEIA/MHHPA system exceeded those of the DGEBA/MHHPA system. These results denote that TEIA may be used as a high-performance epoxy resin [11].

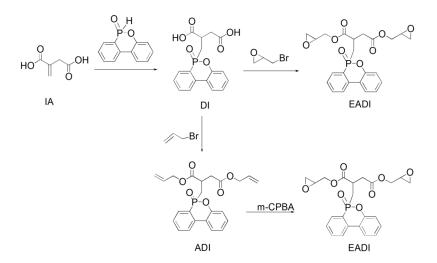


Scheme 3. Synthesis of the trifunctional epoxy resin of itaconic acid (TEIA).

Samples	Flexural Strength (MPa)	Flexural Modulus (MPa)	Elongation at Break (%)
DGEBA/D230	121 ± 1	2952 ± 18	13 ± 2
TEIA/D230	117 ± 2	3603 ± 77	21 ± 1

Table 5. Flexural properties of cured EP resins with D230 curing agents.

Given the presence of double bonds in itaconic acid and the low flame retardancy of EP resins, a flame-resistant DOPO (6H-dibenz(C,E)(1,2)oxaphosphorin-6-oxide) was chemically incorporated into the itaconic-acid-based EP resin, and a phosphorus-containing EP resin (EADI) was obtained (Scheme 4). The property study showed that the cured EADI network presents a comparable glass transition temperature and mechanical properties to those of the DGEBA system. In addition, excellent flame retardancy capacities with the UL94 V-0 grade used during vertical burning tests were observed for the EADI system. EADI may be used as a bio-based candidate for EP flame retardancy [12].



Scheme 4. Synthetic route of phosphorus-containing itaconic-acid-based epoxy resin.

4. Trial Manufacturing and Demonstration

With the promising properties, as one of the project targets, biocomposites were trial-manufactured to produce interior and quasi-structural parts for potential application in airplane and ground transportation vehicles. Figure 5 is an illustration of an interior side panel made of AGMP3600, the rosin-sourced EP, with a honeycomb sandwich core for a MA600 airplane. The side panel was manufactured using AGMP3600 prepregs in an autoclave. The composite panels are strong, lightweight, fire resistant, decorative, and impervious to mold and insects. Structure–decoration integration methods can clearly support to the production of identical or even more complex composite parts while simultaneously presenting mechanical and structural damping advantages in various applications.



Figure 5. MA600 airplane and the composite side panel made of AGMP3600/honeycomb sandwich composites (Photos courtesy of Fangbo Ding, AVIC XAC, Commercial Aircraft Co., Ltd.).

Figure 6 shows an electric race car in cooperation with Tsinghua University, China. In this case, the rosin-sourced epoxy composite was used to produce the carbon composite body with a honeycomb core. The process also used AGMP3600 prepreg. The strong conforming capacities of the materials along the curved contour were well-demonstrated. A manufacturing benefit of the biocomposites cured in an autoclave pertains to their full compatibility with the standard industrial production processes.



Figure 6. Electric race car, its body was manufactured using AGMP3600/honeycomb sandwich composites.

5. Conclusions

1. Rosin-sourced anhydride was developed and used as a hardener for epoxy to formulate a matrix resin with an imidazole-type latent catalyst for biocomposites. The mechanical properties of the biocomposites with the rosin-epoxy as matrix resins were tested, also under hydrothermal conditions. It was shown that the mechanical properties were generally comparable to the state-of-the-art, petroleum-sourced counterpart materials, but yielded a higher glass transition temperature.

- 2. Epoxy resin derived from itaconic acid was also synthesized. It showed comparable or higher mechanical properties and glass transition temperatures compared to a common counterpart. A phosphorus-containing epoxy was also developed by incorporating DOPO into the itaconic acid EP to formulate a flame-retardant resin system.
- 3. Using the rosin epoxy system, which is technologically more mature than the itaconic system, quasi-structural plant fiber reinforced components were manufactured and demonstrated for aircraft and ground transportation vehicles. The process condition was found to be fully compatible with standard industrial processes.

Author Contributions: X.Y. conceived and guided the project and study; X.Z. performed the formulation of the resins; F.D. and J.T. were responsible for the manufacturing of the structural parts.

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Conflicts of Interest: The authors declare no conflict of interest.

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