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Possibilities of Increasing the Low Altitude Measurement Precision of Airborne Radio Altimeters

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Abstract: The paper focuses on the new trend of increasing the accuracy of low altitudes measurement by frequency-modulated continuous-wave (FMCW) radio altimeters. The method of increasing the altitude measurement accuracy has been realized in a form of a frequency deviation increase with the help of the carrier frequency increase. In this way, the height measurement precision has been established at the value of ± 0.75 m. Modern digital processing of a differential frequency cannot increase the accuracy limitation considerably. It can be seen that further increase of the height measurement precision is possible through the method of innovatory processing of so-called height pulses. This paper thoroughly analyzes the laws of height pulse shaping from the differential frequency presented by the number that represents the information about the measured altitude for this purpose. This paper presents the results of the laboratory experimental altitude measurement with the use of a so-called double-channel method. The application of obtained results could contribute to the increase of air traffic safety, mainly in the phase of the aircraft approaching for landing and landing itself.

Keywords: airborne radio altimeter; methodological error; increase of measurement accuracy; height pulses; dual-channel method

1. Introduction

High precision of a flight height measurement is required at low altitude, mainly in the phase of aircraft approaching for landing and landing. For this purpose, an FMCW airborne radio altimeter (radar altimeter) is used for measuring the low altitudes [1]. When the flight height is measured, the principle of radiolocation with the evaluation of the time delay τ between the transmitted and received signal of a radio altimeter is used [2,3].

It can be presented that the flight altitude H directly corresponds to the delay of a received signal. The time delay is not evaluated directly for radio altimeters, but it is performed indirectly through the differential frequency F_d . The differential frequency is created between the immediate value of the

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frequency of the transmitted and time-delayed received signal. The dependence is linear and it can be presented that the flight altitude indirectly corresponds also to the differential frequency.

In this way, the complex measurement of the very short times when measuring the small heights is transformed into a simple measurement of the differential frequency. The relation between the measured altitude and the differential frequency is defined by a so-called "basic formula of radio altimeter"

$$F_d = \frac{8\Delta f F_M}{c} H,\tag{1}$$

where Δf is the frequency deviation, F_M is the modulation frequency c is the speed of light.

For a classical altitude measurement method, the measurement accuracy is defined by the value of so-called critical altitude ΔH of a radio altimeter. The critical altitude presents a minimal altitude range which can be registered by a radio altimeter and displayed for a pilot. The critical altitude is also connected with the radio altimeter measurement accuracy $\pm \Delta H$. It is possible to derive mathematically that the critical altitude depends on the frequency deviation of a transmitted high-frequency signal according to the following formula [3].

$$\Delta H = \frac{c}{8\Delta f}.\tag{2}$$

The dependence can also be presented graphically [4,5] (Figure 1).

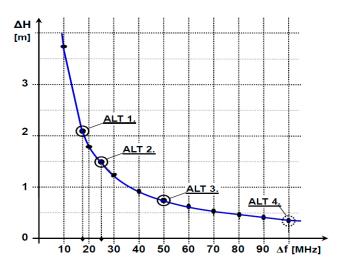


Figure 1. Dependence of the critical altitude ΔH on the frequency deviation Δf .

From Figure 1 we can see that at the low frequency deviation of 10–20 MHz the critical altitude of 4–2 m takes place. This value is relatively significant. Therefore the oldest radio altimeters (ALT 1 in Figure 1) provided the measurement accuracy of about ± 2.2 m only. The medium frequency deviation of 20–40 MHz provides a relatively lower critical altitude of 2–1 m. Some older types of radio altimeters, used until recently (ALT 2), provided the accuracy of about ± 1.5 m. Recent radio altimeters use the rather high frequency deviation of about 50 MHz at which the critical altitude is about 0.75 m that is rather low. Therefore, the recent types of radio altimeters (ALT 3) provide the measurement accuracy of about ± 0.75 m [6,7].

From a historical viewpoint, the accuracy is increased for approximately fifty percent at each stage of radio altimeters development. Going the same way, to decrease the critical altitude of the ALT 3 stage in twice to 0.375 m the frequency deviation of 100 MHz is required to reach a new stage (ALT 4) for the measurement accuracy of about ± 0.375 m. From this viewpoint, the paper offers a more simple solution on how to obtain the precision of the ALT 4 stage maintaining the recently used value of frequency deviation of 50 MHz [8,9].

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2. Materials and Methods

Critical altitude is presented by minimal altitude difference which the radio altimeter can recognize. As the measurement accuracy depends on the value of the critical altitude, it should be considered in more detail.

One stable height pulse N permanently develops (at increase) or terminates (at decrease) in the range of measurement of the critical altitude. A total number of permanent height pulses N carries the information about the measured altitude. It can be understood so that if we divide the total measured altitude H into the critical altitude sections; their number will correspond to the measured altitude as $N = H/\Delta H$. The presented number of pulses N develops (or terminates) within one modulation period T_M and modulation frequency F_M . The resulting evaluated differential frequency F_d is proportional to measured altitude and given by the multiplication of the number of pulses and modulation frequency $F_d = N \times F_M$. A discrete (step-like) change of the number of permanent height pulses is shown in Figure 2 by a thick line. Five changes of the number of permanent height pulses are shown within the presented altitude range in Figure 2.

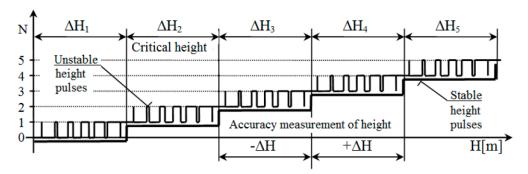


Figure 2. Relation between the critical altitude and measurement accuracy.

It is possible to derive a harmonic course of a differential low-frequency signal [1] from mathematical analysis of mutual ratios, two high-frequency frequency-modulated signals, transmitted and time-delayed received signal of a radio altimeter.

From the viewpoint of a radio altimeter operation principle, the harmonic differential signal, which carried the information about measured height in processing circuits, changes into an orthogonal discreet differential signal. Height pulses, which are the object of this paper's analysis, are shaped by this discreet differential signal. Height pulses are shaped—alternatively creating and ceasing, from the orthogonal differential signal, each time the time course of the differential signal passes a zero point. The number of height pulses k remains constant at the constant height. Their number increases with increasing height, and alternatively, their number decreases with decreasing a height. The increase of a measured height is considered. From the mathematical analysis [1], the height of the creation pulses H_v and the height of the cessation pulses H_z can be derived

$$H_v = \frac{\lambda_0}{8} \frac{2k-1}{1+\xi}, \ H_z = \frac{\lambda_0}{8} \frac{2k-1}{1-\xi},$$
 (3)

where λ_0 is the carrier wavelength, ξ is the relative value of the frequency deviation, $\xi = \Delta f/f_0$.

A height range of the duration of relevant height pulse *S* is determined as the difference between the height the cessation and creation pulses

$$S = H_z - H_v = \frac{\lambda_0}{4} (2k - 1) \frac{\xi}{1 + \xi^2}.$$
 (4)

From Equation (4) it can be seen that the height range increases with increasing the number of height pulses.

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A height range of the creation of different pulses *F* is defined as the difference of heights between two consecutive creating pulses

$$F = H_{v2} - H_{v1} = \frac{\lambda_0}{8} \frac{2(k+1) - 1}{1+\xi} - \frac{\lambda_0}{8} \frac{2k - 1}{1+\xi} = \frac{\lambda_0}{4(1+\xi)},\tag{5}$$

where H_{v1} is the height of the creation of the first pulse, H_{v2} is the height of creation of the second pulse.

A height range of the cessation of different pulses *E* is defined as the difference of heights between two consecutive ceasing pulses

$$E = H_{z2} - H_{z1} = \frac{\lambda_0}{8} \frac{2(k+1) - 1}{1 - \xi} - \frac{\lambda_0}{8} \frac{2k - 1}{1 - \xi} = \frac{\lambda_0}{4(1 - \xi)},$$
 (6)

By defining the relations for the height of the creation and cessation of pulses, it is possible to display the shaping of different height pulses in the general height range H (Figure 3). In the height range $1\Delta H$, it can be seen that with increasing the height of one unstable pulse, the height range of duration continually grows, permanently creates and ceases.

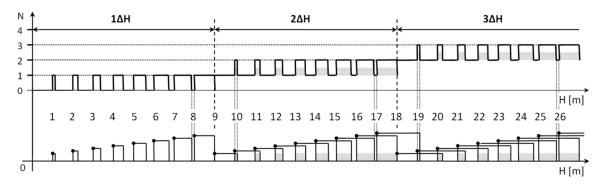


Figure 3. A flow chart of the formation of permanent and non-permanent pulses.

It can also be observed from Figure 3 that the height sections of creating pulses have a constant value similarly to the height pulses of cessation of the height pulses. The height interval of the creation of pulses is smaller than the height interval of the cessation of pulses. The difference produces the parameter $\pm \xi$.

The result of this fact is that from a certain height the pulses start to mutually overlap. At the height where the pulses start to overlap, one permanent pulse is created in the height range $2\Delta H$. But at the same time, with further height growth, one (number two in the row) unstable pulse is created. After crossing the height range $2\Delta H$, the situation repeats in the range $3\Delta H$. The only difference is that there are two permanent pulses and one (number three in the row) unstable pulse in the range $3\Delta H$.

In order to be able to portray two overlapping pulses in a more simple way, the height pulses in the bottom part of the figure have a different amplitude. (The size of the portrayed amplitude is not connected with the amplitude of the actual height impulse, which is constant.)

At a fluent change of measured altitude within the range of critical altitude, the creation of the permanent height pulses is accompanied by the development and termination of unstable height pulse N_V (within all ranges of the critical altitude). The unstable height pulse does not carry the measured altitude but vice versa causes inaccuracy in the altitude measurement. Discreet change of the number of unstable height pulses is presented by a thin line in Figure 2. There are seven changes of the unstable height pulses in the range of critical altitude in the presented altitude range. This phenomenon is based on a physical principle used in the airborne FMCW radio altimeters [2,10].

Based on a thorough mathematical analysis of the creation of permanent and unstable height pulses [2], it is possible to suggest and realize a new method for increasing the altitude measurement accuracy. This method is a so-called double-channel radio altimeter which uses an appropriate Electronics **2018**, 7, 191 5 of 9

procedure of assembling two differential signals mutually phase-shifted and created by the same radio altimeter. In this way, more frequent change of two unstable pulses into one permanent height pulse can be secured. As a result, the original value of the radio altimeter critical altitude decreases in twice. The basics of the double-channel method are based on the theory of the creation of critical altitude, as a result of the alternating creation and termination of unstable height pulses.

The presented law of the unstable pulses creation in a low altitude range can be used in the design and realization of a double-channel radio altimeter, when the methodological error of the altitude measurement decreases in twice (Figure 4) [11].

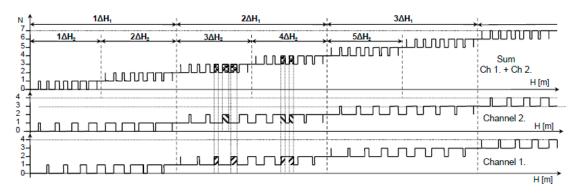


Figure 4. Height pulses creation in a double-channel radio altimeter.

The double-channel radio altimeter has two equal and parallel working channels of processing the differential signal from which one has an artificially time delay of processing signal by the value of $\lambda_0/4$. Both channels must be technically designed in a way that the same signal on the input shapes the same height pulses on the output. A time delay of the processed signal by value $\lambda_0/8$ in the second channel causes a mutual shift of the creation of those two unstable height pulses. Alternation of the creation and termination of unstable pulses within both channels mutually fit within. When the height within the range of critical altitude ΔH_1 grows, both pulses within the range of the first half of $\Delta H_1/2$ fit within each other and within the range of the second half of $\Delta H_1/2$, they start to mutually overlap. This is the result of increasing the height interval of lasting of the unstable pulse. In this way, the original critical altitude ΔH_1 divides into two halves $\Delta H_1/2$. The original value of ΔH_1 divided into two halves actually present two new values of critical altitude ΔH_2 in a double-channel radio altimeter. The height pulses creation in a double-channel radio altimeter and the logic of the decrease of its methodological error are illustrated in Figure 4.

3. Results and Discussion

Experimental double-channel radio altimeter has been constructed in a laboratory with the use of two classical one-channel radio altimeters operating at the carrier frequency f_0 = 444 MHz with the frequency deviation Δf = 17 MHz. For the purpose of experimental measurement, those radio altimeters have been disassembled mechanically and re-configured. A block diagram of those two radio altimeters connection into one double-channel radio altimeter is shown in Figure 5. The first altimeter (1st channel) worked as a complete construction in the original connection. The second altimeter (2nd channel) was adjusted so that to use only the circuit of a high-frequency converter, the circuit of a low-frequency amplifier, and the circuit of shaping the height pulses of differential frequency.

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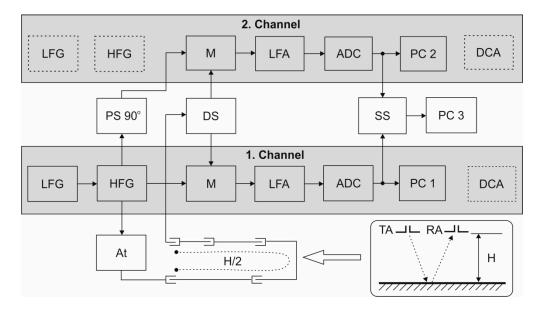


Figure 5. Laboratory double-channel radio altimeter block diagram created from two one-channel radio altimeters: LFG is the low-frequency generator, HFG is the high-frequency generator, PS 90° is the 90-degree phase shifter, At is the attenuator, M is the mixer, DS is the signal divider, LFA is the low-frequency amplifier, ADC is the analog-to-digital converter, SS is the signal summator, PC is the pulse counter, DCA is the direct current amplifier, TA is the transmitting antenna, RA is the receiving antenna, H is the altitude, are the original blocks of a one-channel radio altimeter not used in the laboratory double-channel radio altimeter.

Both channels have the common transmitter and high frequency (HF) outputs, one for transmitting and the other for receiving antennas. To create a double-channel radio altimeter, other blocks have been made, such as the high-frequency signal attenuator of the transmitter, the delay line into the second channel, the high-frequency attenuator of a received signal as well as the merger of an output low-frequency differential signal [12].

A real altitude measurement has not been performed between the transmitting and receiving antennas. That HF line has been replaced by a coaxial line, the input of which has been connected instead of the transmitting antenna, and the output instead of the receiving antenna. The attenuator, which imitated a signal attenuation in realistic conditions, has been connected into a HF route. The change of measured altitude during the laboratory measurements has been realized up to the basic altitude of 7.54 m by adding the coaxial sections of 0.5 m length. Six sections of coaxial lines with the following length have been realized: 0.5 m, 1 m, 2 m, 4 m, 8 m, and 16 m. By their mutual connection, it was possible to create an additional measuring route of 31.5 m length with a 0.5 m step.

Considering the shortening coefficient of 0.8 for the line, and the fact that the line replaces the route of the signal to the ground and back, the 25.2 m coaxial line imitated measured altitude of 12.6 m with a 0.2 m step. The measuring results with the double-channel radio altimeter are shown in Figure 6.

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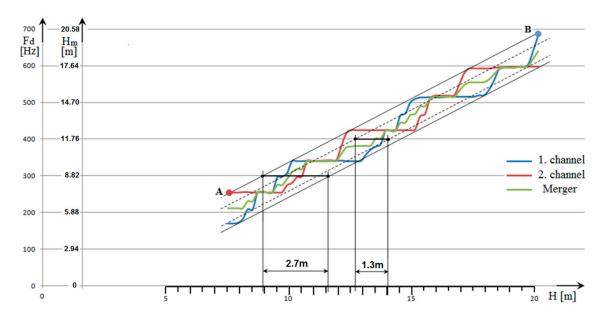


Figure 6. Measuring results.

From the viewpoint of the laboratory experiments, the evaluation of the measured altitude through the differential frequency is more precise and objective than using a pointer height indicator. The altitude evaluation could be done by recording the value of the differential frequency on three readers: the 1st channel, 2nd channel, and common channel. The differential frequency value of the common channel was divided by two after reading. The measured altitude $H_m = F_d/34$ could be evaluated through the constant of radio altimeter (K = 34) by dividing the measured value of the differential frequency [13].

Figure 6 presents three curves of measured values of the differential frequency: the 1st channel (blue curve), the 2nd channel (red curve), and the common channel (green curve). The differential frequency value corresponds with the altitude so that the number of height pulses shaped during the time of the modulation period is multiplied by the modulation frequency. A discrete increase of the number of pulses by one pulse within one modulation period means a discreet increase of the differential frequency by the value of modulation frequency. In this way, the differential frequency increase has a discreet course which can be observed in the presented graphs. The step-like course of measured altitude is created.

Two straight lines can be constructed on the presented "steps" of each graph: one, which connects tops—"tips" of minimal values of altitude on a constant level of the differential frequency (upper straight line A–B); another one, which connects the tops—"heels" of maximum values of altitude on a constant level of the differential frequency (unmarked bottom straight line). Those two leaning straight lines are connected by a horizontal line on a constant value of the differential frequency of 300 Hz.

The plan of horizontal line cross point with both full straight lines into the horizontal altitude axis expresses the critical altitude ΔH_1 measured by a classical single-channel radio altimeter. In case of the critical altitude of one of the channels of a double-channel radio altimeter, the value $\Delta H_1 = 2.7$ m has been measured. A theoretical value of the critical altitude of the experimental radio altimeters is 2.2 m. From the presented results, it can be seen that due to construction changes and interconnections of the original radio altimeters, their critical altitude ΔH_1 has increased from 2.2 m to 2.7 m [14,15].

Created "steps" of the first and second channel height pulses (blue and red curves) are mutually shifted so that it is possible to create a sum of height pulses of both channels. The created sum of pulses of the differential frequencies of both channels has a double value and their graphic curve could get out of the area of single-channel dependences. Therefore, each following sum value of the differential

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frequencies pulses of both channels is divided by two. It is shown by the green curve of the height dependence between both channels courses.

This course also has a step-like character of the graph on which two similar, but chain-dotted straight lines have been constructed. At a constant value of the differential frequency of 400 Hz, there are also two inclined chain-dotted straight lines connected by a horizontal line. The plan of the cross points of this horizontal line with both chain-dotted straight lines into the horizontal altitude axis expresses the measured critical altitude ΔH_2 of the double-channel radio altimeter. In case of the methodological error of a double-channel radio altimeter, a critical altitude of 1.3 m has been evaluated.

The value of the critical altitude ΔH_1 of each original single-channel radio altimeters was 2.7 m. So, the "new" double-channel radio altimeter should have the critical altitude of 1.35 m. However, a better value of 1.3 m has been obtained during the experiment.

4. Conclusions

The paper has presented a new possibility of increasing the measurement accuracy of small altitudes by airborne radio altimeters. The new trend of the increase of the altitude measurement accuracy is based on creating the conditions for a more frequent change of the unstable pulses into permanent pulses.

The results of the experimental measurements presented in the paper have proved the feasibility of the new approach to increase the altitude measuring accuracy. Application of the new method allowed to increase the altitude measuring accuracy in twice. In case of the application of this new method into recent types of radio altimeters, the accuracy of which is about ± 0.75 m, the accuracy of ± 0.325 m could be obtained. This solution makes it possible to increase the accuracy without having to increase the frequency deviation and to change the carrier frequency.

This method can also be applied to a so-called four-channel radio altimeter, by which it could be possible to obtain the methodological error lower than ± 0.2 m that is very interesting too for the further research and practical implementation.

The application of obtained results could contribute to the increase of air traffic safety, mainly in the phase of the aircraft approaching for landing and landing on land as well on water [16,17].

Author Contributions: J.L. proposed the concept, methodology and wrote the manuscript; J.L., M.K., P.K., and M.Č. performed experimental design and conducted experiments; A.N. and M.G. contributed to the algorithm, interpretation and validation of results and editing the manuscript.

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References

- 1. Nebylov, A.V. *Aerospace Sensors*; Momentum Press: New York, NY, USA, 2013; p. 348, ISBN 1-60650-059-7. [CrossRef]
- 2. Labun, J.; Adamčík, F.; Pil'a, J.; Madarász, L. Effect of the measured pulses count on the methodical error of the air radio altimeter. *Acta Polytech. Hung.* **2010**, *7*, 41–49.
- 3. Soták, M.; Labun, J. The new approach of evaluating differential signal of airborne FMCW radar-altimeter. *Aerosp. Sci. Technol.* **2012**, *17*, 1–6. [CrossRef]
- 4. Taylor, J. Aircraft Operation of Radio Altimeters. In Proceedings of the 24th Meeting of Working Group F, Aeronautical Communications Panel (ACP), Paris, France, 17–21 March 2011.
- 5. Alivizatos, E.G.; Petsios, M.N.; Uzunoglu, N.K. Architecture of a multistatic FMCW direction-finding radar. *Aerosp. Sci. Technol.* **2008**, 12, 169–176. [CrossRef]
- 6. Stove, A.G. Linear FMCW radar techniques. IEE Proc. F (Radar Signal Process.) 1992, 139, 343–350. [CrossRef]

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7. Skolnik, M.I. *Introduction to Radar Systems*, 2nd ed.; McGraw Hill Book Company: New York, NY, USA, 1981; p. 581, ISBN 0-07-057909-1.

- 8. Baskakov, A.I.; Komarov, A.A.; Mikhailov, M.S.; Ruban, A.V. Modeling of the methodical errors of high-precision aircraft radar altimeter operating above the seasurface at low altitudes. In Proceedings of the 2017 Progress In Electromagnetics Research Symposium—Spring (PIERS), St. Petersburg, Russia, 22–25 May 2017; pp. 3236–3240. [CrossRef]
- 9. Singh, R.; Peterson, R.; Riaz, A.; Hood, C.; Bacchus, R.; Roberson, D. A method for evaluating coexistence of LTE and radar altimeters in the 4.2–4.4 GHz band. In Proceedings of the 2017 Wireless Telecommunications Symposium (WTS), Chicago, IL, USA, 26–28 April 2017; pp. 1–9.
- 10. Labun, J.; Soták, M.; Kurdel, P. Technical note innovative technique of using the radar altimeter for prediction of terrain collision threats. *J. Am. Helicopter Soc.* **2012**, *57*, 85–87. [CrossRef]
- 11. Liu, J.; Shen, C.; Wu, S.; Huang, W.; Li, C.; Zhu, Y.; Wang, L. Correction method of the manned spacecraft low altitude ranging based on γ ray. *Aerosp. Sci. Technol.* **2016**, *50*, 71–76. [CrossRef]
- 12. Grega, M.; Labun, J. Aircraft Radar Altimeter with Frequency Modulation Design. Patent 262626; Prague, Czechoslovak Republic, 16 August 1988.
- 13. Fasano, G.; Accardo, D.; Tirri, A.E.; Moccia, A.; Lellis, E. Radar/electro-optical data fusion for non-cooperative UAS sense and avoid. *Aerosp. Sci. Technol.* **2015**, *46*, 436–450. [CrossRef]
- 14. Metzger, J.; Meister, O.; Trommer, G.F.; Tumbrägel, F.; Taddiken, B. Adaptations of a comparison technique for terrain navigation. *Aerosp. Sci. Technol.* **2005**, *9*, 553–560. [CrossRef]
- 15. Estrada, J.; Zurek, P.; Popović, Z. Harvesting of aircraft radar altimeter side lobes for low-power sensors. In Proceedings of the 2018 International Applied Computational Electromagnetics Society Symposium (ACES), Denver, CO, USA, 24–29 March 2018; pp. 1–2.
- 16. Kayton, M.; Fried, W.R. *Avionics Navigation Systems*; John Wieley & Sons: New York, NY, USA, 1997; p. 773, ISBN 0-471-54795-6.
- 17. Nekrasov, A. Foundations for Innovative Application of Airborne Radars: Measuring the Water Surface Backscattering Signature and Wind; Springer: Dordrecht, The Netherlands, 2014; p. 116, ISBN 978-3-319-00620-8. [CrossRef]



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