



Article Study on Carbonation Resistance of Polymer-Modified Sulphoaluminate Cement-Based Materials

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Abstract: The use of tricyclic copolymer latex (AMPS) can effectively improve the carbonation resistance of sulphoaluminate cement. This paper investigated polymer AMPS and polycarboxylic acid to modify sulphoaluminate cement materials by exploring the carbonation level of sulphoaluminate cement paste and mortar and the strength before and after carbonation. Then, the optimal dosage of polymer and polycarboxylic acid was obtained so that the carbonation resistance of sulphoaluminate cement reached the best state. The compressive strength was significantly improved by adding AMPS for sulphoaluminate cement paste and mortar. After carbonation, the strength decreased and combined with the carbonation level; it was concluded that the carbonation resistance of sulphoaluminate cement materials was the best when the optimal dosage of AMPS and polycarboxylic acid was 5% and 1.8%, respectively. Due to the addition of AMPS, the hydrated calcium aluminosilicate (C-A-S-H) and hydrated calcium silicate (C-S-H) gels, generated by the hydration of sulphoaluminate cement and the surface of unreacted cement particles, are wrapped by AMPS particles. The water is discharged through cement hydration. The polymer particles on the surface of the hydration product merge into a continuous film, which binds the cement hydration product together to form an overall network structure, penetrating the entire cement hydration phase and forming a polymer cement mortar with excellent structural sealing performance. To prevent the entry of CO₂ and achieve the effect of anti-carbonation, adding polycarboxylic acid mainly improves the sample's internal density to achieve the anti-carbonation purpose.

Keywords: sulphoaluminate cement; carbonation; polymer; polycarboxylic acid; carbonation level

1. Introduction

With the acceleration of China's modernization process, various infrastructures have been constructed. Most of these are reinforced concrete structures. In the design process, the durability, practicability, and comfort of these structures should also be considered in addition to their traditional mechanical properties, such as strength, earthquake resistance and low-carbon [1,2]. Concrete is the most widely used artificial material and an essential building material. With the increase in the service life of concrete, the design life of the structure will often be lower than its service life and it may be destroyed prematurely. This arouses people's attention and research on structural durability, something which has become a common concern in the engineering field. The durability of concrete refers to a property in which the concrete maintains the original mechanical properties and changes slightly during the service process of the structure [1,3,4]. The durability of concrete is closely related to its internal and external environment. Internal factors include concrete strength, permeability, the thickness of the protective layer, cement type, cement label, cement dosage, admixture dosage, etc.; external factors mainly include ambient temperature, humidity, carbon dioxide content, and corrosive environment. The durability problems of concrete in practical applications mainly include [5,6]: (1) carbonation of concrete and



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Copyright: © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). corrosion of steel bars; (2) freeze–thaw damage of concrete; (3) erosion of chemical medium; (4) corrosion of physical concrete wear; (5) alkali–aggregate reaction [7,8]. Among the many durability problems, more attention has been paid to concrete carbonation [9–11]. Acid gases in the air, such as CO₂, HCl, SO₂, Cl₂, and others, dissolve in water and enter the component's interior. Reacting with the alkaline substances after the cement hardens is called the neutralization of concrete [12–14].

In some cases, the carbonation of concrete can increase the internal compactness, thereby improving the concrete's resistance to chemical attack [15–17]. However, carbonation will reduce the alkalinity of concrete, destroy the passivation film on the surface of the steel bar, and make the concrete lose its protective effect on the steel bar, which harms the corrosion of the steel bar in the concrete. At the same time, concrete carbonation will also increase the shrinkage of concrete, which may lead to substantial cracks and structural damage [18]. Since concrete is a loose and porous material, there are capillaries, pores, air bubbles, and even defects of different sizes. The CO₂ gas in the air penetrates the pores of the concrete and chemically reacts with the carbonate substances in the pores. Carbonate substances are produced in the hydration process of sulphoaluminate cement, mainly AFt, AFm, and gels C-A-S-H, C-S-H, and aluminum hydroxide gel (AH₃) produced by hydration [19–21].

In recent years, using organic polymers as part of cementitious materials in the preparation of polymer-modified concrete mortar has been a critical way to improve the tensile strength, toughness, and impermeability of cement-based materials [22]. Tests show that a variety of replacement polymers forms part of the cement. After being mixed into the cement mortar, the compressive and flexural strength of the polymer cement mortar is significantly enhanced, the toughness of the cement-based material is improved considerably, and the air tightness is increased, thereby achieving carbonation resistance [23]. Figures 1 and 2 show the polymers and polymer mortars used in existing cement concretemodified materials.



Figure 1. Types of polymers and classification of polymer mortar composite materials.

When the polymer emulsion is mixed with the cement mortar, the emulsion is uniformly dispersed in the cement mortar. With water loss from the cement paste, the hydration products AFt, AFm, and the gels C-A-S-H, C-S-H, and aluminum hydroxide gel (AH₃) produced by hydration gradually aggregated. At the same time, the polymer particles were partially deposited in the gel and untreated and hydrated cement particle mixture surface. The polymer particles on the surface of the cement hydration product merge into a continuous film, which binds the cement hydration product together to form an overall network structure. The film formed by the polymer in the network runs through the entire cement hydration product, creating a dense structural polymer cement mortar [24]. Sulphoaluminate cement, as a kind of low-carbon cement, has a wide range of market application prospects [25–27].



Figure 2. Classification of polymers used in polymer-modified cement concrete.

In this experiment, AMPS polymer emulsion and polycarboxylic acid were selected as modified substances to be mixed into sulphoaluminate cement paste, mortar, and concrete to enhance the compactness of cement and achieve the purpose of anti-carbonation. This paper's research focuses on the carbonation resistance of sulphoaluminate cement, including: the carbonation mechanism of polymer-modified sulphoaluminate cement; change in compressive strength before and after carbonation; determination of carbonation depth and carbonation area.

2. Raw Materials and Experimental Methods

2.1. Raw Materials

Sulphoaluminate cement is mainly composed of $3CaO \cdot 3Al_2O_3 \cdot CaSO_4$ minerals. The cement has excellent properties, such as early strength, high strength, frost resistance, impermeability, corrosion resistance, and low alkalinity [28–30]. The 42.5 fast-hardening sulphoaluminate cement used in this study was produced by Tangshan Polar Bear Building Materials Co., Ltd. (Tangshan, China). In order to compare the carbonation resistance of sulphoaluminate cement (SAC), 42.5 ordinary Portland cement was also used in the test. Table 1 shows the elements and properties of sulphoaluminate cement (OPC).

Table 1. Composition and properties of sulphoaluminate cement.

Туре	CaO (%)	SiO ₂ (%)	Al ₂ O ₃ (%)	SO ₃ (%)	MgO (%)	Fe ₂ O ₃ (%)	Specific Surface Area (m²/kg)
SAC	43.85	16.15	18.53	12.91	2.86	2.62	350
OPC	64.1	20.9	4.8	3.3	1.8	2.6	430

In this experiment, 3% terpolymer latex (AMPS) was used and its solid content was 38.16%, which is produced by Changshu BATF Technology Co., Ltd. (Changshu, China). The polymer's ionic stability, mechanical stability, centrifugation stability, dilution stability, and storage stability all meet the requirements. The polymer does not stratify after being placed for a long time and the viscosity does not change significantly. SR3 is a polycarboxy-late superplasticizer produced by Chongqing Sansheng Industrial Co., Ltd. (Chongqing, China), with a water-reducing rate of 30%, which is used in the experiment to design the molecular structure of the carboxylic acid copolymer according to the principle of cement dispersion. The molecular structure of this type of water-reducing agent is comb shaped. Therefore, the water-reducing agent does not fall off from the particle surface with the progress of cement hydration, which helps the cement paste to have good fluidity for a long time [31].

2.2. Experimental Methods

Through this experimental research on the carbonation depth and strength of the sulphoaluminate cement paste and mortar mixed with a polymer, and compared with ordinary Portland cement, the anti-carbonation performance of sulphoaluminate-cementbased materials was explored. The content of AMPS was 5%, 10%, and 20% of the mass of sulphoaluminate cement, and the content of polycarboxylate was 0.6%, 1.2%, and 1.8% of the mass of sulphoaluminate cement, respectively. The specific experimental mixture is shown in Tables 2 and 3. The preparation method of the test piece is as follows: after weighing the specified amount, pour it into the cement paste mixer, respectively, stir the material according to the operating specifications, and then quickly put the material into the mold; while loading the fabric, use a scraper to insert the material evenly and then jump. Vibrate on the table, smooth it with a scraper, and put it into a standard curing box for curing. The formed cement paste is demolded after 1 day and then put into water for curing. The SAC specimens were cured in water for 2 days, the OPC specimens were taken out after curing in water for 27 days, and the compressive strength was measured. The prepared test block was placed in a carbonation test box for carbonation, the carbonation pressure was 5 bar (that is, 5 atmospheres), and the carbonation time was 1.5 h. The concrete carbonation test box used in the experiment is NELD-CA070. The specific practical steps in the carbonation of the test samples are as follows: (1) put the test piece into an oven to dry at 50 °C for 24 h; (2) the dried test sample is placed in the test box for carbonation; (3) after carbonation, take out the test samples. The test samples were split into two equal parts and a 1% concentration of phenolphthalein indicator was sprayed on the fracture surface. As shown in Figure 3, from purple to red, or the junction with a noticeable color change, measure the vertical distance of 8 places, calculate the arithmetic mean as the carbonation depth, and then convert it into the area.

Abbroviation	Content							
Abbieviation	Cement/g	AMPS (wt%)	Polycarboxylic Acid (wt%)	W/C				
PO-1 (1)	OPC/140 g	0	0	0.3				
SA-1 (8/17)	OPC/140 g	0	0	0.3				
SA-2 (9/18)	SAC/140 g	0	0	0.35				
SA-3 (5/14)	SAC/140 g	5	0	0.3				
SA-4 (6/15)	SAC/140 g	10	0	0.3				
SA-5 (7/16)	SAC/140 g	20	0	0.3				
SA-6 (10)	SAC/140 g	0	0.6	0.3				
SA-7 (11)	SAC/140 g	0	1.2	0.3				
SA-8 (12)	SAC/140 g	0	1.8	0.3				

Table 2. List of cement paste ingredients.

Abbraviation	Content									
Abbieviation	Cement/g	Polycarboxylic Acid (wt%)	W/C	L/S						
PO-2 (2)	OPC/450 g	0	0	0.5	0.4					
SA-9 (4)	SAC/450 g	0	0	0.5	0.4					
SA-10 (19)	SAC/450 g	5	0	0.5	0.4					
SA-11 (20)	SAC/450 g	10	0	0.5	0.4					
SA-12 (21)	SAC/450 g	20	0	0.5	0.4					
SA-13 (22)	SAC/450 g	0	0.6	0.5	0.4					
SA-14 (23)	SAC/450 g	0	1.2	0.5	0.4					
SA-15 (24)	SAC/450 g	0	1.8	0.5	0.4					

Table 3. List of cement mortar ingredients.



Figure 3. Measurement method of carbonation depth.

The experimental instruments used in the experiment include: electronic scale accurate to 0.1 g; cement paste mixer; $2 \text{ cm} \times 2 \text{ cm} \times 2 \text{ cm}$ cement paste forming mold; jumping table; standard curing oven; oven; self-made carbonized sample; compressive strength test instrument; vernier caliper; beaker; measuring cylinder; scraper; etc.

3. Results and Discussion

3.1. Cement Paste

3.1.1. Compressive Strength of Cement Paste before and after Carbonation

Figure 4 shows the compressive strength of the corresponding specimens before and after carbonation. Compared with the samples of PO-1 and SA-1, the sulphoaluminate cement paste with a water-cement ratio of 0.3 is compared with the Portland cement paste, and the 3-day compressive strength of the sulphoaluminate cement paste was improved. The 28-day compressive strength of sulphoaluminate cement paste is slightly higher than that of Portland cement paste, which verifies the characteristics of early strength and high strength of sulphoaluminate cement. Compared with SA-2, the compressive strength of cement paste decreased slightly with the increase in the water-cement ratio, and the strength loss rate was 10.14%. With the rise in AMPS latex content, the 3-day compressive strength of the sulphoaluminate cement paste with a water-cement ratio of 0.3 gradually decreased. Still, it was higher than the sulphoaluminate cement blank samples with a water-cement ratio of 0.35. Compared with the SA-1 blank sample, when the AMPS polymer emulsion content was 5% and 10% of the cement content, the compressive strength of the

paste test block increased significantly, indicating that after the polymer emulsion was added to the cement paste, the emulsion was lost. The water forms a continuous film, and the film binds the cement hydrates together to create an overall network structure. At the same time, the polymer emulsion fills the micro-cracks inside the cement mortar, improving the specimen's overall compactness. However, when the content of polymer emulsion is 20%, the sample's compressive strength is lower than that of the blank group SA-1. Excessive polymer emulsion is added to the cement paste because the emulsion will lose water and form a film. The hydrated cement particles were wrapped, which hindered the cement's hydration, so the specimen's compressive strength was lower than that of the blank group. For sulphoaluminate cement paste, the optimum dosage of AMPS polymer emulsion is 5%. Compared with the SA-6, SA-7, and SA-8 specimens, it can be found that with the increase in the polycarboxylic acid content, the 3-day compressive strength of the sulphoaluminate cement paste with a water-cement ratio of 0.3 increases gradually and all are higher than SA-1 because adding an appropriate amount of waterreducing agent is beneficial to improve the compactness and working performance of the specimen. SA-6–SA-8 shows a trend of increasing compressive strength. The optimum dosage of polycarboxylate superplasticizer is 1.8% of the cement dosage. According to the requirements of the specification, the obtained test pieces were carbonized, respectively. It can be found that the compressive strength of each test piece after carbonation is lower than that before carbonation. Still, the changing strength trend between groups after carbonation is consistent with that before. Table 4 shows the loss rate of compressive strength of each cement paste specimen after carbonation. Among them, the compressive strength loss rate of ordinary Portland cement paste after carbonation is the smallest, which is 1.01%. The carbonation resistance of the block is better than that of sulphoaluminate cement. For the sulphoaluminate cement paste, the compressive strength loss rate of the paste with a water-cement ratio of 0.3 after carbonation is smaller than that of the paste with a watercement ratio of 0.35. With the increase in the polymer emulsion content, the loss rate of the compressive strength of the pure paste specimens after carbonation increases gradually.



Figure 4. Compressive strength of cement paste before and after carbonation.

Number	PO-1	SA-1	SA-2	SA-3	SA-4	SA-5	SA-6	SA-7	SA-8
The loss rate of compressive strength (%)	1.01	3.06	7.34	5.24	6.58	9.82	5.93	3.98	7.44

Table 4. Loss rate of compressive strength of cement paste after carbonation.

3.1.2. Carbonation Depth/Area of Sulphoaluminate Cement Paste

The carbonized sample of the above sulphoaluminate cement paste was split into two equal parts. The phenolphthalein indicator with a concentration of 1% was sprayed on the fracture surface, as shown in Figure 5. According to the schematic diagram in Figure 3, from the surface of the specimen to the discoloration boundary, measure eight distances, obtain the arithmetic mean value as the carbonation depth h, and then calculate the carbonation area S according to Formula (1). The calculation results of the specific carbonation depth and carbonation area are shown in Table 5.

$$S = 20^2 - (20 - 2h)^2$$
(1)





Figure 5. SA-1–SA-8 after carbonation with 1% concentration of phenolphthalein indicator.

Number	PO-1	SA-1	SA-2	SA-3	SA-4	SA-5	SA-6	SA-7	SA-8
h (mm)	0	0.66	0.76	0.20	0.60	0.80	0.10	0.08	0.05
S (mm ²)	0	51.06	58.49	15.84	46.56	61.44	7.96	6.37	3.99
Carbonation (%)	0	12.765	16.623	3.96	11.64	15.36	1.99	1.593	0.998

Table 5. Carbonation depth and carbonation area of PO-1, SA-1–SA-8.

The following conclusions can be drawn from Table 5: from the carbonation depth (h)/area (S) of the SA-3–SA-5 specimens, it can be seen that with the increase in the amount of incorporated polymer emulsion, the values of h and S gradually increased. It shows that when the amount of polymer emulsion is too great, the internal compactness of the test piece decreases, and the carbonation depth and area of the test piece increase. This phenomenon corresponds to the compressive strength of the test piece and the strength loss rate after carbonation. The carbonation depth and area of SA-3 and SA-4 are smaller than those of SA-1 and SA-2; adding an appropriate amount of polymer emulsion (5–10%) can improve the carbonation resistance of sulphoaluminate cement. Comparing the carbonation depth and area of SA-6–SA-8 specimens, it can be found that the carbonation depth/area are the largest when the polycarboxylate content is 0.6% and the minimum when the content is 1.8%. However, the carbonation depth/area of the samples under these three dosages are smaller than those of SA-1 and SA-2; adding polycarboxylic acid can improve the carbonation resistance of sulphoaluminate cement, and when the dosage is at 1.8%, the carbonation resistance is the best.

3.2. Carbonation of Cement Mortar

3.2.1. Compressive Strength of Cement Mortar before and after Carbonation

It can be seen from Figure 6 that the 3-day compressive strength of sulphoaluminate cement mortar is 31.08% higher than that of PO-2 28-day strength; 5% AMPS polymer emulsion helps to improve the compressive strength of sulphoaluminate cement mortar, and the improvement rate is 20.62%, which is the optimal dosage of polymer emulsion under this system. After carbonating the cement mortar specimens, each specimen's compressive strength loss rate was obtained, as shown in Table 6. After carbonation, the compressive strength of each sample decreased and the changing trend of compressive strength among the groups was consistent with the compressive strength before carbonation. In Table 6 SA-9–SA-12, the compressive strength loss rate increases gradually with the increase in polymer emulsion content. When AMPS was added with 5%, although the carbonation of the specimens had a more significant loss in strength, the strength after carbonation was higher than that of the blank sample (SA-9) before carbonation, indicating that the addition of polymer emulsions can improve the strength of sulphoaluminate and the carbonation resistance of cement mortar. The effect of polycarboxylate on the strength loss rate of sulphoaluminate cement mortar (SA-13-SA-15) after carbonation also showed the same trend; when the content of polycarboxylate was 1.2%, the sulphoaluminate carbonation resistance of the cement mortar specimen is the best. At the same time, it can also be found that the carbonation resistance of ordinary Portland cement mortar specimens is better, and the carbonation loss rate is only 2.43%.



Figure 6. Compressive strength of cement mortar before and after carbonation.

Table 6. Loss rate of compressive strength of cement mortar after carbonation.

Number	PO-2	SA-9	SA-10	SA-11	SA-12	SA-13	SA-14	SA-15
The loss rate of compressive strength (%)	2.43	11.96	15.90	18.35	20.41	14.43	15.51	21.58

3.2.2. Carbonation Depth/Area of Sulphoaluminate Cement Mortar

The cement mortar carbonized sample was split into two equal parts; see Section 3.1.2 for the specific operation method, as shown in Figure 7. According to the schematic diagram in Figure 3, from the surface of the specimen to the discoloration boundary,

measure eight distances, obtain the arithmetic mean value as the carbonation depth h, and then calculate the carbonation area S according to Formula (1). The calculation results of the specific carbonation depth and carbonation area are shown in Table 7. From the carbonation depth/area of SA-10 to SA-12, it can be seen that with the increase in the amount of polymer emulsion incorporated, the carbonation depth/area gradually increase, and the carbonation depth/area ratio of SA-10 and SA-11 is SA. The -9 is smaller, while the SA-12 is significantly larger than the SA-9. That is to say, when the addition of polymer emulsion is 5% and 10%, the carbonation resistance of sulphoaluminate cement can be improved. When the addition amount reaches 20%, its carbonation resistance ability is reduced. It can be seen from the carbonation depth/area of SA-13 to SA-15 that the carbonation depth/area is the smallest when the content of polycarboxylic acid is 1.8%. However, the carbonation depth/area of the samples under these three dosages are smaller than those of the blank sample (SA-9); the polycarboxylate increases the carbonation resistance of sulphoaluminate cement under these three dosages. The best resistance to carbonation is when the dosage is 1.8%.



Figure 7. PO-2, SA-9–SA-15 after carbonation with 1% concentration of phenolphthalein indicator.

Number	PO-2	SA-9	SA-10	SA-11	SA-12	SA-13	SA-14	SA-15
h (mm)	0	2.9	2.2	2.4	3.10	1.6	0.80	0.42
S (mm ²)	0	198.36	156.64	168.96	209.56	117.76	61.44	32.89
Carbonation (%)	0	49.59	39.16	42.24	52.39	29.44	15.36	8.223

 Table 7. Carbonation depth and carbonation area of PO-2, SA-9–SA-15.

4. Conclusions and Outlook

In this paper, research was conducted on the optimal dosage of sulphoaluminate cement paste and mortar mixed with polymer emulsion and polycarboxylic acid. Research was also conducted on the carbonation level and strength before and after carbonation of sulphoaluminate cement paste and mortar-mixed polymer, and polycarboxylic acidwas obtained. The following conclusions were obtained.

- (1) For the cement paste, with the increase in polymer emulsion AMPS content, the 3-day strength of the sulphoaluminate cement with a water-cement ratio of 0.3 gradually decreased. When the addition amount is 5% and 10%, the carbonation resistance of sulphoaluminate cement can be improved. In contrast, the addition amount of 20% can reduce its carbonation resistance. The optimum amount of polymer emulsion for the sulphoaluminate cement paste system is 5%. The addition of polycarboxylic acid improves the carbonation resistance of sulphoaluminate cement, and the carbonation resistance is the best when the addition amount is 1.8%.
- (2) For the cement mortar, with the increase in the polymer emulsion content, the compressive strength of the sulphoaluminate cement mortar showed a downward trend, but it was higher than that of the blank sample (SA-9). The compressive strength of

sulphoaluminate cement increases with the increase in acid content. After carbonation, the compressive strength of each sample decreased, and the changing trend of compressive strength among the groups was consistent with that before carbonation; with the increase in the amount of polymer emulsion incorporated, the carbonation depth/area gradually increased and the polymer emulsion carbonation resistance of sulphoaluminate cement mortar is the best when the addition amount is 5%.

This paper aimed to find a polymer that can be incorporated into sulphoaluminate cement to improve its anti-carbonation ability and to determine the optimal amount of polymer to achieve the best anti-carbonation effect for sulphoaluminate cement concrete. After repeated tests, it was found that the anti-carbonation result of sulphoaluminate cement paste and mortar is the best when the content of polycarboxylic acid is 1.8%. On this basis, it is necessary to try adding other types of polymers and different types of concrete additives to improve the carbonation resistance of sulphoaluminate cement. Follow-up research is urgently needed.

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References

- 1. Xue, W.; Liu, W.; Gao, C.; Fan, H.; Zhang, H. Experimental study of permeability evolution in modified desulfurization gypsum under complete stress–strain process. J. Clean. Prod. 2022, 359, 132185. [CrossRef]
- Vo, D.-H.; Do, N.-D.; Mamuye, Y.; Liao, M.-C.; Hwang, C.-L.; Tran, Q.-T. Engineering, properties and durability of concrete samples designed by densified mixture design algorithm (DMDA) method incorporating steel reducing slag aggregate. *Constr. Build. Mater.* 2022, 354, 129180. [CrossRef]
- 3. Ho, L.S.; Huynh, T.-P. Recycled waste medical glass as a fine aggregate replacement in low environmental impact concrete: Effects on long-term strength and durability performance. *J. Clean. Prod.* **2022**, *368*, 133144. [CrossRef]
- 4. Looney, T.; Leggs, M.; Volz, J.; Floyd, R. Durability and corrosion resistance of ultra-high performance concretes for repair. *Constr. Build. Mater.* **2022**, *3*45, 128238. [CrossRef]
- Singh, P.; Roy, A.B.D.; Singh, H. Mechanical and durability properties of concrete incorporating weathered coarse Linz-Donawitz (LD) steel slag. J. Build. Eng. 2022, 61, 105301. [CrossRef]
- 6. Praseeda, D.; Srinivasa Rao, K. Durability performance and microstructure analysis of nano engineered blended concrete. *Clean. Mater.* **2022**, *6*, 100155. [CrossRef]
- Kalyana Chakravarthy, P.R.; Namratha, K. Strength and durability properties of high strength self compacting concrete. Mater. Today Proc. 2022, 69, 896–900. [CrossRef]
- 8. Taffese, W.Z.; Espinosa-Leal, L. Prediction of chloride resistance level of concrete using machine learning for durability and service life assessment of building structures. *J. Build. Eng.* **2022**, *60*, 105146. [CrossRef]
- 9. Xue, W.; Mao, X.; Xu, W.; Zhang, H.; Gao, C. Macro-and meso-scale study on dynamic mechanical properties of shaft lining concrete exposed to high water pressure. *Case Stud. Constr. Mater.* **2022**, *17*, e1502. [CrossRef]
- 10. Chen, D.; Liu, S.; Shen, J.; Sun, G.; Shi, J. Experimental study and modelling of concrete carbonation under the coupling effect of freeze-thaw cycles and sustained loads. *J. Build. Eng.* **2022**, *52*, 104390. [CrossRef]
- Ding, Z.; Quy, N.X.; Kim, J.; Hama, Y. Evaluations of frost and scaling resistance of fly ash concrete in terms of changes in water absorption and pore structure under the accelerated carbonation conditions. *Constr. Build. Mater.* 2022, 345, 128273. [CrossRef]
- 12. Liu, Z.; van den Heede, P.; Zhang, C.; Shi, X.; Wang, L.; Li, J.; Yao, Y.; de Belie, N. Influence of sustained compressive load on the carbonation of concrete containing blast furnace slag. *Constr. Build. Mater.* **2022**, *335*, 127457. [CrossRef]
- Chang, J.; Jiang, T.; Cui, K. Influence on compressive strength and CO₂ capture after accelerated carbonation of combination β-C₂S with γ-C₂S. *Constr. Build. Mater.* 2021, 312, 125359. [CrossRef]
- 14. Ming, J.; Wu, M.; Shi, J. Passive film modification by concrete carbonation: Re-visiting a corrosion-resistant steel with Cr and Mo. *Cem. Concr. Compos.* **2021**, *123*, 104178. [CrossRef]

- 15. Mei, K.; He, Z.; Yi, B.; Lin, X.; Wang, J.; Wang, H.; Liu, J. study on electrochemical characteristics of reinforced concrete corrosion under the action of carbonation and chloride. *Case Stud. Constr. Mater.* **2022**, *17*, e1351. [CrossRef]
- Andrade, H.D.; de Carvalho, J.M.F.; Costa, L.C.B.; Elói, F.P.D.F.; e Silva, K.D.D.C.; Peixoto, R.A.F. Mechanical performance and resistance to carbonation of steel slag reinforced concrete. *Constr. Build. Mater.* 2021, 298, 123910. [CrossRef]
- Wu, K.; Luo, S.; Zheng, J.; Yan, J.; Xiao, J. Influence of carbonation treatment on the properties of multiple interface transition zones and recycled aggregate concrete. *Cem. Concr. Compos.* 2022, 127, 104402. [CrossRef]
- 18. Li, T.; Wang, S.; Xu, F.; Meng, X.; Li, B.; Zhan, M. Study of the basic mechanical properties and degradation mechanism of recycled concrete with tailings before and after carbonation. *J. Clean. Prod.* **2020**, *259*, 120923. [CrossRef]
- 19. Cui, K.; Chang, J.; Sabri, M.M.S.; Huang, J. Influence of Graphene Nanoplates on Dispersion, Hydration Behavior of Sulfoaluminate Cement Composites. *Materials* **2022**, *15*, 5357. [CrossRef]
- 20. Cui, K.; Chang, J.; Sabri, M.M.S.; Huang, J. Study of Dispersion, Hydration, and Microstructure of Graphene Nanoplates-Modified Sulfoaluminate Cement Paste. *Nanomaterials* **2022**, *12*, 2708. [CrossRef]
- Cui, K.; Chang, J.; Feo, L.; Chow, C.L.; Lau, D. Developments and Applications of Carbon Nanotube Reinforced Cement-Based Composites as Functional Building Materials. *Front. Mater.* 2022, *9*, 146. [CrossRef]
- Dakwale, V.A.; Pachpor, P.D.; Mahesh, S.; Namdeo, D. Use of metakaolin with polymer modified concrete in repairing of structures. *Mater. Today Proc.* 2022, *in press.* [CrossRef]
- 23. Gwon, S.; Jang, S.Y.; Shin, M. Microstructure evolution and strength development of ultra rapid hardening cement modified with redispersible polymer powder. *Constr. Build. Mater.* **2018**, *192*, 715–730. [CrossRef]
- 24. Chang, J.; Li, W.; Wang, D.; Zhang, Y. Effect of silicate modulus on tensile properties and microstructure of waterproof coating based on polymer and sodium silicate-activated GGBS. *Constr. Build. Mater.* **2020**, 252, 119056. [CrossRef]
- 25. Cui, K.; Lau, D.; Zhang, Y.; Chang, J. Mechanical properties and mechanism of nano-CaCO₃ enhanced sulphoaluminate cement-based reactive powder concrete. *Constr. Build. Mater.* **2021**, *309*, 125099. [CrossRef]
- Cui, K.; Liang, K.; Chang, J.; Lau, D. Investigation of the macro performance, mechanism, and durability of multiscale steel fiber reinforced low-carbon ecological UHPC. *Constr. Build. Mater.* 2022, 327, 126921. [CrossRef]
- Cui, K.; Chang, J. Hydration, reinforcing mechanism, and macro performance of multi-layer graphene-modified cement composites. J. Build. Eng. 2022, 57, 104880. [CrossRef]
- 28. Ioannou, S.; Chowdhury, M.; Badr, A. Conformity of the performance of calcium sulfoaluminate cement based concretes to empirical models in current international design standards. *Constr. Build. Mater.* **2022**, *326*, 126748. [CrossRef]
- Kleib, J.; Aouad, G.; Benzerzour, M.; Zakhour, M.; Abriak, N. Effect of calcium sulfoaluminate cements composition on their durability. *Constr. Build. Mater.* 2021, 307, 124952. [CrossRef]
- Tambara, L.U.D., Jr.; de Matos, P.R.; Lima, G.S.; Silvestro, L.; Rocha, J.C.; Campos, C.E.M.; Gleize, P.J. effect of the nanosilica source on the rheology and early-age hydration of calcium sulfoaluminate cement pastes. *Constr. Build. Mater.* 2022, 327, 126942. [CrossRef]
- 31. Hao, Y.; Yang, G.; Liang, K. Development of fly ash and slag based high-strength alkali-activated foam concrete. *Cem. Concr. Compos.* **2022**, *128*, 104447. [CrossRef]