

Article

Hydraulic Performance Optimization of a Submersible Drainage Pump

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Abstract: Small submersible drainage pumps are used to discharge leaking water and rainwater in buildings. In an emergency (e.g., heavy rain or accident), advance monitoring of the flow rate is essential to enable optimal operation, considering the point where the pump operates abnormally when the water level is increased rapidly. Moreover, pump performance optimization is crucial for energy-saving policy. Therefore, it is necessary to meet the challenges of submersible pump systems, including sustainability and pump efficiency. The final goal of this study was to develop an energy-saving and highly efficient submersible drainage pump capable of performing efficiently in emergencies. In particular, this paper targeted the hydraulic performance improvement of a submersible drainage pump model. Prior to the development of driving-mode-related technology capable of emergency response, a way to improve the performance characteristics of the existing submersible drainage pump was found. Disassembling of the current pump followed by reverse engineering was performed instead of designing a new pump. Numerical simulation was performed to analyze the flow characteristics and pump efficiency. An experiment was carried out to obtain the performance, and it was validated with numerical results. The results reveal that changing the cross-sectional shape of the impeller reduced the flow separation and enhanced velocity and pressure distributions. Also, it reduced the power and increased efficiency. The results also show that the pump's efficiency was increased to 5.56% at a discharge rate of 0.17 m³/min, and overall average efficiency was increased to 6.53%. It was concluded that the submersible pump design method is suitable for the numerical designing of an optimized pump's impeller and casing. This paper provides insight on the design optimization of pumps.

Keywords: submersible pump; computational fluid dynamics; experiment; impeller shape; flow balance block; optimum model



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1. Introduction

This study focused on the performance improvement of submersible drainage pumps. Submersible drainage pumps are divided into two categories. One is referred to as “large submersible pumps”, which are used for drainage (rainwater) pumping stations, and the other is known as “small submersible pumps”, which are used in buildings. Small submersible drainage pumps are used for draining from buildings when leakage and rainwater flow into the basement [1–3]. The TRL (Technology Readiness Level) of submersible drainage pumps is 7–9, and it is a situation from which no unique technology will arise. Existing technology patents also utilize technology used in other fields. According to patent acquisition, vibration sensors are installed on the pump shaft to solve the blocking

phenomenon caused by foreign substances and vibration problems caused by, e.g., cavitation. The shape of the impeller can be changed without impacting performance to prevent the clogging of foreign substances or improve existing monitoring technologies. Pump efficiency is a significant energy-saving policy factor [4,5]. If pump efficiency increases, a significant amount of energy will be saved.

Due to the complicated, implicit relationship between hydraulic performance and the complex geometry shape of impeller passages, the study of optimization and the inverse problem of the submersible pump is moving slowly [6,7]. Shi et al. [8] started to design a new submersible pump for deep wells with the computational fluid dynamics (CFD) technique. They achieved sufficient pump efficiency compared with that of traditional pumps. Zhu et al. [9] investigated a mechanistic model for improving system performance with gas–liquid flow in a submersible pump. Manivannan [10] conducted a study on the computational fluid dynamics of a mixed-flow pump to predict the flow pattern inside the impeller. Different parameters and optimization techniques were used to obtain optimal output for the pump impeller numerically [11]. The pump impeller head was optimized using various optimization algorithms to reduce frictional loss during pump operation [12]. Using an inverse design, Zangeneth et al. [13] investigated using a mixed-flow pump for suppressing secondary flows. Afterwards, they [14] performed an experimental study to confirm the validity of the model pump. Kim et al. [15] attempted to improve suction performance and efficiency by optimizing a mixed-flow pump with the CFD technique. Another researcher [16] studied the suction performance improvement of mixed-flow pumps. The result exhibited that the specific speed and shape of the pump's impeller greatly influence the suction performance.

Yan et al. [17] investigated a CFD-based pump redesign of a centrifugal to improve efficiency and decrease unsteady radial forces. The CFD method was applied to study the effect of the volute and the number of impeller blades and trailing-edge modification of pumps [18,19]. Qian et al. [20] adopted the Plackett–Burman test design method for the performance optimization of multistage centrifugal pumps. The results showed a significantly impacted pump axial force and hydraulic performance when considering the blade exit angle, outlet diameter, blade wrap angle, etc. Liu et al. [21] studied the RBF neural network and particle swarm optimization method to improve the performance of submersible well pumps. They found that the pressure gradient in the impeller was increased, and the pressure amplitude of the impeller was significantly reduced. Ling Bai et al. [22] highlighted the performance improvement of an EPS impeller based on the Taguchi approach and found that the front and rear shrouds of the impeller meridian significantly affect the ESP performance. Chen et al. [23] studied performance improvement of a mixed-flow pump based on the entropy production method. They found that the geometric and hydrodynamic parameters greatly influenced the pump's energy characteristics. Suh et al. [24] optimized impeller and suction performance to increase the hydraulic efficiency of a mixed-flow pump. Jeon et al. [25] conducted a study on a regenerative pump impeller and enhanced the model's efficiency by numerical simulation and design of experiments (DoE). Siddique et al. [26] investigated the impeller design optimization of a centrifugal pump by numerically enhancing the pump head and significantly reducing the input power. Shim et al. [27] presented a study on enhancement flow recirculation and cavitation of a centrifugal pump by controlling the meridional profile of the blade. Yang et al. [28] investigated multistage ESP to improve hydraulic performance using the Taguchi optimization method. The Taguchi method was a remarkably handy tool for optimizing the ESP. Arocena et al. [29] designed and analyzed the intake structure of a submersible pump numerically. Wei et al. [30] investigated the influence of impeller gap drainage width on the performance of a low-specific-speed centrifugal pump, and the results revealed that using a smaller gap width could significantly improve the performance. Han et al. [31] presented the influence of various impeller blade outlet angles on the performance of a high-speed ESP using experimental and computational methods. It was found that the impeller vane exit angle had a significant effect on the pump performance

curve. Tong et al. [32] conducted axial flow pump performance analysis experimentally and numerically. The results showed that a higher head led to increased pump rotation speed. Fakher et al. [33] studied the efficiency improvement of an electric submersible pump. They replaced the conventional motor with a permanent magnetic one to achieve prolonged ESP mean failure. The flow patterns inside an electrical submersible pump are presented using CFD and compared with visualization experiments [34]. However, the study did not show whether optimizing the shape of the pump casing and impeller can improve the hydraulic performance in a single-stage submersible drainage pump.

Therefore, this study focused especially on the hydraulic performance optimization of a centrifugal-type submersible drainage pump as a development target. To improve our understanding of the flow characteristics inside pumps, existing and developed pumps' performances were analyzed through simulations and experiments. Moreover, this study was intended to provide a basic design of the pump shape to enhance the performance of significant parts, manufacture parts and conduct pump tests using 3D printing technology. In addition, primary research findings were patented based on the developed technology.

2. Materials and Methods

2.1. Pump Dimensions and 3D Model

Three-dimensional scanning was performed to accurately obtain the dimensions of the pump casing and impeller to be analyzed. For this purpose, a DWE-08B submersible drainage pump was disassembled, as shown in Figure 1. The exact dimensions of the pump were required for analysis through computational methods. Of the pump components, only the significant parts of the pump impeller and casing were scanned using a noncontact portable 3D scanner (Creaform 50, with a tolerance of 1/100, Creaform, Lévis, QC, Canada). The software generated the three-dimensional geometrical shape and imported it to CAD software (ANSYS-ICEM (21R2)) for cleaning.

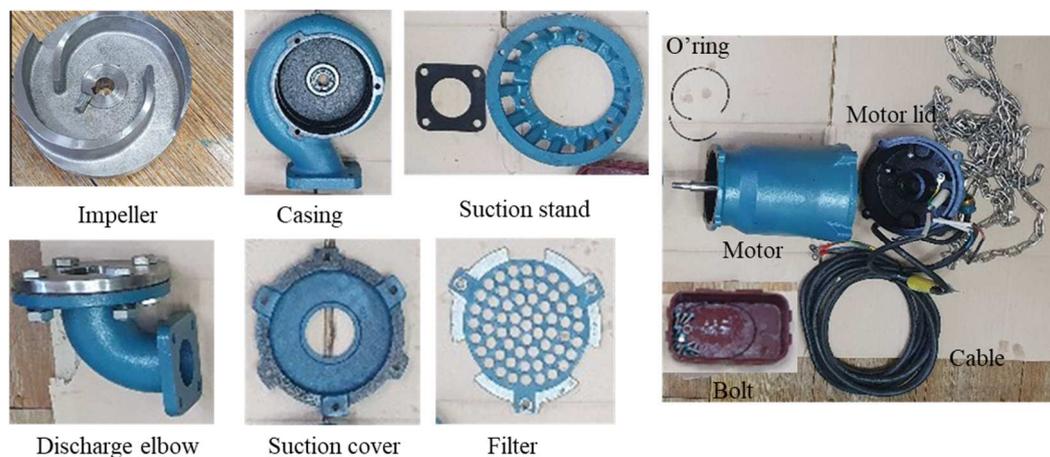


Figure 1. Disassembling the submersible drainage pump (DWE-08).

This study used ANSYS-ICEM commercial software to clean-scan 3D geometry and create an .STP file. Figure 2 shows an assembly and disassembly drawing of the vertical semi-open-type submersible pump (model—DWE-08B). Figure 3 illustrates the cross-sectional view of the main components of the pump. Table 1 presents the major design dimensions of the pump impeller and the casing obtained from the pump company's catalog.

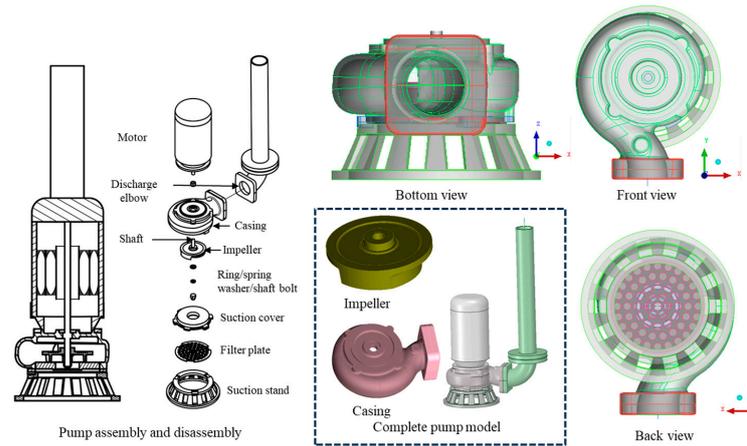


Figure 2. Assembly and disassembly drawing of the submersible drainage pump (DWE-08B) and different views.

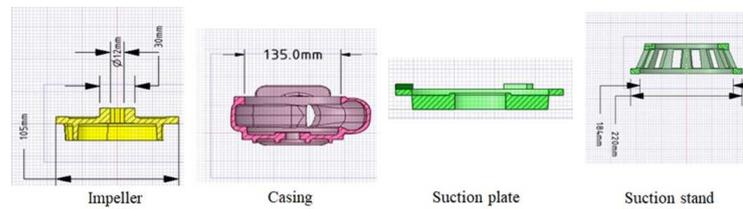


Figure 3. Cross-sectional view of the pump's key components.

Table 1. Original submersible pump model (DWE-08B) design parameters.

Description	Power	Flow Rate	Head	Impeller			Casing		
				Blades	D1	D2	Flow Path Height	Inlet Height	Outlet Dia.
Model	H.P.	m ³ /min	m	No.	mm	mm	mm	mm	mm
DWE-08B	1	0.16	10	2	25	105	54	135	60

2.2. Specifications of the Submersible Pump

The pump company only provided the major pump specifications. Figure 4 illustrates the various pump models' performance curves. The DWE-08B model performance data are represented in the black curve with a circle and red line. Table 2 shows the submersible pump's data, as presented in the pump company's catalog [2]. Specific points of the subject pump were determined from the record. Figure 5 illustrates the hydraulic performance optimization procedure.

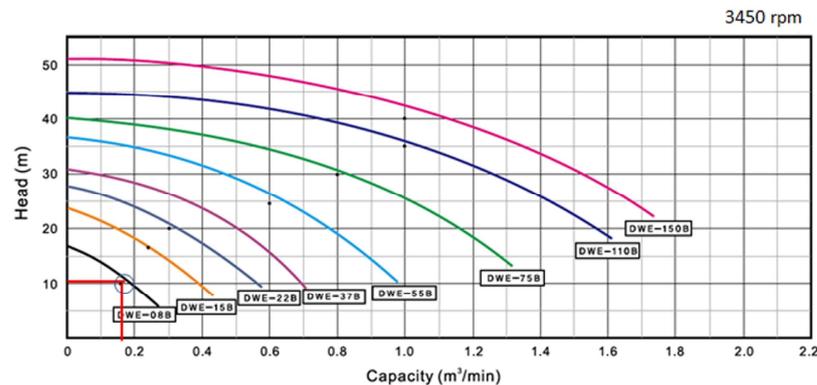


Figure 4. Hydraulic performance curve of various submersible pumps [2].

Table 2. Submersible pump performance data [2].

Model	Outlet Height (mm)	Power (H.P.)	Flow Rate (m ³ /min)	Head (m)
DWE-08B	50	1	0.16	10

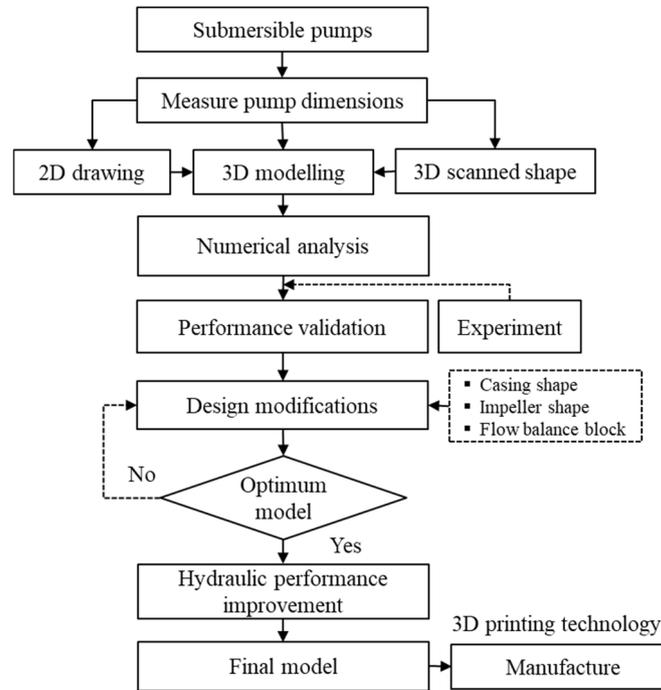


Figure 5. Procedure for hydraulic performance optimization of the submersible drainage pump.

2.3. Computational Domain and Boundary Conditions

The ANSYS ICEM-CFX commercial software (21R2, ANSYS Inc., Canonsburg, PA, USA, 2021) based on the finite volume method was utilized for grid generation and analysis of the pump. Then, unconstructed tetrahedral meshing grids were created, as shown in Figure 6. Changing the number of meshing grids confirms the grid dependency [35]. Table 3 shows the various pump meshing grids performance and relative errors. The proposed total meshed grids had 272,563 nodes and 1,374,829 elements.

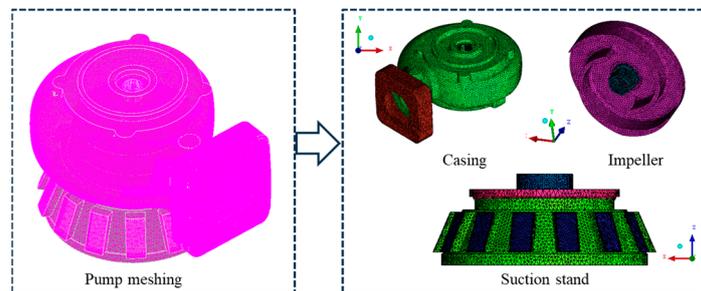


Figure 6. Submersible pump meshing grids used for computation.

Table 3. Meshing grids of the DWE-08 submersible pump.

Description	Elements	Nodes	Head (m)	Relative Error (%)
Model 1	205,962	1,241,365	9.824	-
Model 2	272,563	1,374,829	9.871	0.47842
Model 3	532,924	2,733,319	9.853	0.18235
Model 4	1,085,683	5,648,730	9.816	0.37552

To run the computer simulation, this study accounted for the Reynolds Average Navier–Stokes (RANS) equations for calculating the flow analysis of the pump [36]. The following assumptions were considered: (i) incompressible, (ii) steady-state flow and (iii) turbulence model. The fluid was assumed to be Newtonian fluid, and the thermophysical properties were constant with temperature. Under the assumptions of incompressible and steady state, the governing equations of the continuity and momentum equations (known as Navier–Stokes) are expressed as [36,37]

$$\frac{\partial u_i}{\partial x_i} = 0 \tag{1}$$

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = -\frac{\partial p}{\partial x_i} + \frac{\partial \tau_{ij}}{\partial x_j} + S \tag{2}$$

In the above equations, u_i represents the velocity vector, x is the component of the position vector, p is the scalar pressure, ρ is the density of the fluid, τ_{ij} designates the stress tensor, S is the source term, and i and j represent tensor notations.

To calculate the turbulent flow, eddy viscosity was added. The SST (shear stress transport turbulence) model was considered to calculate the fluid’s turbulent shear stress [38,39]. The standard k - ω model was originally developed by Wilcox [38]. The k - ω -based SST model was developed by Menter [39] and can be used to effectively blend the robust and accurate formulation of the model in the near-wall region. This model is widely applicable in turbomachinery and pumps and can also predict the onset of flow separation under an adverse pressure gradient. Therefore, the SST model was chosen for the current application. Turbulent viscosity μ_t was determined by solving two-transport equations: turbulent energy k and the turbulence frequency ω . The two k - ω -based equations can be expressed as k -equation:

$$\rho \frac{\partial k}{\partial t} + \rho u_j \frac{\partial k}{\partial x_j} = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + P_k - \rho \beta^* k \omega + P_{kb} \tag{3}$$

ω -equation:

$$\rho \frac{\partial \omega}{\partial t} + \rho u_j \frac{\partial \omega}{\partial x_j} = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_\omega} \right) \frac{\partial \omega}{\partial x_j} \right] + \alpha \frac{\omega}{k} P_k - \rho \beta \omega^2 + P_{\omega b} \tag{4}$$

The turbulent eddy viscosity μ_t was calculated from

$$\mu_t = \rho \frac{k}{\max(\omega, S \cdot F_2)} \tag{5}$$

where P_{kb} and $P_{\omega b}$ are the shear production of turbulence, S is the invariant measure of the strain rate, and F_2 is a blending function that restricts the limiter to the wall boundary layer defined by

$$F_2 = \tanh \left[\max \left(\frac{2\sqrt{k}}{\beta^* \omega y}, \frac{500\mu}{\rho y^2 \omega} \right) \right]^2 \tag{6}$$

The first SST blending function is formulated as

$$F_1 = \tanh \left[\min \left\{ \max \left(\frac{\sqrt{k}}{\beta^* \omega y}, \frac{500\mu}{\rho y^2 \omega} \right); \frac{4\rho k}{CD_{k\omega} \sigma_\omega 2y^2} \right\} \right]^4 \tag{7}$$

where y is the distance to the nearest wall, and $CD_{k\omega}$ is the positive part of the cross-diffusion term, i.e.,

$$CD_{k\omega} = \max \left(2\rho \frac{1}{\sigma_\omega 2\omega} \frac{\partial k}{\partial x_j} \frac{\partial \omega}{\partial x_j}, 10^{-10} \right) \tag{8}$$

The turbulence model coefficients are given as

$$\alpha = 0.55, \beta = 0.075, \beta^* = 0.09, \sigma_k = 2.0, \sigma_\omega = 2.0$$

In this work, the boundary conditions used for the simulation were mass flow rate as the inlet and 0 Pa as the pressure outlet. All boundary walls were assumed to be smooth walls with no-slip conditions. A frozen rotor operating at a specific rotational speed of 3450 rpm was selected for steady-state, incompressible flow analysis. Figure 7 represents the boundary conditions for numerical analysis of the DWE-08 pump domain. The velocity and pressure residual value was 1×10^{-5} , controlled by convergence criteria.

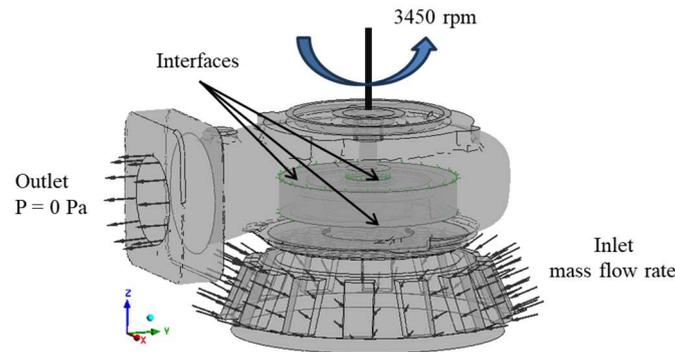


Figure 7. Boundary conditions of the computational domain.

3. Results and Discussion

Section 3.1 provides the pump performance validation of the computed data. Section 3.2 describes the performance analysis of the submersible pump under different operating conditions. Additionally, design modifications of the casing and impeller are illustrated in Section 3.3. Moreover, Section 3.4 presents the pump’s hydraulic performance improvement and optimum model.

3.1. Verification of the Numerical Results

An experimental setup was constructed for comparison with the computed data to verify the reliability of the test pump that the test facility employed to meet the KSB 6321 and ISO 5198 standards [40,41]. The measurement sensors used in the test pump to obtain the test data allowed a standard deviation of $\pm 2\%$. The test environmental working fluid temperature and relative humidity were $13 \pm 1 \text{ }^\circ\text{C}$ and $32 \pm 5\%$, respectively.

The hydraulic performance parameters such as head, volume flow rate, power and efficiency are sufficient for comparing the measured with the calculated data. The equations for pump head, energy and efficiency are expressed as

$$H = \frac{p_2 - p_1}{\rho g} + \frac{V_2^2 - V_1^2}{2g} + (z_2 - z_1) \tag{9}$$

$$P = \omega T \tag{10}$$

$$\eta = \frac{\rho g Q H}{\omega T} \tag{11}$$

where H represents the pump head in m , p is the static pressure of the pump in N/m^2 , V is the velocity of the pump in m/s , z is the elevation of the pump in m , P is the shaft power in kW , Q is the volumetric flow rate in m^3/min , ω is the rotational speed in rad/s , T is the torque in $\text{N}\cdot\text{m}$, ρ is the working fluid density in kg/m^3 , and g is the gravitational acceleration in m/s^2 , respectively. Subscripts 1 and 2 denote the inlet and outlet sections of the pump.

Figure 8 presents the experimental measurement data tested by the KTC (Korea Testing Certification Institute) at the pump test facility center. By examining the results in Figure 8,

it can be seen that when the flow-specific point (volumetric flow rate) was $0.165 \text{ m}^3/\text{min}$, the total head was 10 m, and the overall efficiency was only 32.14%, which was not the same as the pump efficiency. Because the test pump was in the water and could not measure the torque, the motor’s power factor (0.78) must be considered in comparing it with the experimental results. In addition, the catalog’s performance data, test data and analysis data were all presented for each outcome. When comparing all data, the average head error value was only 0.0456%, the power average error was only 0.0808%, and the efficiency average error was only 0.0617%. The head and efficiency differences were only 0.07% and 10.18% at the design flow rate. The lower difference was observed at the higher flow rate of the pump. The standard deviation of the pump head was 0.046%, the power was 0.0047%, and the rotational speed was 1.54%. At the 95% confidence limit, the normal distribution of the test pump was measured, revealing that the uncertainty of the pump head was $H \pm 0.00989 \text{ m}$, the discharge rate was $Q \pm 0.00178 \text{ m}^3/\text{min}$, the power was $P \pm 0.0102 \text{ kW}$, and the rotational speed was $N \pm 3.298 \text{ rpm}$.

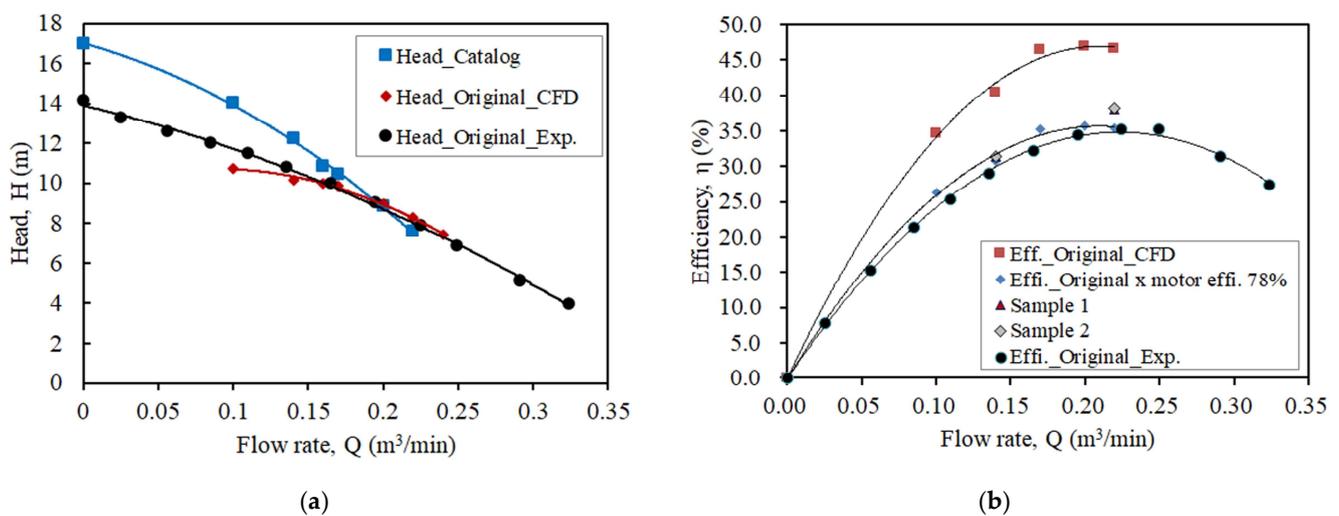


Figure 8. Performance comparison between the experiment and computational results for the submersible pump: (a) head vs. flow rate and (b) efficiency vs. flow rate (experimental uncertainty in $N \pm 3.298 \text{ rpm}$, $Q \pm 0.00178 \text{ m}^3/\text{min}$, $H \pm 0.0989 \text{ m}$ and $P \pm 0.0102 \text{ kW}$).

First, looking at Figure 8a, there is a clear difference between the test and catalog results. As observed from the H-Q curve, the analysis results agree relatively well with the experimental data, except for the low flow rate. The two results do not match well in the low-flow region due to the influence of the grid and $y+$. Therefore, we decided it would be best to exclude or modify the catalog data. In comparing this with the test value, it was found that the test results are well matched when considering the motor power factor of 0.78, as mentioned in the shaft power report. The values of Samples 1 and 2 in Figure 8b are the efficiencies mentioned in the high-efficiency energy equipment report. Moreover, in this study, the mechanical losses of the submersible pump were not taken into consideration in the numerical analysis.

3.2. Performance Analysis

Additionally, this study analyzed the flow pattern inside the pump and velocity distributions at the design flow rate. Figure 9 shows the velocity vectors and velocity streamline distribution of the pump. As can be observed, the flow recirculates in the pump discharge region, where the energy dissipates, resulting in significant pump losses. The flow separation in the casing caused relatively large vortices at the outlet of the pump casing. Also, the clearance gap between the pump volute and impeller was large (more than 2 mm). This clearance gap flow creates vortices that separate from the impeller blade and reduce local pressure. Also, the impeller was located in the casing at the bottom

of the pump, as shown in Figure 10. Henceforth, changing the impeller’s center further reduced the pump’s efficiency. Therefore, a CFD-based design modification study and research analyzing the behavior of the flow in various geometries are needed to enhance pump performance.

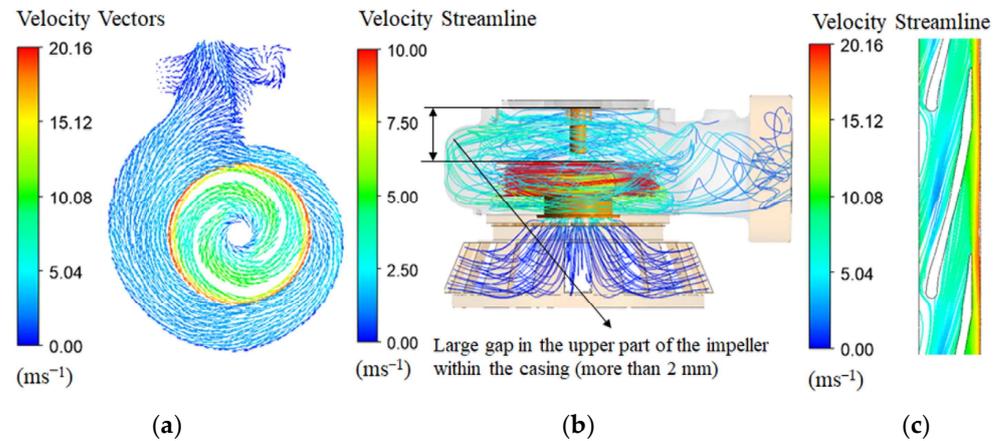


Figure 9. Velocity distributions analysis inside the casing: (a) velocity vectors; (b) velocity streamlines; (c) blade-to-blade velocity streamlines.

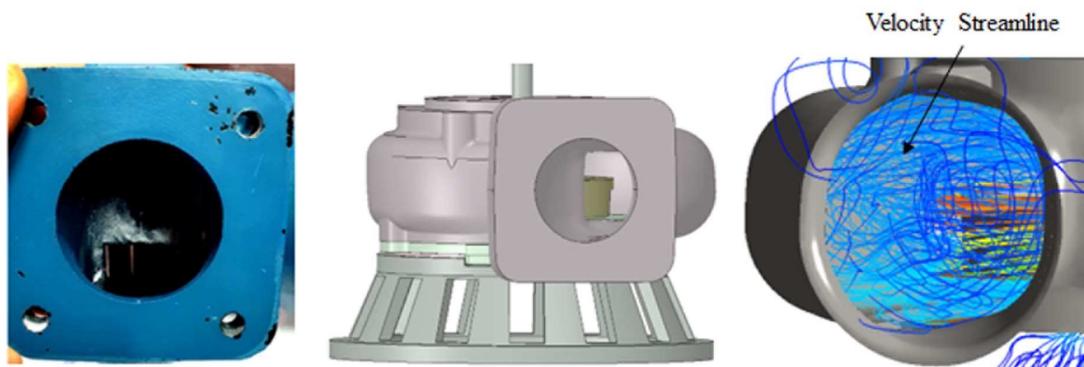


Figure 10. The position of the impeller inside the casing of the pump.

Based on the experimental and simulation results, we determined that there is a possibility of increasing efficiency by using an efficient pump motor and designing or shaping the part where the loss occurs. The use of an efficient pump motor was outside the scope of this study; this study examined the cause of the decrease in efficiency and found a way to supplement the design of the pump components. It was noted from the loss analysis of the pump that the mechanical loss, the ratio of impeller loss to casing, and inlet loss were also high [42]. The efficiency of the DWE-08B pump ranged from 30% to 40%, which is not an optimal performance condition. Of course, since the impeller was a semi-open type, it was less efficient than the closed type, but its efficiency was comparatively low compared with other pumps. Therefore, this study considered improving the efficiency to create the optimal design of the impeller and casing, suggesting improvements in the geometry of the two components.

3.3. Design Modifications of the Casing and Impeller

In this study, two shapes that can reduce the large gap in the upper region of the pump impeller were proposed and analyzed to optimize the shape of the casing. Model 1 was created with a reduced flow path compared with the original model; model 2 was created with a cochlear (tubular) flow passage in the intact casing. Figure 11 shows the casing shape change model.

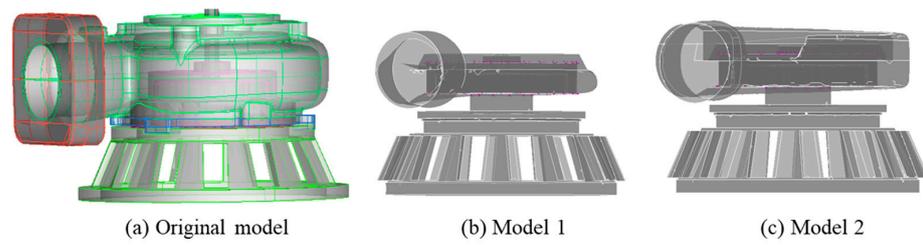


Figure 11. Casing shape change model: (a) original model; (b) model 1 (c) model 2.

Figure 12 displays the comparison of velocity streamlines for the casing shape change model. As shown in Figure 12, the fluid flow formed a streamlined shape, eliminating the idle space at the top; the fluid flow at the outlet of the pump casing was discharged without swirling using a guide rib. Figure 13 shows the performance comparison for the casing shape change model. Table 4 presents the pump efficiency of the casing shape change models. By changing the casing shape, the relative efficiency was improved by up to 4~5%.

However, it is difficult to make a new one with die and casting; therefore, an in-depth investigation is a prerequisite for optimization. We applied the optimization plan of the casing shape to prevent the need for wood-shaped and casting work. One method involves attaching a simple installable member to the pump casing to reduce the space. Optimizing the casing shape utilizes an approach of changing the casing shape using a flow balance block (FBB), which can be easily installed. Here, we employed an FBB instead of the casing shape change model. Figure 14 shows the flow balance block model. We utilized an FBB to reduce secondary and friction losses where the flow in the casing was stagnant.

Table 4. Comparison of pump efficiency for casing shape change model.

Flow Rate (m ³ /min)	Original (%)	Model 1 (%)	Model 2 (%)	Efficiency Improvement (%)	
				Model 1	Model 2
0.10	34.593	40.542	38.904	5.949	4.311
0.14	40.420	48.358	45.474	7.938	5.054
0.16	45.415	50.687	49.230	5.272	3.815
0.17	46.375	51.513	49.301	5.138	2.926
0.20	46.921	52.826	52.357	5.905	5.436
0.22	46.562	53.487	52.221	6.925	5.659

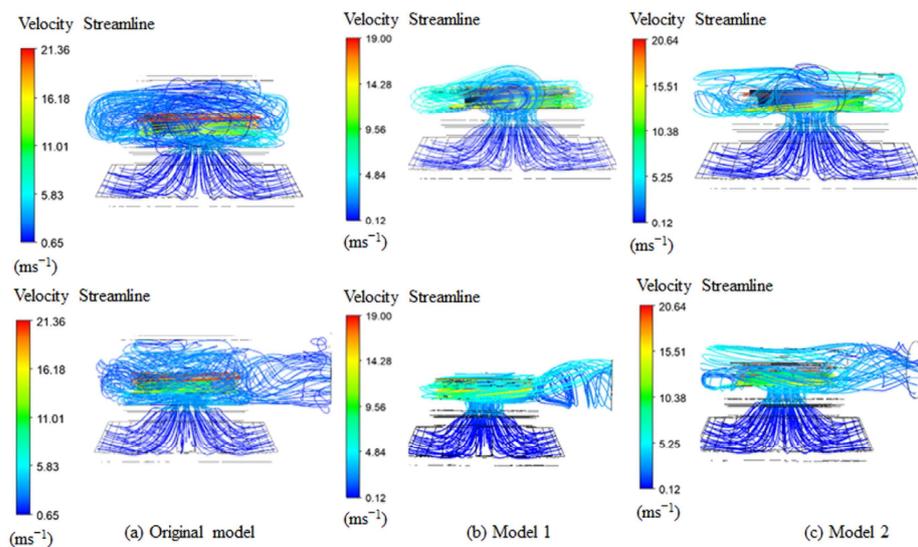


Figure 12. Velocity streamline comparison for shape change model: (a) original model; (b) model 1; (c) model 2.

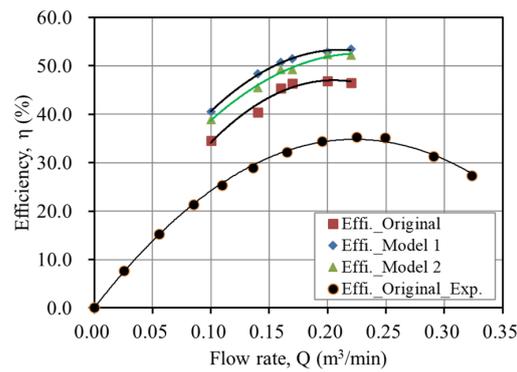


Figure 13. Performance comparison for casing shape change model.

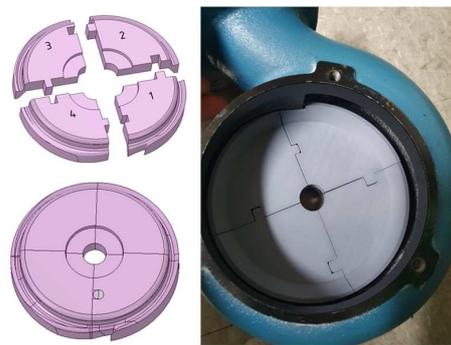


Figure 14. Flow balance block model.

Also, we modified the three different shapes of the impeller. Impeller 1’s vanes were created diagonal (oblique line) in the basic model. Impeller 2 had an extended tip compared with Impeller model 1. Impeller model 3’s vanes were thicker compared with the vanes of the basic model. Figure 15 shows the impeller shape change model. The impeller shape change involved inclining the vane to improve the flow in front of the rear shroud. These pump simulation data were compared to assess the performance characteristics of the different impeller shapes to improve the efficiency of the original model.

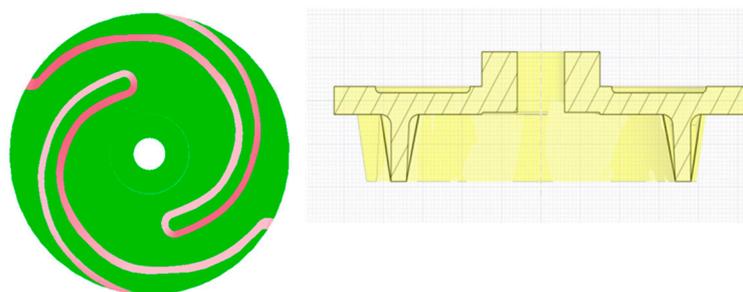


Figure 15. Impeller shape model 1.

Furthermore, Figure 16 illustrates the pressure and velocity streamline distribution in other planes of the pump impeller. As observed, the flow losses could be reduced by improving the streamline in the lower area (planes 1, 2) via a change in the impeller shape. Figure 17 shows the performance comparison of various impeller shape change models. The result shows that changing the shape of the impeller increased the pump efficiency. Hence, changing the impeller shape reduces the shaft power and increases the efficiency to 5.56% by preventing flow disturbance. Therefore, this study found the impeller shape change model 1 optimal for manufacturing.

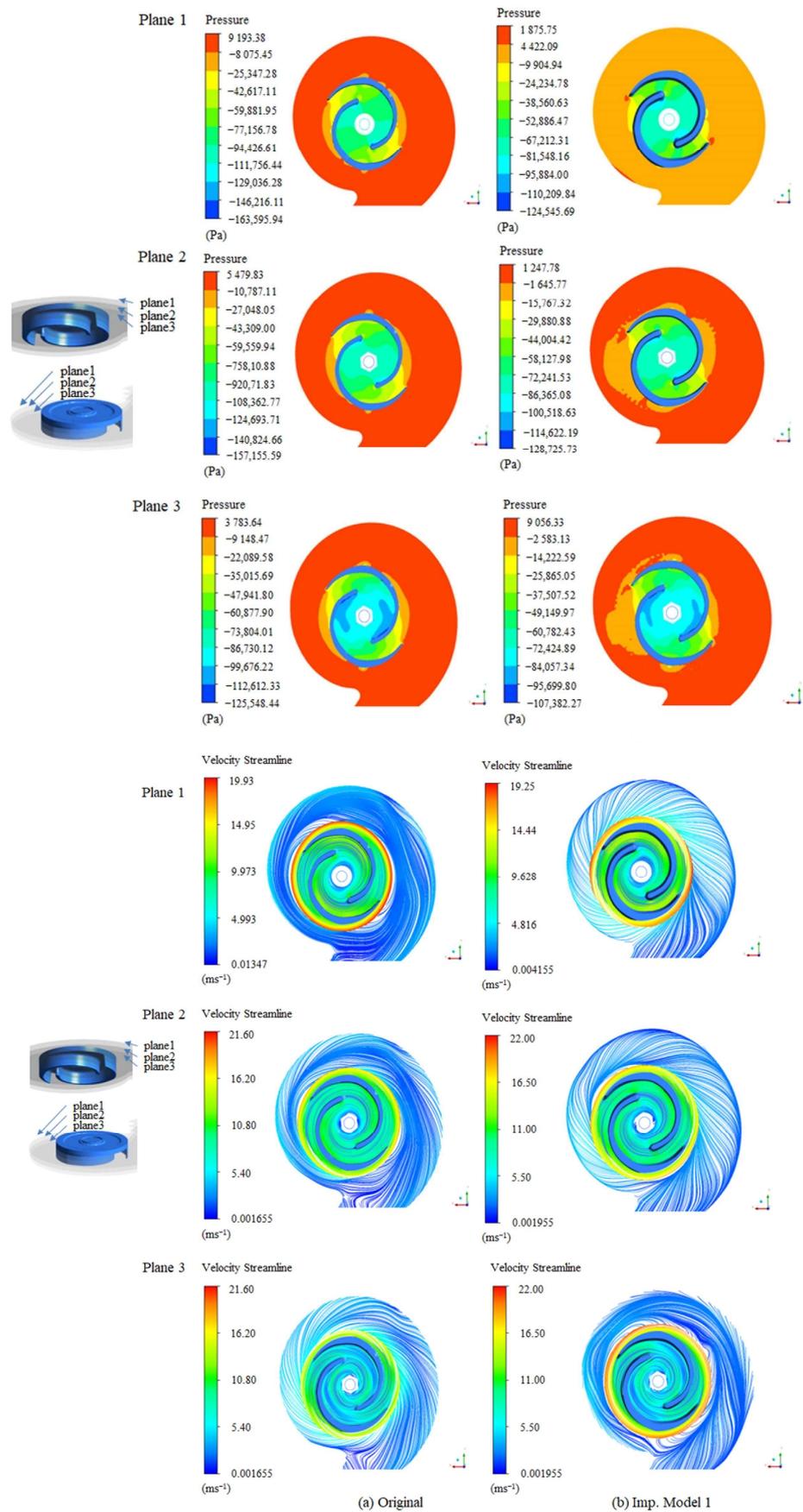


Figure 16. Pressure and velocity streamline distribution in different planes: (a) original impeller; (b) impeller model 1.

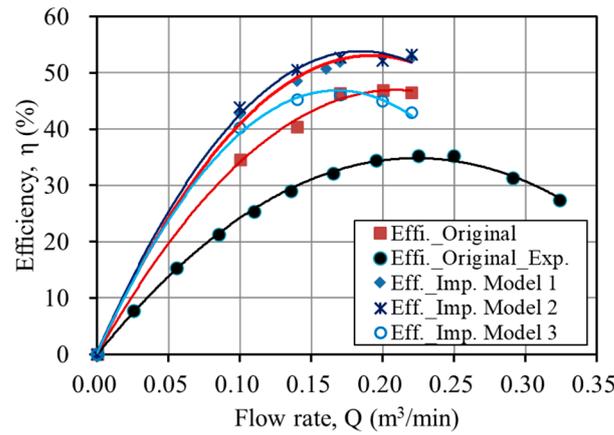


Figure 17. Performance comparison of impeller shape change models.

3.4. Optimum Model

The existing model’s performance analysis and modification of the casing and impeller were reviewed. This study examined the flow around the impeller of the current model and devised a strategy to increase efficiency. The pump efficiency was significantly increased to 49.30%, less than 2.64% of that of the modified impeller, by modifying the casing shape at a 0.17 m³/min flow rate. Also, changing the impeller shape of the pump enhanced the internal pressure distribution and reduced the flow separation at the discharge side and its efficiency. The design flow rate of the pump was shifted from 0.16 m³/min to 0.17 m³/min.

Moreover, the efficiency increased to 5.56% at 0.17 m³/min, and the average efficiency increased to 6.27%. It is understood that changing the shape of the impeller and casing is the best solution to improving a pump’s performance [43]. Figure 18 shows the cross-sectional view of the original and newly designed impellers. Therefore, impeller shape change model 1 was considered optimal for manufacture.

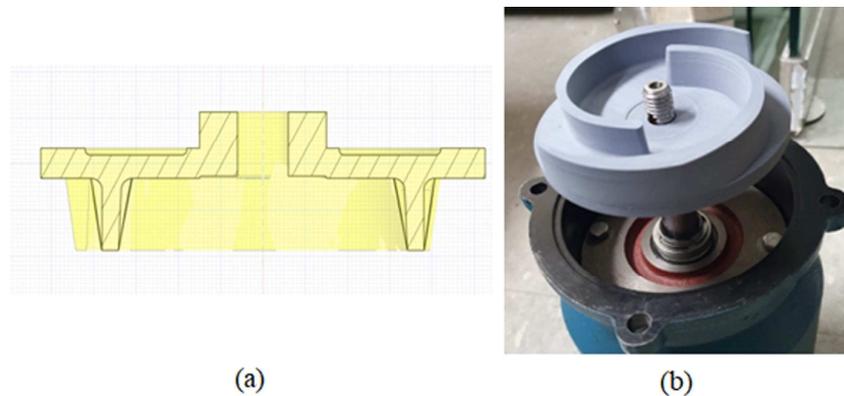


Figure 18. Cross-sectional view of the optimum model: (a) impeller model 1; (b) manufactured model.

4. Conclusions

Hydraulic performance optimization in a submersible pump was performed. A new pump impeller and flow balance block were designed, computational simulation was performed, parts were manufactured, and experiments were conducted. The results of this study on performance improvement are summarized as follows:

- (a) The test data verified the computed results, confirming the pump’s performance.
- (b) We modified the casing and impeller shape to improve hydraulic performance and used a flow balance block to reduce the inner space of the pump.
- (c) Changing the impeller shape reduced the power and increased efficiency, which can prevent flow disturbance. The attachment of the flow balance block increased the efficiency in the flow area more significantly than the operating point.

- (d) The flow separation inside the pump was significantly improved and increased pump performance by up to 5.56% at the design flow rate.
- (e) This research obtained two Korean patents based on the identified performance improvement results.
- (f) Further studies should consider conducting a performance test for the shape change model for a submersible pump.

5. Patents

Impeller for submersible pump (patent no.: 20-2021-0001433) and centrifugal submersible pump (patent no.: 10-2021-0058374). <http://engpat.kipris.or.kr/engpat/searchLogina.do?next=MainSearch> (17 November 2023).

Author Contributions: M.R. conceived and designed the study, analyzed the results, wrote the paper and edited the draft; S.-H.S. contributed to project administration and conceptualization and supervised the work; H.-W.R. managed resources, conducted the experiment and edited the draft; K.H.S. contributed to fund acquisitions and resources for the work; K.C.S. contributed to the experiment; and L.Z. advised on project work. All authors have read and agreed to the published version of the manuscript.

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