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Technical Note

Density Profile Analysis of Laminated Beech Veneer Lumber (BauBuche)

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Abstract: An irreversible swelling was detected in laminated beech veneer lumber within the initial moistening. Supported by the facts that the lay-up of the glued veneers is exposed to high pressure during hot pressing, and that the density of the finished material exceeds that of solid beech, it was hypothesised that the wood substance is compressed. Laboratory X-ray density profile scans were performed to check this and to identify the part of the material cross section in which the densification has taken place. The higher density was found to be located in the area of the adhesive joints, uniformly over the cross section, while the density in the middle of the veneers corresponds to that of solid beech wood.

Keywords: BauBuche; engineered wood; laminated veneer lumber; LVL; X-ray densitometry



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1. Introduction

Within an investigation on the specific dimensional change behaviour of laminated beech veneer lumber (LVLB) in terms of moisture absorption and desorption, an irreversible swelling in radial anatomical wood direction was detected within the first moistening [1]. A possible explanation is a densification of the veneers, which in turn can be explained by the pressure applied to the lay-up of the glued veneers in the hot press. The hot pressing of the phenol-formaldehyde adhesive glued, rotary cut beech veneers to 40 mm thick boards is the first step of forming the LVLB material, namely the product BauBuche Beam GL 75 from Pollmeier Massivholz GmbH & Co. KG, Creuzburg, Germany. In a second step, the 40 mm thick LVLB boards are cut into strips, which are then glued together under lower pressure and temperature using a phenol-resorcinol-based adhesive to form beams. An assumed production-based compression of the wood is supported by the fact that the density of LVLB, which nominally amounts to 800 kg m⁻³ [2], is above the density of solid beech, which averages 720 kg m⁻³ [3]. There are several investigations on the physical and mechanical properties of LVL, which refer to LVL made of different wood species such as beech [4–8], poplar [6,9–11], eucalyptus [5], oak [8], maple and aspen [9]. There is no direct comparability between these studies, as the properties of LVL vary greatly with the type of wood and the adhesive used [5]. In most of the studies listed, the density is determined gravimetrically for the entire sample. In the present study, radiometric density scans were created to check the hypothesis of the wood densification as the reason for the initial irreversible swelling, and further to localize where, in the material's cross section, the assumed compression takes place. Additionally, the density distribution of LVLB across its cross section (density profile) was determined. This research should answer whether the veneers have been compacted completely or only partially and if the steps of material forming (hot pressing, cold gluing of board strips) are reflected by the density profile.

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2. Materials and Methods

Four test specimens of factory-fresh LVLB (*Beam BauBuche GL* 75) were investigated using a *DENSE-LAB X* (Electronic Wood Systems GmbH, Hameln, Germany) laboratory density profile measuring device. The test specimens had dimensions of $(50 \times 25 \times 160)$ mm (length \times width \times height), and the wood moisture content was (5.7 ± 0.1) % (DIN EN 13183-1:2002-07 [12], oven dry method). Figure 1 shows the schematic representation of a test specimen. The test specimen length corresponds to the longitudinal anatomical wood direction, the test specimen width to the tangential and the height to the radial wood direction. The radiography of the test specimens was carried out in the width direction, which means an examination of tangential direction looking at the adhesive joints.

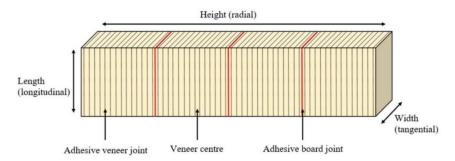


Figure 1. Schematic representation of an LVLB test specimen. Red lines highlight the adhesive joints between the individual laminated veneer boards at 40, 80 and 120 mm.

The measuring speed of the Dense Lab X was set to 0.36 mm s⁻¹, so that a density measurement in width was taken at every 0.044 mm of the specimen's height. In addition to density profiles based on all measured values, all test specimens were measured for height and the positions of the adhesive joints noted. The positions of the veneer centres were calculated based on these measurements. Nine measured values each from the veneer centre areas and three measured values each from the adhesive joint areas were averaged from the raw data set to distinguish the density values for these material zones.

3. Results and Discussion

The densities of all examined specimens were in a similar range and over all measured values averaged (793 \pm 128) kg m⁻³, which is in the range of manufacturer's data that amounts to 800 kg m⁻³ [2]. Table 1 shows the average densities for areas of the adhesive joints and the veneer centres. More detailed information is to be found in the attached file (Supplementary Material).

Table 1. Average densities for areas of the adhesive joints and the vene	eer centres.
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	Density (kg m ⁻³)	
Specimen	Adhesive Joint Area	Veneer Centre Area
1	1192 ± 90	726 ± 67
2	1089 ± 105	737 ± 69
3	1092 ± 102	739 ± 71
4	1118 ± 93	740 ± 61

Mean value \pm standard deviation.

The density of the veneer centre areas is thus within the range of literature data for solid beech, which amounts to $540 \dots 720 \dots 910 \text{ kg m}^{-3}$ (density at 15% moisture content) [3]. Since the results for the different test specimens do not show obvious differences, Figure 2 shows an exemplary density profile based on all measured values of Specimen 1.

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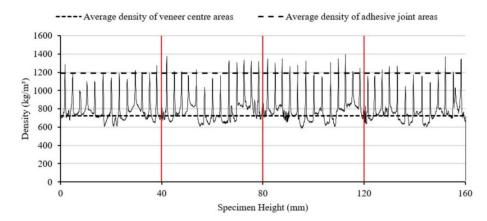


Figure 2. Density profile of a laminated beech veneer lumber test specimen (Specimen 1) based on all values measured. Dotted horizontal lines represent average density values for areas of the adhesive joints and veneer centres. Red vertical lines highlight the adhesive joints between the individual laminated veneer boards at 40, 80 and 120 mm.

Due to the alternating arrangement of veneers and adhesive joints, the density varies strongly over the height of the test specimen. The assumed compression of the wood substance cannot be seen from the density profile shown (Figure 2). The fact that the density of the veneer centre areas is within the range of literature data for solid beech leads to the assumption that the higher density of LVLB compared to solid beech is mainly due to the density of the adhesive used and not only to a compression of the veneers in the production process. Hellerich et al. (1975) state the density of cured phenolic resins at approx. 1.25 g cm^{-3} (1250 kg m⁻³) [13]. However, there is a possibility that in the outer zones of the individual veneers, densification takes place during production, since the adhesives used might have a plasticizing effect here. This is supported by the finding of Mai (2020) in the context of research on wood modification that alkaline phenolic resin solutions are able to plasticise the cell wall and thus facilitate the compression of the wood substance during hot pressing [14]. This might be attributed to partial solubilisation and swelling of the cell wall polymers, particularly of lignin, by the alkaline phenolic solution. The alkaline solubility of lignin is also known to be used in wood pulping, more precisely in the sulphate process using caustic soda due to the formation of phenolate groups within the lignin molecule. Based on the investigations carried out, it is not possible to say whether the higher densities in these areas are due to the penetration of the wood with adhesive or actually to a compression of the wood substance. It is likely that the described effects overlap. Microscopic examinations (on the basis of urea-formaldehyde and beech) by Gavrilović-Grmuša et al. (2010) show a clear penetration of the wood by the adhesive in the area of the adhesive joint [15]. Ongoing microscopic examinations of LVLB are intended to provide information about a possible compression of the wood substance.

4. Conclusions

With the present study, the density of LVLB was investigated in detail using a *DENSE-LAB X* laboratory density profile measuring device. In previous investigations, an initial irreversible swelling in the radial direction was detected and, based on this, a compression of the wood substance in the production process of the material was assumed. However, such a densification of the veneer layers could not be detected. Based on the present investigation, the higher density of LVLB compared to solid beech is mainly due to high densities in the area of the adhesive joints. The density in the area of the veneer centres was found within the range of that of solid beech. The cause of an initial irreversible swelling could not be clearly determined. More detailed information on this material property would be of interest for LVLB manufacture or construction engineers when laying out supporting structures.

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Supplementary Materials: The raw data are available online at https://www.mdpi.com/article/10 .3390/fib9050031/s1.

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