

Article

More Wind Power Integration with Adjusted Energy Carriers for Space Heating in Northern China

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Abstract: In Northern China, due to the high penetration of coal-fired cogeneration facilities, which are generally equipped with extraction-condensing steam turbines, lots of wind power resources may be wasted during the heating season. In contrast, considerable coal is consumed in the power generation sector. In this article, firstly it is revealed that there exists a serious divergence in the ratio of electrical to thermal energy between end users' demand and the cogenerations' production during off-peak load at night, which may negate active power-balancing of the electric power grid. Secondly, with respect to this divergence only occurring during off-peak load at night, a temporary proposal is given so as to enable the integration of more wind power. The authors suggest that if the energy carrier for part of the end users' space heating is switched from heating water to electricity (e.g., electric heat pumps (EHPs) can provide space heating in the domestic sector), the ratio of electricity to heating water load should be adjusted to optimize the power dispatch between cogeneration units and wind turbines, resulting in fuel conservation. With this proposal, existing infrastructures are made full use of, and no additional ones are required. Finally a numerical simulation is performed in order to illustrate both the technical and economic feasibility of the aforementioned proposal, under ongoing infrastructures as well as electricity and space heating tariff conditions without changing participants' benefits. The authors aim to persuade Chinese policy makers to enable EHPs to provide space heating to enable the integration of more wind power.

Keywords: electric heat pumps (EHPs); electric heating; coal-fired cogeneration; energy carriers; wind power integration

1. Introduction

In order to meet the abundant space heating demand efficiently, district heating and coal-fired cogeneration units equipped with extraction-condensing steam turbines have been encouraged. They have seen a high penetration in Northern China [1–3], which has 17.6% of the total fossil fuel power plants with rapid growth up to 18.5%. Northern China covers the northwest grid, north grid and southeast grid [4,5]. This can be attributed to the fuel conservation which may be obtained based on coal-fired cogeneration units [6]. In fact it seems to make sense, because coal has always been the dominant primary fuel in the Chinese power sector [7,8]. Under this condition, heating water is generally treated as an energy carrier for space heating purposes by Chinese policy makers, so that large scale heat-metering and remote control are carried out for energy conservation [9,10]. Because coal-fired cogeneration units have to generate electrical power along with thermal power according to [11,12], practical cogeneration units in Northern China are only allowed by Chinese policy makers to generate electricity in terms of heating water production. However, power balancing may cause a situation where wind power needs to be curtailed in the electric power grid such as in regions like Inner Mongolia [3]. This is at odds with the current power dispatch policy in the electric power grid of China, which emphasizes that utilization of wind power should be a priority [5,13], while the mass introduction of wind power has been available and seems powerful during winter nights [14,15]. With regard to the aforementioned situation in Northern China, it is generally suggested that more transmission infrastructure should be constructed to accommodate the surplus wind power, but this solution relies heavily on the policy framework, capital investment, *etc.*, and cannot be implemented immediately. In addition, surplus wind power mostly occurs during off-peak load at night, which could mainly be attributed to the opposite fluctuation patterns of wind power and grid load [14,15] and makes the new transmission infrastructure not economical enough.

Some promising alternative technologies appear to facilitate the wind power integration, including pumped storage, electric vehicles, heating storage, flexible district heating and cogenerations, as well as electric heat boilers and heat pumps [3,16–19]. Besides, some energy model review works have been carried out so as to enable more integration of renewable energy [20–22]. The impact of various characteristics of electricity and heating demand on optimal configuration of a microgrid is revealed in [23]. In particular, EHPs are recommended as one promising alternative solution in both Europe and Japan in [19,24–30], because they help to change the characteristics of end use of electricity and heat.

Based on the aforementioned works, firstly the authors suggest that a serious divergence may exist in the ratio of electrical to thermal energy between end users' demand and the cogeneration units' production during off-peak load at night that prevents more wind power integration (here, off-peak load at night means from 0:00~7:00 o'clock) instead of inadequate transmission infrastructures. In addition, end users' load patterns of electricity and space heating have not been considered to be adjustable for optimizing the dispatch between cogenerations and wind turbines, which can help to

relieve the link between the electrical and thermal power. Finally because neither performance of cogeneration units nor the market mechanism is like that described in [16–30], it is worth discussing both the technical and economic feasibility of mass introduction of EHPs in Northern China.

In this article, the authors suggest a possible way to adjust the end users' electrical and thermal energy consumption during off-peak load at night without new investments. First, existing various air-conditioners (or EHPs) which have been installed in end-users' site should be enabled to provide space heating in the domestic sector, so that the energy carriers for part of the end users' space heating can be switched from heating water to electricity. Thus no supplemental investment is needed. Secondly, what about the adjustable load pattern in the residential sector? Thirdly, gross electrical and thermal energy production seem to be adjusted so as to optimize the dispatch between coal-fired cogeneration facilities and wind turbines, which depends on the practical performance of cogenerations in Northern China and results in a critical coefficient of performance (COP) of electric heat pumps introduced. Finally, a numerical simulation is performed to illustrate the feasibility of the authors' proposal. This article is configured in six sections. Besides this section that serves as Introduction, the serious divergence of the ratio of electrical to thermal energy between the end users' demand and the cogeneration production is covered in Section 2. The authors' proposal is put forth in Section 3. Section 4 is devoted to a numerical simulation. Results and Discussion are given in Section 5. Finally, Conclusions are drawn in Section 6.

2. Performance of End Users and Cogenerations

In accordance with the present Chinese policy framework: (1) Heating water is generally adopted for the end users' space heating; (2) Cogeneration units have to generate corresponding electricity in terms of heating water. These two issues directly result in a divergence in the ratio of electrical to thermal energy between the end users' demand and the cogenerations' production during off-peak load at night, which to some extent has a negative impact on wind power integration [15].

2.1. End Users' Load

The authors have developed experiment projects [31,32], through which field investigation of 10 households could be conducted in Northern China. Thus both electricity for electric appliances and thermal energy consumption values for space heating purpose have been obtained and are shown in Figures 1–2, respectively, which correspond to about 10 households from 0:00~7:00 o'clock in a day. The ratio of electricity to thermal energy consumption is shown in Figure 3. H1~H10 means household 1~10.

As described in Figures 1–3, little electricity consumption appears, in contrast to much more thermal energy consumption, which results in relatively low values in the ratio of electricity to thermal energy consumption. The present energy market regulations in China result in the existence of two main separate energy service infrastructures. Electric power grid is for electricity service and the district heating networks are for heating service. In addition, the prices of these two energy carriers are regulated by the government.

Figure 1. Electricity consumption of 10 households for electric appliances.

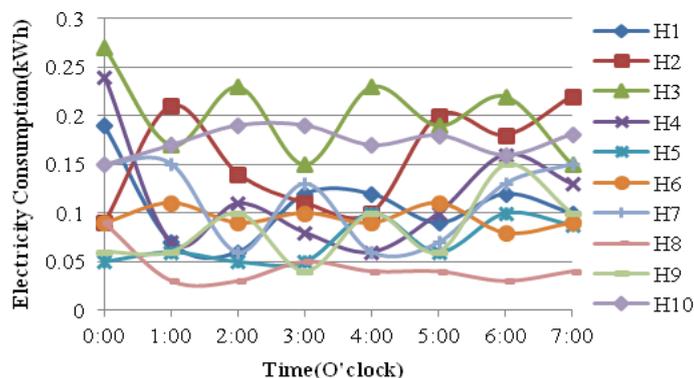


Figure 2. Thermal energy consumption of 10 households for space heating.

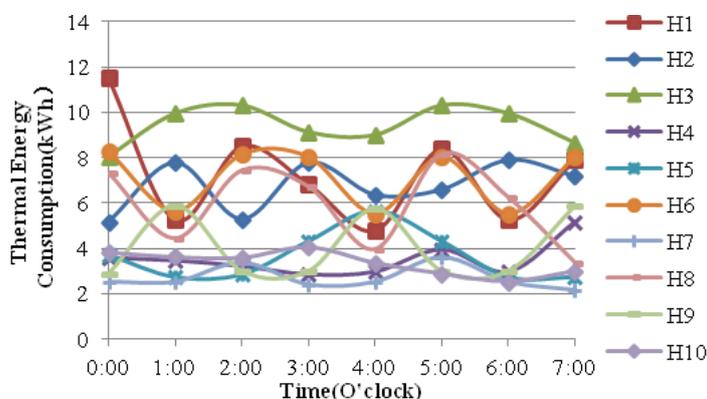
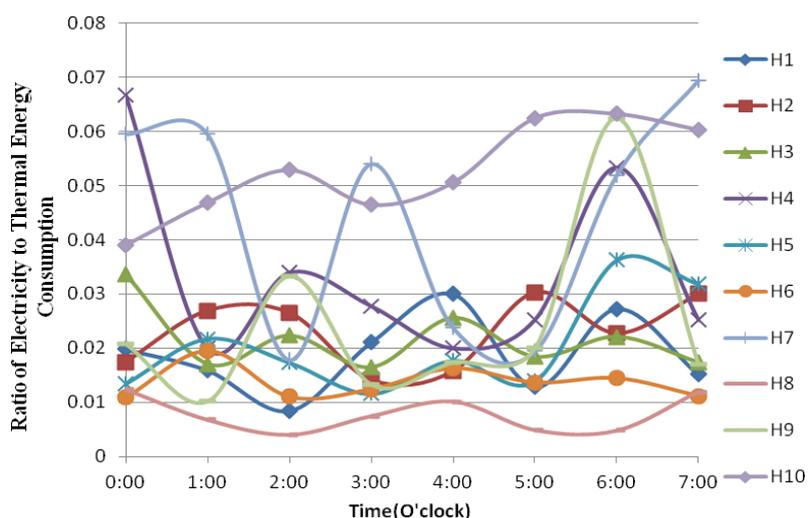


Figure 3. Ratio of electricity to thermal energy consumption of 10 households.

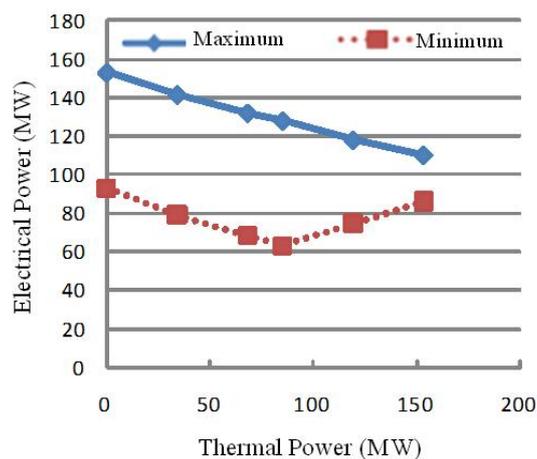


Currently the electricity cost for space heating purposes seems much more expensive than heating water. With regard to Figures 1–3, it can be explained as follows: during the night most end users in the domestic sector are asleep, so little electricity is consumed while abundant heating water is needed for space heating purposes. The small electricity load could be covered by electrical power generated from cogeneration units, while the abundant heating water was covered by thermal power generated from cogenerations. It is emphasized that 10 households seem insufficient, and only reveal the authors’ idea.

2.2. Cogenerations' Production

The authors have established remote metering and dispatch infrastructures in the electric power grid of Northern China [31], so that a PQ-chart (electrical power *versus* thermal power chart) for a condensing-extraction cogeneration C135/N150-13.24 unit is achieved. This PQ-chart is shown in Figure 4 and can be formulated as Equations (1,2).

Figure 4. PQ-chart of C135/N150-13.24.

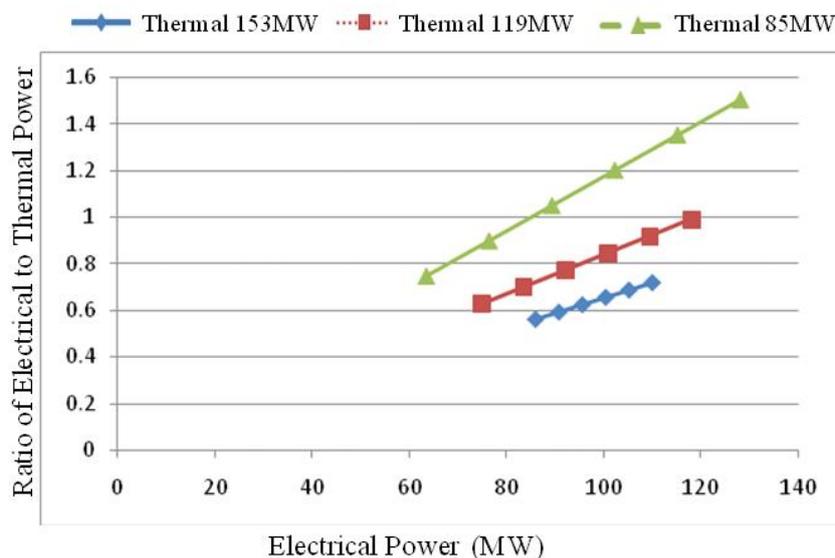


$$P^{\max} = -0.279 \cdot Q + 151.9 \quad 0 \leq Q \leq 153 \tag{1}$$

$$P^{\min} = \begin{cases} -0.344 \cdot Q + 92.06 & 0 \leq Q < 85 \\ 0.33 \cdot Q + 35.32 & 85 \leq Q \leq 153 \end{cases} \tag{2}$$

where P^{\max} and P^{\min} are the maximum and minimum electrical power, respectively, *versus* a certain thermal power Q generated. According to the PQ-chart of Figure 4, the electrical power relies on thermal power, so the ratio of electrical to thermal power is limited within a certain range. This ratio is shown in Figure 5.

Figure 5. Ratio of electrical to thermal power of C135/N150-13.24.



It can be found that the more thermal power generated, the lower is the ratio of electrical to thermal power generated. It can be seen that this ratio of cogeneration in Figure 5 is much more than that of the end users in Figure 3. This can be attributed to the fact that the households' electrical energy consumption is separated from thermal energy consumption, which is different from that of cogeneration units' production. From Figures 3 and 5, it can be inferred that there is a considerable diversity between the end users' energy consumption and cogeneration facilities' production, even though it is only based on 10 households. It is deduced that as long as high penetration coal-fired cogeneration power is available, the electric power grid is rigid and wind power may be curtailed.

From the abovementioned investigation of both the end users and cogenerations, it can be found that heating water should not be treated as sole energy carrier for space heating purposes in Northern China, because it has a negative impact on the wind power integration.

3. Proposal

In Section 3, the authors suggest that both heating water and electricity should be used as energy carriers for space heating, so that part of the end users' space heating load could be switched from heating water to electricity. Thus the ratio of electricity to thermal load is changed and this leads to a new optimal dispatch scenario between cogeneration units and wind turbines. While cogeneration units' heating water is shaved, less electricity from cogeneration will be obtained and more wind power may be integrated.

With regard to the authors' proposal, three issues should be emphasized: (1) The authors' proposal is to be performed temporarily during off-peak load at night (e.g., 0:00~7:00), when most end users are asleep and are not so sensitive to thermal comfort; (2) All kinds of existing EHPs, including air source EHPs, geothermal EHPs, and water source EHPs can be used. Generally speaking, the coefficient of performance (COP) under electrical resistance heater mode is minimum and around 1 [19,24–28]. In China, air-conditioners (they can also perform in EHP mode for space heating) installed in the domestic sector for space cooling with mandatory minimum COP values above 3 [33], the authors' proposal seems to guarantee the COP of EHPs for space heating beyond 1 without much auxiliary investment; (3) Based on the emerging infrastructures such as smart grids, remote control on either heating water radiators or EHPs for end users' space heating in domestic sector is enabled [9,10,31,32]. The authors aim to persuade the Chinese policy makers from three aspects that:

1. Is it technically feasible according to the COP of present EHPs?
2. In 3.1, the authors formulate one optimization problem for a critical COP of EHPs cooperating with a single cogeneration to serve space heating, beyond which fuel conservation is achieved.
3. Is it of fuel conservation while introducing EHPs?
4. In 3.2, the authors formulate the other new optimization problem so as to calculate the fuel conservation from more wind power integration while COP is in the range of 1.0~6.0. This is separated from the optimization problem for a critical COP of EHPs abovementioned.
5. Is it economically feasible?

In Section 3.3, the authors are devoted to economic feasibility of this proposal based on present policy framework in China. In this article, the unit for power is set as MW, and for energy as MWh.

3.1. Mathematic Model Regarding Critical COP of EHPs

Currently original end users' space heating load Q_{Load}^* (MW) is assumed to be thoroughly served by cogeneration units' thermal power production (heating water), which is formulated as Equation (3). The original end users' electricity load P_{Load}^* (MW) for electric appliances is provided by the cogeneration units' electrical power production, which is formulated as Equation (4). Both Q_{Load}^* and P_{Load}^* are the boundary conditions of this optimization model. Variables with subscript * mean performing under existing operation mode like Equations (3,4):

$$Q_{Load}^* = \sum_{i=1}^I (Q_i^* \cdot \eta_i^q) \quad (3)$$

$$P_{Load}^* = \sum_{i=1}^I (P_i^* \cdot \eta_i^e - L_i^*) \cdot \eta_{GRD} \quad (4)$$

where Q_i^* (MW) is the thermal power generated from the i th cogeneration; η_i^q is the heating efficiency of the i th cogeneration, 0.97; P_i^* (MW) is the minimum electrical power generated from the i th cogeneration; η_i^e is electricity efficiency of the i th cogeneration, 0.95; L_i^* (MW) is the electricity consumption of the i th cogeneration for circulating heating water, and formulated in Equation (5); η_{GRD} is transmission efficiency of the electric grid (0.94 in [13]):

$$L_i^* = Q_i^* \cdot EHR \quad (5)$$

where EHR is the constant of circulating heating water, 0.03 [34]. The gross original fuel consumed by cogenerations F_{CHP}^* (MWh) is formulated as Equation (6):

$$F_{CHP}^* = \sum_{i=1}^I F_i^* = \sum_{i=1}^I T \cdot (k_i \cdot Q_i^* + m_i \cdot P_i^* + c_i) \quad (6)$$

where F_i^* (MWh) is the original fuel consumed by the i th cogeneration; T (h) is the operating duration of cogeneration (hours); k_i , m_i and c_i are various unit constants of the i th cogeneration respectively.

Compared with Equations (3–6) through which Q_{Load}^* and P_{Load}^* are served by cogeneration units only, the authors' new proposal is that part of the end users' space heating load Q_{Load}^* should be served by EHPs consuming electrical power P_{EHP}^{\wedge} (MW) as Equation (7), and electrical power consumed by EHPs is only from cogeneration as indicated by Equation (8):

$$Q_{Load}^* = \sum_{i=1}^I (Q_i^{\wedge} \cdot \eta_i^q) + COP_{cri}^{\wedge} \cdot P_{EHP}^{\wedge} \quad (7)$$

$$P_{Load}^* = \sum_{i=1}^I (P_i^{\wedge} \cdot \eta_i^e - Q_i^{\wedge} \cdot EHR) \cdot \eta_{GRD} - P_{EHP}^{\wedge} \quad (8)$$

where Q_i^{\wedge} (MW) is the new thermal power generated from the i th cogeneration; COP_{cri}^{\wedge} is the critical coefficient of performance (COP) of the corresponding EHPs; positive P_{EHP}^{\wedge} (MW) is the electrical power consumed by the EHPs for space heating purpose; P_i^{\wedge} (MW) is the new electrical power generated from the i th cogeneration. New allowed minimum and maximum electrical power generated by the i th cogeneration are $P_i^{\min^{\wedge}}$ (MW) and $P_i^{\max^{\wedge}}$ (MW) respectively, which are formulated as Equations (9,10) respectively:

$$P_i^{\min\hat{}} = l_i^{\min} \cdot Q_i^{\hat{}} + n_i^{\min} \quad (9)$$

$$P_i^{\max\hat{}} = l_i^{\max} \cdot Q_i^{\hat{}} + n_i^{\max} \quad (10)$$

where l_i^{\min} , n_i^{\min} , l_i^{\max} and n_i^{\max} are various constants of the i th cogeneration. The fuel consumption of the i th cogeneration $F_i^{\hat{}}$ (MWh) is formulated as Equation (11):

$$F_i^{\hat{}} = T \cdot (k_i \cdot Q_i^{\hat{}} + m_i \cdot P_i^{\hat{}} + c_i) \quad (11)$$

where $P_i^{\hat{}}$ is electrical power of the i th cogeneration (MW). Constraints are formulated as Equations (12–15):

$$0 \leq Q_i^{\hat{}} \leq Q_i^{\max\hat{}} \quad (12)$$

$$P_i^{\min\hat{}} \leq P_i^{\hat{}} \leq P_i^{\max\hat{}} \quad (13)$$

$$F_{CHP}^{\hat{}} = \sum_{i=1}^I F_i^{\hat{}} = \sum_{i=1}^I T \cdot (k_i \cdot Q_i^{\hat{}} + m_i \cdot P_i^{\hat{}} + c_i) \quad (14)$$

$$0 \leq P_{EHP}^{\hat{}} \quad (15)$$

$$F_{CHP}^{\hat{}} \leq F_{CHP}^* \quad (16)$$

where $Q_i^{\max\hat{}}$ (MW) is the allowed maximum thermal power generated from the i th cogeneration. $F_{CHP}^{\hat{}}$ (MWh) is the gross fuel consumption. This optimization problem is devoted to finding the critical COP of EHPs $COP_{cri}^{\hat{}}$, above which fuel conservation can be achieved solely by adjusting cogenerations' electrical and thermal power generated. In this optimization problem, the objective function is formulated as Equation (17):

$$\text{Minimum: } COP_{cri}^{\hat{}} \quad (17)$$

3.2. Mathematic Model for Fuel Conservation

A considerable number of wind turbines have been installed in Northern China [35,36]. Besides, there exist high penetration coal-fired cogeneration units whose heating water production is accompanied by minimal electricity production. Compared with Equations (3–6) through which Q_{Load}^* and P_{Load}^* are served by cogeneration units only, the authors' proposal is that part of the end users' space heating load Q_{Load}^* should be served by EHPs consuming electrical power P_{EHP} (MW) as Equation (18), and more wind power P_{WIND} (MW) may be utilized as Equation (19):

$$Q_{Load}^* = \sum_{i=1}^I (Q_i \cdot \eta_i^q) + COP \cdot P_{EHP} \quad (18)$$

$$P_{Load}^* = \sum_{i=1}^I (P_i \cdot \eta_i^e - Q_i \cdot EHR) \cdot \eta_{GRD} + P_{WIND} \cdot \eta_{WIND} - P_{EHP} \quad (19)$$

where Q_i (MW) is the new thermal power generated from the i th cogeneration; COP is the coefficient of performance of the corresponding EHPs; positive P_{EHP} (MW) is the electrical power consumed by the EHPs for space heating purpose; P_i (MW) is the new electrical power generated from the i th cogeneration; P_{WIND} (MW) is the additional wind power utilized; η_{WIND} is the efficiency of the wind

turbines (0.95). New minimum and maximum electrical power generated by the i th cogeneration are P_i^{\min} (MW) and P_i^{\max} (MW) respectively, which are formulated as Equations (20,21) respectively:

$$P_i^{\min} = l_i^{\min} \cdot Q_i + n_i^{\min} \quad (20)$$

$$P_i^{\max} = l_i^{\max} \cdot Q_i + n_i^{\max} \quad (21)$$

where l_i^{\min} , n_i^{\min} , l_i^{\max} and n_i^{\max} are various constants of the i th cogeneration. The new fuel consumption of the i th cogeneration F_i (MWh) is formulated as Equation (22):

$$F_i = T \cdot (k_i \cdot Q_i + m_i \cdot P_i + c_i) \quad (22)$$

where P_i is new electrical power of the i th cogeneration (MW). Constraints are as Equations (23–26):

$$0 \leq Q_i \leq Q_i^{\max} \quad (23)$$

$$P_i^{\min} \leq P_i \leq P_i^{\max} \quad (24)$$

$$F_{CHP} = \sum_{i=1}^I F_i = \sum_{i=1}^I T \cdot (k_i \cdot Q_i + m_i \cdot P_i + C_i) \quad (25)$$

$$0 \leq P_{EHP} \quad (26)$$

where Q_i^{\max} (MW) is the new allowed maximum thermal power generated from the i th cogeneration. F_{CHP} (MWh) is the new gross fuel consumption.

The objective function is to maximize the fuel conservation ΔF , which is formulated as Equation (27):

$$\text{Maximum: } \Delta F = \frac{F_{CHP}^* - F_{CHP}}{F_{CHP}^*} \times 100\% \quad (27)$$

3.3. Mathematic Model Regarding Economy

The authors' proposal may bring about economic benefits in the following aspects after fuel conservation is achieved by application of Equations (18–27). Firstly, participants, including end users, cogeneration facilities and the electric grid may obtain delta benefits compared with the current mode of operation. Secondly, after participants' delta benefits are compensated in accordance with the current operation mode, the tariff of auxiliary wind power utilized will be deduced. Any changes to the present policy are avoided by authors. Thus participants' delta benefits and tariffs of auxiliary wind power utilized are discussed in accordance with present policy framework in China [37,38] which results in the power and cash flow shown in Figure 6.

Because electricity is introduced for space heating purposes, the delta expense of end users ΔC_{END} is formulated as Equation (28). In addition, because fuel consumption and generation change, the delta profit of cogeneration ΔP_{CHP} changes as Equation (29). Furthermore, because electricity transmitted through electric power grid varies, the delta profit of the grid ΔP_{GRD} is formulated as Equation (30). ε_e^{wind} is formulated as Equation (31) on the condition that all participants' benefits are unchanged:

$$\Delta C_{END} = T \cdot (COP \cdot P_{EHP} \cdot \varepsilon_q - P_{EHP} \cdot \varepsilon_e^{end}) \quad (28)$$

$$\Delta P_{CHP} = (F_{CHP}^* - F_{CHP}) \cdot \varepsilon_f + T \cdot \sum_{i=1}^I (Q_i - Q_i^*) \cdot \eta_i^q \cdot \varepsilon_q + T \cdot \left(\sum_{i=1}^I (P_i \cdot \eta_i^e - Q_i \cdot EHR) - \sum_{i=1}^I (P_i^* \cdot \eta_i^e - Q_i^* \cdot EHR) \right) \cdot \varepsilon_e^{grd} \tag{29}$$

$$\Delta P_{GRD} = T \cdot \left(\sum_{i=1}^I (P_i \cdot \eta_i^e - Q_i \cdot EHR) - \sum_{i=1}^I (P_i^* \cdot \eta_i^e - Q_i^* \cdot EHR) \right) \cdot (\eta_{GRD} \cdot \varepsilon_e^{end} - \varepsilon_e^{grd}) \tag{30}$$

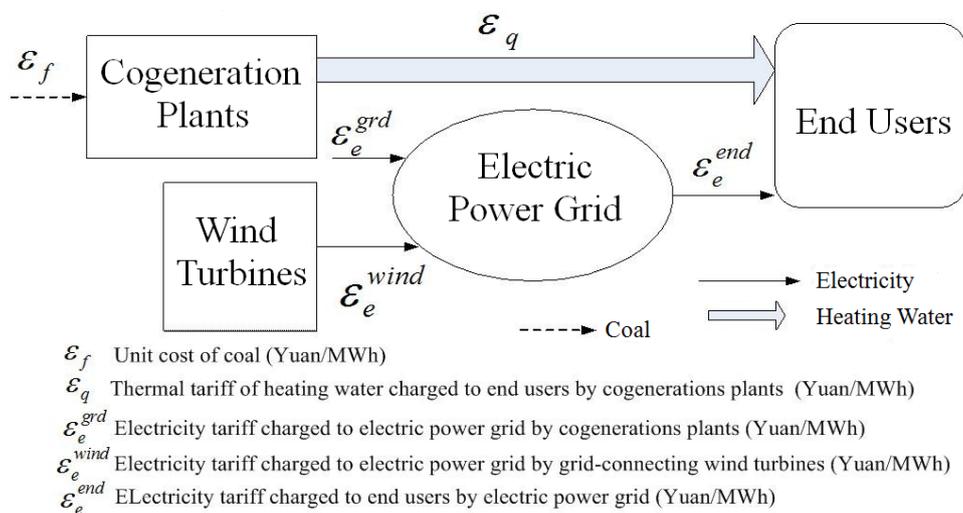
$$\varepsilon_e^{wind} = \frac{T \cdot \sum_{i=1}^I (Q_i \cdot \eta_i^q \cdot \varepsilon_q) + T \cdot (P_{sum}^* + P_{EHP}) \cdot \varepsilon_e^{end} - F_{CHP} \cdot \varepsilon_f - P_{CHP} - P_{GRD} - \Delta C_{END}}{P_{WIND} \cdot \eta_{WIND}} \tag{31}$$

where P_{CHP} is the cogenerations' profit formulated as Equation (32); P_{GRD} is the profit of the electric grid and is formulated as Equation (33):

$$P_{CHP} = T \cdot \sum_{i=1}^I (P_i^* \cdot \eta_i^e - Q_i^* \cdot EHR) \cdot \varepsilon_e^{grd} + T \cdot \sum_{i=1}^I Q_i^* \cdot \eta_i^q \cdot \varepsilon_q - F_{CHP}^* \cdot \varepsilon_f \tag{32}$$

$$P_{GRD} = T \cdot \sum_{i=1}^I (P_i^* \cdot \eta_i^e - Q_i^* \cdot EHR) \cdot (\eta_{GRD} \cdot \varepsilon_e^{end} - \varepsilon_e^{grd}) \tag{33}$$

Figure 6. Schematic of power and cash flow.



4. Numerical Simulation

With regard to the C135/N150-13.24 condensing-extraction cogeneration unit, constants l_i^{max} and n_i^{max} are shown as Equation (1); constants l_i^{min} and n_i^{min} are as given by Equation (2); constants k_i , m_i and c_i are as shown in Equation (34):

$$F = \left\{ \begin{array}{ll} 0.73 \cdot Q + 2.48 \cdot E + 3.59 & 34 \leq Q < 68 \\ 0.66 \cdot Q + 2.43 \cdot E + 12.73 & 68 \leq Q < 85 \\ 0.73 \cdot Q + 2.42 \cdot E + 8.11 & 85 \leq Q < 119 \\ 0.59 \cdot Q + 2.45 \cdot E + 22.47 & 119 \leq Q < 53 \end{array} \right. \tag{34}$$

The electricity and heating water tariffs under the present policy framework are shown in Table 1.

Table 1. Present heating water and electricity tariffs.

	ϵ_e^{end}	ϵ_e^{grd}	ϵ_q	ϵ_f
Tariff (Yuan/MWh)	500	300	100	100

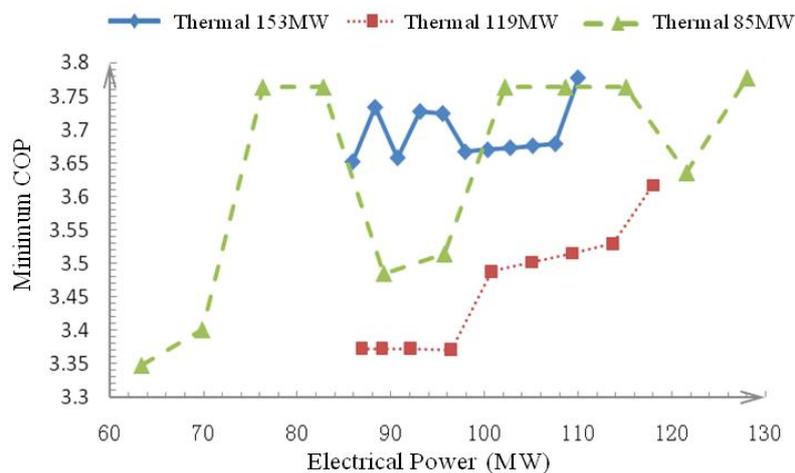
1. COP_{cri} is calculated in the cases of a single cogeneration being available, so that economic dispatch influence can be avoided. For calculating COP_{cri} , the thermal load Q_{Load}^* is set as 153 MW, 119 MW and 85 MW, respectively. In addition, the electrical load P_{Load}^* is set as various values between the allowed minimum and maximum electrical power generated under a certain Q_{Load}^* , $T = 1$ (h).
2. The results of ΔF , ϵ_e^{wind} , ΔC_{END} , ΔP_{CHP} and ΔP_{GRD} are calculated in the case assuming there are 100 MW of surplus wind power and twelve C135/N150-13.24 extraction-condensing cogeneration units available. Original electrical load P_{Load}^* is set as 878 MW, original thermal load Q_{Load}^* is set as 1781 MW, and $T = 1$ (h). Under the original operation mode, 153 MW heating water and 85.9 MW electricity are supposed to be generated from each cogeneration unit, all of which meet the Q_{Load}^* and P_{Load}^* . 100 MW wind power is abandoned. Nonlinear Programming (NLP) is performed with GAMS[®]. It is explained that during off-peak load at night 0:00~7:00 o'clock, 100 MW wind power is about 11.3% of 878 MW electrical load, which is a rational assumption in the practical electric power grid of Northern China [3]. In addition, COP of EHPs is set 1.0~6.0 for numerical simulation.

5. Results and Discussion

5.1. Critical COP of EHPs

Figure 7 shows the value of COP_{cri}^{\wedge} at different thermal and electricity loads. COP_{cri}^{\wedge} ranges around 3.3~3.8, indicating that if $COP < COP_{cri}^{\wedge}$, there is no fuel conservation, and if $COP \geq COP_{cri}^{\wedge}$, there exists fuel conservation.

Figure 7. Critical COP of EHPs for fuel conservation.



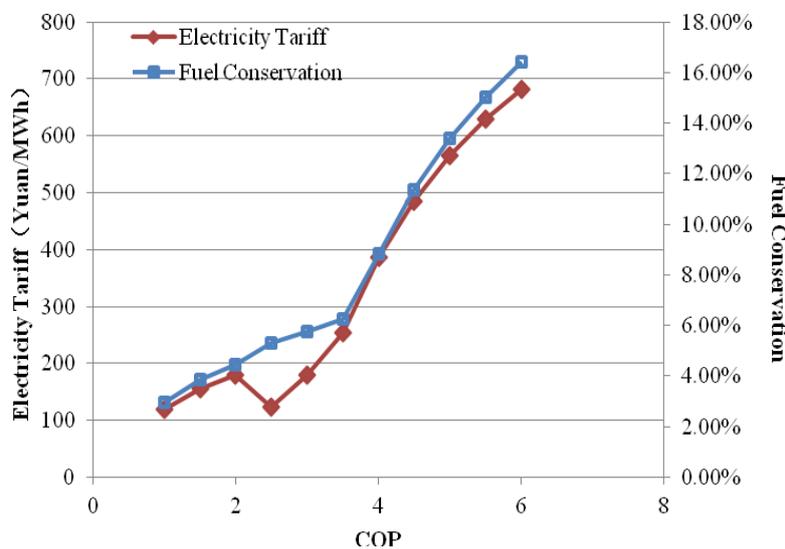
5.2. Fuel Conservation and Economic Feasibility

Both fuel conservation and economic feasibility are related to the *COP* of the EHPs used. *COP* is set in the range of 1.0~6.0 for numerical simulation. Generally speaking, the higher the outdoor temperature the higher *COP* is. *COP* of air-conditioners in China is usually considered under 1.0~3.0, and it is convenient to use according to the authors' proposal. *COP* of either geothermal EHPs or water source EHPs is around 4.0~6.0. It is emphasized that COP_{cri}^{\wedge} in Section 5.1 is separated from *COP* here. Because the authors' proposal is only focused on enabling more wind power integration during off-peak load at night 0:00~7:00 o'clock, the tradeoff of choosing EHPs should be considered in practice.

5.2.1. Delta Benefits of Participants

Figure 8 shows the change of the benefits of the participants for different values of *COP*. When *COP* is lower than 5, ΔC_{END} is lower than zero, meaning that end users are charged more. According to the authors' proposal a corresponding subsidy should be given to these end users. When *COP* is more than 5, $\Delta C_{END} > 0$, and these end users are charged less because of the high *COP* of EHPs. These end users are supposed to refund the auxiliary profit for deducing the wind power tariff. In Figure 8, when delta benefits of cogenerations and electric power grid are $\Delta P_{CHP} < 0$, $\Delta P_{GRD} < 0$, they should be provided a corresponding subsidy so as to keep profits unchanged. Otherwise, if $\Delta P_{CHP} > 0$, $\Delta P_{GHD} > 0$, they should refund any additional profits.

Figure 8. Delta benefits of participants.

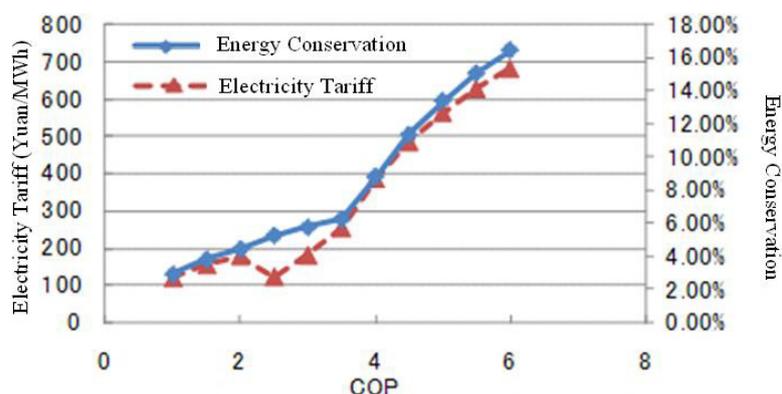


5.2.2. Fuel Conservation and Tariff of More Wind Power Integrated

In Figure 9, fuel conservation ΔF increases with *COP* which is in the range of 1.0~6.0. The slope of the fuel conservation curve increases sharply when *COP* is larger than the value of COP_{cri}^{\wedge} shown in Figure 7 (3.3~3.8). Here, COP_{cri}^{\wedge} works as a critical value with regard to the C135/N150-13.24 cogeneration unit. While *COP* is below COP_{cri}^{\wedge} , the fuel conservation obtained is attributed to more wind power integration only; it is about 3.0%~6.2%. If *COP* is beyond COP_{cri}^{\wedge} , fuel conservation is

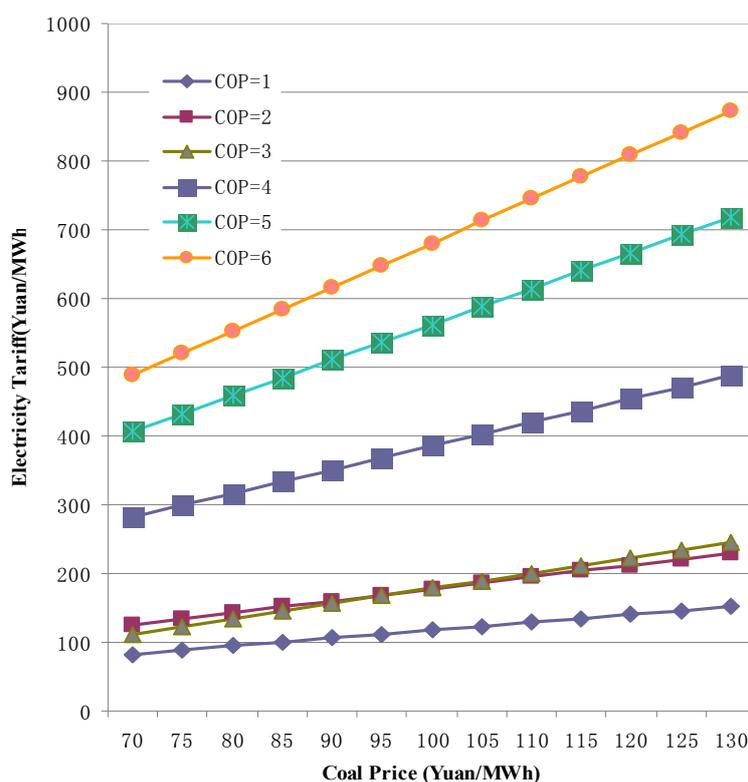
about 8.8%~16.4% which will be from both wind power and cogeneration units generating more electricity and less heating water. If keeping participants' benefit unchanged, a positive electricity tariff of wind power ε_e^{wind} can be observed in Figure 9. The more wind power integrated is able to receive a competitive electricity rate, in contrast to the present electricity rate of wind power set as 510, 540, 580, 600 (Yuan/MWh).

Figure 9. Fuel conservation and electricity tariff of wind turbines.



In Equation (31), ε_f has something to do with ε_e^{wind} , so in Figure 10, a sensitivity analysis considering the price of coal ε_f has been performed, which reveals that ε_e^{wind} goes higher with increasing ε_f and COP of EHPs. Because ε_e^{wind} arises from the fuel conservation ΔF , both more ε_f and higher COP result in higher ε_e^{wind} .

Figure 10. Sensitivity analysis towards the price of coal.



In Northern China currently wind farms with 49.5 MW capacity are popular because they can be easily approved by the provincial government instead of the China National Energy Administration, so according to the numerical simulation, one wind farm and six cogeneration units should cooperate with each other to serve the corresponding end users in accordance with the authors' proposal, so that the curtailment of wind power can be avoided. This seems dependent on the installation capacity of cogeneration units.

6. Conclusions

In Northern China, a large amount of wind power is lost during the heating season. This arises from: (1) a serious divergence in the ratio of electrical to thermal energy between the end users' load and cogeneration units' production; (2) high penetration of coal-fired cogeneration units equipped with extraction-condensing steam turbines; (3) abundant wind turbines installed. The authors propose that the use of heating water as energy carrier for space heating should be shaved and the amount of electricity used as an energy carrier for space heating should be increased, which adjusts the ratio of electrical to thermal energy consumption on the end users' side. With adjusted thermal and electrical load constraints, a new optimal dispatch would be performed. A numerical study on the feasibility of the authors' proposal is carried out and the following results are obtained:

1. While single cogeneration itself and EHPs cooperate to serve space heating, there exists a critical COP of EHPs, beyond which fuel conservation is achieved. For a C135/N150-13.24 extraction-condensing cogeneration, this critical COP (COP_{cri}^{\wedge}) is around 3.3~3.8.
2. If COP of EHPs is set as 1.0~6.0, while COP is below COP_{cri}^{\wedge} , fuel conservation arises from more wind power integration only, it is about 3.0%~6.2%; while COP is beyond COP_{cri}^{\wedge} , additional fuel conservation can be achieved due to the cooperation of CHP and EHPs besides wind power, it is about 8.8%~16.4%.
3. While EHPs are introduced for space heating, the end users are charged more if COP is below 5, and charged less if COP is above 5. In addition, the economic benefits of both cogeneration facilities and the electric grid change following the authors' proposal. It is also observed that if all participants' economy benefits are kept unchanged, positive and competitive electricity tariff of wind power is achievable, which is about 119.3~682.5 (Yuan/MWh).

The key point of the authors' proposal is devoted to improving the electricity-heat ratio through the use of end-users' electric heat pumps.

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