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Uncertainty Assessment of Differential Absorption Lidar Measurements of Industrial Emissions Concentrations

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Abstract: Differential absorption lidar (DIAL) has been shown to be a very effective technique for the location and quantification of emissions of pollutants and greenhouse gases at industrial facilities. Several field trials have demonstrated the DIAL system performances and contributed to the development of the DIAL methodology, which is the basis of the protocols described in the European Standard EN 17628. While numerous papers have focused on different aspects of DIAL uncertainties, a rigorous propagation of the uncertainties in the DIAL equation has not been found. In this study, all the uncertainty sources contributing to a DIAL concentration measurement are assessed and the impact they have on the calculation of the mass emission rate. We derive the equations for both a DIAL system path-concentration integral and concentration uncertainties. The results from a methane measurement are presented, showing that for a signal to noise ratio on the backscattered lidar signals of 500, the path-concentration integral standard uncertainty is 2.3 ppb km and the concentration standard uncertainty is 92 ppb over a sampling spacing of 45 m. An equation is also presented enabling calculation of the contribution of the concentration uncertainty to the mass emission rate uncertainty.

Keywords: DIAL; industrial pollutants; GHG; methane; uncertainty



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1. Introduction

The European Union, as part of its Industrial Emissions Directive 2010/75/EU, has published the Best Available Techniques (BAT) reference document for the refining of mineral oil and gas [1]. The BAT conclusion includes differential absorption lidar (DIAL) as a technique to monitor diffuse volatile organic compound (VOC) emissions from an industrial site. In response to this, the European Committee for Standardisation (CEN) produced a new standard, EN 17628 [2], for the use of systems such as DIAL to monitor the fugitive emissions of VOCs.

DIAL is a remote sensing laser-based technique capable of making spatially resolved measurements of concentrations of a target gas along the path of a laser beam transmitted into the atmosphere [3]. It combines the use of light detection and ranging (lidar) to measure back-scattered light from the atmosphere and the targeted species at two known, pre-selected, wavelengths of light. One of these (λ_{on}) is strongly absorbed by the species of interest while the second pulse (λ_{off}) is at a wavelength that has a much weaker absorption. The difference in the absorption of the two wavelengths allows the concentration of the gas to be calculated along the optical path. The ability to scan the optical measurement beam through a vertical plane in the atmosphere enables the gas concentrations to be mapped within the atmosphere and the emission rates to be determined when the concentration data are combined with wind data.

The mobile DIAL systems developed at the National Physical Laboratory (NPL) for the remote measurements of pollutants and greenhouse gases have been used worldwide for over 30 years at different industrial facilities such as refineries, liquid natural gas terminals, tank farms, biogas, wastewaters, and landfills utilising both the ultraviolet (UV)

and infrared (IR) regions for different species such as volatile organic compound (VOCs), methane, ethane, SO₂, NO_x, HCl, and benzene [4–7].

In a DIAL system, the two wavelengths are selected to have a small wavelength separation to minimise differences in atmospheric scattering and interference compounds and therefore minimise the effect on the concentration measurements from the parameters describing atmospheric variability in the lidar equation [3]. These terms are assumed to be the same for both on and off wavelengths and are then cancelled by taking the ratio of the on and off returned signals in the DIAL Equation (1). The potential sources of uncertainties from this assumption, such as the backscatter and extension coefficients in the lidar equation, have been extensively discussed by previous authors [8–14]. These works were focused on DIAL nadir or zenith measurements, hence looking at backscatter and extension coefficients variations over several kilometres into the troposphere and lower stratosphere rather than measurements at industrial facilities over just a few hundred meters within the boundary layer. In such applications plumes of gases, vapour and heat sources at industrial facilities can limit the sensitivity of the DIAL as a consequence of differences in the backscatter coefficients between the on and off beams. This can be caused by a number of factors such as imperfect beam overlap, movement of the atmosphere, inhomogeneities between the on and off pulses, and differences between the detection system collection efficiencies due to the asymmetries in the transmitted on and off beams as described in detail in the work of Walmsley and O'Connor [15]. Most previous DIAL uncertainty papers addressed the variance of the return on and off signals as proportional to the signal to noise ratio (S/N) of the detector system and used the detector specs to characterise the noise [8,9,11,12,15–19]. Various authors also addressed the effect of different averaging methods of the on and off return pulses. The conclusion was that averaging the on and off pulses before processing the data (log of the ratio of the on and off signals) performs well in a strong signal regime. This method holds some advantages over other averaging methods when averaging the signal offsets as it deals with negative values better. This averaging method also reduces the effect of high-frequency fluctuations and it is more useful in practical situations [20–24]. It was also observed by Lindstrom et al. [23] that this averaging method performance is not affected by fluctuations due to the variation in the concentration levels as the plume is traversed.

This paper is concerned with deriving for the first time the exact parametric functions of the uncertainties in the DIAL path-concentration integral, concentration, and mass emission rates starting from the DIAL Equation (1). All uncertainty sources are considered not just the detector S/N. We also do not assume that the range dependence of the signal is not significant [16], which we will show in this paper not to be entirely correct, particularly for a DIAL system optimised for industrial emission measurements to work at relatively short distances from the DIAL. Throughout this paper, an example DIAL methane measurement is used to present the results. However, all the calculations reported in this paper are applicable to any DIAL measurement that uses Equations (1) and (2). The specific results for the methane example are also applicable to other species measured at similar IR wavelengths such as VOCs and ethane. Methane was selected since in recent years, the NPL DIAL system has increasingly been used for methane emission measurements and validation work mainly at landfill and gas facilities [7,25,26]. This is a critical tool for the industry to limit global warming to well below two degrees pre-industrial levels [27] and to meet the Global Methane Pledge to reduce methane emissions at least 30% from 2020 levels by 2030 [28] and their various strategy targets such as achieving the Oil and Gas Methane Partnership (OGMP) 2.0 gold standard [29].

2. Materials and Methods

Previous work from Robinson et al. [6] and Innocenti et al. [7] described the NPL DIAL system deployed at industrial facilities. The current NPL DIAL system uses a neodymium-doped yttrium aluminum garnet (Nd-YAG) pumped tunable laser with a repetition rate of 10 Hz and a pulse length < 10 ns, providing energies for the frequency conversion stages to

achieve the required output energy of ~ 15 mJ with a bandwidth of <0.1 cm^{-1} for the methane, ethane, and VOCs absorption lines at ~ 3000 cm^{-1} . The returned atmospheric backscatter is collected by a 500-mm-diameter Dall Kirkham telescope, which is then collimated and focused onto a 1-mm-diameter 4-stage thermoelectrically cooled HgCdTe photovoltaic detector coupled with a transimpedance preamplifier with selectable gain (1 to 100) and bandwidth (1.5, 15, and 200 MHz) settings. These signals are then digitised using a 40 MHz 12-bit transient digitiser that provides a sample for every 3.75 m of path length.

A small fraction of the output beam is directed into two pyroelectric detectors (PEDs). One detector is used as a continuous monitor of the differential absorption between the on and off pulses using an in-line calibration gas cell filled with known concentrations of the targeted species traceable to national standards. These data are used to normalise the differential absorption coefficient ($\Delta\alpha$) for each path-line measurement, ensuring no assumptions are made about the spectral performance or stability of the optical source. The other PED detector is used to provide a value of the transmitted energies (p_{on} and p_{off}), used for normalisation of the associated on and off return signals to compensate for any variation in the output beam energy. Equation (1) shows the DIAL path-concentration integral column $CL(x)$ as a function of the range x from the DIAL along the scanning line, calculated by dividing the logarithm of the ratio of the signals ($f_{on}(x)$ and $f_{off}(x)$), after the offset subtraction (o_{on} and o_{off}) and normalisation for the transmitted energies (p_{on} and p_{off}), by $\Delta\alpha$. The offsets are typically estimated by either averaging the return signal before the pulse is fired or by averaging the far-field return signal where the backscatter intensity is effectively zero:

$$CL(x) = \frac{1}{2 \Delta\alpha} \log \left(\frac{f_{off}(x) - o_{off} p_{on}}{f_{on}(x) - o_{on} p_{off}} \right) \quad (1)$$

Measurements are based on signal averaging over n laser shots, typically 250 for each on and off return signal, with the averaging being carried out before processing of the data, i.e., the $f_{on}(x)$ and $f_{off}(x)$ values are the average over n pulses. The concentration $C(x)$, in the case of the discrete data points, is calculated as the difference between two data points separated by the sampling spacing l :

$$C(x) = \frac{CL(x + l/2) - CL(x - l/2)}{l} \quad (2)$$

For measurements at industrial facilities, the DIAL system is generally optimised to detect emissions at an approximately 100 to 300 m distance from the DIAL. Range-resolved remote DIAL measurements that enable total site emissions and area-specific emissions to be determined with no disruption to normal operational activities are performed with the DIAL system typically positioned at a suitable location downwind of the area to be measured. A DIAL scan is recorded by scanning the laser beam in a vertical plane through the atmosphere, performing a series of range-resolved concentration measurements at different vertical elevation angles. These are then combined to provide a 2D concentration map distribution of the targeted species in the vertical measurement plane [6,7]. The concentration plane is then combined with the horizontal wind vector perpendicular to the measurement plane to determine the mass emissions distribution in kg/h after using the targeted gas density to convert the ppm concentration measurement to kg/m^3 .

2.1. Technique Validation

The DIAL approach in the CEN Standard EN 17628 [2] is based on the NPL DIAL method that has been developed over a number of years with supporting evidence from two field campaigns carried out during the standardisation work to validate the measurement techniques [30]. Several field intercomparisons have been carried out in the past involving the DIAL system such as at landfill sites in France [31] and the US [32]. Several validation studies have also been carried out over the last few years showing the standard uncertainty of a set of at least four DIAL scans, estimated based on the standard deviation of the

individual emission rate measurements from which each mean emission rate value has been determined, to be representative of the measurement uncertainty [30,33,34]. These studies confirmed the dominant DIAL uncertainty sources have a random behaviour, with the systematic biases in the DIAL measured emission estimates being less than 4% and each set of DIAL measurements has shown agreement with known emission sources of typically between 5% and 20%. The reported experimental DIAL uncertainty encapsulates variability occurring during the measurements, which includes the measurement itself (random DIAL concentration measurement uncertainty), variability in the source emissions, and variability in the wind direction and speed used since for each scan, a different wind profile is calculated from the wind data collected on site.

While there is empirical evidence that the DIAL uncertainty can be estimated from the standard deviation of repeat scans, it is important to understand all the uncertainty sources of a DIAL system and the focus of this paper is to fully characterise for the first time the DIAL system concentration uncertainty. This can be derived parametrically from the uncertainties of the seven parameters defined in Equation (1) and this enables its contribution to the mass emission rate uncertainty to be determined. The impact of the uncertainties from the meteorological measurements to the mass emission rate uncertainty will be addressed separately in another paper.

2.2. Quality Assurance Procedures

In addition to the on-line spectroscopic and power normalisation processes discussed earlier, it is important to review the quality assurance (QA) procedures that are used to address uncertainties that can arise from the assumption made when deriving Equation (1) from the lidar equation. Effects due to atmospheric fluctuations, beam quality, and alignment have been described by Walmsley and O'Connor [15]. The authors also reported examples of return signals manifesting these issues. Some of these issues can be addressed by the technology improvement over the last few decades while others can be addressed by following QA procedures both at the data acquisition and at the analysis stages. A significant issue arises when atmospheric fluctuations due to plumes of gases, vapour, and heat sources cause the detector signal to saturate, on both the on and the off channels. This produces a clearly incorrect path-concentration integral column equal to zero. Partial saturation of only a few of the n laser shots may be less obvious; however, it should always be possible to observe an unphysical dip in the integrated concentration column content if partial saturation has occurred. While in the past, the dynamic range of the detection system was the main limiting factor, the detector and amplifier system used recently allows a selectable gain up to a factor 100, accommodating the signal without saturation in most scenarios. In the field, it is therefore important for the DIAL operators to monitor the return signals and to change the amplifier gain whenever an increase in the backscatter is observed to ensure the strongest signals do not saturate.

The QA checks in place at the analysis stage should also ensure that, if saturation is observed in the integrated concentration column, only the part outside this region is analysed. The DIAL scan should be deemed invalid whenever the targeted measurement area emission falls inside the saturated region. This situation is usually avoided at the measurement stage by the operators varying the scanning plane, for example, by scanning at a sufficient distance downwind of heat sources such as flares to minimise the effect of the heat in the backscatter signal. The beam asymmetries and misalignments would have no effect if the on and off beams were collected with equal efficiency. If this is not the case, any asymmetries arising from misalignment or asymmetrical beam profiles can lead to a range-dependent offset in the path-concentration integral column [15]. In most cases, the collection efficiency is fixed and such offsets or 'shapes' in the path-concentration integral column can be removed at the analysis stage by subtracting a clean-air column. A non-zero clean air column could also be due to ambient levels of the target species or an interference species. QA procedures are also in place in the field to carefully align the on and off beams to either minimise this issue or to optimise the collection at a certain range depending on

where the targeted area is located with respect to the DIAL. For example, if the emission from the targeted area was expected to be detected at 200 m from the DIAL, then it would be possible to optimise the return signals in that region while moving the imbalance in the collection efficiency and the offset at shorter ranges where it has no impact on the measurement.

By following such QA procedures, a DIAL system at industrial facilities can operate, in the vast majority of the cases, under experimental conditions where the measured concentration uncertainty is dominated by the uncertainties of the variables defined in Equation (1), and the following analysis is based on this assumption.

2.3. Sources of Uncertainty

In Equation (1), there are seven sources of uncertainty: $u(\Delta\alpha)$, $u(f_{on})$, $u(o_{on})$, $u(p_{on})$, $u(f_{off})$, $u(o_{off})$, and $u(p_{off})$. As described in detail in Appendix A, these uncertainties can be propagated in quadrature to calculate in order:

- The total uncertainty of the DIAL path-concentration integral $u(CL(x))$;
- The concentration uncertainty $u(C(x))$;
- The concentration plane uncertainty $u(C_{plane}(x))$;
- The emission rate uncertainty due to the DIAL concentration measurement $u_c(M(x))$.

It should be noted that the calculations and values provided in this paper are for standard uncertainties, unless otherwise specified. To support this DIAL system uncertainty work and to aid the visualisation of the results from the analysis in Appendix A, both on and off DIAL return signals can be fitted using the empirical function given in Equation (A41) in Appendix B. The result of fitting this function to an example methane return signal, $f_{on}(x)$, is shown in Appendix B (Figure A1). Fitting both return signals, $f_{on}(x)$ and $f_{off}(x)$, enables derivation of the parametric functions for the equations presented in this work. The main assumption made by propagating all the uncertainties in quadrature is that these uncertainties, particularly from the return signals in Equations (1) and (2), are independent and non-correlated [16,35]. In the case of atmospheric backscatter, the noise on successive n DIAL pulses used to calculate the average return signals $f_{on}(x)$ and $f_{off}(x)$ can be assumed to be uncorrelated; such temporal independence from pulse to pulse allows the average signals to reduce the standard deviation with an $n^{-1/2}$ dependence [20–22]. The residual noise, calculated as the difference between each return signal data point and the corresponding fitted value, showed similar noise at all ranges and a Gaussian-like distribution, as shown in Figures A2 and A3 in Appendix B, indicating a lack of spatial correlation. The return signals are often smoothed by combining several adjacent range bins, typically between 3 and 7 bins, that would cause correlation between data points separated by less than ~ 25 m. However, emissions at industrial sites are usually analysed over sampling spacings $l > 25$ m. As noted in the previous section, one of the analysis QA methods involves a clean air column subtraction; this would introduce an additional source of uncertainty, which is not covered in this paper.

3. Results

3.1. Determination of Uncertainty Sources

The values of the uncertainty sources in Equation (1) can be estimated from the experimental data. For the scanning line shown in Figure A1, the signal zero offset was calculated by averaging the data recorded from about 1700 to 3200 m from the DIAL. The standard uncertainties of the offsets $u(o_{on})$ and $u(o_{off})$ can be estimated by calculating the standard deviation of the mean of these datapoints; the uncertainty of the offset of the example scanning line was 1.0 μ V. The standard uncertainties of the return signals $u(f_{on})$ and $u(f_{off})$ can be estimated by calculating the standard deviation of the detector noise in the region where the back-scatter signal is effectively zero, typically in the far-field at distances further than 1500 m, the same region where the offset is calculated. The assumptions are that the signal noise has a Gaussian-like distribution and that it is the same in the whole region, which is confirmed to be the case by the plots shown in Figures A2 and A3. The

noise uncertainty for the example signal was 22 μV , which is mainly dominated by the detector and amplifier noise averaged over n laser shots (250 in this example), but it also includes any other electrical noise in the system such as noise due to the transient digitiser. The standard uncertainties of the transmitted energies $u(p_{on})$ and $u(p_{off})$ can be estimated by calculating the standard deviation of the mean of a set of n pulses at constant energy. This is typically about 50–100 μV , 86 μV for the example scanning line, for energy readings that are typically in the 50–250 mV range. The methane $\Delta\alpha$ value used for this work is ~ 0.6 (ppm.km) $^{-1}$ with an uncertainty u_α defined in Equation (A3) of about 1.1%. The absorption coefficient and associated uncertainty were derived from the analysis of several calibration cell scans acquired over 15 years using reference gases with a traceable amount of methane. The ratio of the difference in the transmittance between the λ_{on} and λ_{off} wavelengths is recorded in each calibration scan of a reference gas concentration in a cell of a known length. From these values, it is possible to calculate for each scan a value of $\Delta\alpha$. The average value used in this work was calculated from all the calibration cell scans analysed and the uncertainty was derived from the standard deviation of the mean of this set of scans.

3.2. Mass Emission Rate Uncertainty

The mass emission rate $M(x)$ is calculated by combining the DIAL concentration measurements with the meteorological measurements as described in Equation (A35). The plane concentration C_{plane} measured within an area A of a vertical measurement plane using s scanning lines is defined in Equation (A32). Using the approximated Equation (A34) for the plane concentration uncertainty due to the DIAL system concentration measurement, $u_{sys}(C_{plane}(x))$, it is possible to rewrite the mass emission rate uncertainty due to the DIAL system concentration measurement $u_{sys}(M(x))$ defined in Equations (A40) as:

$$u_{sys}(M(x)) \cong \frac{u_{sys}(C(x))}{\sqrt{s}} A v \sin \theta, \quad (3)$$

where $u_{sys}(C(x))$ is defined in Equation (A15) as the system concentration uncertainty for a scanning line at a range x from the DIAL, v is the wind speed, and θ is the angle between the wind direction and the DIAL vertical measurement plane. It should be noted that the dependent variable x in Equation (3) is the range from the DIAL that defines the location of the plane, the region within which the concentration is determined. The size of the plane A is related to the sampling spacing l over which the concentration of each scanning line (s) is determined. Therefore, the uncertainty in $M(x)$ is related to the region over which $C(x)$ are determined.

As described in Section 2 and Appendix A, the targeted gas density must be added to Equation (3) in order to convert the concentration expressed in ppm to kg/m^3 when the absorption coefficient unit used is (ppm km) $^{-1}$. The assumptions made in Equation (3), from Equation (A34), are that each of the s scanning lines is analysed in the same range l and each of them has a similar $u_{sys}(C(x))$ value. The former is typically correct when analysing the emission from a specific plume or targeted area while the latter assumption is reasonable since the same range l is analysed and both the detector signal uncertainty and signal return shapes are unlikely to change significantly over the period (10 to 15 min) a DIAL scan is recorded. The contribution of u_α is constant across the measured plane; it is proportional to $M(x)$ and independent of the number of scanning lines s used in the scan. It can therefore be added in quadrature to $u_{sys}(M(x))$, which is independent from $M(x)$, to calculate the total emission rate uncertainty due to the DIAL concentration measurement, $u_c(M(x))$ as shown in Equation (A39).

Typically, a DIAL scan is made up by a minimum of 7 scanning lines up to a maximum of 20, with $s = 10$ being a typical value. An example analysis spacing of $l = 45$ m can be chosen as a representative of a plume dimension typically observed with DIAL at industrial facilities. For simplicity, we can assume that such an emission plume was measured over an area $A = 45 \text{ m} \times 45 \text{ m}$. To define a DIAL system performance and therefore be able

to compare different DIAL systems and species measured, a fixed S/N value should be defined as a reference. In the DIAL system examined in this paper, an S/N better than 500 is achieved in favourable atmospheric conditions at a typical measurement range when averaging $n = 250$ laser shots. It should also be noted that an $S/N = 500$ can also be achieved in unfavourable atmospheric conditions by simply increasing the number laser shots n . The maximum value in the return signal shown in Figure A1 is at a distance $x \sim 100$ m from the DIAL. This value can be normalised so that its $S/N = 500$ and both $f_{on}(x)$ and $f_{off}(x)$ signals can then be normalised using the same factor.

Figure 1 shows $u_c(M(x))$ (red line) and $u_{sys}(M(x))$ (blue line) for an example 50 kg/h plume measured with $l = 45$ m, $A = 45$ m \times 45 m, $s = 10$, $v = 4$ m/s, $\theta = 90^\circ$, and $S/N = 500$ at $x \sim 100$ m. The contribution of u_α to $u_c(M(x))$ is significant at distances from the DIAL where S/N is bigger and $u_{sys}(M(x))$ is smaller while it decreases at further distances from the DIAL since the intensity of the return DIAL signals decreases and $u_{sys}(M(x))$ becomes dominant. Equation (A39) shows that the impact of u_α is expected to decrease as the plume mass emission rate decreases. This is confirmed in Figure 2, where the contribution of u_α is negligible for a 15 kg/h plume as $u_c(M(x)) \sim u_{sys}(M(x))$ through the whole range. The value of $u_{sys}(M(x))$ at $x \sim 100$ m from the DIAL where the $S/N = 500$ is ~ 0.6 kg/h and it is independent from the mass emission rate measured. However, this value depends on l and A , for example, it would decrease to ~ 0.3 kg/h if the plume was analysed with $l = 30$ m and $A = 30$ m \times 30 m.

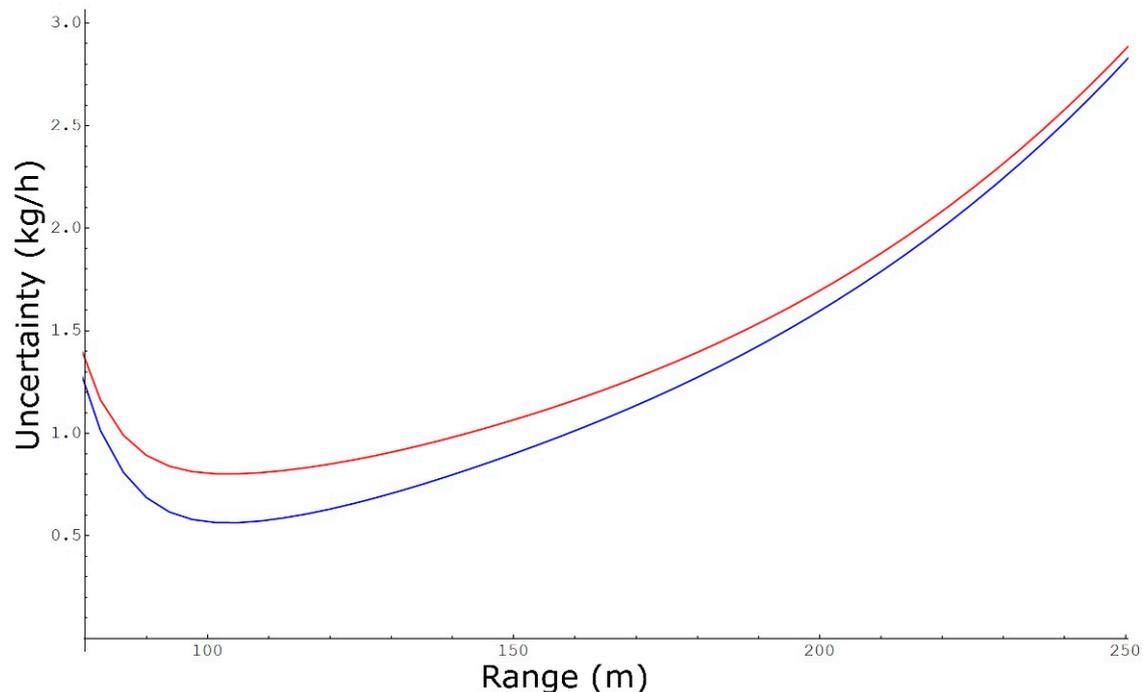


Figure 1. $u_{sys}(M(x))$ (blue line) and $u_c(M(x))$ (red line) for a 50 kg/h plume up to 250 m from the DIAL for $l = 45$ m, $A = 45$ m \times 45 m, $s = 10$, $v = 4$ m/s and $\theta = 90^\circ$, and $S/N = 500$ at $x \sim 100$ m. Note that the range starts at $x \sim 80$ m since this is equivalent, for $l = 45$ m, to starting the analysis just after the near field backscatter light at ~ 60 m distance from the DIAL ($x - l/2$).

Figure 3 shows the uncertainty fractions $u_{sys}(M(x))/M(x)$ (yellow line) and $u_c(M(x))/M(x)$ (blue line) as a function of the plume mass emission rate measured at $x \sim 100$ m from the DIAL, where $S/N = 500$ for $l = 45$ m, $A = 45$ m \times 45 m, $s = 10$, $v = 4$ m/s, and $\theta = 90^\circ$. For mass emission rates less than ~ 15 kg/h, $u_{sys}(M(x))$ is the dominant term while at higher emission rates, u_α becomes the dominant term in $u_c(M(x))$. In this exemplar case, a plume mass emission rate of 1.5 kg/h has an uncertainty fraction lower than 40%, which quickly decreases below 10% for mass emission rates higher than ~ 6 kg/h.

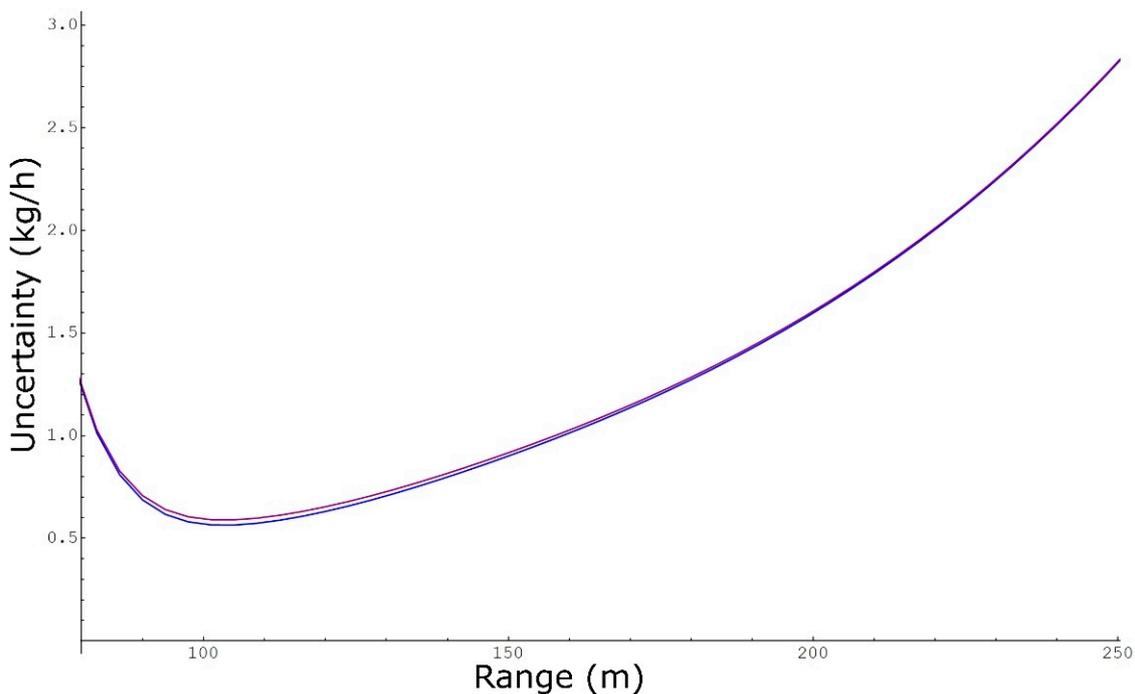


Figure 2. $u_{sys}(M(x))$ (blue line) and $u_c(M(x))$ (purple line) for a 15 kg/h plume up to 250 m from the DIAL for $l = 45$ m, $A = 45$ m \times 45 m, $s = 10$, $v = 4$ m/s and $\theta = 90^\circ$, and $S/N = 500$ at $x \sim 100$ m.

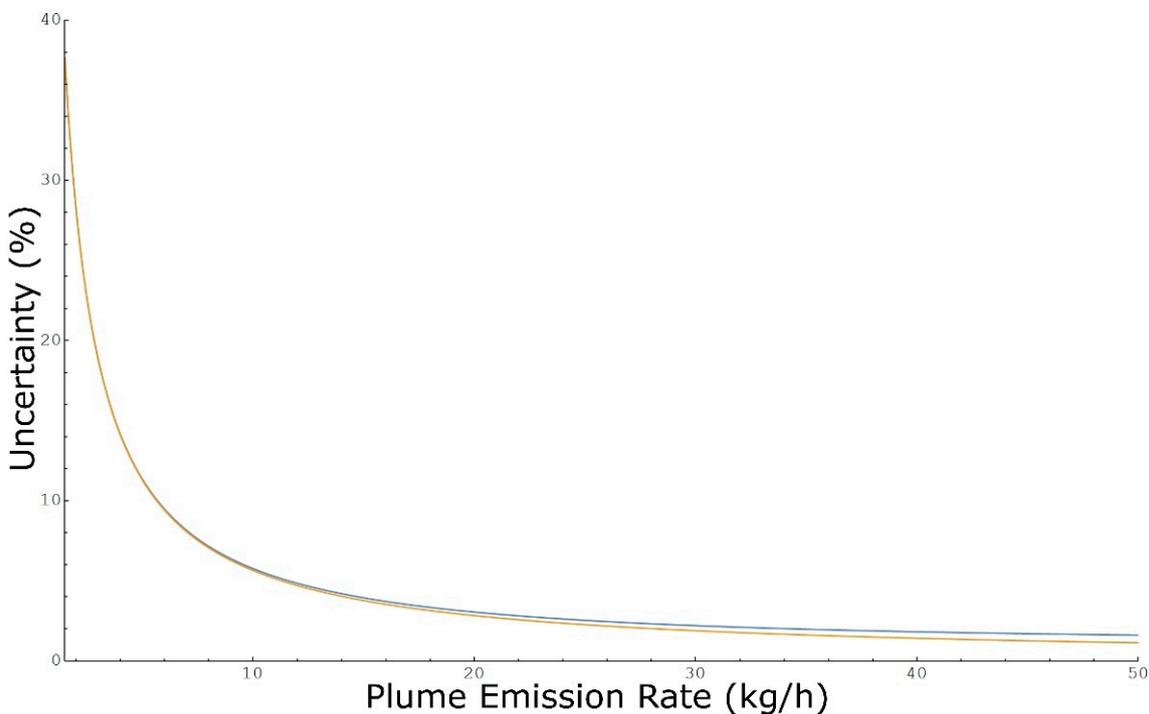


Figure 3. $u_{sys}(M(x))/M(x)$ (yellow line) and $u_c(M(x))/M(x)$ (blue line) in the function of the plume mass emission rate centred at $x \sim 100$ m from the DIAL ($S/N = 500$) for $l = 45$ m, $A = 45$ m \times 45 m, $s = 10$, $v = 4$ m/s, and $\theta = 90^\circ$.

It should be noted the uncertainty plots reported will vary according to Equation (3) when using different values of l , A , s , v , and θ . Moreover, all the uncertainties reported here are from a DIAL scan, not a DIAL measurement, that is defined as the average emission rate measured from at least four DIAL scans. The uncertainty of a DIAL measurement

and the impact of the uncertainties from the meteorological measurements as defined in Equation (A36) will be addressed in a follow-up paper.

3.3. Concentration Uncertainty

The total concentration uncertainty $u(C(x))$ for a DIAL concentration measurement line s can be derived from Equation (A16):

$$u(C(x)) = \sqrt{u_{sys}(C(x))^2 + C(x)^2 u_{\alpha}^2} \quad (4)$$

The impact of u_{α} varies depending on the measured plume concentration and the distance of the centre of the plume from the DIAL as can be seen in Figures 4 and 5. Figure 4 shows $u(C(x))$ (red line) and $u_{sys}(C(x))$ (blue line) for an example 10 ppm concentration plume measurement with $l = 45$ m and $S/N = 500$ at $x \sim 100$ m. The contribution of u_{α} to $u(C(x))$ is significant at distances from the DIAL where S/N is bigger and $u_{sys}(C(x))$ is smaller while it decreases at further distances from the DIAL since the intensity of the return DIAL signals decreases and $u_{sys}(C(x))$ becomes dominant. Equation (4) shows that the impact of u_{α} is expected to decrease as the concentration decreases. This is confirmed in Figure 5, where the contribution of u_{α} is negligible for the 3 ppm concentration plume as $u(C(x)) \sim u_{sys}(C(x))$ through the whole range.

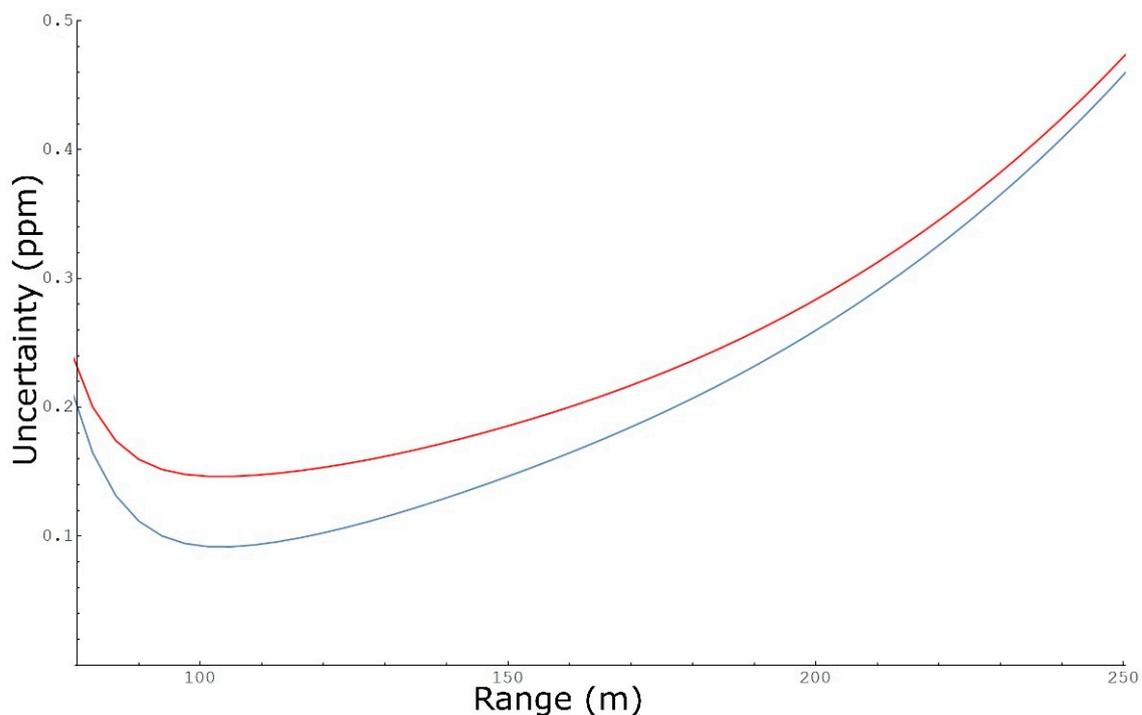


Figure 4. $u_{sys}(C(x))$ (blue line) and $u(C(x))$ (red line) for the 10 ppm concentration plume up to 250 m from the DIAL for $l = 45$ m and $S/N = 500$ at $x \sim 100$ m.

Figure 6 shows the concentration system uncertainty fraction $u_{sys}(C(x))/C(x)$ (yellow line) and the concentration uncertainty fraction $u(C(x))/C(x)$ (blue line) in the function of the plume concentration measured at $x \sim 100$ m from the DIAL where $S/N = 500$ for $l = 45$ m. For concentrations less than ~ 3 ppm, $u_{sys}(C(x))$ is the dominant term while at higher concentrations, u_{α} becomes the dominant term in $u(C(x))$. In this exemplar case, a plume concentration of 250 ppb has an uncertainty of about 35%, which quickly decreases below 10% for concentrations higher than ~ 1 ppm.

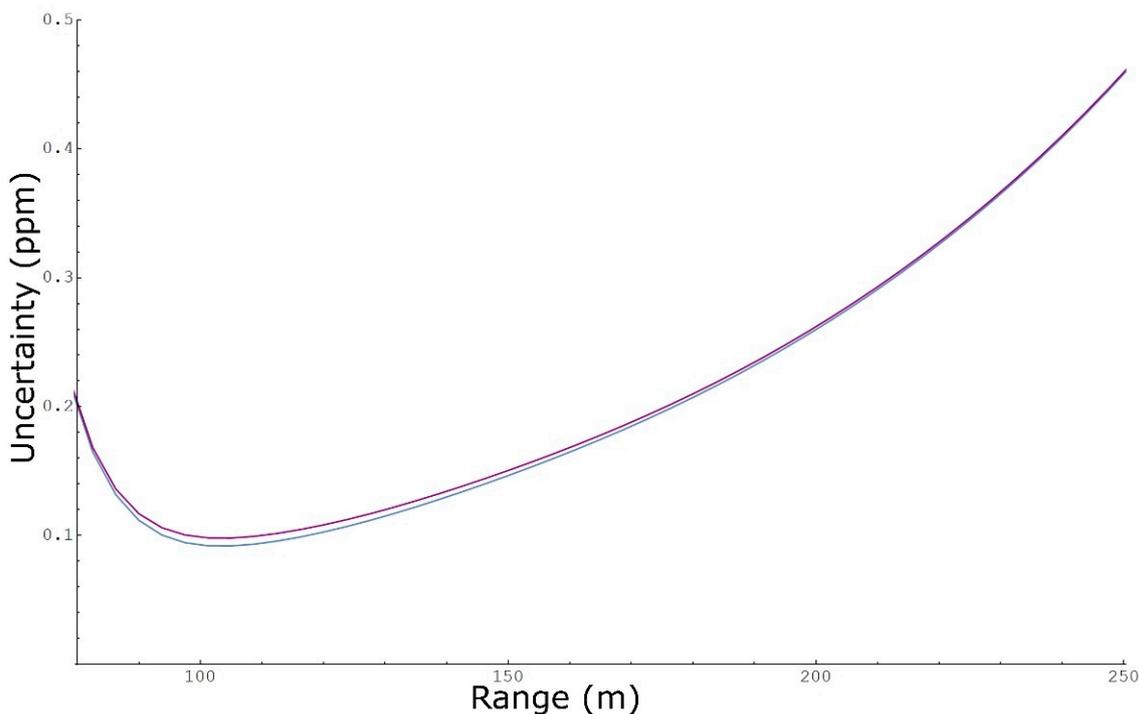


Figure 5. $u_{sys}(C(x))$ (blue line) and $u(C(x))$ (purple line) for the 3 ppm concentration plume up to 250 m from the DIAL for $l = 45$ m and $S/N = 500$ at $x \sim 100$ m.

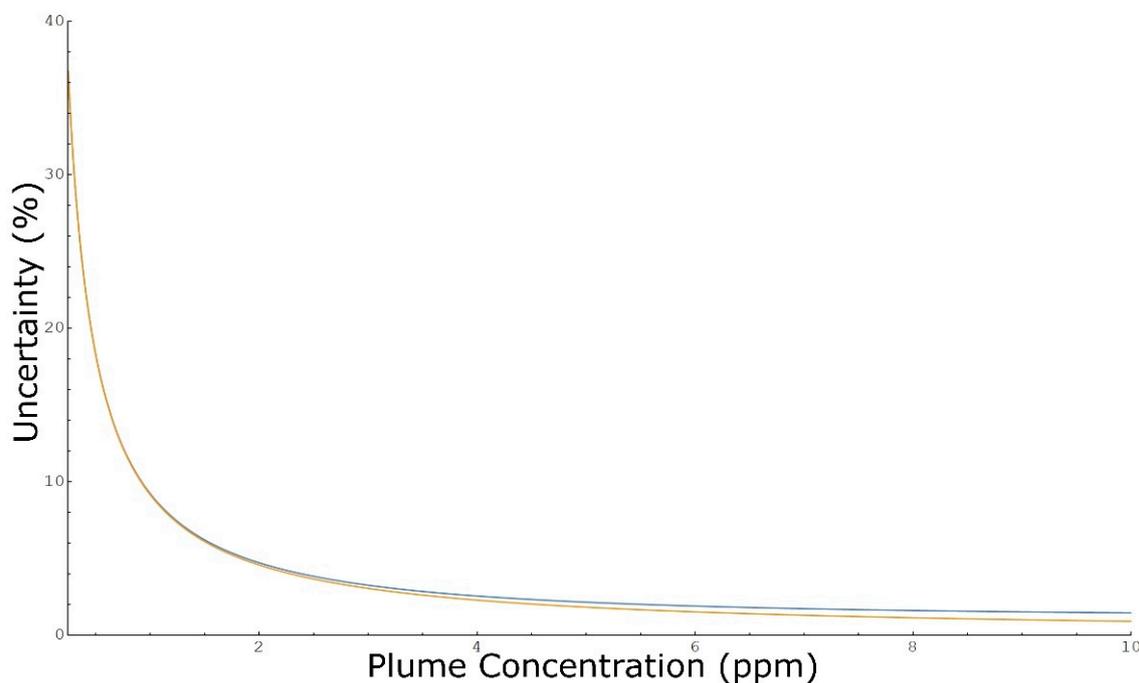


Figure 6. $u_{sys}(C(x))/C(x)$ (yellow line) and $u(C(x))/C(x)$ (blue line) in the function of the plume concentration centred at $x \sim 100$ m from the DIAL ($S/N = 500$) for $l = 45$ m.

Figure 7 shows the contribution to the system uncertainty fraction $u_{sys}(C(x))/C(x)$ reported in Equation (A23) of the four sources of uncertainty defined in Equations (A19) to (A22) calculated for $l = 45$ m. It is clear the signal uncertainties $u_{fon}(C(x))$ (purple line) and $u_{foff}(C(x))$ (light purple line) are the dominant terms when compared to the offset uncertainties $u_{on}(C(x))$ (blue line) and $u_{off}(C(x))$ (light blue line). Given the shape of the return signal in Figure A1, with the maximum signal intensity at 100 m, it is expected

that the lower uncertainty is obtained when measuring a plume centred at about a 100 m distance from the DIAL. However, the shape and intensity of a DIAL return signal varies with the atmospheric (backscatter) conditions and by focusing the detection optics at shorter or longer distances from the DIAL. Therefore, the return signals (and uncertainty) can be optimised at different distances from DIAL depending on the location of the targeted measurement area.

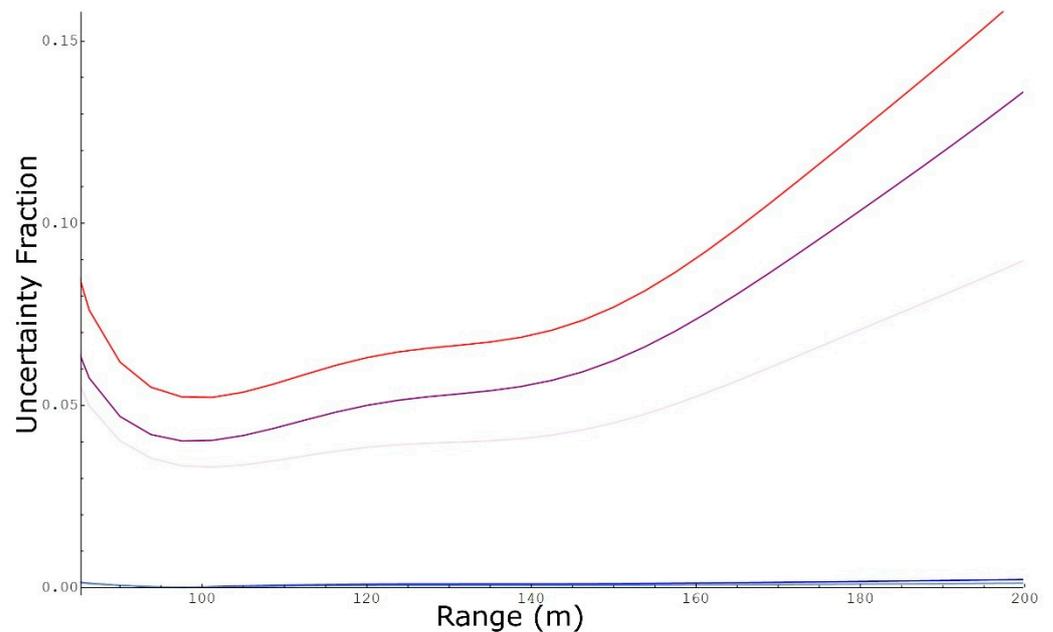


Figure 7. $u_{sys}(C(x))/C(x)$ (red line) up to 200 m from the DIAL and the contributing terms as shown in Equation (A23): $u_{f_{on}}(C(x))$ (purple line), $u_{f_{off}}(C(x))$ (light purple line), $u_{o_{on}}(C(x))$ (blue line), and $u_{o_{off}}(C(x))$ (light blue line) calculated for $l = 45$ m and $S/N = 500$ at $x \sim 100$ m.

For any DIAL system, it is important to assess the contribution of the offset uncertainties to $u_{sys}(C(x))$ to determine if they are negligible as in the case of this DIAL system. Equation (A25) describes $u_{sys}(C(x))$ as an approximation of Equation (A15) by ignoring the small contribution from the offset uncertainties. It is also reasonable to assume the on and off signal uncertainties defined in Equations (A26) and (A27) to be similar since these are dominated by the noise of the same detector. Another approximation could be made if the value of data points separated by the spacing l were similar, i.e., Equations (A28)–(A31), which is typically correct only for very small values of l . A further approximation can be made by assuming that the on and off signals are similar, i.e., Equations (A28)–(A31), which can be considered roughly valid only if the on and off laser beam powers were well balanced. With all these assumptions, Equation (A25) can be simplified to:

$$u_{sys}(C(x)) \cong \frac{1}{\Delta\alpha} \frac{N}{l S}, \quad (5)$$

which is the same equation reported by Fukuda et al. [16], assuming that the range dependence of the signal is not significant, i.e., the four terms in Equations (A25) are identical. In the case of the example scanning line used in this paper, the correct value of $u_{sys}(C(x))$ is 92 ppb when calculated using the full uncertainty analysis in Equation (A15) at $x \sim 100$ m from the DIAL where $S/N = 500$ for $l = 45$ m. If the approximated Equation (5) was used, $u_{sys}(C(x))$ would be calculated to be 74 ppb, which is about 20% lower than the correct value. The assumption that the range dependence of the signal is not significant is therefore incorrect as the approximation used to derive Equation (5) becomes worse for larger l values. The $u_{sys}(C(x))$ value is expected to decrease for measurements carried out over larger distances l while it increases for smaller l .

Equation (A15), or the approximate Equations (A25) and (5), could also be considered as representative of the minimum detectable concentration. It should be noted that some papers report a minimum detectable concentration equation that gives values that are exactly half of Equation (5) [17,18]. In these works, the minimum detectable concentration was derived from the DIAL path-concentration integral Equation (1) rather than the differential Equation (2) and therefore do not consider that uncertainties arise from both the start and end points of the selected range l . Moreover, the S/N value was only used once while both $f_{on}(x)$ and $f_{off}(x)$ signals have an associated uncertainty due to the detector S/N value. Essentially, only one of the four terms under the square root in Equation (A25) was considered, explaining the factor of two difference.

3.4. Path-Concentration Integral Uncertainty

The total uncertainty of a DIAL path-concentration integral $u(CL(x))$ and the system path-concentration integral uncertainty $u_{sys}(CL(x))$ are defined in Equations (A1) and (A2), respectively. The contribution of u_{α} can be added in quadrature to $u_{sys}(CL(x))$ as defined in Equation (A4) to calculate $u(CL(x))$. Figure 8 shows the $CL(x)$ data points (black dots) for the example scanning line up to 500 m from the DIAL, $CL(x)$ calculated by fitting the on and off return signals (blue line), $CL(x) \pm u_{sys}(CL(x))$ (red lines) indicating the standard uncertainty, and $CL(x) \pm 2u_{sys}(CL(x))$ (purple lines) providing a 95% level of confidence expanded uncertainty. The expanded uncertainty captures the variability of the data points from a straight line well, which represents the methane background concentration. Such an agreement indirectly confirms that the main uncertainty sources of a DIAL system can be derived from Equation (1) and that the assumptions made about these sources not being correlated was justifiable. In the case of the example scanning line used in this paper, the value of $u_{sys}(CL(x))$ is 2.3 ppb km at $x \sim 100$ m from the DIAL where S/N = 500.

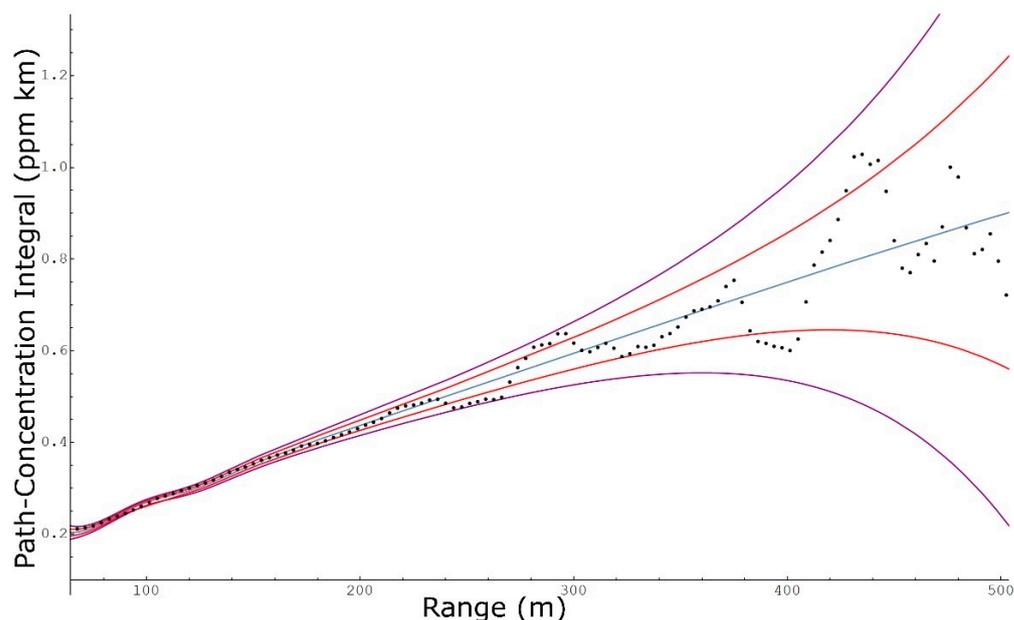


Figure 8. $CL(x)$ data points (black dots) up to 500 m from the DIAL, $CL(x)$ fit (blue line), $CL(x) \pm u_{sys}(CL(x))$ (red lines), and $CL(x) \pm 2u_{sys}(CL(x))$ (purple lines).

Figure 9 shows the contribution to the integrated system uncertainty fraction $u_{sys}(CL(x))/CL(x)$ reported in Equation (A11) of the six sources of uncertainty defined in Equations (A5) to (A10). It is clear the signal uncertainties $u_{f_{on}}(CL(x))$ (purple line) and $u_{f_{off}}(CL(x))$ (light purple line) are the dominant terms. The weight of the offset uncertainties $u_{o_{on}}(CL(x))$ (blue line) and $u_{o_{off}}(CL(x))$ (light blue line) increases at further distances from the DIAL, where the signals $f_{on}(x)$ and $f_{off}(x)$ decrease, when compared to the transmitted energy uncertainties $u_{p_{on}}(CL(x))$ (yellow line) and $u_{p_{off}}(CL(x))$ (light yellow

line). As the signal uncertainties are the main uncertainty sources, it is clear the example scanning line presented here was optimised to measure sources located at a distance from the DIAL of about 80 m up to a maximum of about 300 m.

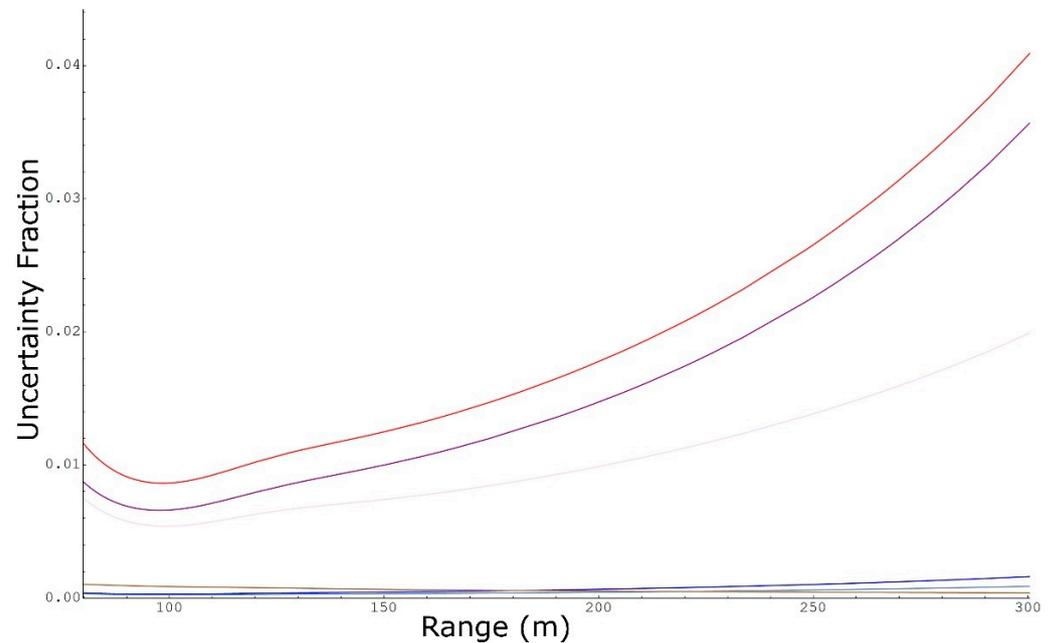


Figure 9. $u_{sys}(CL(x))/CL(x)$ (red line) up to 300 m from the DIAL and the contributing terms as shown in Equation (A11): $u_{f_{on}}(CL(x))$ (purple line), $u_{f_{off}}(CL(x))$ (light purple line), $u_{o_{on}}(CL(x))$ (blue line), $u_{o_{off}}(CL(x))$ (light blue line), $u_{p_{on}}(CL(x))$ (yellow line), and $u_{p_{off}}(CL(x))$ (light yellow line overlapping with the yellow line).

4. Discussion

For the example methane measurement presented in this work, the smaller uncertainty was obtained in the region where the return signal was higher, which was at about 100 m from the DIAL. At a representative S/N value of 500, the system methane concentration uncertainty for a concentration measurement over 45 m was calculated to be 92 ppb. The total concentration uncertainty can be calculated by adding the uncertainty from the absorption coefficient. This is negligible for concentrations lower than ~2 ppm, but given that the ambient methane concentration is around this level, the absorption coefficient uncertainty is often a significant contributor. However, the fractional uncertainty is higher at lower concentrations while it quickly decreases below 10% for concentrations higher than ~1 ppm.

Equations to calculate the mass emission rate uncertainty associated to a DIAL concentration scan through a vertical plane downwind of the targeted measurement area were also derived. For S/N = 500, $s = 10$, $v = 4$ m/s, and $\theta = 90^\circ$, the emission rate system uncertainty was calculated to be ~0.6 and ~0.3 kg/h for a methane plume measured over a $45\text{ m} \times 45\text{ m}$ and $30\text{ m} \times 30\text{ m}$ plane, respectively. The total mass emission rate uncertainty due to DIAL concentration measurement can be calculated by adding the uncertainty from the absorption coefficient, which is negligible for mass emission rates lower than ~15 kg/h while it becomes dominant for concentrations higher than ~15 kg/h for the methane absorption line used in this work. However, the fractional mass uncertainty is higher at lower mass emission rates, and it quickly decreases below 10% for mass emission rates higher than ~6 kg/h. The mass emission uncertainty for each DIAL concentration scan will vary depending on the actual analysis range, number of lines used in the analysis, and the meteorological conditions, and it can be evaluated numerically using Equation (3). This evaluation can either be carried out by including all the sources of uncertainties when evaluating the system concentration $u_{sys}(C(x))$ in Equation (A15) or

using an underestimated value from Equation (5) as a rough approximation. for any S/N and l values as long as $\Delta\alpha$ is known for the targeted species.

It is possible to calculate the expected performances of the IR measurements of other species that use the same detection system and the same laser system, at similar wavelengths and energies, by normalising the methane value to the differential absorption coefficient of the targeted species. These conditions are satisfied for VOCs and ethane measurements that are regularly made with the NPL DIAL system. The mass emission rate uncertainty due to the DIAL system concentration measurement can also be calculated using Equation (3) by replacing the methane gas density with the gas density of either VOCs or ethane. Table 1 shows the results of these calculations performed at $x \sim 100$ m from the DIAL where S/N = 500. The $u_{sys}(C(x))$ values are calculated for $l = 45$ m while two $u_{sys}(M(x))$ are reported for each species using $l = 45$ m ($A = 45$ m \times 45 m) and $l = 30$ m ($A = 30$ m \times 30 m) with $s = 10$, $v = 4$ m/s, and $\theta = 90^\circ$. As mentioned in Section 3.2, the $u_{sys}(M(x))$ values reported in Table 1 are representative of the mass emission rate uncertainties expected from the concentration measurement of a single DIAL scan, not from a DIAL measurement, which is the average of at least four DIAL scans. It is also possible to easily calculate the $u_{sys}(M(x))$ values for different values of s , v , and θ using Equation (3) by scaling the values in Table 1 to the different s , v , and θ values.

Table 1. Summary of methane, ethane, and VOCs $u_{sys}(C(x))$ values calculated at $x \sim 100$ m where S/N = 500 and $l = 45$ m and $u_{sys}(M(x))$ values calculated with $l = 45$ m ($A = 45$ m \times 45 m) and $l = 30$ m ($A = 30$ m \times 30 m) with $s = 10$, $v = 4$ m/s, and $\theta = 90^\circ$.

	l	Methane	Ethane	VOC	Units
$u_{sys}(C(x))$	45 m	92	22	37	ppb
$u_{sys}(M(x))$	45 m	0.6	0.3	1.1	kg/h
$u_{sys}(M(x))$	30 m	0.3	0.2	0.6	kg/h

5. Conclusions

In this work we presented, for the first time, parametric functions of the DIAL path-concentration integral, concentration, and mass emission rates and their associated uncertainties. All of the seven sources of uncertainty of a DIAL concentration measurement of a target gas along a path line were assessed and propagated through each step of the data analysis to determine the mass emission rate uncertainty. The expanded uncertainty of the path-concentration integral captures the variability observed in the experimental data points well, confirming all uncertainty sources were correctly evaluated. The DIAL on and off signals are the dominant source of uncertainty for IR measurements by the NPL DIAL system, which are proportional to the detector S/N value. While the backscattered signal collected by the DIAL telescope can vary significantly during the day, based on the number of particles in the atmosphere, the main limiting factor for DIAL IR measurements is the noise performance of the IR detector. However, it is critical for any DIAL system to assess and control the contribution of the other sources of uncertainty to determine whether they are negligible when compared to the noise contribution of the detector in the relevant measurement ranges.

In the future, a full DIAL measurement uncertainty budget will be developed by adding the uncertainties from the meteorological measurements and considering the effect of averaging several DIAL scans when reporting a DIAL measurement.

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Appendix A

By propagating the uncertainties in quadrature from $CL(x)$ in Equation (1), it is possible to calculate the total uncertainty of the DIAL path-concentration integral $u(CL(x))$:

$$u(CL(x)) = \frac{1}{2 \Delta\alpha} \sqrt{\frac{u(f_{off})^2 + u(o_{off})^2}{(f_{off}(x) - o_{off})^2} + \frac{u(f_{on})^2 + u(o_{on})^2}{(f_{on}(x) - o_{on})^2} + \frac{u(p_{off})^2}{p_{off}^2} + \frac{u(p_{on})^2}{p_{on}^2} + \frac{u(\Delta\alpha)^2}{\Delta\alpha^2} \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right)^2} \tag{A1}$$

The absorption uncertainty, $u(\Delta\alpha)$, is not directly related to the DIAL system path-concentration integral $u_{sys}(CL(x))$ defined in Equation (A2). The absorption uncertainty fraction u_α defined in Equation (A3) gives a constant contribution to the path-concentration integral uncertainty fraction in Equation (A4) and it can be added in quadrature to $u_{sys}(CL(x))$ as a percentage of $CL(x)$:

$$u_{sys}(CL(x)) = \frac{1}{2 \Delta\alpha} \sqrt{\frac{u(f_{off})^2 + u(o_{off})^2}{(f_{off}(x) - o_{off})^2} + \frac{u(f_{on})^2 + u(o_{on})^2}{(f_{on}(x) - o_{on})^2} + \frac{u(p_{off})^2}{p_{off}^2} + \frac{u(p_{on})^2}{p_{on}^2}} \tag{A2}$$

$$u_\alpha = \frac{u(\Delta\alpha)}{\Delta\alpha} \tag{A3}$$

$$\frac{u(CL(x))^2}{CL(x)^2} = \frac{u_{sys}(CL(x))^2}{CL(x)^2} + u_\alpha^2 \tag{A4}$$

By defining:

$$u_{f_{off}}(CL(x)) = \frac{u(f_{off})}{f_{off}(x) - o_{off}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A5}$$

$$u_{f_{on}}(CL(x)) = \frac{u(f_{on})}{f_{on}(x) - o_{on}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A6}$$

$$u_{o_{off}}(CL(x)) = \frac{u(o_{off})}{f_{off}(x) - o_{off}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A7}$$

$$u_{o_{on}}(CL(x)) = \frac{u(o_{on})}{f_{on}(x) - o_{on}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A8}$$

$$u_{p_{off}}(CL(x)) = \frac{u(p_{off})}{p_{off}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A9}$$

$$u_{p_{on}}(CL(x)) = \frac{u(p_{on})}{p_{on}} / \log\left(\frac{f_{off}(x) - o_{off}}{f_{on}(x) - o_{on}} \frac{p_{on}}{p_{off}}\right) \tag{A10}$$

the path-concentration integral system uncertainty fraction $u_{sys}(CL(x))/CL(x)$ and the total path-concentration integral uncertainty fraction $u(CL(x))/CL(x)$ can be defined as in Equations (A11) and (A12):

$$\frac{u_{sys}(CL(x))}{CL(x)} = \sqrt{u_{f_{off}}(CL(x))^2 + u_{f_{on}}(CL(x))^2 + u_{o_{off}}(CL(x))^2 + u_{o_{on}}(CL(x))^2 + u_{p_{off}}(CL(x))^2 + u_{p_{on}}(CL(x))^2} \tag{A11}$$

$$\frac{u(CL(x))}{CL(x)} = \sqrt{u_{f_{off}}(CL(x))^2 + u_{f_{on}}(CL(x))^2 + u_{o_{off}}(CL(x))^2 + u_{o_{on}}(CL(x))^2 + u_{p_{off}}(CL(x))^2 + u_{p_{on}}(CL(x))^2 + u_{\alpha}^2} \tag{A12}$$

The concentration $C(x)$ can be calculated by differentiating the parametric function of the path-concentration integral $CL(x)$:

$$C(x) = \frac{\partial CL(x)}{\partial x} \tag{A13}$$

or, in case of the discrete data points, using Equation (2). The exact uncertainty of the concentration $u(C(x))$ can be calculated by propagating in quadrature all uncertainty terms in Equation (2):

$$u(C(x)) = \frac{1}{2 \Delta \alpha l} \sqrt{\left(\frac{u(f_{off}(x-1/2))^2}{(f_{off}(x-1/2) - o_{off})^2} + \frac{u(f_{off}(x+1/2))^2}{(f_{off}(x+1/2) - o_{off})^2} + \frac{u(f_{on}(x-1/2))^2}{(f_{on}(x-1/2) - o_{on})^2} + \frac{u(f_{on}(x+1/2))^2}{(f_{on}(x+1/2) - o_{on})^2} \right.} \tag{A14}$$

$$\left. + \frac{(f_{off}(x+1/2) - f_{off}(x-1/2))^2 u(o_{off})^2}{(f_{off}(x-1/2) - o_{off})^2 (f_{off}(x+1/2) - o_{off})^2} + \frac{(f_{on}(x+1/2) - f_{on}(x-1/2))^2 u(o_{on})^2}{(f_{on}(x-1/2) - o_{on})^2 (f_{on}(x+1/2) - o_{on})^2} \right. \\ \left. + \frac{u(\Delta \alpha)^2}{\Delta \alpha^2} \left(\log\left(\frac{f_{off}(x+1/2) - o_{off}}{f_{on}(x+1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right) - \log\left(\frac{f_{off}(x-1/2) - o_{off}}{f_{on}(x-1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right) \right)^2 \right)$$

The absorption uncertainty's contribution to the concentration uncertainty u_{α} defined in Equation (A3) is constant. As in the case of the path-concentration integral uncertainty, it can be added in quadrature to the system concentration uncertainty $u_{sys}(C(x))$ as a percentage of $C(x)$ as defined in Equations (A15) and (A16):

$$u_{sys}(C(x)) = \frac{1}{2 \Delta \alpha l} \sqrt{\left(\frac{u(f_{off}(x-1/2))^2}{(f_{off}(x-1/2) - o_{off})^2} + \frac{u(f_{off}(x+1/2))^2}{(f_{off}(x+1/2) - o_{off})^2} + \frac{u(f_{on}(x-1/2))^2}{(f_{on}(x-1/2) - o_{on})^2} + \frac{u(f_{on}(x+1/2))^2}{(f_{on}(x+1/2) - o_{on})^2} \right.} \tag{A15}$$

$$\left. + \frac{(f_{off}(x+1/2) - f_{off}(x-1/2))^2 u(o_{off})^2}{(f_{off}(x-1/2) - o_{off})^2 (f_{off}(x+1/2) - o_{off})^2} + \frac{(f_{on}(x+1/2) - f_{on}(x-1/2))^2 u(o_{on})^2}{(f_{on}(x-1/2) - o_{on})^2 (f_{on}(x+1/2) - o_{on})^2} \right)$$

$$\frac{u(C(x))^2}{C(x)^2} = \frac{u_{sys}(C(x))^2}{C(x)^2} + u_{\alpha}^2 \tag{A16}$$

Considering that:

$$u(f_{off}(x - 1/2)) = u(f_{off}(x + 1/2)) = u(f_{off}), \tag{A17}$$

$$u(f_{on}(x - 1/2)) = u(f_{on}(x + 1/2)) = u(f_{on}), \tag{A18}$$

and by defining:

$$u_{f_{off}}(C(x)) = u(f_{off}) \sqrt{\left(\frac{1}{(f_{off}(x-1/2) - o_{off})} \right)^2 + \left(\frac{1}{(f_{off}(x+1/2) - o_{off})} \right)^2} \tag{A19}$$

$$\frac{\log\left(\frac{f_{off}(x+1/2) - o_{off}}{f_{on}(x+1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right)}{\log\left(\frac{f_{off}(x-1/2) - o_{off}}{f_{on}(x-1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right)}$$

$$u_{f_{on}}(C(x)) = u(f_{on}) \sqrt{\left(\frac{1}{(f_{on}(x-1/2) - o_{on})} \right)^2 + \left(\frac{1}{(f_{on}(x+1/2) - o_{on})} \right)^2} \tag{A20}$$

$$\frac{\log\left(\frac{f_{off}(x+1/2) - o_{off}}{f_{on}(x+1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right)}{\log\left(\frac{f_{off}(x-1/2) - o_{off}}{f_{on}(x-1/2) - o_{on}} \frac{p_{on}}{p_{off}}\right)}$$

$$u_{o_{off}}(C(x)) = u(o_{off}) \frac{\frac{f_{off}(x+1/2)-f_{off}(x-1/2)}{(f_{off}(x-1/2)-o_{off})(f_{off}(x+1/2)-o_{off})}}{\log\left(\frac{f_{off}(x+1/2)-o_{off}}{f_{on}(x+1/2)-o_{on}} / \frac{f_{off}(x-1/2)-o_{off}}{f_{on}(x-1/2)-o_{on}}\right)} \tag{A21}$$

$$u_{o_{on}}(C(x)) = u(o_{on}) \frac{\frac{f_{on}(x+1/2)-f_{on}(x-1/2)}{(f_{on}(x-1/2)-o_{on})(f_{on}(x+1/2)-o_{on})}}{\log\left(\frac{f_{off}(x+1/2)-o_{off}}{f_{on}(x+1/2)-o_{on}} / \frac{f_{off}(x-1/2)-o_{off}}{f_{on}(x-1/2)-o_{on}}\right)} \tag{A22}$$

the concentration system uncertainty fraction $u_{sys}(C(x))/C(x)$ and the concentration uncertainty fraction $u(C(x))/C(x)$ can be rewritten as:

$$\frac{u_{sys}(C(x))}{C(x)} = \sqrt{u_{f_{off}}(C(x))^2 + u_{f_{on}}(C(x))^2 + u_{o_{off}}(C(x))^2 + u_{o_{on}}(C(x))^2} \tag{A23}$$

$$\frac{u(C(x))}{C(x)} = \sqrt{u_{f_{off}}(C(x))^2 + u_{f_{on}}(C(x))^2 + u_{o_{off}}(C(x))^2 + u_{o_{on}}(C(x))^2 + u_{\alpha}^2} \tag{A24}$$

By ignoring the small contribution from the offset uncertainties $u_{o_{on}}(C(x))$ and $u_{o_{off}}(C(x))$, Equation (A15) can be approximated to:

$$u_{sys}(C(x)) \cong \frac{1}{2\Delta\alpha l} \sqrt{\frac{N(f_{off})^2}{(S_{off}(x-1/2))^2} + \frac{N(f_{off})^2}{(S_{off}(x+1/2))^2} + \frac{N(f_{on})^2}{(S_{on}(x-1/2))^2} + \frac{N(f_{on})^2}{(S_{on}(x+1/2))^2}} \tag{A25}$$

by defining:

$$N(f_{off}) = u(f_{off}(x-1/2)) = u(f_{off}(x+1/2)) \tag{A26}$$

$$N(f_{on}) = u(f_{on}(x-1/2)) = u(f_{on}(x+1/2)) \tag{A27}$$

$$S_{off}(x-1/2) = f_{off}(x-1/2) - o_{off} \tag{A28}$$

$$S_{off}(x+1/2) = f_{off}(x+1/2) - o_{off} \tag{A29}$$

$$S_{on}(x-1/2) = f_{on}(x-1/2) - o_{on} \tag{A30}$$

$$S_{on}(x+1/2) = f_{on}(x+1/2) - o_{on} \tag{A31}$$

All the above equations are valid for a DIAL concentration measurement of a target gas along the path of a laser beam transmitted into the atmosphere. A DIAL scan is recorded by scanning the laser beam vertically through the atmosphere, using s DIAL path measurement lines, to build up a 2D concentration map downwind of the targeted measurement area. If each of the s scanning lines was analysed in the same range l , then each of them contributes to the total plane concentration $C_{plane}(x)$ by covering a similar area of the plane A (A/s):

$$C_{plane}(x) = \sum_{i=1}^s \left(C_i(x) \frac{A}{s} \right) \tag{A32}$$

and each of the s scanning lines has approximately the same uncertainty as in Equations (A14) and (A16). The total plane concentration uncertainty $u(C_{plane}(x))$ can be defined as:

$$u(C_{plane}(x)) = \sqrt{u_{sys}(C_{plane}(x))^2 + C_{plane}(x)^2 u_{\alpha}^2} \tag{A33}$$

with the system concentration plane uncertainty $u_{sys}(C_{plane}(x))$ calculated by propagating in quadrature the s uncertainties $u_{sys}(C_i(x))$ dominated by the random signal uncertainty and assumed to be similar to each other:

$$u_{sys}(C_{plane}(x)) \cong \sqrt{s u_{sys}(C_i(x))^2 \frac{A^2}{s^2}} = \frac{u_{sys}(C(x)) A}{\sqrt{s}} \tag{A34}$$

The absorption coefficient uncertainty contribution is constant across the measured plane and proportional to the plane concentration independently of the number of s lines utilised.

The plane concentration map is then combined with the horizontal wind vector perpendicular to the vertical cross-section plane of the scan that intersects the emitted plume to calculate the mass emission rate in kg/h. The plane concentration (unit ppm m^2) is multiplied by the measured wind vector (\bar{v} unit m/s) and by the methane gas density to convert the ppm concentration to kg/m^3 to calculate the mass emission rate across the plane in kg/s. This value can then be multiplied by 3600 and converted to kg/h. By ignoring the fixed conversion factors that are not sources of uncertainties, the mass emission rate in the function of the distance from the DIAL, $M(x)$, can be written as:

$$M(x) = C_{plane}(x) \bar{v} = C_{plane}(x) v \sin \theta \quad (A35)$$

The wind vector is measured at the same time as the DIAL scans, and it consists of the wind speed (v) and the sine of the angle between the wind direction and the DIAL vertical measurement plane (θ). The meteorological measurements are also a source of uncertainty and the uncertainty of each of the three terms in Equation (A35) can be propagated in quadrature. The mass emission rate uncertainty fraction can therefore be defined as:

$$\frac{u(M(x))^2}{M(x)^2} = \frac{u(C_{plane}(x))^2}{C_{plane}(x)^2} + \frac{u(v)^2}{v^2} + \frac{u(\sin \theta)^2}{(\sin \theta)^2} \quad (A36)$$

The impact of the wind speed and wind direction uncertainties, $u(v)$ and $u(\sin \theta)$, will be addressed separately in another paper while in this paper, the focus is on the emission rate uncertainty due to the DIAL concentration measurement, $u_c(M(x))$, which can be defined as the square root of the first term in Equation (A36) multiplied by $M(x)$:

$$u_c(M(x)) = \sqrt{u(C_{plane}(x))^2 v^2 \sin^2 \theta} \quad (A37)$$

$$\frac{u_c(M(x))^2}{M(x)^2} = \frac{u(C_{plane}(x))^2}{C_{plane}(x)^2} \quad (A38)$$

Using Equation (A33) $u_c(M(x))$ can then be rewritten as:

$$u_c(M(x)) = \sqrt{u_{sys}(C_{plane}(x))^2 v^2 \sin^2 \theta + M(x)^2 u_\alpha^2} = \sqrt{u_{sys}(M(x))^2 + M(x)^2 \Delta u_\alpha^2} \quad (A39)$$

with the emission rate uncertainty due to the DIAL system concentration measurement defined as:

$$u_{sys}(M(x)) = \sqrt{u_{sys}(C_{plane}(x))^2 v^2 \sin^2 \theta} \quad (A40)$$

Appendix B

When no plume of the targeted gas is present, both DIAL on and off return signals can be fitted by an empirical equation of two exponential functions deconvoluted by a Gaussian function, as shown in Equation (A41):

$$f(x) = v_5 + \frac{\sqrt{\pi}}{2} v_4 \left(v_1 e^{\frac{4xv_3 + 4v_2v_3 + v_4^2}{4v_3^2}} \left(1 - \operatorname{erf} \left(\frac{v_4^2 + 2(v_2 - x)v_3}{2v_4v_3} \right) \right) + v_6 e^{\frac{4xv_7 + 4v_2v_7 + v_4^2}{4v_7^2}} \left(1 - \operatorname{erf} \left(\frac{v_4^2 + 2(v_2 - x)v_7}{2v_4v_7} \right) \right) \right) \quad (A41)$$

One exponential reflects the signal shape of the central obscuration in a co-axial DIAL system still affecting the return signal while the other exponential reflects the signal shape in the region where there is no influence from the central obscuration. This is a seven-variable function, including a variable ($v5$) that represents the signal offset. Figure A1 shows the fit of an example methane return signal calculated using Equation (A41) that matches the data points well. The chi-square test returned a very small number (~ 0.02), demonstrating the goodness of fit and ensuring the residuals shown in Figures A2 and A3, calculated by subtracting each data point from the corresponding fit value, are representative of the signal noise.

The feature observed in Figure A1 between about 0 and 50 m is the near-field backscatter light from the output optics, which is strong due to the fact the beam is emitted coaxially with the telescope. The signal at negative distances is due to the beam travelling inside the truck before being emitted from the scanner optics and triggering time differences between the acquisition system and laser pulse. The DIAL signal is fitted from about 70 to 3500 m and the extrapolated fitted curve from -120 to 70 m, not taking into account the near field peak, matches the data points before (signal offset) and after the near-field shape well.

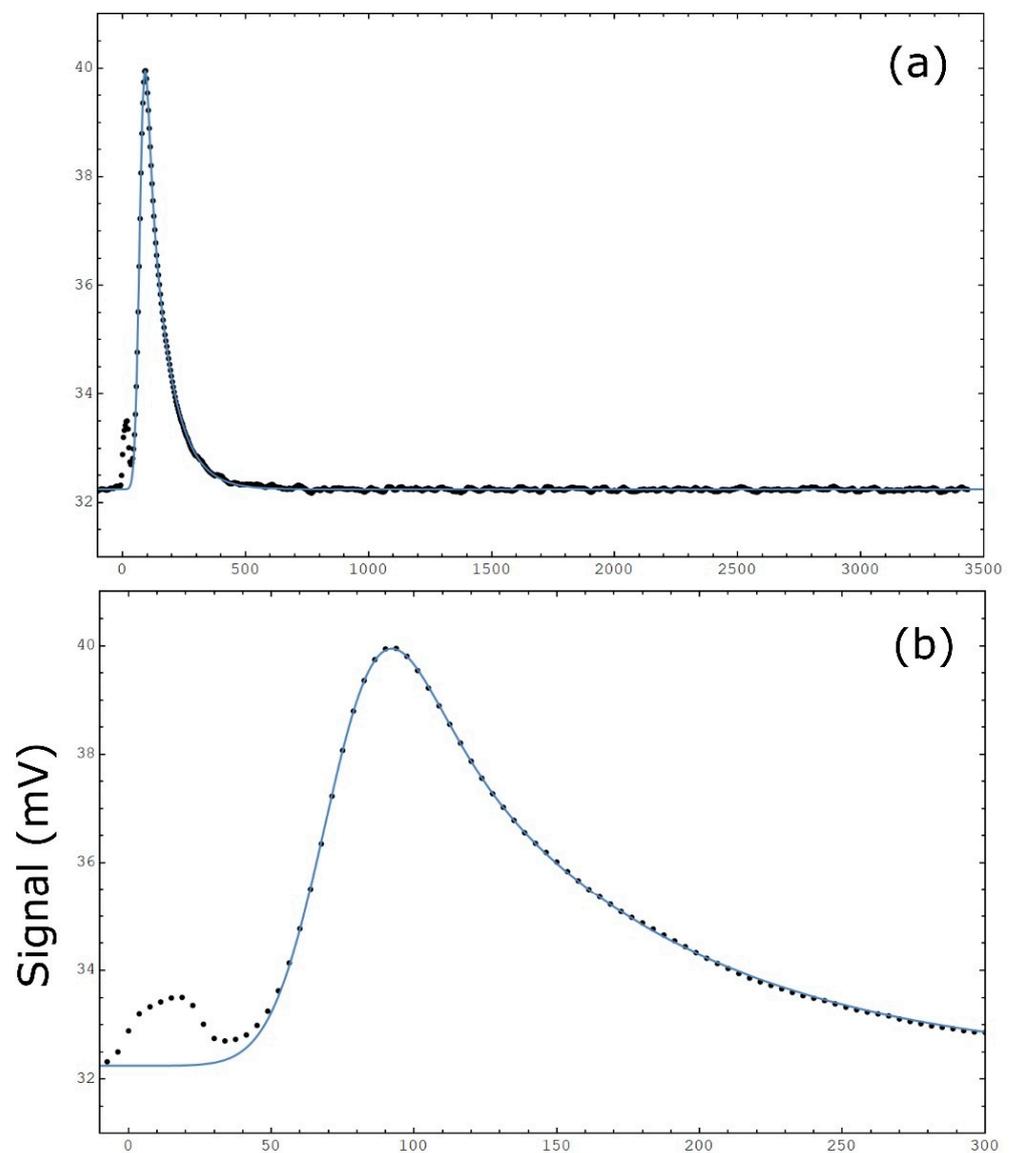


Figure A1. Cont.

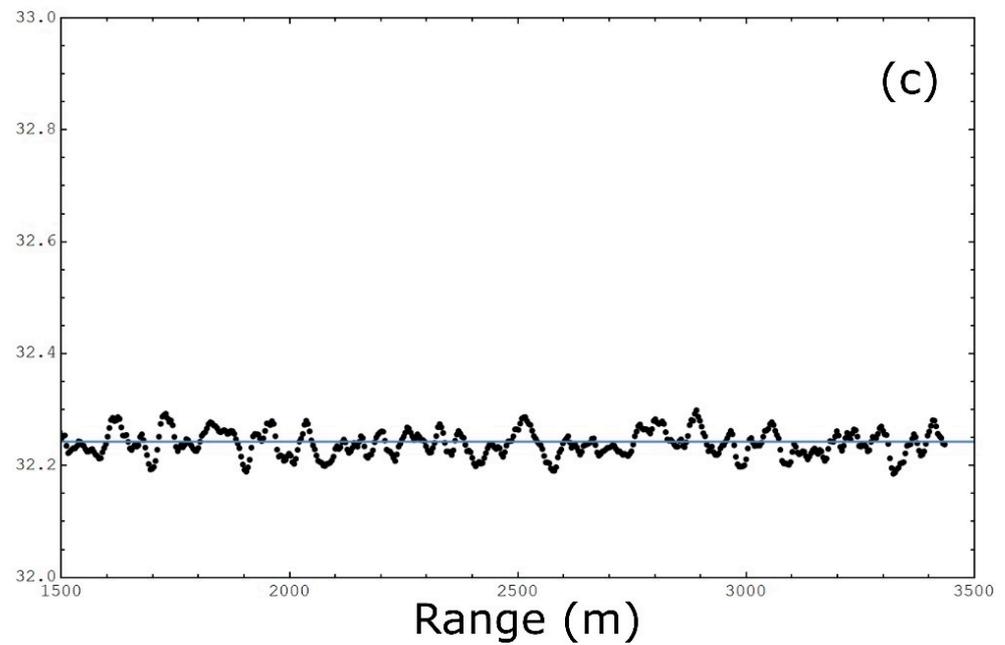


Figure A1. Exemplar fit (blue line) of an experimental methane return signal (black dots) up to ~3500 m from the DIAL (a). Zoomed-in plots covering the near-field (b) and far-field (c) regions.

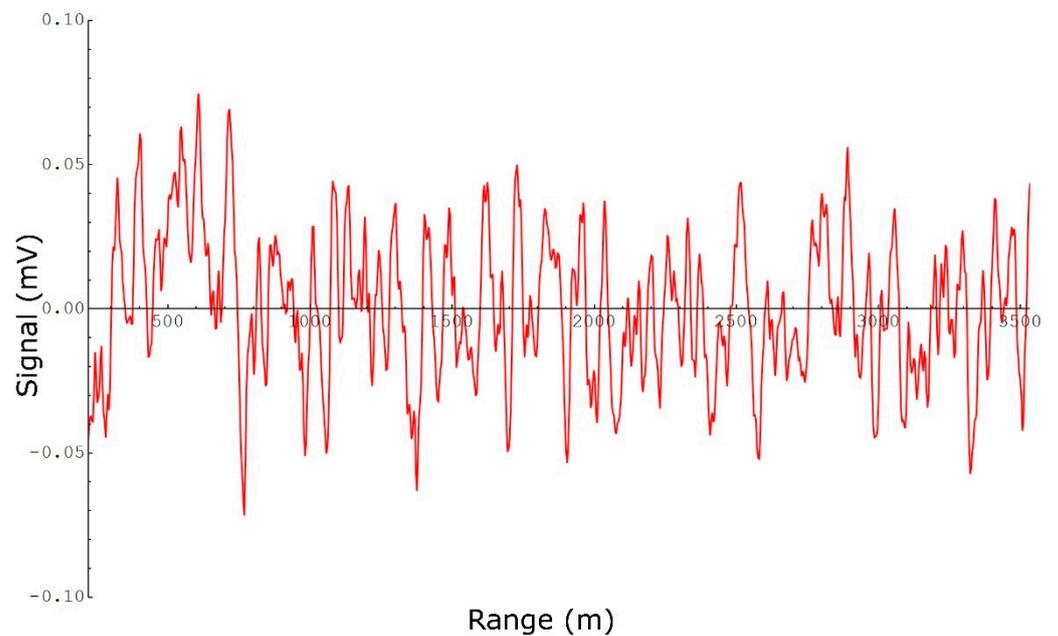


Figure A2. Plot of the residuals calculated by subtracting each data point from the corresponding fit value of an experimental return signal.

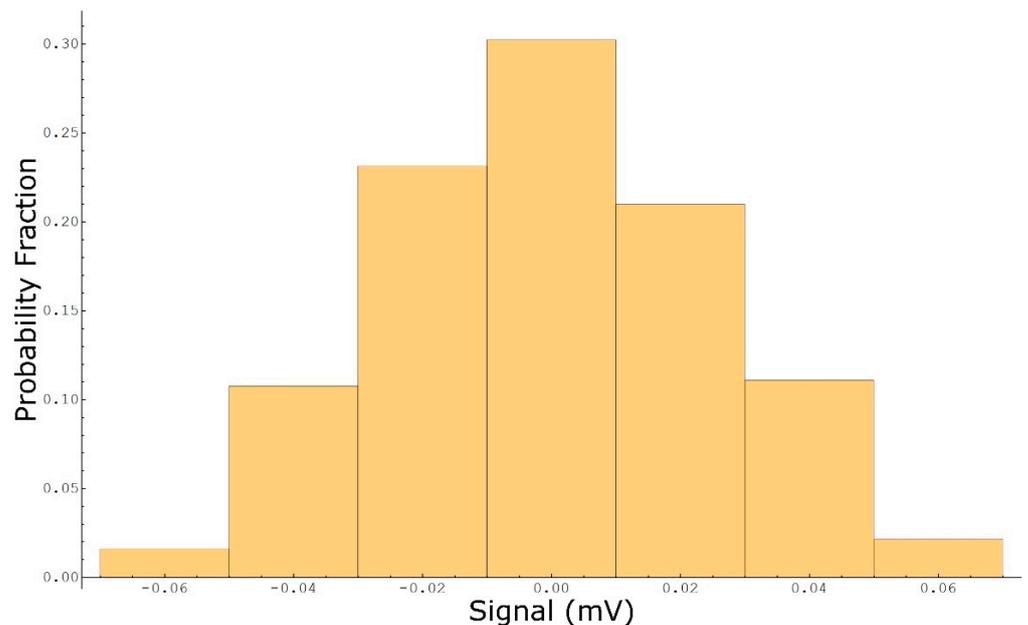


Figure A3. Histogram probability of the residuals calculated by subtracting each data point from the corresponding fit value of an experimental return signal.

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