

Figure S-1. Maslia et al. 2016



Figure S-2. Maslia et al. 2016





Figure S-3. Maslia et al. 2016



Figure S-4. Maslia et al. 2016





## Supplemental Information: Tables — Maslia et al. 2016

**Table S-1.** Chronology of selected evens related to water supply and environmental contamination at U.S. Marine Corps Base Camp Lejeune, North Carolina, and vicinity. <sup>#,\*</sup>

Event	Date or approximate date
Hadnot Point water treatment plant (WTP)	1941–42
Tarawa Torrace W/TP comes on line	1052 52
Holcomb Bouloward WTP comes on line	1992-99 June 1972
Several Tarawa Terrace and Hadnot Point water-supply wells shut down due to documented volatile organic compound (VOC) contamination	November 1984–February 1985
Marston Pavilion interconnection valve opened and booster pump 742 continuously operated for eight days (because of shut down of Holcomb Boulevard WTP) to augment Holcomb Boulevard drinking-water supply with contaminated Hadnot Point drinking water	January 27–February 4, 1985
Holcomb Boulevard WTP expanded to provide water to Tarawa Terrace and Camp Johnson water-distribution system areas	1987
Tarawa Terrace WTP and remaining operating supply wells shut down and taken out of service	March 1987
ABC One-Hour Cleaners placed on the USEPA's National Priorities List (NPL) of contaminated sites	March 1989
USMCB Camp Lejeune placed on the USEPA's NPL of contaminated sites	October 1989

\*Refer to [1,4] for details; \*see Figure 1 for location of water-supply areas.

Table S-2. Calibrated model parameter values used to simulate groundwater flow and contaminant fate and transport at U.S. Marine Corps Base Camp Lejeune, North Carolina.<sup>1</sup>

Model	Model layer number <sup>#</sup>						
Parameter⁺	1	2	3	4	5	6	7
Pre-development (stead	y-state) groundwater fl	ow model, condition	ns prior to 1942 — U	niform grid (300 ft x	300 ft cells)§		
Horizontal hydraulic conductivity, <i>K</i> <sub>xx</sub> (ft/d)	0.5–46.8	1.0-20.0	1.0-50.0	1.0–35.0	2.3–50.0	1.0-20.0	20.0
Ratio of vertical to horizontal hydraulic conductivity, Kzz/Kxx	1:10	1:15	1:10	1:15	1:10	1:15	1:10
Infiltration (recharge), <i>I</i> <sub><i>i</i>, <i>j</i></sub> (in./yr)	2.5–22.0	_	_	_	_	_	_
Transient groundwater	flow model, January 19	942–June2008 — Vari	iable-spaced grid (30	00 ft x 300 ft – 50 ft x	50 ft cells)§		
Specific yield, Sy	0.05	-	_	-	_	-	-
Specific stoage, S <sub>s++</sub> (1/ft)	_	1.3x10-5-1.9x10-4	4.3x10-6-3.6x10-5	1.0x10 <sup>-5</sup> –3.8x10 <sup>-5</sup>	4.0x10-6-8.3x10-6	1.4x10-5-3.6x10-5	3.4x10-6-7.7x10-6
Infiltration (recharge), <i>I</i> <sub>i</sub> , (in./yr)	Varies##	_	_	_	_	_	_
Pumpage, Q (ft³/d) §§	Varies	Varies	Varies	Varies	Varies	Varies	Varies
Contaminant fate and tr	ansport models, Janua	ry 1942 1951–June200	08 — subdomain are	a (50 ft x 50 ft cells)	3		
Distribution coefficient, K⊅ (ft³/mg)***							
PCE	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>	5.0x10 <sup>-6</sup>
TCE	5.3x10 <sup>-9</sup>	5.3x10-9	5.3x10 <sup>-9</sup>	5.3x10 <sup>-9</sup>	5.3x10 <sup>-9</sup>	5.3x10 <sup>-9</sup>	5.3x10-9
Benzene	4.0x10-9	4.0x10 <sup>-9</sup>	4.0x10-9	4.0x10-9	4.0x10-9	4.0x10-9	4.0x10 <sup>-9</sup>
Bulk density, $\rho_b$ (g/ft <sup>3</sup> )	47,000	47,000	47,000	47,000	47,000	47,000	47,000
Effective porosity, <i>n</i> <sub>E</sub>	0.2	0.2	0.2	0.2	0.2	0.2	0.2
Biodegradation, $\lambda$ (d <sup>-1</sup> ) HPIA (TCE)	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>	2.0x10 <sup>-3</sup>
HPIA (benzene)	1.0x10-4	1.0x10 <sup>-4</sup>	1.0x10 <sup>-4</sup>	1.0x10 <sup>-4</sup>	1.0x10 <sup>-4</sup>	1.0x10 <sup>-4</sup>	1.0x10 <sup>-4</sup>
HPLF (PCE and TCE)	1.4x10 <sup>-4</sup>	1.4x10-4	1.4x10 <sup>-4</sup>	1.4x10 <sup>-4</sup>	1.4x10 <sup>-4</sup>	1.4x10 <sup>-4</sup>	1.4x10-4
Effective molecular diffusion coefficient, D* (ft²/d)	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>	1.0x10 <sup>-3</sup>

Disperssivity (ft)								
Longitudinal, $\alpha_L$	25		25	25	25	25	25	25
Transverse, $\alpha$ T	2.5		2.5	2.5	2.5	2.5	2.5	2.5
Vertical, $\alpha$ v	0.25		0.25	0.25	0.25	0.25	0.25	0.25
Source concentration, $C$ (mg/L)								
HPIA (TCE)		640	640	640	640	640	640	640
HPIA (benzene-diss	olved)	1.7	—	—	—	—	—	—
HPIA (benzene–LNA	APL)	17	—	—	—	—	—	—
HPLF (PCE)		42-105	33–83	27–66	18-46	6–16	0	0
HPLF (TCE)		256-384	256-384	256-384	256-384	256-384	256-384	256-384

<sup>¶</sup>Refer to [31,35,36] for details;

\*Symbolic notation used to describe model parameters obtained from [34,37,38];

\*See [1] for correlation between geologic and hydrogeologic units and model layers for the Hadnot Point and Holcomb Boulevard areas; refer to [32,35] for details; aquifers are designated as model layers 1, 3, 5, and 7; confining units are designated as model layers 2, 4, and 6;

See Figure SI-2 for groundwater-flow model domain and contaminant fate and transport model subdomains;

<sup>++</sup> Specific storage (S<sub>s</sub>)was specified as input for MOFLOW-2005 [34]; based on cell-by-cell thicknesses, specific storage was varied to assure a constant storage coefficient (or storativity) of 4 x 10<sup>-4</sup> using the equation S = S<sub>s</sub> x b, where S is the storage coefficient (dimensionles), S<sub>s</sub> is specific storage (1/ft), and b is the cell thickness (ft);

#Transient infiltration was varied on a monthly basis using the ratio of monthly precipitation divided by average, long-term precipitation; [35] for details;

<sup>§§</sup>Pumpage varies by month and model cell; refer to [10,29] for details on the derivation of historical monthly water-supply well operations; refer to [35] for details pertaining to assigning monthly water-supply well pumpage to cells and model layers using the multi-node well-flow package for MODFLOW-2005;

\*\*\*Refer to [36] for derivation of K<sub>D</sub> values based on a survey reported in the scientific literature; to convert from model K<sub>D</sub> units of ft<sup>3</sup>/mg to units of L/kg reported in [36], multiply model K<sub>D</sub> values by 28,381,652.21.

				-			
Source Location	Contaminant	Source concentration (μg/L)*	Number of model sources <sup>§</sup>	Source duration			
Hadnot Point Industrial Area (Figure SI3a)							
Building 900 area	TCE	640	3	Jan. 1957–Dec. 1994			
Building 1115	TCE	640	1	Jan. 1951–Jun. 1993			
Building 1401	TCE	640	1	Jan. 1951–Dec. 1993			
Building 1601	TCE	640	1	Jan. 1951–Jun. 1993			
Building 1601	Benzene (dissolved)	1.7	1	Jan. 1951–Dec. 1994			
Building 1613	Benzene (LNAPL)**	17	Multiple**	Jan. 1964–Jun. 2008			
Hadnot Point fuel farm	Benzene (LNAPL)**	17	Multiple**	Jan. 1951–Jun. 2008			
Hadnot Point landfill area (Figure SI3b)							
Source 1 <sup>++</sup>	TCE	256-384±	2	Jan. 1948–Jun. 2008			
Source 2 <sup>++</sup>	PCE	6–105±	2	Jan. 1948–Jun. 2008			

**Table S-3.** Contaminant sources, locations, and durations used for historical reconstruction of TCE, PCE, and benzene concentrations in groundwater at U.S. Marine Corps Base Camp Lejeune, North Carolina <sup>#, ¶</sup>.

<sup>#</sup>See [1] for complete details.

<sup>¶</sup>All model sources are specified concentration; model simulation time is January 1942–June 2008; refer to [31,36] for details.

<sup>+</sup>Current maximum contaminant level (MCL) for TCE, PCE, and benzene is 5 μg/L; density (20°C): TCE, 1.464 g/cm<sup>3</sup>; PCE, 1.623 g/cm<sup>3</sup>; benzene, 0.876 g/cm<sup>3</sup> [2]; solubility in water (25°C): TCE, 1,280 mg/L; PCE, 210 mg/L; benzene, 1,780 mg/L [2].

§ Refer to [31,36] for details.

\*\*Benzene source for model is areally distributed based on LNAPL distribution; refer to [31] for details.

<sup>++</sup>There are no designated building numbers within the Hadnot Point landfill; location of sources based on Installation Restoration Program Site 82 history and contaminant analyses [9] and model calibration [36].

\*Source concentration values vary by model layer, refer to [1 (Table A12),31,36] for details.

	TYPE OF VARIATION						
		Physical parameters	Numerical parameters				
TYPE OF SIMUALTION MODEL	Groundwater flow	Historical monthly pumping: <i>Q</i> <sub>monthly</sub> Input parameters/hydraulics: <i>K</i> <sub>xx</sub>	Cell size: <i>Δx, Δy</i>				
	Contaminant fate and transport	Input parameters/fate and transport: $\rho_{b}$ , $n_{E}$ , $\alpha_{L}$ , $K_{D}$ , $\lambda$ , $C$ Benzene source area and release Trichloroethylene source-release date	Cell size: Δx, Δy Time-step size: Δt				
	Water distribution system*	Pipe roughness: C-factor Storage-tank mixing	Demand factor				

Table S-4. Types of sensitivity analyses applied to models and parameters (from [1]).

\*Sensitivity analyses using water-distribution system model conducted as part of the Tarawa Terrace study area [46].