

## *Supplementary Material*

### **CeFeO<sub>3</sub>–CeO<sub>2</sub>–Fe<sub>2</sub>O<sub>3</sub> systems: synthesis by solution combustion method and catalytic performance in CO<sub>2</sub> hydrogenation**

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Chemical equations with fuel to calculate the amount of reagents

#### **Glycine**

Total valency of glycine:  $C_2H_5NO_2 = 4 \cdot 2 + 1 \cdot 5 - 2 \cdot 2 = +9$

Total valency of oxidizers:  $Ce(NO_3)_3 = 3 - 2 \cdot 3 \cdot 3 = -15$ ;  $Fe(NO_3)_3 = 3 - 2 \cdot 3 \cdot 3 = -15$

1)  $\varphi=1$ :  $3Ce(NO_3)_3(aq) + 3Fe(NO_3)_3(aq) + 10C_2H_5NO_2 \rightarrow 3CeFeO_3 + 20CO_2 + 14N_2 + (25H_2O)$

2)  $\varphi=1.25$ :  $24Ce(NO_3)_3(aq) + 24Fe(NO_3)_3(aq) + 100C_2H_5NO_2 + 45O_2 \rightarrow 24CeFeO_3 + 200CO_2 + 122N_2 + (250H_2O)$

3)  $\varphi=1.4$ :  $3Ce(NO_3)_3(aq) + 3Fe(NO_3)_3(aq) + 14C_2H_5NO_2 + 9O_2 \rightarrow 3CeFeO_3 + 28CO_2 + 16N_2 + (35H_2O)$

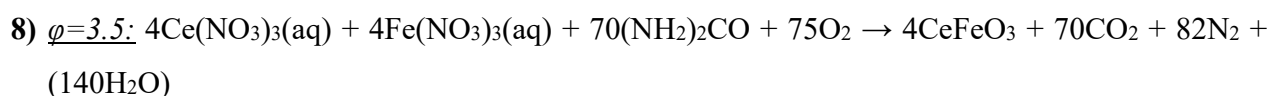
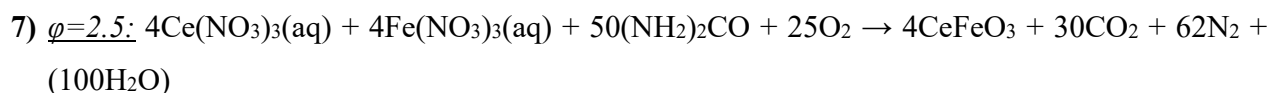
4)  $\varphi=1.5$ :  $4Ce(NO_3)_3(aq) + 4Fe(NO_3)_3(aq) + 20C_2H_5NO_2 + 15O_2 \rightarrow 4CeFeO_3 + 40CO_2 + 22N_2 + (50H_2O)$

#### **Urea**

Total valency of urea:  $(NH_2)_2CO = 1 \cdot 4 + 4 - 2 = +6$

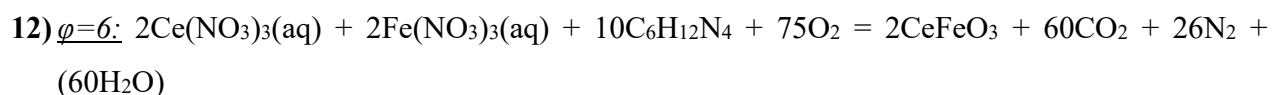
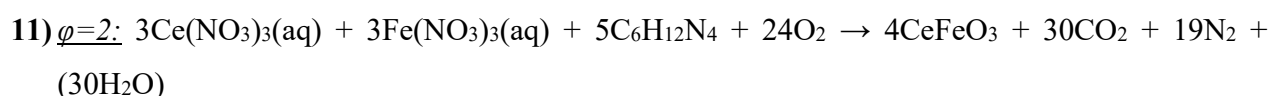
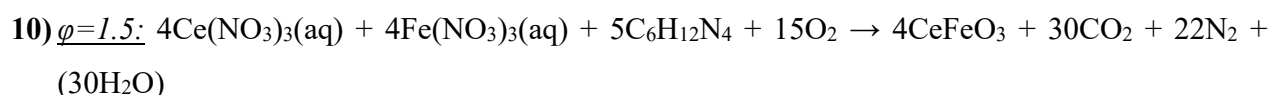
5)  $\varphi=1$ :  $Ce(NO_3)_3(aq) + Fe(NO_3)_3(aq) + 5(NH_2)_2CO \rightarrow CeFeO_3 + 5CO_2 + 8N_2 + (10H_2O)$

6)  $\varphi=1.5$ :  $4Ce(NO_3)_3(aq) + 4Fe(NO_3)_3(aq) + 30(NH_2)_2CO + 15O_2 \rightarrow 4CeFeO_3 + 30CO_2 + 42N_2 + (60H_2O)$



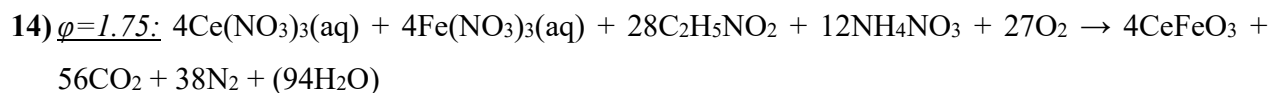
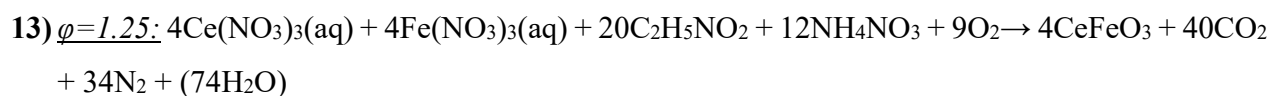
### **Urotropine**

Total valency of urotropine:  $\text{C}_6\text{H}_{12}\text{N}_4 = 4 \cdot 6 + 1 \cdot 12 = +36$



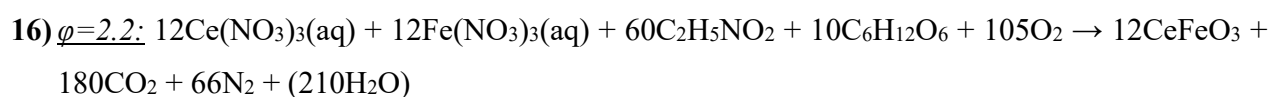
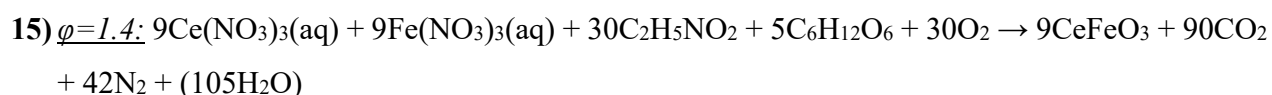
### **Glycine and $\text{NH}_4\text{NO}_3$**

Total valency of oxidizers:  $\text{NH}_4\text{NO}_3 = 1 \cdot 4 - 2 \cdot 3 = -2$

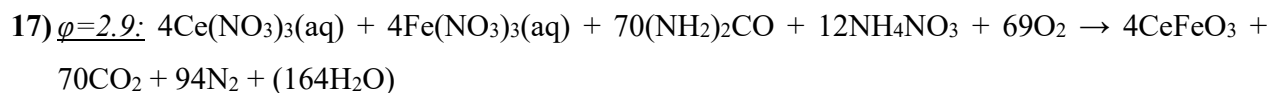


### **Glycine and glucose**

Total valency of glucose:  $\text{C}_6\text{H}_{12}\text{O}_6 = 4 \cdot 6 + 1 \cdot 12 - 2 \cdot 6 = +24$



### **Urea and $\text{NH}_4\text{NO}_3$**



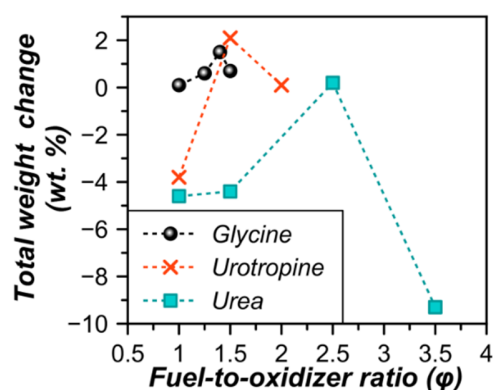


Figure S1. Total weight change during heating in air from 25 to 800 °C for the as-prepared samples produced by SCS using different fuels, additives and fuel-to-oxidizer ratios.

Table S1. Assignment of major absorption IR spectra peaks for the as-prepared samples produced by solution combustion synthesis using different fuels.









Wavenumber, $\text{cm}^{-1}$	Assignment	Substance
3727	$\nu(\text{OH})$	adsorbed $\text{H}_2\text{O}$
3343–3453	$\nu_s, \nu_{as}(\text{H}_2\text{O})$	
3212–3430	$\nu_s, \nu_{as}(\text{NH}_3)$	
2959	$\nu(\text{CH})$	unreacted fuel
2920–2924	$\nu_{as}(\text{CH}_2)$	
2852–2854	$\nu_s(\text{CH}_2)$	
2100–2105	$\nu(-\text{C}\equiv\text{C}-)$	
1709	$\nu(\text{C}=\text{O})$	
1664–1667	$\nu_{as}(\text{COO}), \nu(\text{C}=\text{O})$	
1619–1621	$\beta_{as}(\text{NH}_3)$	
1446	$\delta(\text{CH}_2)$	
1383–1385	$\nu_s(\text{NO}_3^-)$	unreacted nitrate groups
1115–1156	$\rho(\text{NH}_3)$	unreacted fuel
548–552, 404–406	$\nu(\text{FeO})$	$\text{CeFeO}_3$
Symbols for vibrations: $\nu$ , stretching; $\delta$ , deformation; $\beta$ , bending; $\rho$ , rocking; as, antisymmetric; s, symmetric.		

Table S2. Data on the phase composition, crystallinity and reproducibility of the synthesized materials according to the refinement by the Rietveld method.

Sample N	Fuel	n(AN)/ n(MeN)	$\phi$	Phase composition (Rietveld refinement), wt%			D (1), nm	D (2), nm	D (3), nm	$R_{wp}/R_e$
				CeFeO <sub>3</sub>	CeO <sub>2</sub>	$\gamma$ -Fe <sub>2</sub> O <sub>3</sub>				
1	Glycine	–	1	81	19	0	67.5	4.7	–	–
2		–	1.25	78	12	10	66.0	7.5	6.7	1.14
3-1		–	1.4	95	5	0	61.3	25.0	–	1.16
3-2				93	7	0	64.0	14.5	–	1.11
4		–	1.5	87	13	0	56.8	9.0	–	–
5-1		1.5	1.25	96	4	0	69.1	15.6	–	1.13
5-2				94	6	0	72.0	18.6	–	1.13
6			1.75	33	47	20	32.7	14.8	14.7	1.03
7	Glycine+ glucose	–	1.4	63	23	14	52.0	19.4	14.3	–
8	Urea	–	2.5	52	28	20	68.6	5.8	4.0	–
9-1		–	3.5	80	13	7	72.0	4.7	6.3	1.09
9-2				84	16	0	60.4	4.2	–	1.10
10-1		1.5	2.9	91	9	0	66.5	22.0	–	1.17
10-2				92	8	0	72.0	13.1	–	1.11
11-1	Urotropine	–	1.5	48	33	19	75.1	22.1	15.8	–
11-2				42	42	16	74.5	12.5	25.3	1.05
12		–	2	61	23	16	60.0	16.4	7.1	1.09

Note: AN – ammonium nitrate; MeN – cerium and iron nitrates;  $\phi$  – fuel-to-oxidizer ratio; 1 – CeFeO<sub>3</sub>; 2 – CeO<sub>2</sub>; 3 –  $\gamma$ -Fe<sub>2</sub>O<sub>3</sub>; the ratio of the weighted ( $R_{wp}$ ) and expected ( $R_e$ ) R-factors characterizes goodness of fit, if the squared value is equal to one or constant the refinement procedure is complete.

Table S3. Influence of additions (glucose, NH<sub>4</sub>NO<sub>3</sub>) on glycine(or urea)-nitrate solution combustion process and the obtained SCS products.

Fuel, addition	Glycine, glucose	Glycine, NH <sub>4</sub> NO <sub>3</sub>	Glycine, NH <sub>4</sub> NO <sub>3</sub>	Urea, NH <sub>4</sub> NO
$\phi$	1.4	1.25	1.75	2.9
Course of the reaction				
Macromorphology of the obtained materials				
Total $\Delta m$ during heating up to 800 °C in air, wt%	+0.9	+1.2	–1.2	–1.0
Weight gain, wt%	1.6	2.5	0.5	2.5

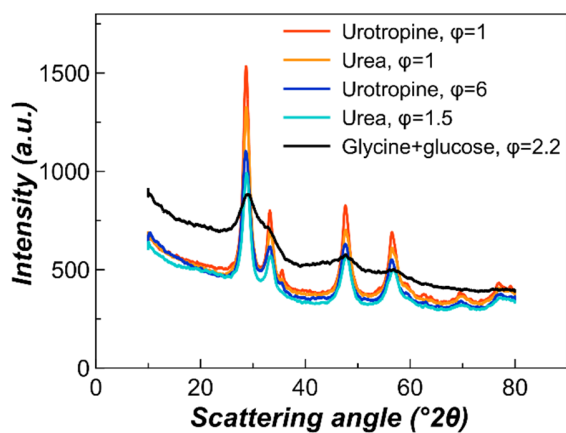


Figure S2. XRD data for Ce-Fe oxide systems obtained by the SCS method using various types of fuel and fuel-to-oxidizer ratios.

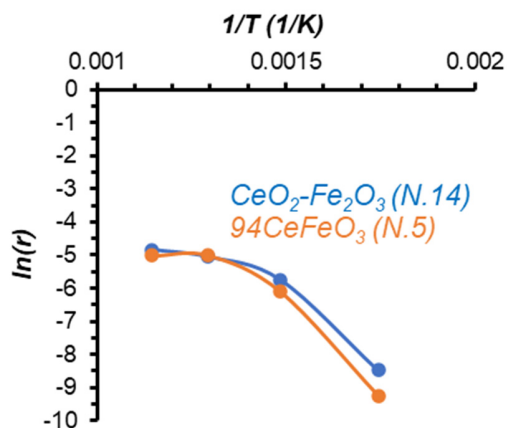
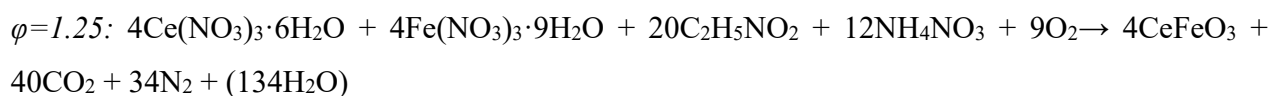


Figure S3. Dependence of the rate for a heterogeneous catalytic reaction on temperature.

### Mass balance

Given:



$$m(\text{CeFeO}_3) = 1 \text{ g}$$

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$$V(\text{CO}_2) = ?$$

Solution:

Table S4. The mass balance of combustion process

Compound	M, g/mol	Input		Output	
		m <sub>1</sub> , g	N <sub>1</sub> , mol	m <sub>2</sub> , g	N <sub>2</sub> , mol
Ce(NO <sub>3</sub> ) <sub>3</sub> ·6H <sub>2</sub> O	434.2	1.780	0.004	0	0

Fe(NO <sub>3</sub> ) <sub>3</sub> ·9H <sub>2</sub> O	404.0	1.656	0.004	0	0
C <sub>2</sub> H <sub>5</sub> NO <sub>2</sub>	75.1	1.539	0.020	0	0
NH <sub>4</sub> NO <sub>3</sub>	80.0	0.984	0.012	0	0
O <sub>2</sub>	32.0	0.295	0.009	0	0
CeFeO <sub>3</sub>	244.0	0	0	1.000	0.004
CO <sub>2</sub>	44.0	0	0	1.804	0.041
N <sub>2</sub>	28.0	0	0	0.976	0.035
H <sub>2</sub> O	18.0	0	0	2.474	0.137
<b>Sum</b>	<b>-</b>	<b>6.254</b>	<b>0.050</b>	<b>6.254</b>	<b>0.217</b>

Table S5. Calculation of the volume of released CO<sub>2</sub> and time for its conversion

<b>m(CeFeO<sub>3</sub>), g</b>	<b>V(CO<sub>2</sub>), L</b>	<b>H<sub>2</sub>:CO<sub>2</sub> ratio</b>	<b>WHSV, mL· g<sup>-1</sup>·h<sup>-1</sup></b>	<b>Volumetric flow rate of CO<sub>2</sub> for hydrogenation, L/min</b>	<b>Conversion of CO<sub>2</sub> at 600 °C</b>	<b>Conversion time, min</b>
1	0.92	-		-	-	-
0.3	0.28	3:1	10,000	0.01	0.41	11.5
0.1	0.09	1:1	72,000	0.04	0.28*	0.63

Note: \*the mean value