



Article

A Bio-Refinery Concept for N and P Recovery—A Chance for Biogas Plant Development

Magdalena Szymańska ^{1,*}, Ewa Szara ¹, Tomasz Sosulski ¹, Adam Wąs ², Gijs W. P. van Pruissen ³, René L. Cornelissen ³, Mieczysław Borowik ⁴ and Marcin Konkol ⁴

- Department of Soil Environment Sciences, Warsaw University of Life Sciences–SGGW, Nowoursynowska 159, 02–776 Warsaw, Poland; ewa_szara@sggw.pl (E.S.); tomasz_sosulski@sggw.pl (T.S.)
- Department of Economics and Organisation of Enterprises, Warsaw University of Life Sciences—SGGW, Nowoursynowska 166, 02–787 Warsaw, Poland; adam_was@sggw.pl
- Cornelissen Consulting Services BV, Binnensingel 3, 7411 PL Deventer, The Netherlands; vanpruissen@ccsenergieadvies.nl (G.W.P.v.P.); Cornelissen@ccsenergieadvies.nl (R.L.C.)
- ⁴ New Chemical Syntheses Institute, Al. Tysiąclecia P.P. 13a, 24–110 Pulawy, Poland; Mieczyslaw.Borowik@ins.pulawy.pl (M.B.); marcin.konkol@ins.pulawy.pl (M.K.)
- * Correspondence: magdalena_szymanska@sggw.pl; Tel.: +48-22-593-26-27

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Abstract: Biogas is an alternative source of energy for fossil fuels. In the process of transforming organic materials into biogas significant amounts of valuable digestate are produced. In order to make the whole process sustainable digestate should be utilized this is a constraining factor in the development of the biogas industry. Consequently, there is an on-going search for new technologies to process digestate, allowing to broaden the range of possible ways of digestate utilization. One of such possibilities is technology of nitrogen (N) and phosphorus (P) recovery from the anaerobic digestate. In this study results of physicochemical analysis of materials flowing through the farm-scale bio-refinery producing struvite (STR) and ammonium sulphate (AS) are presented. Struvite was precipitated from the liquid fraction of digestate (LFDS). Ammonia was bound by sulphuric acid resulting in obtaining ammonium sulphate. The STR obtained was of medium purity and contained other macronutrients and micronutrients that further enhanced its agronomic value. The P recovery effectiveness, counted as the difference between the P_{tot} content in the material before and after STR precipitation was 43.8%. The AS was characterized by relatively low Ntot and Stot content. The Ntot recovery efficiency reached 43.2%. The study showed that struvite precipitation and ammonia stripping technologies can be used for processing digestate however, the processes efficiency should be improved.

Keywords: biogas plant; struvite precipitation; ammonia stripping; circular bioeconomy; digestate treatment

1. Introduction

The progressing concentration of animal production causes a growing problem of environmental pollution. The problem is so serious that in some European countries systemic solutions began to be introduced forcing farmers to implement technologies aimed at the export of nitrogen and phosphorus (P) from farms [1]. This is exemplified by Dutch agriculture [2]. Due to a large excess of phosphorus occurring in farms with intensive livestock production, the Dutch government introduced legislation to limit the amount of phosphate used in agriculture. Farmers are eligible for state-founded payments when they exported phosphorus from their farm.

Proper allocation of nitrogen (N) and P from manure between areas with excess of the components and those where their deficits are supplemented with mineral fertilizers will provide measurable

Energies **2019**, 12, 155

benefits in the form of limiting water eutrophication and reduction of N_2O emissions from the soil [3]. The closing of the N and P cycle by recovering and recycling can be implemented through farm expansion and creating a system of the organic materials treatment consisting in the struvite (STR) (MgNH₄PO₄·6H₂O) precipitation and subsequent stripping of ammonia. The obtained products: STR and ammonium sulphate (AS) can be used as substitutes for currently used artificial fertilizers which corresponds with the idea of the circular bioeconomy. One of its objectives is to increase efficiency of natural resources use and to decrease the dependence European agriculture on imports of raw materials necessary for fertilizer production [4]. This implies a necessity to search for new N and P sources for fertilizer use [5].

Nowadays anaerobic digestion has become an increasingly important source of renewable energy. During the anaerobic digestion, organic compounds are subject to degradation, leading to the accumulation of mineral forms of N and P in the remaining digestate [6–8]. Digestate is usually subject to solid-liquid separation [9]. The solid fraction is applied on fields managing large amounts of liquid fraction, which contains 3-5% dry matter is difficult to achieve [10]. Further processing of the liquid fraction of digestate permits a recovery of nutrients. They can be exported from the farms over large distances to places where the soil is deficient in these nutrients [11,12]. This allows for obtaining additional income from the sale of the obtained product [13]. It is possible to apply several technologies of the digestate liquid fraction processing, such as struvite precipitation, ammonia stripping, evaporation, or membrane separation, resulting in the nutrient recovery and production of nutrient-rich products [14-17]. Struvite precipitation and ammonia stripping are promising methods for recovering the nitrogen and phosphorus from the liquid fractions of digestate. However, these processes are still at an experimental level [18]. According to Rahaman et al. [19], equi-molar concentration (1:1:1) of magnesium (Mg), phosphorus (P) and ammonium (NH₄⁺) with alkaline (optimal pH value 8.5–9.0) are required to precipitate struvite. Depending on the chemical reaction conditions, struvite may be formed at reactants ratios different from the optimal molar ones [20–22]. Czajkowska and Siwiec [23] proved that at pH \leq 7.5 struvite precipitates from a solution at the concentration of substrates: $>300 \text{ mg PO}_4^{3-} \cdot \text{kg}^{-1}$, $>250 \text{ mg NH}_4^+ \cdot \text{kg}^{-1}$ and \geq 111.5 mg Mg·kg⁻¹. Results of the cited research indicate that increase in phosphate concentration up to 1000 mg PO₄³⁻·kg⁻¹ allows crystallization of struvite with a lower content of other substrates $(49.4 \text{ mg Mg} \cdot \text{kg}^{-1} \text{ and } 100 \text{ mg NH}_4^+ \cdot \text{kg}^{-1})$. However, a decrease in the content of one substrate must be accompanied by an increase in the concentration of the other substrate. At pH 8.0, struvite does not crystallize from the solution at a concentration of 100 mg PO₄³⁻·kg⁻¹, <200 mg NH₄⁺·kg⁻¹ and <113 mg Mg·kg⁻¹. However, in the pH range 8.5–9.0, the ion concentrations that do not allow crystallization from the solution are as follows: 200 mg PO₄³⁻·kg⁻¹, <100 mg NH₄⁺·kg⁻¹ and <48 mg Mg·kg⁻¹ [23]. A potentially high content of competing elements can inhibit struvite crystallization. The content of potassium (K) [18], calcium (Ca) [17], and organic compounds [24] could decrease the N and P removal efficiency from the liquid fraction of digestate. The ammonia stripping process depends on pH, temperature and mass transfer area. The process is typically conducted at a temperature higher than 20 °C and pH above 9 [25]. Guštinet et al. [26] reached high efficiency of N removal (approximately 93%) from liquid fraction of digestate at pH 10.5 and temperature of 50 °C. The remaining material could still contain nutrients. However, it can be used in the agriculture after pH neutralization [25]. An alternative method is cultivation of duckweed. Oron et al. [27] used duckweed for domestic wastewater treatment to recycle the nutrients. Additionally production of duckweed is aimed at the recovery of nutrients, especially ammonium and phosphorus, from swine lagoon water [28]. Duckweed is well known for its high productivity and high protein content, ranging between 15% and 45% of the dry mass [29,30]. Considering the above, production of duckweed can substitute imported fodders and therefore limit the inflow of another portion of nitrogen and phosphorus within protein-rich fodders to the farm.

Energies **2019**, 12, 155 3 of 10

Thus far N and P has been recovered mainly from municipal sludge digester effluent and swine wastewater [17]. Moreover, the growing problem of point accumulation of these nutrients in digestate from biogas plants encourages the undertaking of research aiming at N and P recovery.

The aim of the study was to assess the possibility of using digestate processing technology in biogas plants, designed for N and P recovery and production of innovative substances that could be transported over long distances and used as mineral fertilizers.

2. Materials and Methods

2.1. The Farm Biogas Plant Scheme

The bio-refinery was located at the Experimental Dairy Farm 'De Marke' in Hengelo (Gld), the Netherlands ($52^{\circ}03''$ N, $6^{\circ}18''$ E). In the bio-refinery (Figure 1), cattle slurry (S) was subject to anaerobic digestion (1), and the obtained biogas was used to produce energy (2). The CHP (Combined Heat and Power) installation consisted of a gas engine (MAN E0824 E302) and generator. The electrical capacity is 36 kW_e and thermal capacity is 51 kW_{th} . The produced heat is being used to maintain the temperature of the digestion process. Electricity is being used to cover the own electricity consumption at the Experimental Dairy Farm De Marke and the surplus is being sold over the public electricity grid.

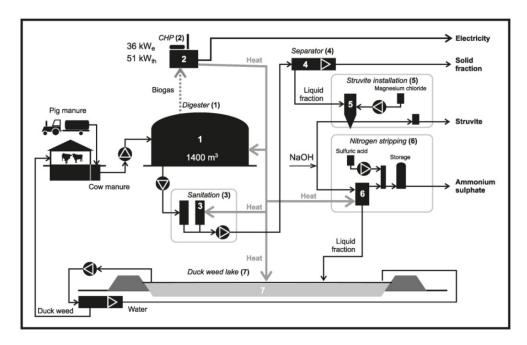


Figure 1. Scheme of the integrate bio-refinery system on farm scale.

The remaining digestate (DS) after sanitation (3) was separated into the solid (SFDS) and liquid fractions (LFDS) (4). Digestate was hygienized in order to reduce the amount of pathogens and to prevent infections. In this case the standard method of sanitation was used—pasteurization, which involves keeping the material at 70 °C for at least 60 min. The first stage of LFDS processing was struvite (STR) precipitation (5). MgCl₂ was added to the LFDS as a source of magnesium. Moreover, the pH of LFDS was adjusted to 9 by means of continuous 5N NaOH addition. At the second stage, ammonium sulphate (AS) was produced at 70 °C in the ammonia stripping installation: H₂SO₄ vessel, stripping tower and reactor (6). in order to increase the N recovery efficiency from the liquid fraction of digestate. (6). The liquid fraction after STR precipitation was alkalised by means of 5N NaOH, reaching a pH of 10.5. In such conditions, the released ammonium was bound by sulphuric acid resulting in obtaining AS. At the third stage, the effluent (EFL) after ammonia stripping was directed to the duckweed pond, where duckweed was cultivated (7). The produced duckweed served as fodder for cattle on the farm. The concept of our installation assumes that the duckweed will be kept in the

Energies **2019**, 12, 155 4 of 10

pond and will absorb the nutrients until they reach a level that is acceptable for dumping the pond water to the surface waters.

2.2. Analytical Methods

The samples were collected in 2017. The chemical analysis of the S, DS, LFDS, SFDS, EFL, STR and AS was carried out in triplicate. The S, DS, LFDS, SFDS and EFL samples were dried out at 60°C using drier PREMED (Marki, Poland) to estimate Total Solids content (TS). The Volatile Solids (VS) content was measured in accordance with the Polish Standard PN-Z-15011-3:2001 after roasting samples at 550 °C in a muffle furnace model FCF 12SHM (Czylok, Jastrzębie Zdrój, Poland). The pH value was measured by the potentiometric method using a pH meter (Schott, Mainz, Germany). The total N content (N_{tot}) was measured by means of the Kjeldahl method using a Vapodest analyzer model VAP 30 (Gerhardt, Bonn, Germany). The $\mathrm{NH_4}^+\text{-}\mathrm{N}$ content was measured using the Skalar San Plus analyzer (Breda, Netherlands), after wet basis samples extraction in 0.01 mol·dm⁻³ CaCl₂ with sample/extractant ratio of 1:10. The total phosphorus (P_{tot}), potassium (K_{tot}), magnesium (Mg_{tot}), calcium (Catot), sodium (Natot), zinc (Zn), manganese (Mn), copper (Cu) and iron (Fe) content were determined after digestion in HNO₃ and HClO₄ acids using a Model DK 20 digestion unit (VELP Scientifica, Usmate, Italy). Ktot, Mgtot, Catot, Natot, Zn, Mn, Cu and Fe were measured by AAS (Atomic Absorption Spectrometry) method using a spectrometer SOLAAR (Thermo Elemental, Cambridge, UK). The total content of sulphur (Stot) was measured by inductively coupled plasma atomic emission spectrometry (ICP-AES) (IRYS Advantage ThermoElementar, Cambridge, UK). Ptot was determined by the molybdenum-blue ascorbic method using the spectrophotometer Genesys 10 UV-VIS (Thermo Electron Corporation, Madison, USA). Water-soluble forms of Pws, Mgws and Caws were determined in water/the samples solution with ratio of 1:100. The crystal morphology of the STR deposit was observed using an optical polarization microscope (Model MN-800, POL OPTA-TECH) with a 5MP digital camera (OPTA-TECH) and Opta View software. X-ray Diffraction (XRD) measurements were performed on a diffractometer by PANalyticalEmpyreanin Bragg-Brentano geometry equipped with a PIXcel^{3D} detector. The measurements were performed on a Cu lamp with parameters I = 40 mA and U = 40 kV. The analysis of the diffractogram was performed in HighScorePlus software.

2.3. Statistical Analysis

Statistical analysis was carried out using the Statistica PL 13.0 software (Tulsa, USA). The data were subjected to ANOVA and the differences between the means were determined according to Tukey's test (P < 0.05).

3. Results and Discussion

The total content of studied macronutrients was similar in raw (S) and digestated slurry (DS) (Table 1). After anaerobic digestion the relation between total and water soluble forms of nutrients changed, especially concerning P. In the S the content of P_{ws} was 41.6 mg·kg⁻¹ WB, whereas in the DS it was 212.6 mg·kg⁻¹ WB. It constituted of 10.6% and 56.8% of P_{tot} , respectively. After mechanical DS separation, the remaining SFDS contained a significantly higher content of N_{tot} , P_{tot} , K_{tot} , Mg_{tot} and Ca_{tot} compared to the LFSD. However, the contribution of water-soluble nutrients in total forms was higher in the LFDS (Table 1).

The chemical composition of LFDS was not optimal for struvite precipitation. In the LFSD, the content of NH₄-N was 3000.0 mg·kg $^{-1}$ WB, P_{ws} 183.0 mg·kg $^{-1}$ WB and Mg_{ws} 239.4 mg·kg $^{-1}$ WB (Table 1). According to Kataki et al. [31] and Jia et al. [32], the highest effectiveness of struvite precipitation is achieved in solutions where pH is 9.0, whereas the pH of LFSD was 7.8; thus in order to increase the pH NaOH, was added. STR crystals obtained in the bio-refinery were very small. Their linear dimensions reached 1400 μ m (Figure 2). They were colored brown, which indicated the presence of organic pollutants. The content of organic matter in the STR was estimated for 51.3 g VS kg $^{-1}$.

Energies 2019, 12, 155 5 of 10

Additionally Achat et al. [33] found the presence of organic matter between 19.3 and 165.0 g·kg $^{-1}$ in recycled P-products.

Table 1.	The physicochemical	properties	of	organic	materials	flowing	through	the	farm	scale
bio-refine	ery.									

Parameters	S	DS	SFDS	LFDS	EFL
pН	7.0 ^a	7.8 ^b	7.7 ^b	7.8 ^b	12.2 ^c
TS (%)	7.7 ± 0.1 b	$6.8\pm0.2^{ m b}$	$25.7\pm1.1~^{\rm c}$	3.3 ± 0.03 a	2.1 ± 0.1 a
N_{tot} (g·kg ⁻¹ WB)	3.6 ± 0.1 ^c	3.4 ± 0.01 bc	$4.3\pm0.2^{ m d}$	$3.2 \pm 0.01^{\ b}$	1.8 ± 0.1 a
NH_4 -N (g·kg ⁻¹ WB)	2.9 ± 0.1 b	3.0 ± 0.1 b	3.0 ± 0.1 b	3.0 ± 0.03 b	1.4 ± 0.05 a
$P_{tot} (g \cdot kg^{-1} WB)$	0.4 ± 0.01 a	0.4 ± 0.01 a	1.3 ± 0.1 ^c	0.3 ± 0.0 $^{\mathrm{ab}}$	0.2 ± 0.0 b
$K_{tot} (g \cdot kg^{-1} WB)$	4.6 ± 0.1 $^{ m b}$	$4.7\pm0.2^{ m b}$	4.6 ± 0.1 b	3.8 ± 0.2 a	3.8 ± 0.2 a
$Mg_{tot} (g \cdot kg^{-1} WB)$	0.7 ± 0.04 cd	0.6 ± 0.05 bc	0.9 ± 0.2 d	0.5 ± 0.01 b	0.3 ± 0.02 a
Ca _{tot} (g·kg ⁻¹ WB)	1.0 ± 0.1 ^c	0.9 ± 0.1 bc	1.6 ± 0.3 d	0.6 ± 0.06 b	0.4 ± 0.01 a
Na _{tot} (g·kg ⁻¹ WB)	$0.8\pm0.05~^{\mathrm{a}}$	0.7 ± 0.06 a	0.9 ± 0.01 a	0.7 ± 0.01 a	9.2 ± 0.2 a
P_{ws} (mg·kg ⁻¹ WB)	41.6 ± 3.4 a	$212.5\pm9.8~^{\rm d}$	$543.5\pm7.5^{\text{ e}}$	183.0 ± 10.0 ^c	127.7 ± 11.5 b
Mg_{ws} ($mg \cdot kg^{-1}$ WB)	$311.6\pm27.6^{\text{ c}}$	$293.7 \pm 19.9^{\text{ c}}$	200.8 ± 4.3 ab	$239.4 \pm 7.5^{\ b}$	$178.8\pm20.9~^{\rm a}$
Ca _{ws} (mg·kg ⁻¹ WB)	$348.4\pm35.8^{\text{ c}}$	$230.8 \pm 15.6^{\ b}$	$193.6 \pm 31.4^{\ b}$	$238.3 \pm 32.8^{\text{ b}}$	$173.7\pm19.7~^{\rm a}$
Cu (mg⋅kg ⁻¹ WB)	18.2 ± 0.4 b	$15.3 \pm 2.3^{\text{ b}}$	$22.8\pm1.2~^{\rm c}$	7.3 ± 0.3 a	4.4 ± 0.9 a
Mn (mg \cdot kg ⁻¹ WB)	$12.2\pm0.3~^{\rm c}$	$11.0\pm0.1~^{\rm c}$	22.2 ± 0.9 d	$9.6\pm0.1^{ m b}$	7.5 ± 0.4 a
$Zn (mg \cdot kg^{-1} WB)$	$18.0\pm1.8^{\text{ c}}$	16.4 ± 0.7 bc	$25.8\pm2.3~^{\rm d}$	13.1 ± 1.7 ab	10.7 ± 0.9 a

Data (means \pm standard deviation, n = 3) followed by different letters (a, b, c and d) in same rows are significantly different at P < 0.05. S—slurry, DS—digested slurry, SFDS—solid fraction of digested slurry, LFDS—liquid fraction of digested slurry, EFL –effluent from biogas plant after struvite precipitation and ammonia stripping. WB—Wet Basis, N_{tot}, P_{tot}, K_{tot}, Mg_{tot}, Ca_{tot}, Na_{tot}—total forms of nutrients, P_{ws}, Mg_{ws}, Ca_{ws}—water-soluble forms of nutrients.

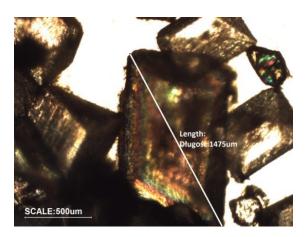


Figure 2. Microscopic image of the struvite precipitated in the farm scale bio-refinery (STR).

The applied X-ray Diffraction (XRD) analysis allowed for the determination of the type of crystalline phases occurring in the sample (Figure 3). The analyzed sample is characterized by well-formed crystallographic phases. The presence of the struvite crystallographic phase is clearly evidenced by a series of characteristic diffraction lines with the highest intensities at 20 15.00 (hkl 110), 15.81 (hkl 020), 16.47 (hkl 011), 20.85 (100% intensity, hkl 111), 21.45 (hkl 021) and 30.60 (hkl 211). In addition to struvite, monohydroxycalcite (CaCO₃·H₂O) and quartz (SiO₂) were found.

Energies 2019, 12, 155 6 of 10

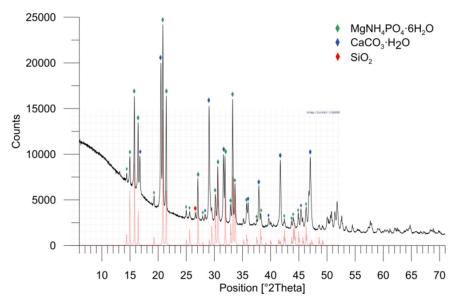


Figure 3. X-ray diffraction pattern of the product from the bio-refinery with struvite (STR) evidence: struvite (MgNH $_4$ PO $_4$ ·6H $_2$ O)-green, monohydroxycalcite (CaCO $_3$ ·H $_2$ O)-blue, and quartz (SiO $_2$)-red; the reference diffractogram of struvite is shown below the diffractogram of the analyzed sample.

Organic and mineral pollutants detected in the STR resulted in a low content of main nutrients (23.1 g $N_{tot} \cdot kg^{-1}$ WB, 39.4 g $P_{tot} \cdot kg^{-1}$ WB and 32.3 g $Mg_{tot} \cdot kg^{-1}$ WB) (Figures 4 and 5). Much higher nutrient content occurs in the struvite fertilizer Crystal Green®, Ostara: 50.0 g $N_{tot} \cdot kg^{-1}$; 122.0 g $P_{tot} \cdot kg^{-1}$, and 100.0 g $Mg_{tot} \cdot kg^{-1}$, produced from sewage sludge sediment [34,35]. However, struvite composition depends on different factors; particularly, on the characteristics of raw materials [36]. According to Kataki et al. [31], struvite from yeast anaerobic effluent contained 35 g $N \cdot kg^{-1}$, 108 g $P \cdot kg^{-1}$ and 79.7 g $Mg \cdot kg^{-1}$, from municipal wastewater 29 g $N \cdot kg^{-1}$, 91 g $P \cdot kg^{-1}$ and 99 g $Mg \cdot kg^{-1}$ and from human urine 29 g $N \cdot kg^{-1}$ and 71 g $P \cdot kg^{-1}$.

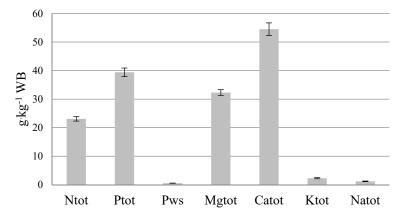


Figure 4. Macronutrients content in STR from the farm scale bio-refinery plant.

The P recovery efficiency, calculated as the difference between the P_{tot} content in the LFSD and the EFL, reached 43.8%. Low P recovery efficiency could be caused by the Ca, K, Na, Cu, Mn and Zn content in the LFSD (Table 1) as these elements are considered to be STR precipitation inhibitors [18]. Moreover, the total solids in the LFSD could hinder STR precipitation. Taddeo et al. [18] proved a strong correlation between the content of total solids in raw materials used to struvite precipitation and process efficiency.

The total ammonia nitrogen (sum of NH_3 and NH_4^+), which remained in the effluent after STR precipitation, was bound to $(NH_4)_2SO_4$ by sulphuric acid in the ammonia stripping process.

Energies **2019**, 12, 155 7 of 10

The obtained AS was characterized by a low content of N_{tot} (14.1 g·kg⁻¹ WB) and S_{tot} (16.8 g·kg⁻¹ WB). The content of pure $(NH_4)_2SO_4$ was only 66.0 g·kg WB (Table 2). In the research conducted by Laureni et al. [37], the ammonium sulphate solution obtained from pig manure contained 400.0–600.0 g·kg⁻¹ $(NH_4)_2SO_4$. A low AS pH (2.1) can affect the reduction of its fertilizer value. It is possible to increase AS pH value using CaCO₃ [38] or caustic magnesite [39]. The N recovery efficiency, calculated as the difference between the N_{tot} content in the LFSD and the EFL, was 43.2%. Depending on flow rate and alkalinity, the total ammonia removal from the digestate might reached 42–80% [40].

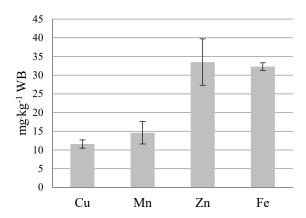


Figure 5. Micronutrients content in STR from the farm scale bio-refinery.

Table 2. Composition of ammonium sulphate (AS) from the farm scale bio-refinery.

Product	N _{tot}	S _{tot}	Pure (NH ₄) ₂ SO ₄	Free H ₂ SO ₄	pН
	$(g \cdot kg^{-1} WB)$	$(g \cdot kg^{-1} WB)$	$(g \cdot kg^{-1} WB)$	$(g \cdot kg^{-1} WB)$	
AS	14.1 ± 0.1	16.8 ± 0.3	66.4 ± 0.6	2.2 ± 0.1	2.1

Data (means \pm standard deviation, n = 3).

4. Conclusion

The disadvantage of biogas production being a renewable energy source is the remaining significant amount of digestate. Because of its constraints, limiting potential use of digestate as a natural fertilizer spread on agricultural land, there is a search for technologies allowing further treatments of digestate to make exporting beyond farms where biogas is processed to energy possible. The digestate can be a substrate for the production of valuable mineral fertilizers. Considering problems of exhaustion of phosphate rock reserve the construction of a bio-refinery recovering N and P as struvite and ammonium sulphate from digestate seems to be fully justified—both may substitute commercial N-P or N fertilizers. The results indicate that the products obtained in the bio-refinery contain smaller amounts of nutrients compared to mineral fertilizers that reduce their fertilizing value. However, besides the main nutrients (N, P, Mg), recovered, struvite contains organic matter and other macro- and micronutrients important for plant growth (K, Ca, Na, Cu, Mn, Zn, Fe) that increase fertilizing value of struvite. Biogas plants can be transformed into a bio-refinery using innovative processes; however, it is necessary to improve nutrient recovery efficiency. Further vegetation experiments are required in order to determine the fertilizer value and optimal doses and methods of application of these recycled products considering their specific properties.

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Energies **2019**, 12, 155 8 of 10

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Conflicts of Interest: The authors declare no conflict of interest.

Abbreviations

TS Total Solids WB Wet Basis S Slurry

DS Digested slurry

SFDS Solid fraction of digested slurry LFDS Liquid fraction of digested slurry

EFL Effluent after struvite precipitation and ammonia stripping

STR Struvite from bio-refinery AS Ammonium sulphate

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Energies **2019**, 12, 155 9 of 10

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Energies 2019, 12, 155 10 of 10

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