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Flame-Made Nb-Doped TiO₂ Ethanol and Acetone Sensors

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Abstract: Undoped TiO₂ and TiO₂ nanoparticles doped with 1–5 at.% Nb were successfully produced in a single step by flame spray pyrolysis (FSP). The phase and crystallite size were analyzed by XRD. The BET surface area (SSA_{BET}) of the nanoparticles was measured by nitrogen adsorption. The trend of SSA_{BET} on the doping samples increased and the BET equivalent particle diameter (d_{BET}) (rutile) increased with the higher Nb-doping concentrations while d_{BET} (anatase) remained the same. The morphology and accurate size of the primary particles were further investigated by high-resolution transmission electron microscopy (HRTEM). The crystallite sizes of undoped and Nb-doped TiO₂ spherical were in the range of 10–20 nm. The sensing films were prepared by spin coating technique. The mixing sample was spin-coated onto the Al₂O₃ substrates interdigitated with Au electrodes. The gas sensing of acetone (25–400 ppm) was studied at operating temperatures ranging from 300–400 °C in dry air, while the gas sensing of ethanol (50–1,000 ppm) was studied at operating temperatures ranging from 250–400 °C in dry air.

Keywords: TiO₂; niobium; flame spray pyrolysis; acetone and ethanol sensor

1. Introduction

TiO₂ is used extensively as a gas sensing material due to its change in electrical conductivity under analyte gas exposure. Sensing capability has been improved with the addition of foreign atoms such as Cr [1], Mo and W [2], Pt and Nb [3], Fe [4], and La and Cu [5]. Nb doping of TiO₂ has been used for O₂, CO, NO₂, and ethanol sensing. Nb doping modifies the microstructure of TiO₂, controls grain growth mechanisms, introduces electronic defects at the surface or in the bulk of grains and so modifies TiO₂ conductivity and gas sensing. TiO₂ presents three crystalline structures: brookite, anatase, and rutile.

The Nb₂O₅-TiO₂ system has been prepared by several methods such as the solid state reaction of Nb₂O₅ and TiO₂ [6-8], sol-gel [9,10], RF-sputtering of thin films [11-13], laser induced pyrolysis [14], pulsed laser deposition [15] and thick film using powder screen printing [16]. The Nb₂O₅-TiO₂ system can be used in applications such as varistors [17], catalysts [18], photocatalysts [19,20], and electrodes applicable to photoelectronic devices such as *p-n* type solar cells [21] and hybrid solar cells [22]. For gas sensing applications, it has been reported that the Nb₂O₅-TiO₂ system shows higher sensitivity and shorter response time as an oxygen gas sensor than undoped TiO₂ [11]. The Nb₂O₅-TiO₂ system can be used for sensing other gases as well, such as CO [23], CO, and ethanol [9,16,24], CO and NO₂ [16,24], and ethanol [3]. Table 1 lists literature examples of the use of Nb-TiO₂ for gas sensing applications, showing the authors, method of preparation, % Nb, sensing gas, range of detection, type of titania, size, and some remarks.

Comini *et al.* [3] reported that Nb- and Pt-doped TiO₂ thin films could be used for ethanol and methanol sensors. The thin films were prepared using the sol-gel process by the spin coating technique on Al₂O₃ substrate. The sensors were tested under exposure of ethanol and methanol gases at 300 °C with the concentration ranging from 500–1,250 ppm, making them feasible for development of breath analyzers (detection limit is 200 ppm). The thicknesses of the film were ranging from 60–100 nm. It was noticed that 1 at.% Nb and 0.5 at.% Pt/TiO₂ showed the best sensing performance. The TiO₂ sensors developed were sensitive at up to 500 ppm of ethanol. The response and recovery dynamics to ethanol were particularly promising for applications in food analysis, electronic noses, and breath analyzers.

In comparison to the same materials, Teleki *et al.* [16] reported the preparation of a flame-made TiO₂ spherical particles film of about 30 µm thickness by drop-coating of a heptanol suspension of these powders, and sensing tests at 500 °C with ethanol at concentrations ranging from 10–75 ppm. The sensor showed the highest sensor signal at 75 ppm ($S = 30$) ethanol concentration. Secondly, Teleki *et al.* [23] reported in 2008 the effect on ethanol and CO gas sensing of flame-made Nb- and Cu-doped TiO₂ thick film (5 µm) sensors fabricated by doctor-blading. All sensors were tested with gas concentrations ranging from 25–300 ppm during forward and backward cycles at 400 °C. Niobium stabilized the anatase phase and retarded grain growth up to 600 °C. The sensitivity increased by addition of either Cu and Nb to titania, and the best improvement was found for the 4 at.% Nb/TiO₂

sensor. Decreasing the Nb concentrations from 10 to 4 at.% increased the response. The response of 10 at.% Nb/TiO₂ sensor was high, but the baseline was not stable. The response time decreased with increased ethanol concentration, from 180 to 15 s for 25 and 300 ppm, respectively. The recovery time was very slow, within the 5–10 min range. This, however, decreased with increasing ethanol concentration. The anatase phase seems to be crucial as the Nb/TiO₂ sensor showed the highest response while Cu doping had no influence on the response relative to undoped TiO₂.

Flame spray pyrolysis (FSP) is a very promising technique for synthesis of high purity nanosized materials with controlled size and high surface area in one step. FSP has been demonstrated to produce high surface area of tin dioxide nanoparticles for gas sensing [24]. The aim of this research was to apply this technique to synthesize niobium-doped TiO₂ nanoparticles. Characterization of the nanoparticles and their acetone and ethanol sensing properties were performed.

Table 1. Literature review on Nb-TiO₂ for gas sensing applications showing the authors, method of preparation, % Nb, sensing gas, range of detection, type of titania, size and some remarks.

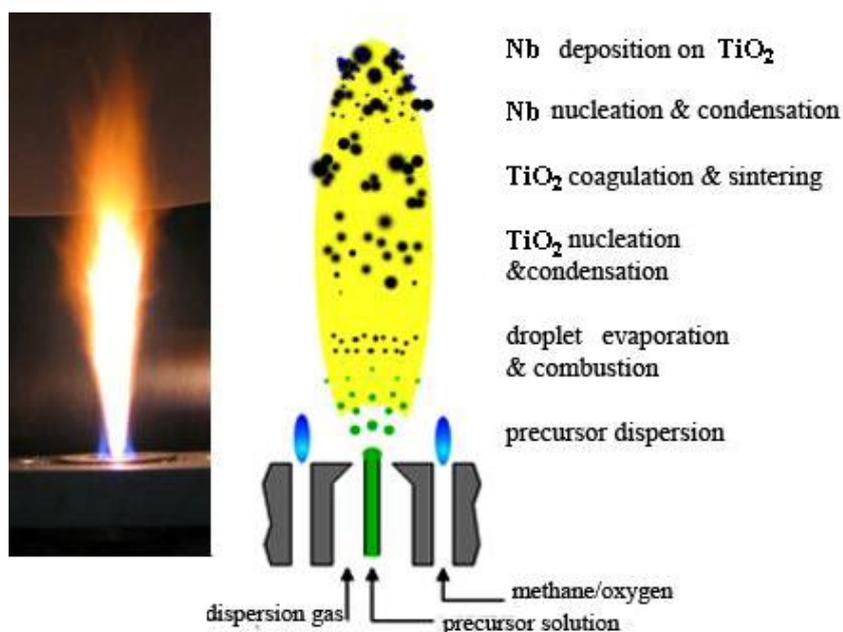
Authors	Method	% Nb	Gas	Range	Titania	Size	Remarks
Sharma <i>et al.</i> [7]	Thick film using screen printing of powder at 1,300 °C for 5 h	0, 0.2, 0.4 wt.% Nb	O ₂	1,200 ppm Nb-doped 1,000 ppm Cr-doped	Rutile	0.7 mm Nb-doped, 1–5 µm Cr-doped	Highest sensitivity of Nb-doped at 550 °C and Cr-doped at 700 °C
Bonini <i>et al.</i> [16]	Laser induced Pyrolysis of powders Screen printing at 650–1,050 °C	10 at.% Nb, Ta, Ga	CO NO ₂	100 ppm	Anatase + rutile	50–150 nm	Addition of dopants inhibits grain growth and hinders conversion of anatase to rutile
Ruiz <i>et al.</i> [8]	Sol-gel powders	0, 2, 4, 6, 8, 10 at.%	CO EtOH	CO 0–1,000 ppm EtOH 0–150 ppm	Rutile 100% (0 at.% Nb) Anatase 87% (10 at.% Nb)	8.5 nm (6 at.%Nb) 10 nm (10 at.% Nb)	CO sensitivity increases with addition of Nb, EtOH is slightly inhibited
Traversa <i>et al.</i> [9]	Sol-gel powders, Screen printing	0, 5, 10 at.% Nb, Ta	CO	0.5 ppm	Anatase (400 °C) Rutile (850 °C)	200–600 nm	Ta and Nb inhibit anatase to rutile transformation
Teleki <i>et al.</i> [16]	FSP	undoped	EtOH	1–75 ppm	Anatase + rutile	20–50 nm	Highest sensor signal at 75 ppm (S = 30)
Teleki <i>et al.</i> [23]	FSP	4, 10 at.%	CO EtOH	25–300 ppm	Anatase + rutile		4 at.% Nb gave higher sensitivity towards EtOH at 400 °C

2. Experimental

2.1. Flame Synthesis of Nanopowders

Titanium isopropoxide (Aldrich, 97%) and niobium (IV) 2-ethylhexanoate (Strem Chemicals) were used as titanium and niobium precursors, respectively. Both precursors were dissolved in xylene (Fluka, >98.5%) and acetonitrile (Fluka, >99.5%) in equal volume with the total metal atom concentration maintained at 0.5 mol/L. The niobium concentration was varied between 1 and 5 at.%. The precursor was fed into a flame spray pyrolysis reactor [24] by a syringe pump (Inotech) with a rate of 5 mL/min and was dispersed into droplets by 5 L/min of oxygen (Pan Gas, purity > 99%) using a gas assisted nozzle. The pressure drop at the nozzle tip was kept at 1.5 bar. The water-cooled system of the reactor avoided any evaporation of the precursor within the liquid feed lines or overheating of the nozzle. The spray flame was maintained by a concentric supporting flamelet ring of premixed methane/oxygen (CH₄ 1.5 L/min, O₂ 3.2 L/min). In order to assure the presence of enough oxidant for complete conversion of the reactants, an additional outer oxygen flow (5 L/min) was supplied. The powder was collected with the aid of a vacuum pump (Vaccubrand) on a glass fiber filter (GF/D Whatman, 25.7 cm in diameter). During the experiment, the filter was placed in a water-cooled holder, 40 cm above the nozzle, keeping the off-gas temperature below 200 °C. Scheme 1 shows the formation of Nb-doped TiO₂ by flame spray pyrolysis.

Scheme 1. The formation of Nb-doped TiO₂ by flame spray pyrolysis.



2.2. Powder Characterization

X-ray diffraction (XRD) patterns were recorded with a Bruker AXS D8 Advance (40 kV, 40 mA) operating with Cu K_α. The relative amounts of anatase and rutile and their respective crystallite sizes were calculated from the XRD data using the Rietveld method. BET powder-specific surface area (SSA), was measured by nitrogen adsorption at 77 K (Micromeritics Tristar) after degassing the sample for 1 h at 150 °C in nitrogen. The equivalent average primary particle diameter d_{BET} was calculated by

$d_{\text{BET}} = 6/(SSA \rho_P)$. Here, ρ_P is the average density of TiO_2 calculated from weight percent and density of anatase and rutile where d_{anatase} and d_{rutile} are 3.97 g/cm^3 and 4.17 g/cm^3 respectively. Morphologies of all the flame-made powders were investigated by Transmission Electron Microscopy (TEM, Hitachi H600, operated at 100 kV).

2.3. Paste and Sensor Preparations

An appropriate quantity of homogeneous mixed solution (0.28 mL) was prepared by stirring and heating at $80 \text{ }^\circ\text{C}$ for 12 h ethyl cellulose (Fluka, 30–70 mPa s) as the temporary binder and terpineol (Aldrich, 90%) as a solvent. The liquid mixture was combined with 60 mg of samples 1–5 at.% Nb/ TiO_2 nanopowders and mixed for 30 min to form a paste prior to spin-coating. The resulting paste was firstly spin-coated (700 rpm) 1 time for 10 s, and then subsequently at 3,000 rpm, 2 times for 30 s on the Al_2O_3 substrates interdigitated with Au electrodes ($0.5 \times 0.5 \text{ cm}$) to deposit sensing films. The resulting substrates were annealed in an oven at $150 \text{ }^\circ\text{C}$ for 1 h with an annealing rate of $1 \text{ }^\circ\text{C/min}$ and at $400 \text{ }^\circ\text{C}$ for 1 h with an annealing rate of $1 \text{ }^\circ\text{C/min}$ for binder removal prior to the sensing test.

2.4. Sensor Measurement

The sensor characteristics of the sensing films were determined with acetone (25–400 ppm) and ethanol (50–1,000 ppm). The flow through technique was used to test the gas-sensing properties of sensing films. A constant flux of synthetic air of 2 L/min as gas carrier was flowed to mix with the desired concentration of pollutants dispersed in synthetic air. All measurements were conducted in a temperature-stabilized sealed chamber at $20 \text{ }^\circ\text{C}$ under controlled humidity. The gas flow rates were precisely manipulated using a computer controlled multi-channel mass flow controller. The external NiCr heater was heated by a regulated DC power supply to different operating temperatures. The operating temperature was varied from $250 \text{ }^\circ\text{C}$ to $400 \text{ }^\circ\text{C}$. The resistances of various sensors were continuously monitored with a computer-controlled system by voltage-amperometric technique with 5 V DC bias and current measurement through a picoammeter. The sensor was exposed to the gas mixed sample for ~5 min for each gas concentration testing and then the air flux was restored for 15 min. The response (S) is defined in the following as the resistance ratio R_a/R_g [25], where R_a is the resistance in dry air, and R_g is the resistance in the test gas. The response time (T_{res}) is defined as the time required until 90% of the response signal is reached. The recovery time (T_{rec}) denotes the time needed until 90% of the original baseline signal is recovered [25]. After the sensors fabricated using samples undoped TiO_2 , 1 at.% Nb/ TiO_2 , 3 at.% Nb/ TiO_2 , and 5 at.% Nb/ TiO_2 had been tested with varied operating temperatures, they were designated as S0, S1, S3, and S5, respectively.

3. Results and Discussion

3.1. Nanopowder Properties

The XRD technique was used to study the relative amounts of anatase and rutile phases and the evolution of crystallite sizes as a function of composition of the flame-made undoped TiO_2 and Nb-doped TiO_2 . Figure 1 shows the XRD patterns of nano-sized undoped TiO_2 and 1–5 at.% Nb/ TiO_2 samples. The nanopowders were highly crystalline, and all peaks can be confirmed to be the anatase

phase (JCPDS file no. 21-1272). No amorphous phase and the characteristic peaks attributed to Nb or NbO₂ were found in the XRD patterns. It can be assumed that the amount of Nb doping particles was very low, which resulted in non-appearance of the Nb peaks. The relative amounts of anatase and rutile and their respective crystallite sizes were calculated from the XRD data using the fundamental parameter approach Rietveld method [26]. The average crystal sizes (d_{XRD} ave.) were calculated based on the half-maximum widths in Scherrer equation [27] using the TOPAS-3 software, which compared with the average BET-equivalent particle diameter (d_{BET}) as shown in Table 2. The d_{XRD} (rutile) was slightly increased with increasing Nb-doped concentrations. On the other hand, the d_{XRD} (anatase) decreased with increasing Nb-doping concentrations. The rutile weight fraction percentage and d_{BET} remained almost the same with increasing Nb concentrations. It can be concluded from Table 2 that (1) d_{XRD} anatase were smaller than d_{XRD} rutile (2) d_{BET} and d_{XRD} anatase were not affected by the amount of dopant but d_{XRD} rutile were.

Figure 1. XRD patterns of undoped and Nb-doped TiO₂ flame-made samples.

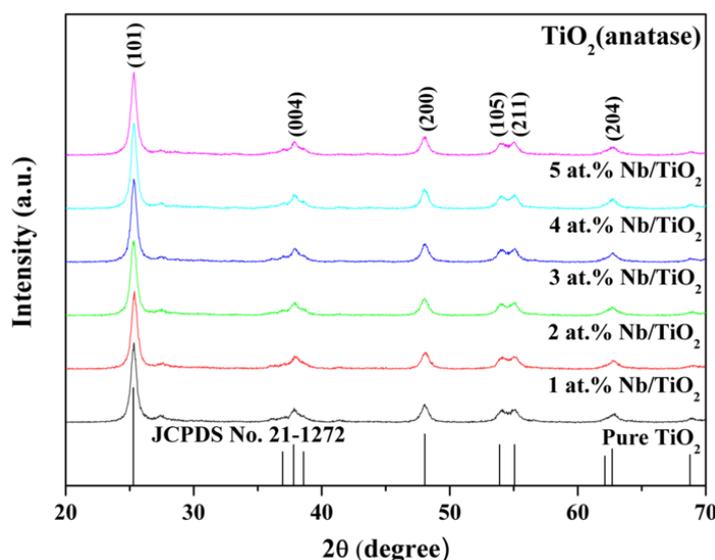


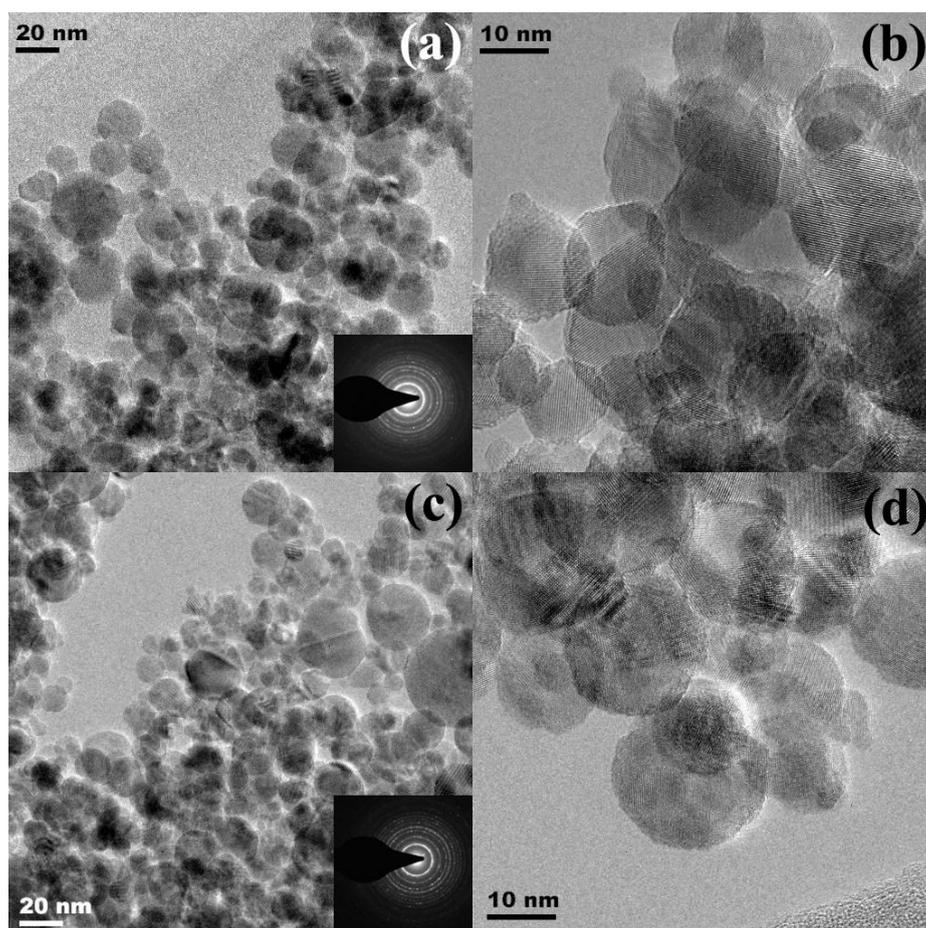
Table 2. The relative amounts of anatase, rutile and their crystallite sizes calculated from the XRD data using the Rietveld method and BET average primary particle size of undoped TiO₂ and Nb-doped TiO₂ FSP samples.

at.% Nb	Anatase (wt.%)	d_{XRD} , Anatase (nm)	Rutile (wt.%)	d_{XRD} , Rutile (nm)	d_{BET} (nm)
0	86.3	17.9	13.7	12.5	15.0
1	86.7	17.5	13.3	10.9	14.1
2	88.1	17.7	11.9	11.3	14.0
3	90.5	18.1	9.5	13.6	14.3
4	90.9	18.8	9.1	14.3	14.8
5	93.4	17.3	6.6	15.2	14.4

Figure 2 shows HR-TEM bright-field images of (a,b) undoped TiO₂ and (c,d) 5 at.% Nb/TiO₂ nanoparticles with different magnifications. The corresponding diffraction patterns were shown in the

insets. Both samples were highly crystalline as seen from the intense electron diffraction patterns (Figure 2(a,c): insets), which were in good agreement with the XRD data. Figure 2(a–d) show the TEM bright-field images of the FSP-made (5/5) nanoparticles, which were aggregated of primary particles. Nb-doped TiO_2 nanopowder formed $\text{Ti}_{1-x}\text{Nb}_x\text{O}_2$ with a fully solid solution due to diffusion of Nb atom into the TiO_2 nanoparticles because Nb^{4+} has a similar ionic radius (0.64 Å) to Ti^{4+} (0.605 Å). Teleki *et al.* [23] reported that niobium was partly incorporated in the titania lattice promoting anatase formation.

Figure 2. (a,b) HR-TEM bright-fields images of highly crystalline flame-made (5/5) TiO_2 nanoparticles and (c,d) 5 at.% Nb/ TiO_2 nanoparticles with different magnifications. Insets show the corresponding diffraction patterns of the particles and clearly the TiO_2 lattice planes.



Figures 2(a,b) show the morphologies of flame-made (5/5) undoped TiO_2 and 5 at.% Nb/ TiO_2 nanoparticles containing spherical nanoparticles with average diameters of 13 and 11 nm, respectively. The primary particle diameters observed by TEM were consistent with both the d_{BET} and the d_{XRD} . Particularly, the lattice fringes of 5 at.% Nb/ TiO_2 nanoparticles were also clearly visible in a HRTEM image at higher magnification (Figures 2(b,d)). TEM bright-field images can reveal internal structure and a more accurate measurement of particle size and morphology.

3.2. Gas Sensing Properties

The gas sensitivity is usually dependent on the sensor operating temperature and the dopant. Figure 3 shows the response as a function of sensor operating temperature for undoped and doped with different Nb concentrations (1, 3, and 5 at.% Nb) for ethanol (Figure 3(a)) and acetone (Figure 3(b)) vapors in dry air atmosphere. The measurement of the resistance vs. temperature (R/T) profile of undoped TiO₂ sensor revealed a strong temperature dependence of their resistance and quite low response. It was evident from these results that the response of the undoped sensor (S0) was very poor compared to the doped sensors in different concentration concentrations. With 3 at.% Nb doped TiO₂ sensor (S3), the sensor showed maximum response to ethanol vapor at an operating temperature of 350 °C for sensor S3 and 400 °C for the other sensors, and for acetone vapor maximum sensitivity at an operating temperature of 400 °C for all sensors. The best sensitivities can be seen at the highest concentration of gases (to 1,000 ppm; $S_{eth} = 41.4$ (350 °C), $S_{eth} = 31.7$ (400 °C), to 400 ppm, $S_{acet} = 13.0$) and response time was extremely fast about 1 s (400 °C) and 9 s (350 °C) for ethanol vapor and of about 33 s for acetone vapor. On the other hand, the response decreased at higher Nb concentration (5 at.% Nb/TiO₂; S5). Further increase of the dopant concentration decreased the ethanol and acetone sensitivity and deteriorated the response time. The optimum concentration of Nb doping on TiO₂ sensor was found to be 3 at.% Nb. Possibly a segregated Nb phase was formed on the surface at a higher Nb content (5 at.% Nb/TiO₂). For low Nb content (3 at.%), Nb nanoparticles are very small compared to TiO₂ nanoparticles and they can be well dispersed on TiO₂ nanoparticles. Thus, Nb nanoparticles are very effective catalyst. In contrast, larger Nb nanoparticles, which are formed at higher Nb contents, cannot be well dispersed and cause possible separation among TiO₂ nanoparticles. Therefore, catalytic action of Nb becomes considerably less effective. This is the reason why the gas sensitivity decreases significantly at the higher Nb content of 5 at.%.

Traversa *et al.* [9] reported a solubility of up to 5 at.% Nb in anatase TiO₂. They attributed this to small segregated crystalline domains of niobia (Nb₂O₅), which were not visible in the TEM bright-field images (Figure 2). Our results agreed well with those of Comini *et al.* [28] showing that Nb doping improved the response to ethanol with respect to undoped TiO₂. Teleki *et al.* [23] reported that 4 at.% Nb/TiO₂ showed higher response towards 25–300 ppm ethanol than 10 at.% Nb/TiO₂ at 400 °C.

Figures 4(a,b) show the change in resistance of sensor S0 (Undoped TiO₂), S1(1 at.% Nb/TiO₂), S3 (3 at.% Nb/TiO₂), and S5 (5 at.% Nb/TiO₂) under exposure to reducing gas ethanol (Figure 4(a)) and acetone (Figure 4(b)) at the concentration ranging from 50–1,000 ppm and 25–400 ppm, respectively with the same operating temperature of 400 °C during the backward cycle. The original baseline (dry air) of ethanol sensing was stable during the sensing test. The resistance drastically decreased during the gas exposure with increasing VOC analyte gas concentration, typical for anatase TiO₂ as an n-type semiconductor. Nb-doped TiO₂ could exhibit a stronger n-type character and a higher electronic conductivity than undoped TiO₂ as the electron concentration in the titania lattice might increase and the Fermi level might be shifted closer to the conduction band level. The stabilized original baselines of sensors led to sensor response accuracy in terms of sensitivity and response time detection. The base-resistance of the sensor S3 (3 at.% Nb/TiO₂) was the lowest compared to the other sensors. This is because the sensor S3 had the appropriate amount of concentration and also could

perform the sensing properties on the surface and by bulk interaction. The gas sensing behavior of semiconducting oxide sensors could be attributed to both regions of surface and bulk interactions, depending on the small grain size and the appropriate thickness of sensing films. The effects of a high conductivity of the sensor are described clearly from the interactions between VOCs gases and the surface-absorbed oxygen species such as peroxide ion (O_2^{2-}) and superoxide ion (O_2^-). These reactions produce more electrons and thus increased the conductivity of TiO_2 upon exposure to ethanol and acetone vapor.

Figure 3. The sensitivity as a function of sensor operating temperature for undoped and doped with different Nb concentrations (1, 3, and 5 at.% Nb) for (a) ethanol and (b) acetone vapors in dry air atmosphere.

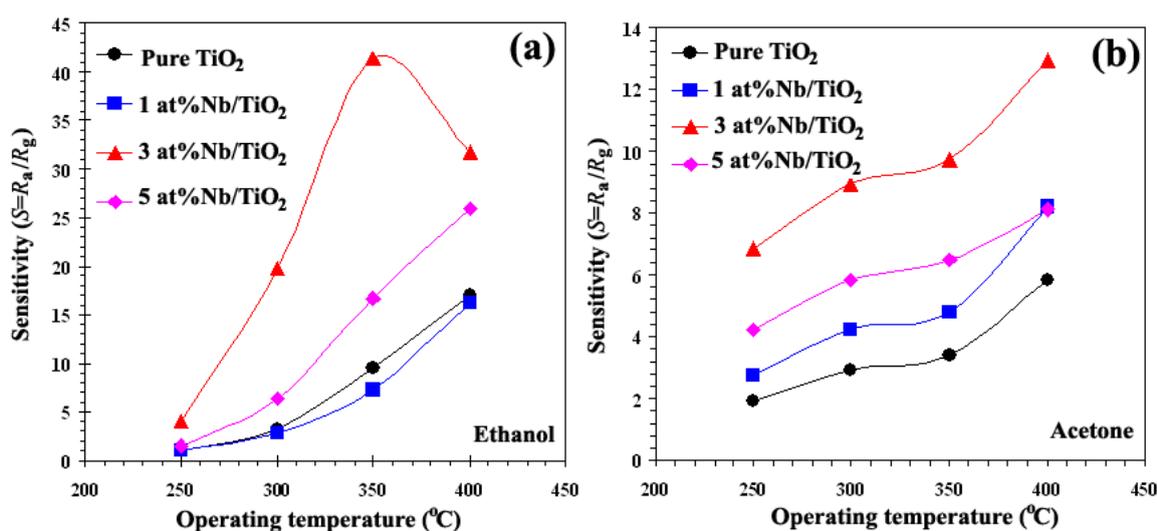
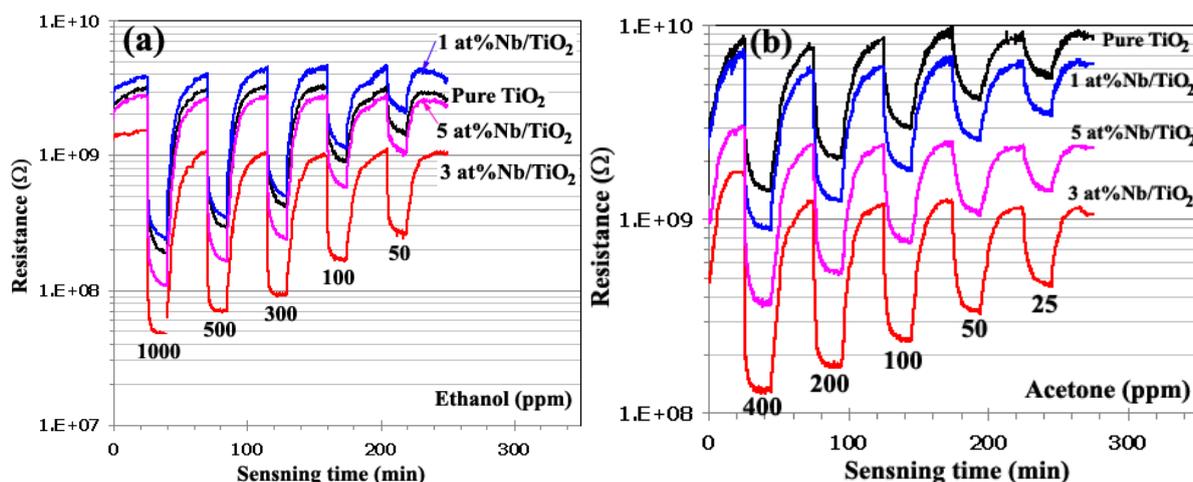


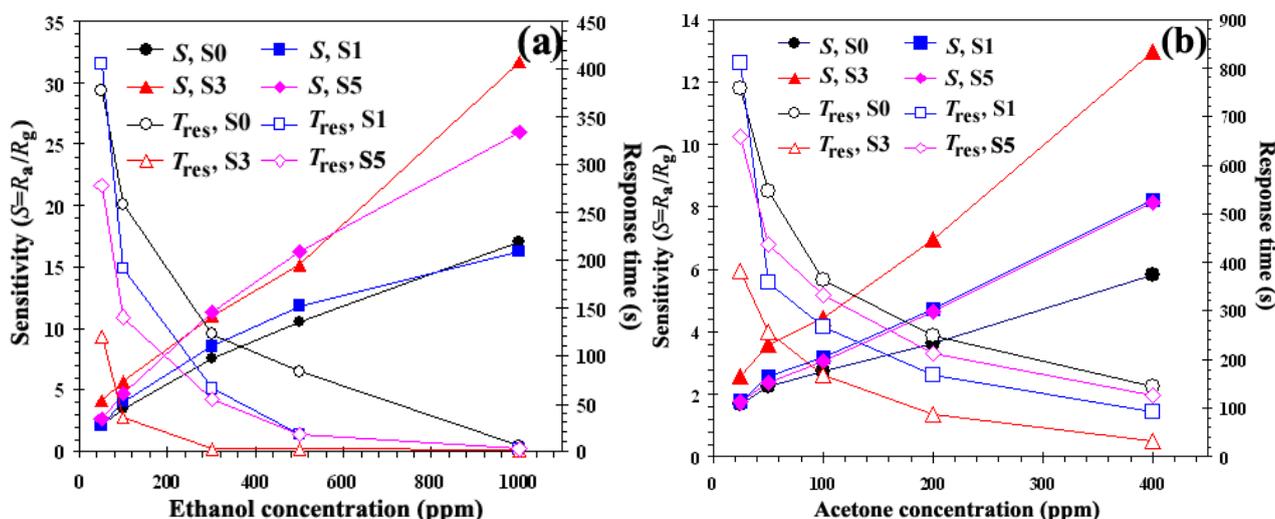
Figure 4. Change in resistance of sensors under exposure to reducing (a) ethanol and (b) acetone gases during backward cycle with various concentration of ethanol (50–1,000 ppm) and acetone (25–400 ppm) in dry air at 400 °C.



Figures 5(a,b) show the plots of response (S) and response times (T_{res}) versus the ethanol and acetone vapor concentrations ranging from 50–1,000 ppm and 25–400 ppm plot for the sensors S0, S1, S3, and S5 during the backward cycle at the operating temperature of 400 °C. Because the particle size

of TiO₂ was in the nanometer range and Nb is known as an excellent catalyst for VOC gases, we paid close attention to the gas sensing activity of this material. From the data, the response of all Nb doping concentrations (S1, S3, and S5) appeared to be higher than that of an undoped TiO₂ sensor (S0). The response of both gases (filled symbols, left axis) increased linearly and the response time (open symbols, right axis) decreased drastically with increasing ethanol and acetone concentrations. Moreover, it was found that the 3 at.% Nb concentration (S3) sensor showed the best sensing performance in terms of response ($S = 31.7$) and response time. The response time of 3 at.% Nb/TiO₂ sensor (S3) for 1,000 ppm at 400 °C was very fast—within 1 s (open triangles, right axis)—which was better than that of undoped TiO₂ (6 s) (open circles, right axis) and other doping concentrations (1 at.% Nb/TiO₂ = 3 s (open rectangles, right axis), and 5 at.% Nb/TiO₂ = 2 s (open diamonds, right axis)). The fast response time suggests a surface controlled sensing mechanism, where a steady-state adsorption of ethanol and desorption of CO₂ [25] on the sensing films was rapidly reached. This is the common interaction between the reducing gas ethanol and surface-adsorbed oxygen species of sensing layer including ethanol with those of its oxidation products (CO₂ and H₂O) *versus* times in dry air. This is because CO₂ was the majority product oxidized with oxygen on the surface of semiconductor materials. This indicates a partial combustion of ethanol to CO₂ and H₂O, as well as a release of ethoxides formed during the adsorption of ethanol on the sensing surface. Also, Nb possible increases the number of surface-adsorbed oxygen species, thus promoting reaction sizes for CO oxidations. Teleki *et al.* [23] reported the response of 30 with response time of 375 seconds towards 75 ppm ethanol at 500 °C for undoped TiO₂ sensing film by the drop-coating technique.

Figure 5. Sensitivity of S0, S1, S3, and S5 (filled symbols, left axis) and the corresponding response time (open symbols, right axis) of (a) ethanol and (b) acetone detections.



With the acetone response, the sensing performances were lower than for ethanol vapor in terms of the sensor response, sensitivity, and response time. It was noticed that the Nb concentration (3 at.%; S3) sensor showed the best sensing performance at an operating temperature of 400 °C for the highest acetone concentration to 400 ppm in terms of response ($S = 13.0$) and response time. The response time of acetone sensors were with a few minutes. The best response time of 3 at.% Nb/TiO₂ sensor (S3) for 400 ppm at 33 s which was better than undoped TiO₂ (147 s) (open circles, right axis) and the

other doping concentrations (1 at.% Nb/TiO₂ = 93 s (open rectangles, right axis), and 5 at.% Nb/TiO₂ = 126 s (open diamonds, right axis)). The response time of 3 at.% Nb/TiO₂ sensor (S3) for 400 ppm at 400 °C was slightly sluggish compared to 300 ppm of an ethanol (2 s) (Figure 5(a), open triangles, right axis) sample. Doping the TiO₂ with 3 at.% Nb resulted in a much steeper calibration curve and the highest sensor signal compared to undoped TiO₂ (see Figures 5(a,b)). The higher sensor signal and especially the higher response (*i.e.*, the steeper response curve) increased sensor performance.

4. Conclusions

FSP was successfully used for the preparation of undoped TiO₂ and 1–5 at.% Nb/TiO₂ nanopowders for application to acetone and ethanol gas sensing. The trend of SSA_{BET} on the doping samples increased and the d_{XRD} (rutile) increased with the higher Nb-doping concentrations while d_{BET} remained almost the same. Nb could form a solid solution in the crystal structure of TiO₂ due to the fact the size of Nb⁵⁺ (0.64 Å) is similar to that of Ti⁴⁺ (0.605 Å), thus the size of particles in the doping samples were not affected by Nb atoms as shown from the HRTEM. The crystallite sizes of undoped and Nb-doped TiO₂ spherical were in the 10–20 nm range. The gas sensing of acetone (25–400 ppm) was studied at operating temperatures ranging from 300–400 °C in dry air while the gas sensing of ethanol (50–1,000 ppm) was studied at operating temperatures ranging from 250–400 °C in dry air. The 3 at.% Nb-dispersed on TiO₂ sensing film showed a response of 31.7 and a very fast response time of 1 second towards 400 ppm ethanol, as compared to an undoped TiO₂ sensing film. The 3 at.% Nb-dispersed on TiO₂ sensing film also showed a response of 13 and a response time of 33 seconds towards 400 ppm acetone. The response times in our study were faster than the previously reported values [16,23]. The highest responses for acetone and ethanol occurred at 400 and 350 °C, respectively.

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