# Supplement

## Investigation on Mechanical Behavior of Iron Foams under Different Compression Test Conditions

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### A. Structure of the iron foam samples

Figure S1: Measurement of cell size, pore size and different strut thicknesses on an IF58 specimen.

Nominal	Number of	Mean	SD	Min	Median	Max		
cell size	measured cells	(µm)		(µm)	(µm)	(µm)		
Cell size								
IF45	81	461.77	72.26	275	455.5	641.3		
IF58	113	617.73	76.08	433.6	601.9	836.2		
IF80	45	828.11	79.87	691.2	805.2	1008		
Pore size between 40-100 μm								
IF45	24	69.5	17.08	39.23	68.3	99.35		
IF58	6	68.01	12.42	59.01	62.73	92.15		
IF80	5	66.78	18.72	42.4	67.59	91.16		
Pore size between 100-200 μm								
IF45	43	155.59	27.94	102.3	155	199.3		
IF58	31	150.8	29.43	101.2	150.5	198.9		
IF80	29	157.33	28.5	100.5	164.8	198.3		
Pore size >200 μm								
IF45	27	238.47	45.03	103.5	244.6	310.2		
IF58	94	319.98	71.81	200.4	318.75	525.3		
IF80	82	333.61	87.07	213	315.65	546.4		
End-strut thickness								
IF45	86	74.73	10.3	54.92	71.44	103.1		
IF58	78	63.62	9.95	42.23	62.41	93.12		
IF80	39	97.79	17.54	71.45	95.88	167.3		
Branch-strut thickness								
IF45	52	55.52	6.18	43.71	56.56	78.33		
IF58	53	59.88	7.55	44.39	60.88	74.66		
IF80	30	80.91	12.27	61.16	76.77	123.8		
		Saddle	e-strut thickne	ss				
IF45	70	25.52	4.8	16.61	25.11	38.45		
IF58	51	21.67	4.12	13.82	21.01	30.6		
IF80	13	29.066	5.14	20.61	29.14	37.09		

### Table S1: Results of the measurement

#### B. Determination of the compression tests parameters

Figure S2 shows the experimental design and parameters with the number of specimens used in each group. For each cell-size group of iron foam specimens, 20 samples were considered 10 of which had a nominal compression area of 100 mm<sup>2</sup> ( $A_1 = 10 \times 10$ ) and the other 10 had a nominal compression area of 25 mm<sup>2</sup> ( $A_2 = 5 \times 5$ ). For each compression area group, 5 specimens underwent the compression tests with the cross-head speed of 0.001 mm/s ( $S_1$ ) and the other 5 underwent that of 0.01 mm/s ( $S_2$ ). Considering all the experimental configurations, 60 trials (or treatments) were carried out. Therefore, the trials contained 12 blocks of 5 specimens where each block had a unique set of configuration, i.e. average cell size, compression area and cross-head speed.

<ul> <li>IF 45 → Iron Foam of 450 µm cell size</li> <li>IF 58 → Iron Foam of 580 µm cell size</li> </ul>	• IF 45 $10$ A1 $5$ S1 5 S2 10 A1 $5$ S2 5 S2
<ul> <li>IF 80 → Iron Foam of 800 µm cell size</li> <li>A1 → Nominal compression area of 100 mm<sup>2</sup></li> <li>A2 → Nominal compression area of 25 mm<sup>2</sup></li> </ul>	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
<ul> <li>S1 Crosshead Speed of 0.001 mm/s</li> <li>S2 Crosshead speed of 0.01 mm/s</li> </ul>	• IF 80 10 A1 5 51 5 52 5 51 5 51 5 51 5 51 5 51 5 52

Figure S2: Experimental design and parameters with the number of specimens used in each group.

Evaluating the results of different cell-size group indicated that in most cases the stress-strain curves associated to the larger compressed area (A<sub>1</sub>) and the cross-head speed (S<sub>1</sub>) were either more consistent or steadier and easier to evaluate (due to the presence of more clear compression strength, longer plateau region, or more linear densification regime) than other groups of curves associated with the same cell-size but different areas and strain rates. Therefore, specimens with compression area of A<sub>1</sub>=100 mm<sup>2</sup> (A = 10x10 mm<sup>2</sup>) and the cross-head speed of S<sub>1</sub>= 0.001 mm/s were chosen for all the tests and analyses. Another reason for using the slower cross-head speed is the small thickness of the specimens, making it difficult to verify the reaction of the samples to compression loads of higher speeds. Stress-strain curves of iron foam samples of different dimensions and under different cross-head speeds are shown in Figures S3-S5.



**Figure S3:** Stress-strain curves of IF45 samples under compression: (a) compression area A<sub>1</sub> and cross-head speed S<sub>1</sub>, (b) compression area A<sub>2</sub> and cross-head speed S<sub>1</sub>, (c) compression area A<sub>1</sub> and cross-head speed S<sub>2</sub>, (d) compression area A<sub>2</sub> and cross-head speed S<sub>2</sub>.



**Figure S4:** Stress-strain curves of IF58 samples under compression: (a) compression area A<sub>1</sub> and cross-head speed S<sub>1</sub>, (b) compression area A<sub>2</sub> and cross-head speed S<sub>1</sub>, (c) compression area A<sub>1</sub> and cross-head speed S<sub>2</sub>, (d) compression area A<sub>2</sub> and cross-head speed S<sub>2</sub>.



**Figure S5:** Stress-strain curves of IF80 samples under compression: (a) compression area A<sub>1</sub> and cross-head speed S<sub>1</sub>, (b) compression area A<sub>1</sub> and cross-head speed S<sub>2</sub>, (c) compression area A<sub>2</sub> and cross-head speed S<sub>1</sub>, (d) compression area A<sub>2</sub> and cross-head speed S<sub>2</sub>.

**C.** Calculations of the points for the proposed tabular method (Relative density data from the main document, other data from Table S1)

C1. Cell size effect values (EVs) IF45: 100 IF58:  $\frac{461.77}{1000} = 0.7475$ → 74.75  $IF80: \frac{\frac{617.73}{617.73}}{\frac{461.77}{828.11}} = 0.5576$ → 55.76 C2. Relative density EVs IF45: 100 IF58:  $\frac{(\rho * / \rho s) \text{ IF58}}{\rho s} = \frac{0.027}{\rho s s} = 0.7105$  $\rightarrow$ 71.05 0.038 (ρ\*/ρs) IF45 IF80:  $\frac{(\rho * / \rho s) \text{ IF80}}{(\rho * / \rho s) \text{ IF80}} = \frac{0.025}{0.000} = 0.6579$ 65.79  $\rightarrow$ Mean value of the measured (ρ\*/ρs) IF45 0.038 pore sizes, IF45 C3. Pore size EVs (pore size > 200  $\mu$ m) Mean value of the measured IF45: 100 238.47 pore sizes, IF58 = 0.7453  $\rightarrow$ 74.53 IF58 319.98 333.61 = 0.7148 → 71.48 Mean value of the measured pore sizes, IF80 C4. Pore size EVs (pore size between 100 µm and 200 µm) IF58: 100 EV = 100 is assigned for IF58 sample group as it has IF45:  $\frac{150.8}{1000} = 0.9692$ → 96.92 IF45:  $\frac{155.59}{155.59} = 0.9692$ IF80:  $\frac{150.8}{157.33} = 0.9582$ the smallest mean value of pore sizes between 100 → 95.85 μm and 200 μm. (we assumed that smaller pore size leads to higher compression strength) C5. Final EVs for pore size IF45: 196.92/2 = 98.46 Average values of the IF58: 174.53/2 = 87.265 EVs calculated in C3 IF80: 0.5(71.48+95.85) = 83.66 and C4 C6. Pore number EVs (using ppi data provided by Alantum) IF80: 65/65=1 → 100 IF45: 65/105= 0.6190 → 61.9 EV=100 is assigned for IF80 sample group as it has IF58: 65/95= 0.6842 → 68.42 the highest value of mean end-strut thicknesses. (We assumed that thicker struts lead to higher C7. End-strut thickness compression strength) IF80: 100 74.73 IF45: → 76.42 = 0.764297.79 63.62 Mean value of the measured end-strut thicknesses, 0.6506 → 65.06 IF45 97.79 C8. Branch-strut thickness Mean value of the measured end-strut thicknesses, IF80: 100 IF80 IF45:  $\frac{55.52}{100} = 0.6862$ → 68.62 80.91 IF58:  $\frac{59.88}{80.91} = 0.7401$ → 74.01 C9. Final EV for strut thickness IF80: 100 IF45: 0.5(76.42+68.62) = 72.52 IF58: 0.5(74.01+65.06) = 69.535