

Article

# Large-Signal Linearity and High-Frequency Noise of Passivated AlGa<sub>N</sub>/Ga<sub>N</sub> High-Electron Mobility Transistors

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**Abstract:** This study proposes AlGa<sub>N</sub>/Ga<sub>N</sub>/silicon high-electron mobility transistors (HEMTs) grown by a metallorganic chemical vapor deposition (MOCVD) system. The large-signal linearity and high-frequency noise of HEMTs without and with different passivation layers are compared. The experimental data show that the addition of a TiO<sub>2</sub> passivation layer to undoped AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT's increases the value of the third-order intercept point (OIP<sub>3</sub>) by up to 70% at 2.4 GHz. Furthermore, the minimum noise figure ( $NF_{\min}$ ) of the HEMT with TiO<sub>2</sub> passivation is significantly reduced.

**Keywords:** metallorganic chemical vapor deposition (MOCVD); passivation; HfO<sub>2</sub>; TiO<sub>2</sub>; Ga<sub>N</sub>; high-electron mobility transistor (HEMT)

## 1. Introduction

Heterostructure field-effect transistor (HFET) technology has become essential in microwave communication systems [1,2]. III-nitride high-electron-mobility transistors (HEMTs) are of significant importance in the development of next-generation power applications [3–5]. The AlGa<sub>N</sub>/Ga<sub>N</sub> heterostructure has the advantage of large electron velocity and high breakdown electric field. Furthermore, the polar properties of the AlGa<sub>N</sub>/Ga<sub>N</sub> heterojunction allows the formation of two-dimensional electron gas (2DEG). Even without intentional doping, the 2DEG concentrations of the AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs is as high as the order of  $10^{13}$  cm<sup>-2</sup>.

Many passivation materials have been investigated to effectively passivate the surface of AlGaAs/InGaAs [6] and InAlAs/InGaAs/InP [7] HEMTs by using either a wet or dry process. The performance of AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT technology is limited by charge trapping effects. Consequently, various candidates for passivation has been attempted to neutralize the net surface charge arising from the combination of surface states and the polarized barrier [8–18]. Most works focus on the performance of the passivated AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs at room temperature. The room-temperature characteristics of AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT with HfO<sub>2</sub> and TiO<sub>2</sub> passivation were reported [11]. However, AlGa<sub>N</sub>/Ga<sub>N</sub> heterostructure is a promising material system for high-temperature electronics. HEMTs that can operate at high temperatures are helpful in broad extent of applications [13,19]. Consequently, the high-temperature characteristics of the passivated AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs are measured herein. Furthermore, the linearity in power amplifier is important when we move towards the fifth generation (5 G) wireless systems. Increasing the linearity of HEMTs can supply many advantages at the system level. Consequently, the large-signal linearity of the passivated AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs are also studied. To the best of the authors' knowledge, there has not been a comparison of the large-signal linearity and noise figure for the AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs with HfO<sub>2</sub> and TiO<sub>2</sub> passivation. Experimental results demonstrate the high-performance passivated HEMT with stable operation at elevated temperatures up to 420 K. The measured large-signal linearity and high-frequency noise of the passivated HEMT are better than for the identical geometry unpassivated HEMT.



**Citation:** Lin, Y.-S.; Lin, S.-F. Large-Signal Linearity and High-Frequency Noise of Passivated AlGa<sub>N</sub>/Ga<sub>N</sub> High-Electron Mobility Transistors. *Micromachines* **2021**, *12*, 7. <https://dx.doi.org/10.3390/mi12010007>

Received: 19 November 2020

Accepted: 21 December 2020

Published: 24 December 2020

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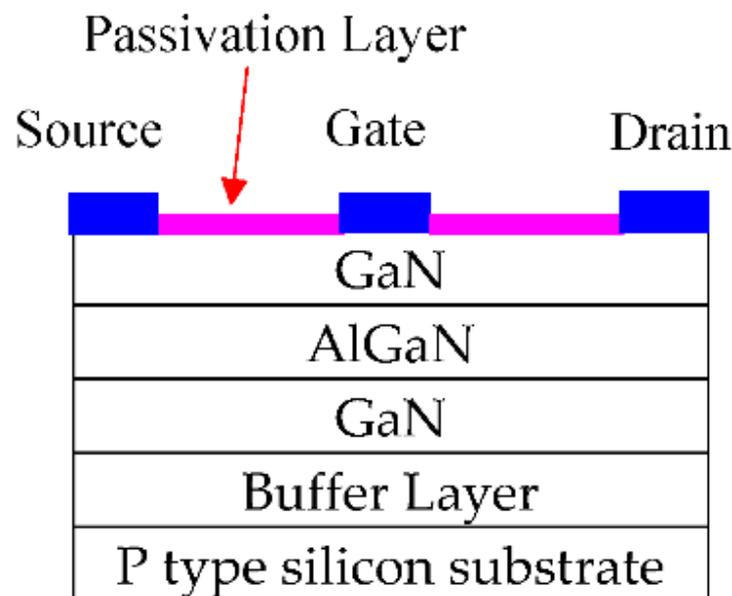


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## 2. Device Structure and Experiments

The studied devices were built on silicon substrate with epilayers that were grown by metal-organic chemical vapor deposition (MOCVD). The layer structure of the HEMT is as follows. First, a buffer was grown, followed by an undoped GaN. Then, 30 nm undoped  $\text{Al}_{0.26}\text{Ga}_{0.74}\text{N}$  layer was formed and capped by a 2 nm GaN layer.

Mesa etching was employed to achieve device isolation. Ti/Al/Au ohmic contacts for the source and drain electrodes were deposited. The gate metallization involved Ni, capped with Au. The HEMT without passivation is the reference HEMT. In our study, the HEMT with  $\text{HfO}_2$  passivation is referred to as  $\text{HfO}_2$ -HEMT. The HEMTs with  $\text{TiO}_2$  passivation is referred to as  $\text{TiO}_2$ -HEMT. The  $\text{TiO}_2$  film was sputtered in a sputtering system using a three-inch high-purity target of titanium dioxide in a mixture of argon and oxygen gas.  $\text{HfO}_2$  film was sputtered using hafnium dioxide. Figure 1 displays the layer structure of the studied HEMTs with passivation. The cross section of the passivated HEMTs was investigated by a transmission electron microscopy (TEM) (JEOL Co., Tokyo, Japan). The probe station was fitted with a heated device stage. The DC characteristics of the HEMTs were measured with a Keithley 4200 semiconductor characterization system (Tektronix, Beaverton, OR, USA). The field-effect transistor had a gate length of 1  $\mu\text{m}$ . The gate-to-drain spacing was 2  $\mu\text{m}$ . The gate-to-source spacing was also 2  $\mu\text{m}$ .



**Figure 1.** Cross section of the studied passivated AlGaIn/GaN high-electron mobility transistor (HEMT).

## 3. Results and Discussion

TEM samples are examined in a JEM-2100F (JEOL Co., Japan) operating at an accelerating voltage of 200 kV. Figure 2 illustrates the TEM cross section of the HEMTs with  $\text{HfO}_2$  and  $\text{TiO}_2$ . The thicknesses of  $\text{HfO}_2$  and  $\text{TiO}_2$  films are approximately 22.65 and 19.79 nm, respectively.

The unpassivated and passivated HEMTs are subjected to high-temperature testing. Figure 3 presents the drain currents ( $I_{\text{DS}}$ ) at different temperatures versus drain-to-source voltage ( $V_{\text{DS}}$ ). The DC measurements are taken as functions of temperatures over the range 300 to 420 K. Figure 4 shows the extrinsic transconductance ( $g_{\text{m}}$ ) and drain current versus gate-to-source voltage of the studied HEMTs at various temperatures. The gate voltage swing (GVS) is defined by the voltage range within which the  $g_{\text{m}}$  value deviates from its maximum value by 20%. The GVS value is increased from 1.7 V to 3.2 V at 300 K after  $\text{TiO}_2$  passivation.  $I_{\text{DS}}$  versus  $V_{\text{DS}}$  at pinch-off conditions and the threshold drain current characteristics at 300 K for the three HEMTs herein were studied [11]. Figure 5a plots

drain current at  $V_{GS} = 0$  V ( $I_{DSS}$ ) versus temperature of the studied HEMTs. Experimental results reveal that  $I_{DSS}$  values of the studied HEMTs are increased when the HEMTs are passivated. The increased drain current density is attributable to the increased sheet electron concentration after passivation [8,11]. The studied three HEMTs depicts good pinch-off characteristics at various temperatures. Increasing the temperature decreases  $I_{DSS}$ . The falloff in drain current density at elevated temperatures result from the degradation of the electron mobility. Furthermore, the threshold voltage ( $V_{th}$ ) is extracted by linear extrapolation of the root of drain current against  $V_g$  curves. The values of  $V_{th}$  of the TiO<sub>2</sub>-HEMT are  $-5.5$ ,  $-5.33$ ,  $-5.2$ ,  $-4.96$ , and  $-4.89$  V at 300, 330, 360, 390, and 420 K, respectively. The magnitude of the  $V_{th}$  value is reduced at high temperature because of the decreased drain current density.

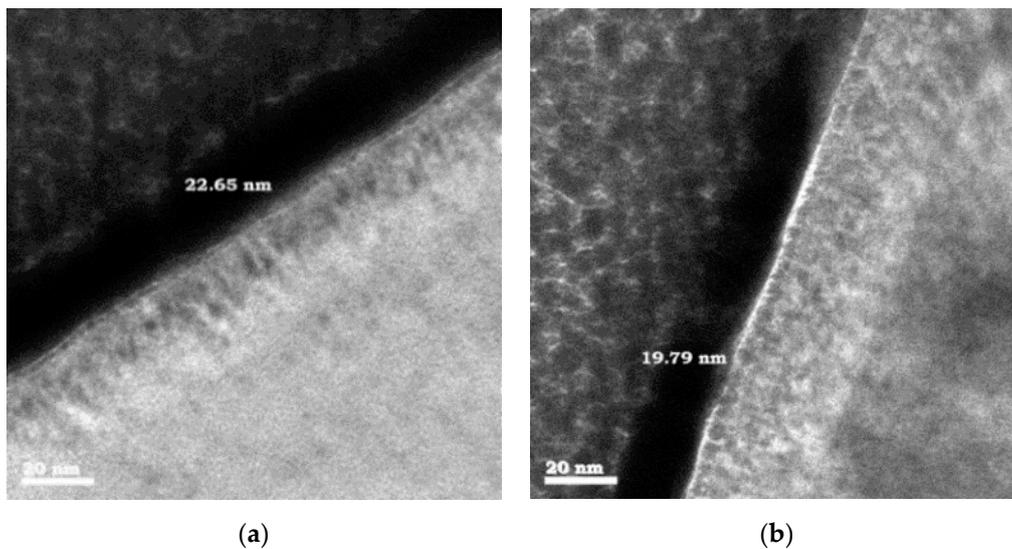


Figure 2. Cross-sectional TEM images of (a) HfO<sub>2</sub>-HEMT and (b) TiO<sub>2</sub>-HEMT.

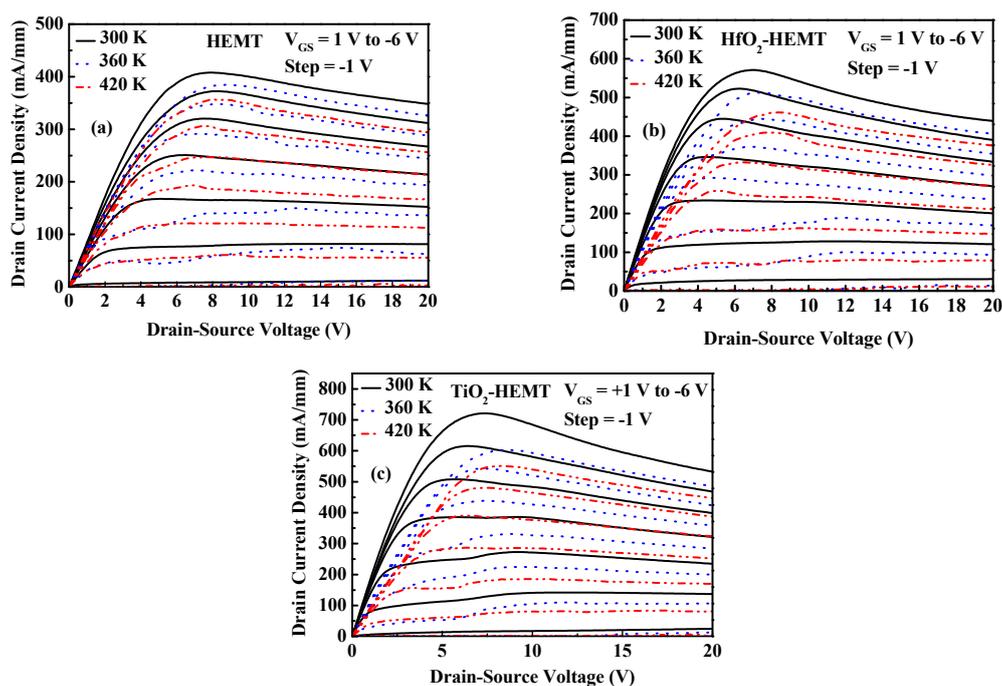
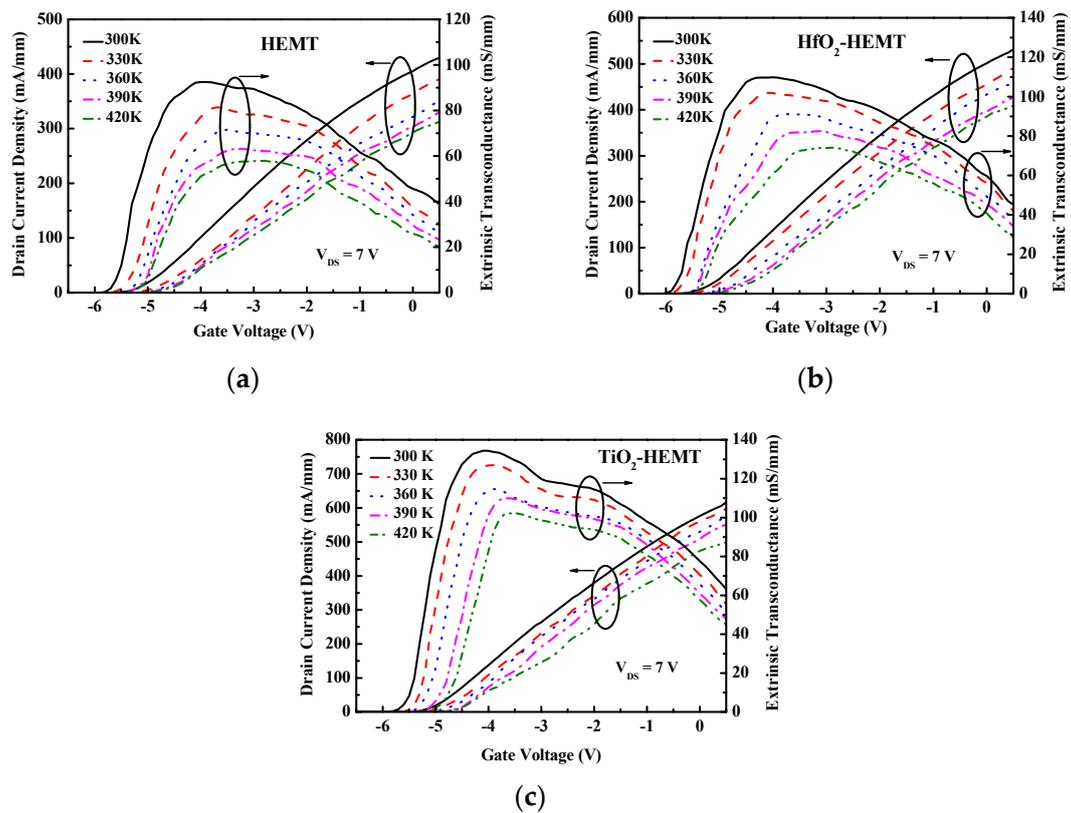
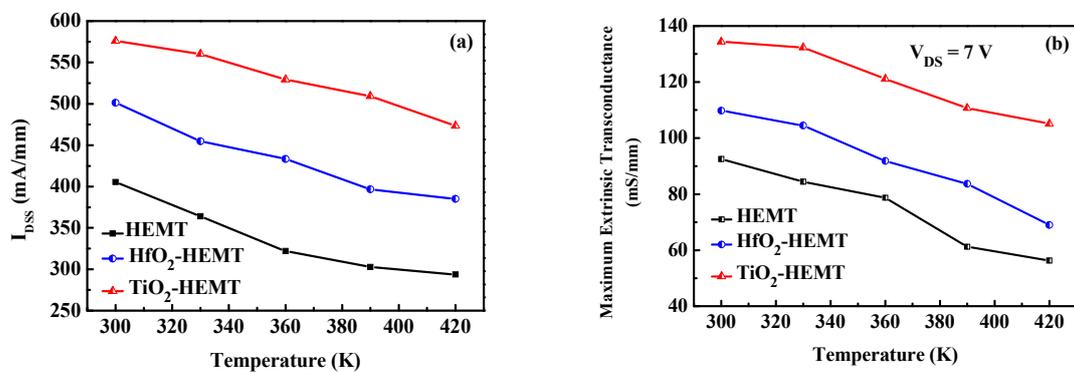


Figure 3. Family of drain-source output curves of (a) HEMT, (b) HfO<sub>2</sub>-HEMT, and (c) TiO<sub>2</sub>-HEMT at various temperatures.



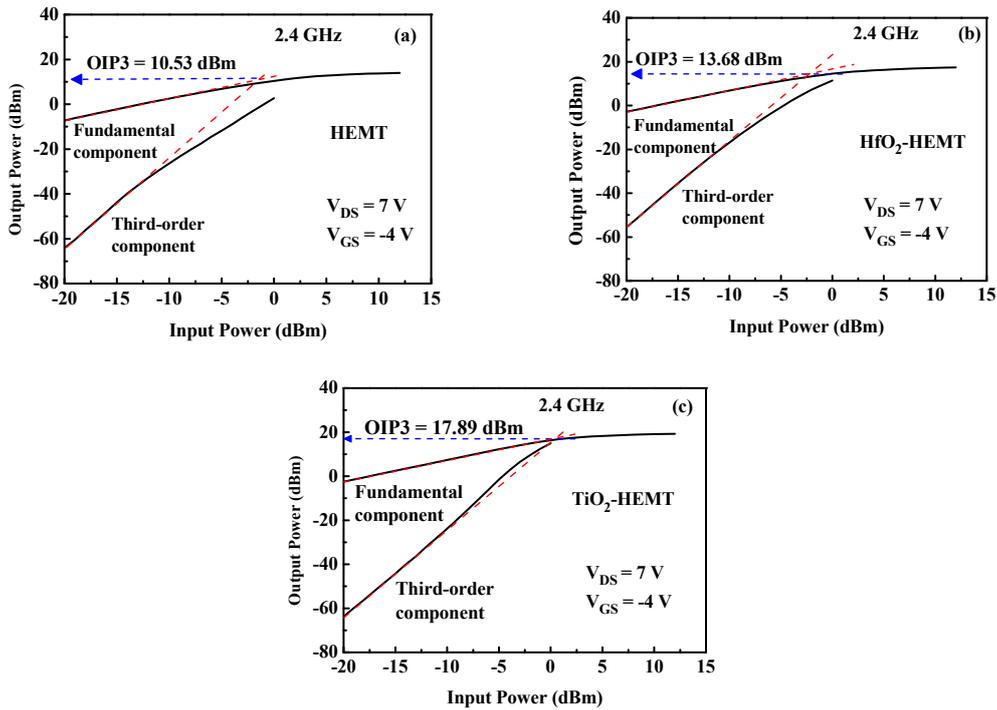
**Figure 4.** Extrinsic transconductance and drain current characteristics of (a) HEMT, (b) HfO<sub>2</sub>-HEMT, and (c) TiO<sub>2</sub>-HEMT at various temperatures.



**Figure 5.** (a)  $I_{DSS}$  and (b)  $g_{m,max}$  of the studied HEMTs at various temperatures.

Figure 5b plots the maximum extrinsic transconductance ( $g_{m,max}$ ) versus temperature of the investigated HEMTs. When the temperature is increased, the maximum extrinsic transconductance varies in the same tendency as  $I_{DSS}$ . At 420 K, the  $g_{m,max}$  values for HEMT, HfO<sub>2</sub>-HEMT, and TiO<sub>2</sub>-HEMT are 56.3, 69, and 105 mS/mm, respectively. Experimental results demonstrate the TiO<sub>2</sub>-HEMT perform well even at high temperatures.

Two-tone intermodulation distortion is measured to demonstrate the large-signal linearity performance. Figure 6 shows the fundamental and third-order output powers versus input power of the studied devices. The red dashed lines are extrapolated to predict the intersection at the third-order intercept point (OIP3). The values of OIP3 are 10.5, 13.7, and 17.9 dBm, respectively. HfO<sub>2</sub> passivation increases the OIP3 value by around 30% and TiO<sub>2</sub> passivation increases it by 70%. The large-signal linearity of the HEMT is significantly improved when the HEMT is passivated by TiO<sub>2</sub>. The improved device linearity of the TiO<sub>2</sub>-HEMT is attributed to increased  $g_{m,max}$  [18] and GVS values [20].

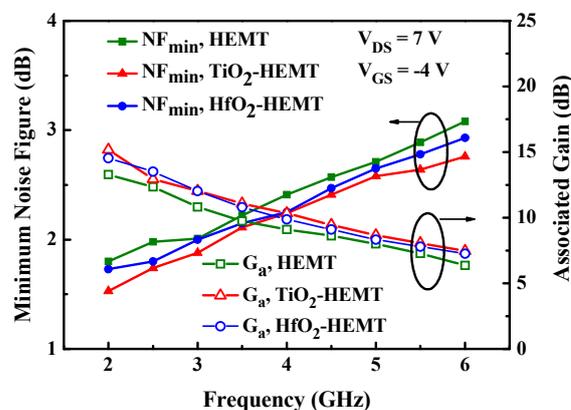


**Figure 6.** Fundamental output power and third-order intermodulation component of (a) HEMT, (b) HfO<sub>2</sub>-HEMT, and (c) TiO<sub>2</sub>-HEMT.

Noise figure is measured over the 2–6 GHz frequency range using an ATN NP5B noise parameter test set in conjunction with the HP-8510C network analyzer. Figure 7 shows the minimum noise figure ( $NF_{min}$ ) and associated power gain ( $G_a$ ) versus frequency for the studied HEMTs. Figure 7 reveals that the relationship between the noise and frequency is near linear. Quantitatively,  $NF_{min}$  is given by [21–23]

$$NF_{min} = 1 + 2\pi f k C_{gs} \sqrt{\frac{R_s + R_g}{g_m}} \quad (1)$$

where  $f$  is frequency;  $k$  is the Fukui constant;  $C_{gs}$  is the input gate-source capacitance;  $R_s$  is the source series resistance, and  $R_g$  is the gate series resistance. The  $NF_{min}$  values of HEMT, HfO<sub>2</sub>-HEMT, and TiO<sub>2</sub>-HEMT are 1.94 dB, 1.79 dB, and 1.68 dB. The TiO<sub>2</sub>-HEMT has the smallest  $NF_{min}$  of the three devices because it has the highest  $g_m$ . Furthermore, the associate gain of the TiO<sub>2</sub>-HEMT is also improved.



**Figure 7.** Minimum noise figure and associated gain of the studied (a) HEMT, (b) HfO<sub>2</sub>-HEMT, and TiO<sub>2</sub>-HEMT.

#### 4. Conclusions

AlGaN/GaN/silicon grown by MOCVD have been successfully fabricated and measured. The high-temperature characteristics of the proposed devices are investigated. TiO<sub>2</sub>-HEMT exhibits the best large-signal linearity of the studied devices. Furthermore, the  $NF_{\min}$  value of TiO<sub>2</sub>-HEMT is smallest of the studied devices herein.

**Author Contributions:** Investigation, Y.-S.L.; data curation, S.-F.L.; writing, Y.-S.L.; supervision, Y.-S.L. All authors have read and agreed to the published version of the manuscript.

**Funding:** This research was funded by the Ministry of Science and Technology, Taiwan, grant number MOST 108-2221-E-259-002-MY2.

**Conflicts of Interest:** The authors declare no conflict of interest.

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