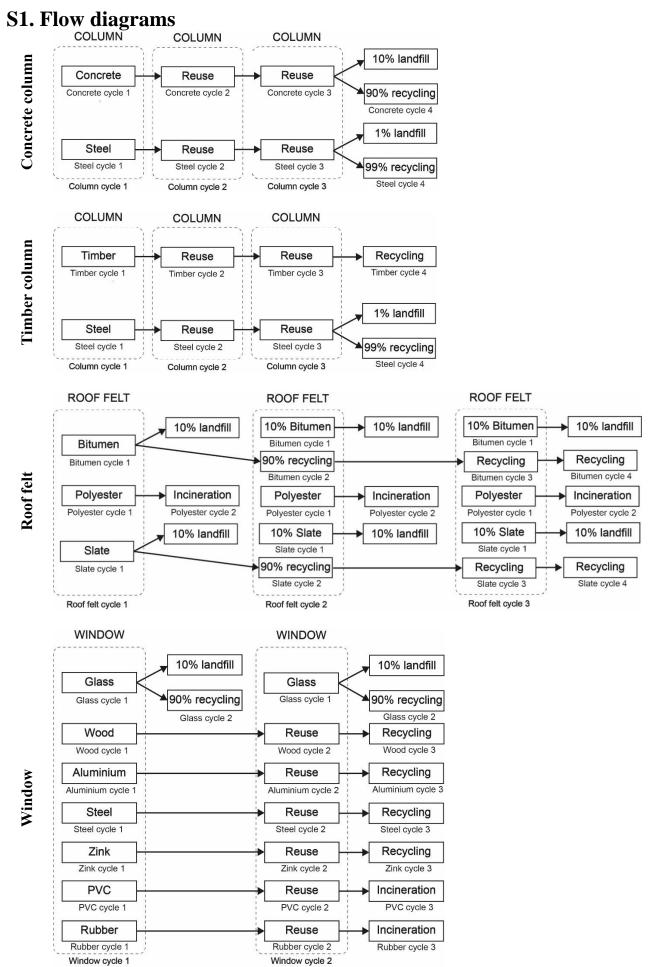
# Development of a life cycle assessment allocation approach for circular economy in the built environment

## **Supplementary material**

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Note: punctered boxes indicate cycles of the primary function i.e. column, roof felt or window

# **S2.** Mathematical expressions for the allocation of the reusable and recyclable material fractions of the exemplary circular building components.

*Note:* Mathematical expressions have been harmonised for comparison reasons. The CFF has been shortened according to each of the circular building components. The LD approach and the impact distribution between the cycles is based on an example from Allacker et al. (2017)

Common	Unit pr. Unit	Definition
abbreviations used in	value	
equations		
V	kg CO <sub>2</sub> eq. /kg	Emissions from virgin material production
R	kg CO <sub>2</sub> eq. /kg	Emissions from reuse/recycling of material
D	kg CO <sub>2</sub> eq. /kg	Emissions from disposal of waste material
A		Allocation factor
R*	kg CO <sub>2</sub> eq. /kg	Emissions assumed to be substituted by reused or recycled material
$\mathbf{r}_1$	unitless	Share of recycled content
$r_2$	unitless	Share of material that will be recycled at EoL
r <sub>3</sub>	unitless	Share of material that will be used for energy recovery at EoL
$Q_p$	unitless	The quality of the primary material respectively
$Q_{i}$	unitless	The quality of the ingoing secondary material
$Q_{o}$	unitless	The quality of the outgoing secondary material
L	MJ/kg	Lower heating value of the material in the component that is used for energy recovery at EoL
$X_{\mathrm{ER,elec}}$	unitless	The efficiency of the electricity energy recovery process
$X_{ER,heat}$	unitless	The efficiency of the heat energy recovery process

$E_{SE,elec}$	$kg CO_2 eq.$	The impact assumed to be substituted by the
		electricity energy recovery
E <sub>SE,heat</sub>	kg CO <sub>2</sub> eq.	The impact assumed to be substituted by the
		heat energy recovery

Allocation	420x420x3500mm Peikko	350x350x3500mm cross	1 m <sup>2</sup> Icopal Top 500 P roof	1230x1480mm Velfac
approach	prefabricated concrete	laminated timber column	felt (recycling)	energy 200 window (reuse)
	column (reuse)	(reuse)		
	Cycle 1 R <sub>1</sub> Cycle 2 R <sub>2</sub> Cycle 3	Cycle 1 R <sub>1</sub> Cycle 2 R <sub>2</sub> Cycle 3	$V_1$ $V_2$ $V_3$ $V_3$ $V_4$ $V_2$ $V_3$ $V_4$ $V_2$ $V_3$ $V_4$ $V_3$ $V_4$ $V_5$ $V_7$ $V_8$ $V_8$ $V_9$	Cycle 1 R <sub>2</sub> Cycle 2
	↓D ↓R₃	$\downarrow_{D} \downarrow_{R_3}$	$\downarrow_{D_1}$ $\downarrow_{D_2}$ $\downarrow_{D_3}$ $\downarrow_{R_3}$	$ \downarrow_{D_1} \downarrow_{R_1} \qquad \downarrow_{D_2} \downarrow_{R_3} $
EN	Cycle $1 = V + R_1$	Cycle $1 = V + R_1$	<b>Cycle 1</b> = $V_1 + R_1 + D_1$	<b>Cycle 1</b> = $V_1 + R_1 + R_2 + D_1$
15804/1597	Cycle $2 = R_2$	Cycle $2 = R_2$	<b>Cycle 2</b> = $V_2 + R_2 + D_2$	<b>Cycle 2</b> = $V_2 + R_3 + D_2$
8 cut-off	Cycle $3 = R_3 + D$	Cycle $3 = R_3 + D$	<b>Cycle 3</b> = $V_3 + R_3 + D_3$	
50:50	<b>Cycle 1</b> = $V+0.5 \cdot R_1$	<b>Cycle 1</b> = $V+0.5 \cdot R_1$	<b>Cycle 1</b> = $V_1 + 0.5 \cdot R_1 + D_1$	<b>Cycle 1</b> = $V_1 + 0.5 \cdot R_1 + D_1$
	<b>Cycle 2</b> = $0.5 \cdot R_1 + 0.5 \cdot R_2$	<b>Cycle 2</b> = $0.5 \cdot R_1 + 0.5 \cdot R_2$	Cycle 2 =	Cycle 2 =
	<b>Cycle 3</b> = $0.5 \cdot R_2 + 0.5 \cdot R_3 + D$	<b>Cycle 3</b> = $0.5 \cdot R_2 + 0.5 \cdot R_3 + D$	$V_2+0.5 \cdot R_1+0.5 \cdot R_2+D_1$ <b>Cycle 3</b> =	$V_2+0.5\cdot R_1+0.5\cdot R_2+D_1$
	Where 0.5·R <sub>3</sub> is allocated to the subsequent cycle	Where 0.5·R <sub>3</sub> is allocated to the subsequent cycle	$V_3+0.5\cdot R_2+0.5\cdot R_3+D_3$ Where $0.5\cdot R_3$ is allocated to	Where $0.5 \cdot R_2$ is allocated to the subsequent cycle
			the subsequent cycle	
CFF	Cycle 1,2,3 = V+(1- A)· $r_2$ ·((R <sub>1</sub> +R <sub>2</sub> +R <sub>3</sub> )- R <sub>3</sub> *·(Q <sub>0</sub> /Q <sub>p</sub> ))+(1- $r_2$ )·D)/3	Cycle 1,2,3 = V+(1- A)· $r_2$ ·(( $R_1+R_2+R_3$ )- $R_3$ *·( $Q_0/Q_p$ ))+(1- $r_2$ )·D)/3	Cycle 1 bitumen/slate = $V_1+(1-A)\cdot V_1\cdot (Q_iQ_p)+(1-A)\cdot r_2+(R_1-V_1^*\cdot (Q_0/Q_p))+(1-r_2)\cdot D_1$	Cycle 1,2 <sub>glass</sub> = $V_{1,2}+(1-A)\cdot r_2\cdot (R_{1,3}+R_{1,3}^*\cdot (Q_o/Q_p))+(1-r_2)\cdot D$
	Where r <sub>2</sub> is 90% concrete and 99% steel recycling at EoL, R <sub>3</sub> * is 90% concrete	Where r <sub>2</sub> is 100% wood and 99% steel recycling at EoL, R <sub>3</sub> * is 90% concrete and 99%	Cycle 2 bitumen/slate = $(1-r_1)\cdot V_2+r_1\cdot (A\cdot R_1+(1-r_1)\cdot V_2+r_1\cdot (A\cdot R_1+r_1)\cdot V_3+r_1\cdot (A\cdot R_1+r_1)\cdot V_3+r_1$	Where r <sub>2</sub> is 90% glass recycling at EoL, R <sub>1,3</sub> * is 90% glass recycling
	and 99% steel recycling.	steel recycling.	A)· $V_2$ · $(Q_i/Q_p)$ )+ $(1-A)$ · $r_2$ · $(R_2$ - $R_2$ *· $(Q_0/Q_p)$ )+ $(1-r_2)$ · $D_2$	Cycle 1,2wood, aluminium, steel, zinc = $V_1+(1-A)\cdot r_2\cdot ((R_3+R_4)-R_4^*\cdot (Q_o/Q_p))/2$

			Cycle 3 bitumen/slate = $(1-r_1)\cdot V_3+r_1\cdot (A\cdot R_2+(1-r_1)\cdot V_3+r_1\cdot (A\cdot R_2+(1-r_1)\cdot R_2+(1-r_2)\cdot R_2+(1-r_$	Cycle 1,2rubber, PVC =
			A)· $V_3$ · $(Q_i/Q_p)$ )+ $(1-A)$ · $r_2$ · $(R_3-$	$V_1+r_3\cdot(D_2-L\cdot X_{ER,heat}\cdot E_{SE,heat}-$
CFF continued			$R_3^* \cdot (Q_0/Q_p)) + (1-r_2) \cdot D_3$	$L \cdot X_{ER,elect} \cdot E_{SE,elec} / 2$
commucu			r <sub>1</sub> is 90% bitumen and slate, r <sub>2</sub> is 90% bitumen and slate that will be recycled at EoL, R <sub>2,3</sub> * is 90% bitumen and slate recycling,	Where r <sub>3</sub> is 100% rubber and PVC energy recovery at EoL
			Cycle 1,2,3 polyester = $V_{1,2,3}+r_3\cdot(D_{1,2,3}-L\cdot X_{ER,heat}\cdot E_{SE,heat}-L\cdot X_{ER,elect}\cdot E_{SE,elec})$	
			Where r <sub>3</sub> is 100% polyester energy recovery at EoL	
LD	Cycle 1 = $0.56 \cdot V + 0.11 \cdot R_3 + 0.11 \cdot D + 0.5 \cdot R_1$ Cycle 2 =	Cycle 1 = $0.56 \cdot V + 0.11 \cdot R_3 + 0.11 \cdot D + 0.5 \cdot R_1$ Cycle 2 =	Cycle 1 = $0.56 \cdot V_1 + 0.11 \cdot R_3 + 0.11 \cdot D_3 + 0.$ $5 \cdot R_1$ Cycle 2 =	Glass: Cycle 1 = $V_1+0.5 \cdot R_1+D_1$ Cycle 2 = $V_2+0.5 \cdot R_3+D_2$
	$0.33 \cdot V + 0.33 \cdot R_3 + 0.33 \cdot D + 0.5 \cdot R_1 + 0.5 \cdot R_2$	$0.33 \cdot V + 0.33 \cdot R_3 + 0.33 \cdot D + 0.5 \cdot R_1 + 0.5 \cdot R_2$	$0.33 \cdot V_2 + 0.33 \cdot R_3 + 0.33 \cdot D_3 + 0,$ $5 \cdot R_1 + 0.5R_2$	Frame: Cycle 1 =
	Cycle 3 =	Cycle 3 =	<b>Cycle 3</b> = $0.11 \cdot V_3 + 0.56 \cdot R_3$	$0.85 \cdot V_1 + 0.5 \cdot R_2 + 0.15 \cdot (D_2 + R4)$
	$0.11 \cdot V + 0.56 \cdot R_3 + 0.56 \cdot D +$	$0.11 \cdot V + 0.56 \cdot R_3 + 0.56 \cdot D +$	$+0.56\cdot D_3 + 0.5\cdot R_2$	)
	$0.5 \cdot R_2$	$0.5 \cdot R_2$		Cycle 2 =
			Where $R_3$ is counted as	$0.15 \cdot V_1 + 0.5 \cdot R_2 + 0.85 \cdot (D_2 + R4)$
	Where $R_3$ is counted as	Where $R_3$ is counted as	disposal	)
	disposal	disposal		

#### S3. Deriving the CE LD approach

A graphical representation of how the CE LD equation for dividing the production impacts was derived is shown in the figure below. The red line represents (in this case) the virgin material production impacts' distribution between the use cycles, where the distribution decreases linear degressively from use cycle 1 to 'n'. The distribution is calculated in percentage emission.

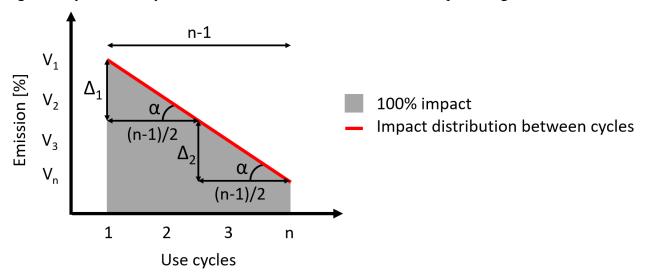


Figure 2. Explanatory illustration of the developed LD equation

The total impact over the use cycles will always be 100% (i.e. the grey area of the graph), thus the average impact in percentage is:

$$Av = \frac{100\%}{n} \tag{1}$$

Where n is the total number of use cycles. The coefficient,  $\alpha$ , i.e. the slope of the graph in Figure 2 is:

$$\alpha = \frac{V_1 - V_n}{n - 1} \tag{2}$$

Where  $V_1$  is the emission from virgin material production allocated to the first use cycle,  $V_n$  is the emission from virgin material production allocated to the last use cycle and (n-1) is the number of spaces between the use cycles. The environmental impact allocated to the first use cycle is then:

$$V_1 = Av + \Delta_1 \text{ where } \Delta_1 = \alpha * \frac{(n-1)}{2}$$

$$V_1 = \frac{100\%}{n} + \frac{V_1 - V_n}{n-1} \cdot \frac{(n-1)}{2}$$
(3)

The average impact is added to the slope of the line to find out how much impact should be added to the average impact towards the first use cycle. The slope is multiplied by (n-1)/2 which represents the distance from the first use cycle to the middle of the line. (n-1)/2 is used as a calculation

technicality to account for situations when there is an odd number of cycles. Similarly, the n'th cycle is:

$$V_n = Av - \Delta$$
, where  $\Delta_2 = \alpha * \frac{(n-1)}{2}$  (4)

$$V_n = \frac{100\%}{n} - \frac{V_1 - V_n}{n - 1} \cdot \frac{(n - 1)}{2}$$

However, here the average impact is subtracted from the slope of the line to find out how much impact should be deducted from the average impact towards the last use cycle.

It is decided that the first use cycle should be impacted 'F'-times as much as the last use cycle:

$$V_1 = F \cdot V_n \tag{5}$$

 $V_1$  from (5) is inserted into (3) which gives:

$$F \cdot V_n = \frac{100\%}{n} + \frac{V_1 - V_n}{n - 1} \cdot \frac{(n - 1)}{2} \tag{6}$$

By adding (4) with (6) the equations can be reduced to:

$$V_n = \frac{100\%}{n} - \frac{V_1 - V_n}{n - 1} \cdot \frac{(n - 1)}{2} \tag{7}$$

+

$$F \cdot V_n = \frac{100\%}{n} + \frac{V_1 - V_n}{n - 1} \cdot \frac{(n - 1)}{2}$$

$$(F + 1) \cdot V_n = 2 \cdot \frac{100\%}{n}$$

The percentage of the total environmental impact from all use cycles allocated to the n'th user is:

$$V_n = 2 \cdot \frac{\frac{100\%}{n}}{(F+1)} = \frac{2 \cdot 100\%}{n \cdot (F+1)} \tag{8}$$

Inserting  $V_n$  from (8) into (5) then gives  $V_1$ :

$$V_1 = F \cdot 2 \cdot \frac{100\%}{(F+1)} = \frac{F \cdot 2 \cdot 100\%}{n \cdot (F+1)} \tag{9}$$

Concrete column calculation example: distribution of virgin concrete production impact between the cycles

Number of cycles:

$$n = 4$$

Allocation factor:

$$F = 50$$

The average impact is:

$$Av = \frac{100\%}{n} = \frac{100\%}{4} = 25\% \tag{1}$$

V<sub>1</sub> is:

$$V_1 = \frac{F \cdot 2 \cdot 100\%}{n \cdot (F+1)} = \frac{50 \cdot 2 \cdot 100\%}{4 \cdot (50+1)} = 49\%$$
(9)

V<sub>4</sub> is:

$$V_4 = \frac{2 \cdot 100\%}{n \cdot (F+1)} = \frac{2 \cdot 100\%}{4 \cdot (50+1)} = 1\%$$
 (8)

The coefficient, 
$$\alpha$$
, (i.e. the difference between one use cycle and the next) is: 
$$\alpha = \frac{V_1 - V_n}{n-1} = \frac{49\% - 1\%}{4-1} = 16\%$$

The impact percentage of intermediate cycle V2 is then:

$$V_2 = V_1 - \alpha = 49\% - 16\% = 33\%$$

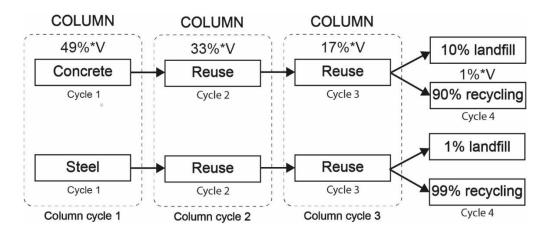
And The impact percentage of intermediate cycle V<sub>3</sub> is:

$$V_3 = V_2 - \alpha = 33\% - 16\% = 17\%$$

The impacts of each cycle are summed to check if the total impact adds up to 100%:

$$V_1 + V_2 + V_3 + V_4 = 49\% + 33\% + 17\% + 1\% = 100\%$$

On the concrete column flow chart from Appendix C, the distribution is thus:



## S4. Expert session evaluation of the developed CE LD approach

**Note:** The percentage of expert sessions in which each issue under each category was raised is shown using a grey-scale were dark grey indicates the most counts and white the least counts.

	Category	Remarks  Remarks	Percentage of expert sessions in which the issue was raised
	Applicability	Suitable for ex-ante assessment (e.g., in policymaking, early stage design)	30%
		Suitable to assess multiple (future) cycles	60%
		Most suitable for (reproducible) building component or product level	60%
		Supports determining more ideal CE (e.g., ideal vision for back-casting)	30%
		Also suitable when materials cannot be re-used or recycled at same value	10%
ges	<b>Incentives CE</b>	Method incentivises not only narrowing, but also slowing and (high-value) closing cycles	30%
Advantages	Levels	CE-LCA introduces 'missing' building component level in LCA	10%
	Fair accounting impacts	The linear degressive method divides burden fairly between cycles; no double crediting possible	20%
		All cycles are included; impacts from other cycles (e.g., production, disposal) remain visible in all cycles	20%
	Ease of use	The allocation formula understandable and transparent (better than the PEF)	30%
	Instrument for discussion	Method stimulates (re)discussing problems and incentives in current LCA standards	20%
		Method show how we could include CE in LCA	30%
		Method shows how complex CE in design and the Built environment is	10%
	Non-	Less suitable for ex-post assessments.	20%
7.0	applicability	Less suitable for building scale (too complex, uncertain, no control by producing supply chain)	40%
ges	<b>Uncertainty in</b>	Difficult to determine and guarantee future cycles; leads to	60%
Disadvantages	assumptions	not-accurate results	0070
		Uncertainty in assumptions far in the future (cycles, processes, energy mix are unknown)	50%
Dis		Sensitive to assumptions on functional, technical and economic lifespan	30%
	Greenwashing impacts	Burdens can be shifted towards [non-existent cycles] the future, diluting impacts	60%

		Easy to mis-use by industry by adding future cycles.	60%
	Challenging to	Requires transition in building industry to determine all cycles	
	implement	(i.e., from one-off projects to a (closed loop) component-wise industry)	50%
		Difficult to implement a new LCA methods in practice, it is easier to adapt the current LCA standard	30%
		All cycles need to be documented and kept tracible over long- term (e.g., government regulation is needed)	30%
	Current LCA tools in practice cannot do a CE-LCA calculation		
	Difficulties in	Method is complex	50%
	use	Method is time consuming	30%
	Urgency	Virgin production burdens should be in first cycles to reduce our impacts now	40%
	Improvements ease of use	Make the method understandable and simple to use, (e.g., include a manual, concrete examples, clarify terms, single indicator system)	50%
		Make method affordable and fast to use	20%
		Provide (more) background data; make data accessible to industry	40%
		Shift burden of proof for CE-LCA proof from building level to component level (i.e., component-EPD's)	10%
		Translate to a design synthesis tool (e.g., guidelines, flowchart) and practice assessment tool	50%
	Improvement accuracy and	Differentiate between different objects of assessment in CE-LCA	10%
S	certainty in allocation	Differentiate different cycles (i.e., known or unknown, high-value or low-value, open or closed)	40%
rovements	approach	Prefer system expansion with up-front crediting over allocation for known cycles, mass production, direct re-use and recycling	20%
ımpr		Include market situation and material quality factors in allocation approach	20%
		Add probability factor for cycles to CE-LCA	10%
		Include (use) time in allocation approach	20%
	Improvement	Differentiate LCA levels (do not interlink them)	30%
	ease of implementation	Develop rules, template or regulation for cycles (i.e., amount, division of impact, types of cycles, system boundary)	60%
	in practice	Prefer an LCA 'tax' system: producer takes initial production and EOL impacts; cycles can be added over time	10%
		Test the method in a real-life case with stakeholders	40%
	Improvement of certainty	Use CE-LCA as an additional informational module "circular potential" next to standard LCA	20%
	and prevention	Obligatory peer review of CE-LCA	10%
	of misuse	Include a sensitivity analysis on influence of varying future cycles	10%

Widen scope	Assessment on other criteria should be part of CE assessment	30%
<b>CE</b> assessment	(i.e., value, costs, material flow, social factors)	30%