Supplementary Materials

CartesianCo-ordinates of optimized geometry at B3LYP/6-31G (d, p) (1)

С	3.19696900	-1.18947100	-0.11479500
С	2.33950900	-0.05164900	-0.16975400
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С	2.78752700	1.36261900	-0.23987600
С	3.95114700	1.73798200	-0.93139500
С	1.98366100	2.36206800	0.33313900
С	4.30492300	3.08110900	-1.03612200
Н	4.56977600	0.98124500	-1.39986500
С	2.35039300	3.70227700	0.24078200
Н	1.07112200	2.07482100	0.84343500
С	3.51180600	4.06586600	-0.44369400
Н	5.20024200	3.35867900	-1.58418000
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С	6.87043100	-2.08726300	-0.20393300
Н	5.09699000	-2.69340400	-1.27320200
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Ν	1.01704000	-0.23682000	-0.21723000
Ν	1.37988100	-2.58962700	-0.46653400
Ν	2.67810600	-2.41301700	-0.32840000
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N	-0.74499500	-1.77426200	-0.27995700
Ν	-1.66932600	-0.79652000	-0.15581500
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С	-5.82548000	-1.79337500	-0.03700100
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С	-4.58220800	2.26595800	0.23421300
С	-7.17296400	-2.08695900	0.00646800

Н	-5.12749400	-2.61655400	-0.13766400
С	-7.71205400	0.24621700	0.22287800
С	-5.90847400	1.93344700	0.27185300
Н	-4.24557500	3.29479900	0.30181700
С	-8.13307600	-1.06173200	0.13743700
Н	-7.49598900	-3.12181200	-0.06113300
Н	-8.43412800	1.05235700	0.32461200
Н	-6.66185100	2.71017300	0.37236400
Н	-9.19042000	-1.30519700	0.17036100
0	-2.31975800	1.69150800	0.07643300
Н	-1.71834000	0.90999600	-0.02875200

CartesianCo-ordinates of optimized geometry at B3LYP/6-31G (d, p) (2)

С	2.97758400	-1.06480900	-0.09537300
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С	2.29672100	1.42541900	-0.24219000
С	3.39498300	1.92055700	-0.96353700
С	1.40729700	2.33481900	0.35282600
С	3.60249400	3.29365700	-1.07506400
Н	4.07769000	1.23259800	-1.44922900
С	1.62851000	3.70633100	0.25465600
Н	0.54415900	1.94850900	0.88354000
С	2.72652200	4.19004900	-0.45948800
Н	4.44898800	3.66348100	-1.64586500
Н	0.94003500	4.39847000	0.73046800
Н	2.89593500	5.25978500	-0.54099400
С	4.42430900	-0.89107000	0.19121200
С	5.36809800	-1.68409600	-0.48115900
С	4.87273500	-0.00090900	1.18046700
С	6.72560600	-1.57267600	-0.18689900
Н	5.02178700	-2.39013800	-1.22797300
С	6.23034700	0.10482800	1.47589800
Н	4.15529700	0.60311100	1.72605700
С	7.16250200	-0.67647100	0.79044800
Н	7.44338600	-2.18826500	-0.72135700
Н	6.55915600	0.79412400	2.24814100
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Ν	0.70595200	-0.35014300	-0.19525400
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Ν	-0.87856100	-2.08342300	-0.23101400
Ν	-1.93255400	-1.24324100	-0.12873300
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С	-5.44944500	1.16741600	0.16610200
С	-6.69875800	0.51990100	0.16571200
Н	-5.43100400	2.24966400	0.24124700
Н	-5.62205800	-2.68703500	-0.10272300
Н	-7.70431700	-1.39760000	0.06539900
0	-7.78448500	1.33702700	0.26308100
С	-9.07539300	0.74585000	0.26445200
Н	-9.20874500	0.06843200	1.11734300
Н	-9.78381100	1.57104100	0.34719600
Н	-9.26874300	0.19548300	-0.66497600
Н	-3.31778200	0.93216900	0.06876700

CartesianCo-ordinates of optimized geometry at B3LYP/6-31G (d, p) (3)

С	3.33597000	-1.04160900	-0.08827100
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С	2.57097100	1.42248800	-0.25338100
С	3.65237500	1.95027900	-0.97687100
С	1.65039600	2.30506000	0.33439100
С	3.81324200	3.32893800	-1.09734100
Н	4.35884400	1.28287600	-1.45728900
С	1.82473800	3.68271400	0.22718200
Н	0.79989300	1.89275300	0.86596800
С	2.90651300	4.19913900	-0.48884000
Н	4.64748400	3.72348000	-1.66970800
Н	1.11226500	4.35403300	0.69761100
Н	3.03953500	5.27349900	-0.57725700
С	4.77538500	-0.81768000	0.19963500
С	5.74649700	-1.58419700	-0.46481000
С	5.19299300	0.09463800	1.18220800
С	7.09908400	-1.42553000	-0.16969000
Н	5.42491800	-2.30754200	-1.20610500

С	6.54596200	0.24821600	1.47818700
Н	4.45504800	0.67834000	1.72253700
С	7.50478000	-0.50718900	0.80053800
Н	7.83764900	-2.02151500	-0.69810700
Н	6.85036700	0.95445600	2.24517100
Н	8.55913100	-0.38479300	1.03075600
Ν	1.04136600	-0.40508300	-0.19829700
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Ν	2.99253900	-2.33013900	-0.27862900
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Ν	-1.56820100	-1.38797800	-0.12467600
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С	-5.19222500	-1.91261200	-0.03359300
С	-4.00789300	0.17600800	0.06316900
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С	-7.66726900	2.29774300	0.22333800
Н	-8.69242500	2.64662700	0.35304700
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Н	-7.28869000	2.69497300	-0.73044800
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Н	-9.73208300	0.81393600	0.26731800
Н	-9.00655500	-0.34191300	-0.86659400
Ν	-7.64886300	0.84547100	0.27398400

CartesianCo-ordinates of optimized geometry at B3LYP/6-31G (d, p) (4)

С	2.33411600	-1.13082900	-0.11277400
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С	-0.22262500	-1.69677700	-0.27897700
С	1.67422800	1.36742200	-0.24721200
С	2.77808800	1.85213500	-0.96789600
С	0.79149800	2.28521100	0.34571600

C	2.99683500	3.22303000	-1.08155600
Н	3.45532100	1.15797800	-1.45226200
С	1.02414100	3.65452500	0.24476400
H	-0.07595600	1.91192400	0.87857200
С	2.12701000	4.12750100	-0.46889500
Н	3.84686200	3.58488400	-1.65209400
Н	0.33950800	4.35237300	0.71724600
Н	2.30478600	5.19563300	-0.55280700
С	3.78292500	-0.97037000	0.17134100
С	4.71860800	-1.76567200	-0.50930400
С	4.23925900	-0.09137300	1.16687100
С	6.07743800	-1.66711100	-0.21656300
H	4.36569100	-2.46282400	-1.26135100
С	5.59804800	0.00076500	1.46107700
H	3.52760000	0.51440800	1.71805900
С	6.52259600	-0.78246900	0.76752400
H	6.78953600	-2.28378400	-0.75718200
H	5.93373200	0.68100700	2.23827000
H	7.58165100	-0.70739300	0.99610800
N	0.06976800	-0.39784000	-0.19972800
N	0.66028600	-2.70480900	-0.43797400
N	1.93645400	-2.40087900	-0.31244800
Η	-1.70283300	-3.09955400	-0.34277800
С	-3.76503400	-1.65600200	-0.09715800
H	-3.98847200	-2.72678900	-0.18127500
N	-1.53343800	-2.10242200	-0.24376700
N	-2.54894500	-1.22138200	-0.11910700
С	-4.88434700	-0.74286500	0.04263000
С	-6.19635300	-1.25410500	0.06415800
С	-4.69486100	0.66243100	0.16276200
С	-7.29692600	-0.42086800	0.20037900
С	-5.81341500	1.49637400	0.30085400
С	-7.09554700	0.96083200	0.31944600
Н	-5.64343800	2.56404500	0.39049100
H	-7.94826500	1.62501800	0.42690800
0	-3.47823900	1.23777000	0.15006400
Н	-2.79512900	0.53595300	0.03285300
Н	-6.33549300	-2.32870500	-0.02847200
Н	-8.29965400	-0.83485800	0.21487100
H H O H	-5.64343800 -7.94826500 -3.47823900 -2.79512900	2.56404500 1.62501800 1.23777000 0.53595300	0.39049 0.42690 0.15006 0.03285



Figure S1. Experimental ¹H-NMR spectrum of 1 measured in *d*₆-DMSO.



Figure S2. Experimental ¹H-NMR spectrum of 2 measured in *d*₆-DMSO.



Figure S3. Experimental ¹H-NMR spectrum of 3 measured in *d*₆-DMSO.



Figure S4. Experimental ¹H-NMR spectrum of 4 measured in *d*₆-DMSO.



Figure S5. Experimental ¹³C-NMR spectrum of 1 measured in *d*₆-DMSO.



Figure S6. Experimental ¹³C-NMR spectrum of **2** measured in *d*₆-DMSO.



Figure S7. Experimental ¹³C-NMR spectrum of **3** measured in *d*₆-DMSO.



Figure S8. Experimental ¹³C-NMR spectrum of 4 measured in *d*₆-DMSO.



Figure S9. Combined simulated UV–vis. spectra of (1–4) measured at TD–B3LYP/6–31G (d, p) level in gas phase.



Figure S10. Combined simulated UV–vis. spectra of Compounds (1–4) measured at TD–B3LYP/6–31G (d, p) level measured in DMSO.

Molecule 1Cif

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cell angle beta
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cell angle gamma
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AFIX 43

H16 2 0.70769 0.12283 -0.10909 11.00000 -1.20000 AFIX 0 $C17 \quad 1 \quad 0.44474 \quad 0.17814 \quad -0.09724 \quad 11.00000 \quad 0.05206 \quad 0.05525 =$ 0.06199 -0.01641 0.00025 0.00187 $O1 \quad 4 \quad 0.26256 \quad 0.14727 \quad 0.01996 \quad 11.00000 \quad 0.07524 \quad 0.09976 =$ 0.08665 - 0.01813 0.02980 0.00230C3 1 0.83687 - 0.04733 0.23186 11.00000 0.05265 0.05078 =0.04977 - 0.00361 0.00787 - 0.00290C1 1 0.78237 0.01918 0.08875 11.00000 0.06045 0.05600 = 0.04846 - 0.00303 0.01089 0.00130C10 1 0.87174 -0.09157 0.30699 11.00000 0.06036 0.04663 = $0.05235 - 0.00234 \quad 0.00782 \quad 0.00138$ C4 1 0.55179 0.02649 0.28247 11.00000 0.06050 0.04692 =0.05020 -0.00025 0.01421 -0.00241 0.06547 -0.01198 -0.01089 0.00379 C15 1 $1.06929 - 0.10474 \quad 0.34288 \quad 11.00000 \quad 0.06098 \quad 0.07059 =$ 0.07676 0.01028 0.00792 0.00616 AFIX 43 H15 2 1.17982 -0.08493 0.32082 11.00000 -1.20000 AFIX 0 C11 1 0.71025 -0.12195 0.34051 11.00000 0.06394 0.05434 = $0.05893 - 0.00102 \ 0.00811 - 0.00285$ AFIX 43 H11 2 0.57684 -0.11354 0.31706 11.00000 -1.20000 AFIX 0 C21 1 0.28750 0.26597 -0.19321 11.00000 0.06510 0.05507 = 0.09240 -0.01992 -0.01384 0.00837 C9 1 0.62712 0.03353 0.36682 11.00000 0.08251 0.05689 = 0.05299 -0.00217 0.00973 0.00318 AFIX 43 H9 2 0.76115 0.02132 0.38527 11.00000 -1.20000 AFIX 0 C23 1 0.61896 0.22284 - 0.21813 11.00000 0.06597 0.05851 =0.06810 - 0.00148 - 0.00348 0.00258AFIX 43 H23 2 0.73035 0.19471 -0.20388 11.00000 -1.20000 AFIX 0 C5 1 0.35235 0.04602 0.25593 11.00000 0.06013 0.06297 =0.06367 0.00198 0.01554 -0.00088 AFIX 43

H5 2 0.30247 0.04287 0.19929 11.00000 -1.20000

AFIX 0 C18 1 0.27932 0.18373 -0.05053 11.00000 0.05927 0.06991 = $0.07449 - 0.02360 \quad 0.00956 - 0.00230$ C19 1 0.11700 0.22897 -0.07540 11.00000 0.05551 0.08524 = 0.11061 -0.03928 0.01213 0.00461 AFIX 43 H19 2 0.00602 0.23186 -0.04421 11.00000 -1.20000 AFIX 0 C12 1 0.74536 -0.16476 0.40862 11.00000 0.08891 0.05719 = 0.06847 0.00651 0.02176 -0.00066 AFIX 43 H12 2 0.63565 -0.18523 0.43051 11.00000 -1.20000 AFIX 0 C24 1 0.62003 0.26500 -0.28631 11.00000 0.09234 0.06469 = 0.07831 0.00716 -0.00299 -0.00408 AFIX 43 H24 2 0.73275 0.26534 -0.31670 11.00000 -1.20000 AFIX 0 C6 1 0.22776 0.07007 0.31319 11.00000 0.06948 0.07181 =0.09393 0.00400 0.03362 0.00546 AFIX 43 H6 2 0.09361 0.08245 0.29521 11.00000 -1.20000 AFIX 0 0.10238 - 0.00167 - 0.03025 0.01510AFIX 43 H26 2 0.18335 0.33513 -0.28242 11.00000 -1.20000 AFIX 0 C20 1 0.12352 0.26795 -0.14449 11.00000 0.06813 0.06830 = 0.11506 -0.02553 -0.01397 0.01567 AFIX 43 H20 2 0.01525 0.29704 -0.16007 11.00000 -1.20000 AFIX 0 C14 1 1.10248 - 0.14725 0.41141 11.00000 0.07616 0.08202 =0.08226 0.01401 - 0.00047 0.01825AFIX 43 H14 2 1.23541 -0.15558 0.43552 11.00000 -1.20000 AFIX 0 C7 1 0.30152 0.07574 0.39652 11.00000 0.10837 0.06968 = 0.08312 -0.00576 0.04938 0.00348 AFIX 43 H7 2 0.21637 0.09105 0.43519 11.00000 -1.20000

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C8
   1 0.50102 0.05887 0.42313 11.00000 0.12174 0.06718 =
   0.05460 - 0.00545 0.02563 0.00032
AFIX 43
H8
    2 0.55165 0.06451 0.47938 11.00000 -1.20000
AFIX 0
C13 1 0.94141 -0.17718 0.44405 11.00000 0.10531 0.06408 =
   0.06807 0.01568 0.01221 0.01992
AFIX 43
H13 2 0.96473 -0.20582 0.49008 11.00000 -1.20000
AFIX 0
C25 1 0.45545 0.30703 -0.31044 11.00000 0.11083 0.06160 =
   0.09242 0.00879 -0.01289 0.00479
AFIX 43
H25 2 0.45689 0.33479 -0.35717 11.00000 -1.20000
H2
     2 0.86974 0.04137 -0.02193 11.00000 0.08658
H1
     2 0.39354 0.11887 0.03188 11.00000 0.12375
HKLF 4
refine special details
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Refinement of F^2^ against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2^,Conventional R-factors R are based on F, with F set to zero forNegative F^2^. The threshold expression of $F^2^2 > 2sigma(F^2^2)$ is used only forCalculating R-factors(gt) etc. and is Not relevant to theChoice of reflections for refinement. R-factors based on F^2^ are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

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```
refine ls structure factor coef Fsqd
refine ls matrix type
                              full
refine ls weighting scheme
                                Calc
refine ls weighting details
'calc w=1/[s^2(Fo^2)+(0.0605P)<sup>2</sup>+0.3132P] where P=(Fo<sup>2</sup>+2Fc<sup>2</sup>)/3'
atom sites solution primary
                                 direct
atom sites solution secondary
                                  difmap
atom sites solution hydrogens
                                  geom
refine ls hydrogen treatment
                                Constr
refine ls extinction method
                                None
refine ls extinction coef
                              ?
refine ls number reflns
                               4304
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refine ls number parameters 291 refine ls number restraints 0 refine ls R factor all 0.0546 refine ls R factor gt 0.0428 refine ls wR factor ref 0.1273 refine ls wR factor gt 0.1156 refine ls goodness of fit ref 1.034 refine ls restrained S all 1.034 refine ls shift/su max 0.000 refine ls shift/su mean 0.000 loop atom site label _atom_site_type_symbol atom site fract x _atom_site_fract_y atom site fract z atom site U iso or equiv atom site adp type atom site occupancy atom site symetry multiplicity atom site calc flag atom site refinement flags atom site disorder assembly atom site disorder group N1N 0.65264(18) 0.03442(6) 0.14503(7) 0.0538(3) Uani 1 1 d . . . C2C 0.6831(2) 0.00284(7) 0.21855(8) 0.0492(3) Uani 1 1 d . . . N2N 0.9417(2) -0.02273(7) 0.10197(8) 0.0599(3) Uani 1 1 d . . . N3N 0.96465(19) -0.05728(6) 0.17355(8) 0.0578(3) Uani 1 1 d . . . N5N 0.6080(2) 0.09574(7) -0.00542(8) 0.0606(3) Uani 1 1 d . . . N4N 0.7593(2) 0.04938(7) 0.01218(8) 0.0659(4) Uani 1 1 d . . . C16C 0.6056(2) 0.12956(8) -0.07406(9) 0.0558(3) Uani 1 1 d ... H16H 0.7077 0.1228 -0.1091 0.067 Uiso 1 1Calc R ... C17C 0.4447(2) 0.17814(8) -0.09724(10) 0.0569(4) Uani 1 1 d ... O1 O 0.2626(2) 0.14727(8) 0.01996(9) 0.0857(4) Uani 1 1 d . . . C3C 0.8369(2) -0.04733(7) 0.23186(9) 0.0509(3) Uani 1 1 d . . . C1C 0.7824(2) 0.01918(8) 0.08875(9) 0.0546(3) Uani 1 1 d . . . C10C 0.8717(2) -0.09157(7) 0.30699(9) 0.0530(3) Uani 1 1 d ... C4C 0.5518(2) 0.02649(7) 0.28247(9) 0.0519(3) Uani 1 1 d . . . C22C 0.4529(2) 0.22129(7) -0.16932(10) 0.0595(4) Uani 1 1 d ... C15C 1.0693(3) -0.10474(9) 0.34288(11) 0.0694(4) Uani 1 1 d ... H15H 1.1798 -0.0849 0.3208 0.083 Uiso 1 1Calc R ...

C11C 0.7102(2) -0.12195(8) 0.34051(10) 0.0590(4) Uani 1 1 d . . . H11H 0.5768 -0.1135 0.3171 0.071 Uiso 1 1Calc R ... C21C 0.2875(3) 0.26597(8) -0.19321(12) 0.0725(5) Uani 1 1 d ... C9C 0.6271(3) 0.03353(8) 0.36682(10) 0.0640(4) Uani 1 1 d . . . H9H 0.7612 0.0213 0.3853 0.077 Uiso 1 1Calc R . . C23C 0.6190(3) 0.22284(8) -0.21812(10) 0.0650(4) Uani 1 1 d ... H23H 0.7303 0.1947 -0.2039 0.078 Uiso 1 1Calc R ... C5C 0.3524(2) 0.04601(8) 0.25593(11) 0.0616(4) Uani 1 1 d . . . H5H 0.3025 0.0429 0.1993 0.074 Uiso 1 1Calc R . . C18C 0.2793(2) 0.18373(9) -0.05053(11) 0.0677(4) Uani 1 1 d . . . C19C 0.1170(3) 0.22897(11) -0.07540(15) 0.0836(6) Uani 1 1 d ... H19H 0.0060 0.2319 -0.0442 0.100 Uiso 1 1Calc R ... C12C 0.7454(3) -0.16476(9) 0.40862(11) 0.0705(4) Uani 1 1 d . . . H12H 0.6356 -0.1852 0.4305 0.085 Uiso 1 1Calc R ... C24C 0.6200(3) 0.26500(9) -0.28631(12) 0.0794(5) Uani 1 1 d ... H24H 0.7328 0.2653 -0.3167 0.095 Uiso 1 1Calc R ... C6C 0.2278(3) 0.07007(9) 0.31319(13) 0.0766(5) Uani 1 1 d . . . H6H 0.0936 0.0824 0.2952 0.092 Uiso 1 1Calc R ... C26C 0.2939(4) 0.30726(9) -0.26564(14) 0.0869(6) Uani 1 1 d . . . H26H 0.1834 0.3351 -0.2824 0.104 Uiso 1 1Calc R ... C20C 0.1235(3) 0.26795(10) -0.14449(15) 0.0856(6) Uani 1 1 d ... H20H 0.0153 0.2970 -0.1601 0.103 Uiso 1 1Calc R ... C14C 1.1025(3) -0.14725(10) 0.41141(12) 0.0808(5) Uani 1 1 d ... H14H 1.2354 -0.1556 0.4355 0.097 Uiso 1 1Calc R ... C7C 0.3015(4) 0.07574(10) 0.39652(13) 0.0842(6) Uani 1 1 d . . . H7H 0.2164 0.0911 0.4352 0.101 Uiso 1 1Calc R ... C8C 0.5010(4) 0.05887(9) 0.42313(11) 0.0800(5) Uani 1 1 d . . . H8H 0.5517 0.0645 0.4794 0.096 Uiso 1 1Calc R ... C13C 0.9414(3) -0.17718(9) 0.44406(12) 0.0790(5) Uani 1 1 d ... H13H 0.9647 -0.2058 0.4901 0.095 Uiso 1 1Calc R ... C25C 0.4555(4) 0.30703(10) -0.31044(14) 0.0901(6) Uani 1 1 d . . . H25H 0.4569 0.3348 -0.3572 0.108 Uiso 1 1Calc R ... H2H 0.8697 0.0414 -0.0219 0.087(6) Uiso 1 1 d R ... H1H 0.3935 0.1189 0.0319 0.124(9) Uiso 1 1 d R ...

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_atom_site_aniso_label _atom_site_aniso_U_11 _atom_site_aniso_U_22 _atom_site_aniso_U_33 _atom_site_aniso_U_23 _atom_site_aniso_U_13 _atom_site_aniso_U_12

N1 0.0584(6) 0.0565(7) 0.0474(6) -0.0024(5) 0.0105(5) 0.0012(5) $C2\ 0.0519(7)\ 0.0489(7)\ 0.0471(7)\ -0.0039(6)\ 0.0066(5)\ -0.0051(6)$ N2 0.0663(7) 0.0635(7) 0.0519(7) 0.0011(6) 0.0159(5) 0.0069(6) N3 0.0618(7) 0.0577(7) 0.0554(7) -0.0006(6) 0.0129(5) 0.0039(6) N5 0.0632(7) 0.0652(8) 0.0544(7) -0.0034(6) 0.0111(5) 0.0084(6) N4 0.0725(8) 0.0750(9) 0.0529(7) 0.0085(6) 0.0193(6) 0.0198(7) C16 0.0566(8) 0.0598(8) 0.0515(8) -0.0059(6) 0.0082(6) 0.0042(7) $C17\ 0.0521(7)\ 0.0552(8)\ 0.0620(8)\ -0.0164(7)\ 0.0002(6)\ 0.0019(6)$ $O1\ 0.0752(8)\ 0.0998(10)\ 0.0866(9)\ -0.0181(8)\ 0.0298(7)\ 0.0023(7)$ $C3\ 0.0526(7)\ 0.0508(7)\ 0.0498(7)\ -0.0036(6)\ 0.0079(6)\ -0.0029(6)$ $C1\ 0.0605(8)\ 0.0560(8)\ 0.0485(7)\ -0.0030(6)\ 0.0109(6)\ 0.0013(7)$ C10 0.0604(8) 0.0466(7) 0.0523(8) -0.0023(6) 0.0078(6) 0.0014(6) C4 0.0605(8) 0.0469(7) 0.0502(7) -0.0003(6) 0.0142(6) -0.0024(6) $C22\ 0.0608(8)\ 0.0482(7)\ 0.0655(9)\ -0.0120(7)\ -0.0109(7)\ 0.0038(6)$ C15 0.0610(9) 0.0706(10) 0.0768(11) 0.0103(8) 0.0079(8) 0.0062(8) $C11\ 0.0639(8)\ 0.0543(8)\ 0.0589(8)\ -0.0010(7)\ 0.0081(7)\ -0.0029(7)$ $C21\ 0.0651(9)\ 0.0551(9)\ 0.0924(12)\ -0.0199(9)\ -0.0138(9)\ 0.0084(7)$ $C9\ 0.0825(10)\ 0.0569(8)\ 0.0530(8)\ -0.0022(7)\ 0.0097(7)\ 0.0032(8)$ C23 0.0660(9) 0.0585(9) 0.0681(10) -0.0015(7) -0.0035(7) 0.0026(7) $C5\ 0.0601(8)\ 0.0630(9)\ 0.0637(9)\ 0.0020(7)\ 0.0155(7)\ -0.0009(7)$ C18 0.0593(9) 0.0699(10) 0.0745(11) -0.0236(9) 0.0096(8) -0.0023(8) $C19\ 0.0555(9)\ 0.0852(13)\ 0.1106(15)\ -0.0393(12)\ 0.0121(9)\ 0.0046(9)$ C12 0.0889(12) 0.0572(9) 0.0685(10) 0.0065(8) 0.0218(9) -0.0007(8) $C24\ 0.0923(13)\ 0.0647(10)\ 0.0783(12)\ 0.0072(9)\ -0.0030(9)\ -0.0041(9)$ C6 0.0695(10) 0.0718(11) 0.0939(13) 0.0040(10) 0.0336(9) 0.0055(9) $C26\ 0.0987(14)\ 0.0504(9)\ 0.1024(15)\ -0.0017(10)\ -0.0303(12)\ 0.0151(10)$ $C20\ 0.0681(11)\ 0.0683(11)\ 0.1151(16)\ -0.0255(11)\ -0.0140(11)\ 0.0157(9)$ $C14\ 0.0762(11)\ 0.0820(12)\ 0.0823(12)\ 0.0140(10)\ -0.0005(9)\ 0.0182(10)$ $C7\ 0.1084(15)\ 0.0697(11)\ 0.0831(13)\ -0.0058(10)\ 0.0494(12)\ 0.0035(11)$ C8 0.1217(17) 0.0672(10) 0.0546(9) -0.0054(8) 0.0256(10) 0.0003(11) C13 0.1053(14) 0.0641(10) 0.0681(10) 0.0157(8) 0.0122(10) 0.0199(10) C25 0.1108(17) 0.0616(11) 0.0924(14) 0.0088(10) -0.0129(13) 0.0048(11)

_geom_special_details

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the fullCovariance matrix. TheCell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles;Correlations between esds inCell parameters are only used when they are defined byCrystal symmetry. An approximate (isotropic) treatment ofCell esds is used for estimating esds involving l.s. planes.

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loop_

_geom_bond_atom_site_label_1 _geom_bond_atom_site_label_2 _geom_bond_distance _geom_bond_site_symmetry_2 _geom_bond_publ_flag N1C2 1.3280(18) . ? N1C1 1.3412(18).? C2C3 1.4204(19) . ? C2C4 1.4854(19) . ? N2N3 1.3289(17).? N2C1 1.3378(19).? N3C3 1.3367(17).? N5C16 1.2858(19) . ? N5N4 1.3633(18) . ? N4C1 1.3568(19).? N4H2 0.9681 . ? C16C17 1.451(2) . ? C16H16 0.9300 . ? C17C18 1.390(2) . ? C17C22 1.443(2) . ? O1C18 1.355(2) . ? O1H1 1.0301 . ? C3C10 1.486(2) . ? C10C11 1.381(2) . ? C10C15 1.385(2) . ? C4C5 1.388(2).? C4C9 1.391(2).? C22C23 1.411(2) . ? C22C21 1.424(2) . ? C15C14 1.382(2) . ? C15H15 0.9300 . ? C11C12 1.382(2) . ? C11H11 0.9300 . ? C21C20 1.399(3) . ? C21C26 1.424(3) . ? C9C8 1.385(2) . ? C9H9 0.9300 . ? C23C24 1.376(2) . ? C23H23 0.9300 . ?

C5C6 1.380(2).? C5H5 0.9300 . ? C18C19 1.419(3) . ? C19C20 1.354(3) . ? C19H19 0.9300 . ? C12C13 1.372(3) . ? C12H12 0.9300 . ? C24C25 1.388(3) . ? C24H24 0.9300 . ? C6C7 1.370(3) . ? C6H6 0.9300 . ? C26C25 1.345(3) . ? C26H26 0.9300 . ? C20H20 0.9300 . ? C14C13 1.368(3) . ? C14H14 0.9300 . ? C7C8 1.375(3).? C7H7 0.9300 . ? C8H8 0.9300 . ? C13H13 0.9300 . ? C25H25 0.9300 . ?

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geom angle atom site label 1 _geom_angle_atom_site_label 2 _geom_angle_atom_site_label_3 _geom_angle _geom_angle_site_symmetry_1 _geom_angle_site_symmetry_3 _geom_angle_publ_flag C2N1C1 116.19(12) . . ? N1C2C3 120.04(12) . . ? N1C2C4 114.59(12) . . ? C3C2C4 125.33(12) . . ? N3N2C1 118.10(12) ...? N2N3C3 120.21(12) . . ? C16N5N4 118.05(13) . . ? C1N4N5 119.47(12)..? C1N4H2 114.8 . . ? N5N4H2 124.8 . . ? N5C16C17 120.44(14) . . ? N5C16H16 119.8 . . ?

C17C16H16 119.8 . . ? C18C17C22 118.78(15) . . ? C18C17C16 120.53(16) . . ? C22C17C16 120.68(14) . . ? C18 O1H1 107.7 . . ? N3C3C2 119.45(13) . . ? N3C3C10 115.01(13) . . ? C2C3C10 125.54(12) . . ? N2C1N1 125.47(13) . . ? N2C1N4 115.22(13) . . ? N1C1N4 119.27(13) . . ? C11C10C15 118.84(14) . . ? C11C10C3 121.11(13) . . ? C15C10C3 120.01(14) . . ? C5C4C9 119.38(14) . . ? C5C4C2 118.69(13) . . ? C9C4C2 121.80(14) . . ? C23C22C21 116.93(16) . . ? C23C22C17 123.64(14) . . ? C21C22C17 119.42(16) . . ? C14C15C10 120.16(16) . . ? C14C15H15 119.9 . . ? C10C15H15 119.9 . . ? C10C11C12 120.50(16) ...? C10C11H11 119.8 . . ? C12C11H11 119.8 . . ? C20C21C22 118.77(19) . . ? C20C21C26 122.02(18) . . ? C22C21C26 119.22(18) . . ? C8C9C4 119.49(17) . . ? C8C9H9 120.3 . . ? C4C9H9 120.3 . . ? C24C23C22 121.56(16) . . ? C24C23H23 119.2 . . ? C22C23H23 119.2 . . ? C6C5C4 120.32(16) . . ? C6C5H5 119.8 . . ? C4C5H5 119.8 . . ? O1C18C17 122.96(16) . . ? O1C18C19 116.43(16) . . ? C17C18C19 120.62(18) . . ? C20C19C18 120.09(18) . . ?

C20C19H19 120.0 . . ? C18C19H19 120.0 . . ? C13C12C11 120.25(17) . . ? C13C12H12 119.9 . . ? C11C12H12 119.9 . . ? C23C24C25 121.0(2) . . ? C23C24H24 119.5 . . ? C25C24H24 119.5 ...? C7C6C5 120.06(18) . . ? С7С6Н6 120.0..? С5С6Н6 120.0..? C25C26C21 121.79(18) . . ? C25C26H26 119.1 . . ? C21C26H26 119.1 . . ? C19C20C21 122.26(17) ...? C19C20H20 118.9 . . ? C21C20H20 118.9 . . ? C13C14C15 120.53(18) . . ? C13C14H14 119.7 . . ? C15C14H14 119.7 . . ?

C6C7C8 120.20(16) . . ? C6C7C8 120.20(16) . . ? C6C7H7 119.9 . . ? C8C7H7 119.9 . . ? C7C8C9 120.49(18) . . ? C7C8H8 119.8 . . ? C9C8H8 119.8 . . ? C14C13C12 119.72(16) . . ? C14C13H13 120.1 . . ? C12C13H13 120.1 . . ? C26C25C24 119.4(2) . . ? C26C25H25 120.3 . . ? C24C25H25 120.3 . . ?

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GRID
PLAN 20
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Refinement of F^2[^] against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2[^],Conventional R-factors R are based on F, with F set to zero forNegative F^2[^]. The threshold expression of $F^2^^ > 2sigma(F^2^)$ is used only forCalculating R-factors(gt) etc. and is Not relevant to theChoice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

;

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C23C 1.7857(5) 0.45639(17) 0.9618(2) 0.0864(12) Uani 1 1 d . . . H23AH 1.8724 0.4608 0.9103 0.130 Uiso 1 1Calc R . . H23BH 1.8803 0.4417 1.0114 0.130 Uiso 1 1Calc R . . H23CH 1.7234 0.4958 0.9766 0.130 Uiso 1 1Calc R . . H1H 0.646(5) 0.4783(8) 0.5642(18) 0.081(12) Uiso 1 1 d D . .

loop_

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$C23\ 0.063(2)\ 0.107(3)\ 0.086(2)\ -0.021(2)\ -0.0188(19)\ -0.002(2)$

_geom_special_details

;

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the fullCovariance matrix. TheCell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles;Correlations between esds inCell parameters are only used when they are defined byCrystal symmetry. An approximate (isotropic) treatment ofCell esds is used for estimating esds involving l.s. planes. ;

loop

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C9H9 0.9300 . ? C10C11 1.376(4) . ? C10C15 1.392(3) . ? C11C12 1.386(3) . ? C11H11 0.9300 . ? C12C13 1.385(4) . ? C12H12 0.9300 . ? C13C14 1.374(4) . ? C13H13 0.9300 . ? C14C15 1.382(3) . ? C14H14 0.9300 . ? C15H15 0.9300 . ? C16C17 1.457(3) . ? C16H16 0.9300 . ? C17C22 1.380(4).? C17C18 1.388(4) . ? C18C19 1.379(3) . ? C18H18 0.9300 . ? C19C20 1.385(4) . ? C19H19 0.9300 . ? C20C21 1.362(4) . ? C21C22 1.391(3) . ? C21H21 0.9300 . ? C22H22 0.9300 . ? C23H23A 0.9600 . ? C23H23B 0.9600 . ? C23H23C 0.9600 . ?

loop_

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loop_

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_geom_torsion_site_symmetry_4 geom torsion publ flag $C1N2N3C3 3.3(4) \dots ?$ C1N4N5C16 -179.3(3)? $C2N1C1N2 2.2(4) \dots ?$ C2N1C1N4 -177.5(3)? $N3N2C1N1 - 5.5(4) \dots ?$ N3N2C1N4 174.2(2)? $N5N4C1N1 - 3.7(4) \dots ?$ N5N4C1N2 176.5(2) ? C1N1C2C3 3.0(4)? C1N1C2C4 -177.6(3)? N2N3C3C2 1.5(4) ? N2N3C3C10 -177.0(2) ? N1C2C3N3 -4.9(4)? C4C2C3N3 175.8(3)? N1C2C3C10 173.3(3)? $C4C2C3C10 - 6.0(4) \dots$? N1C2C4C5 -58.7(3) ? C3C2C4C5 120.6(3)? N1C2C4C9 119.4(3)? $C3C2C4C9 - 61.2(4) \dots ?$ C9C4C5C6 1.7(4) ? C2C4C5C6 179.9(2)? $C4C5C6C7 - 1.9(4) \dots ?$ $C5C6C7C8 0.2(4) \dots ?$ C6C7C8C9 1.6(4) ? $C7C8C9C4 - 1.8(4) \dots ?$ C5C4C9C8 0.2(4) . . . ? C2C4C9C8 -178.0(2)? N3C3C10C11 146.2(3)? C2C3C10C11 -32.2(4) ? N3C3C10C15 - 30.7(4) ? C2C3C10C15 150.9(3) ? $C15C10C11C12 - 0.4(4) \dots ?$ C3C10C11C12 -177.3(3) ? C10C11C12C13 -0.8(5) ? C11C12C13C14 1.5(5) ? $C12C13C14C15 - 1.1(5) \dots ?$ C13C14C15C10 -0.1(4) ? C11C10C15C14 0.8(4) ? C3C10C15C14 177.9(2) ?

N4N5C16C17 177.7(2)? N5C16C17C22 -178.1(3)? N5C16C17C18 0.2(4)? C22C17C18C19 0.9(5)? C16C17C18C19 -177.4(3)? C17C18C19C20 -0.9(5)? C23 O1C20C21 -3.2(4)? C18C19C20C21 0.1(5)? C18C19C20C21 0.1(5)? C18C19C20 O1 179.5(3)? C19C20C21C22 -178.7(3)? C19C20C21C22 0.7(5)? C18C17C22C21 0.0(4)? C16C17C22C21 178.3(3)?

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loop_

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computing data collection 'CrysAlis PRO (Agilent, 2012)' _computing_cell_refinement 'CrysAlis PRO (Agilent, 2012)' _computing_data_reduction 'CrysAlis PRO (Agilent, 2012)' _computing_structure_solution 'SHELXS-97 (Sheldrick, 1990)' _computing_structure_refinement 'SHELXL-97 (Sheldrick, 1997)' ? _computing_molecular_graphics _computing_publication_material ? _iucr_refine_instructions_details TITL 14098 in P-1 CELL 0.71073 8.8933 11.1477 11.7484 91.212 106.044 108.519 ZERR 2.0000 0.0010 0.0011 0.0013 0.009 0.010 0.009 LATT 1 **SFACCHN** UNIT 48 44 12 MERG 2 FMAP 2 GRID PLAN 20 **TEMP 23** SIZE 0.17 0.26 0.32 BOND \$H HTAB CONF L.S. 20 ACTA EXTI 0.01392 WGHT 0.04620 0.35700 0.00000 0.00000 0.00000 0.33330 FVAR 6.11470 N1 3 0.23539 0.20313 0.27176 11.00000 0.03926 0.04955 = 0.03608 -0.00672 0.00955 0.01206 N2 3 -0.00809 0.04621 0.14092 11.00000 0.04349 0.05014 = 0.03287 -0.00682 0.01177 0.01020 3 -0.09474 0.05073 0.21620 11.00000 0.04139 0.04797 = N3 0.03569 -0.00442 0.01054 0.01030 3 0.39670 0.17391 0.10685 11.00000 0.04074 0.04991 = N5 0.03995 -0.00179 0.01314 0.01242 N4 3 0.23205 0.10501 0.09231 11.00000 0.04079 0.05465 = 0.03838 -0.00997 0.01361 0.00774 $C16 \quad 1 \quad 0.44741 \quad 0.15251 \quad 0.01888 \quad 11.00000 \quad 0.04600 \quad 0.04829 =$

0.03846 - 0.00230 0.01396 0.01278AFIX 43 H16 2 0.37164 0.09580 -0.04639 11.00000 -1.20000 AFIX 0 C_{2} 1 0.14505 0.21107 0.34258 11.00000 0.03809 0.04667 = 0.03442 - 0.00394 0.00779 0.01453C3 1 -0.02206 0.13014 0.31745 11.00000 0.03967 0.04331 = 0.03105 - 0.00018 0.00855 0.01431C17 1 0.61704 0.21217 0.01568 11.00000 0.04601 0.04384 = 0.03697 0.00176 0.01341 0.01382 C10 1 -0.12587 0.12870 0.39699 11.00000 0.04057 0.04051 = 0.03657 -0.00144 0.01135 0.01074 C18 1 0.66255 0.17611 - 0.08029 11.00000 0.04693 0.05321 =0.04183 -0.00938 0.01271 0.00835 AFIX 43 H18 2 0.58232 0.11706 -0.14211 11.00000 -1.20000 AFIX 0 C1 1 0.15386 0.11962 0.17231 11.00000 0.04059 0.04192 =0.03392 -0.00085 0.01035 0.01365 C22 1 0.74240 0.30237 0.10573 11.00000 0.05630 0.04677 =0.03490 0.00149 0.01558 0.01370 AFIX 43 H22 2 0.71625 0.32991 0.17072 11.00000 -1.20000 AFIX 0 N6 3 1.10876 0.36140 -0.00191 11.00000 0.04474 0.06378 =0.06240 -0.00211 0.01653 0.00591 C20 1 0.94894 0.31381 0.00399 11.00000 0.04504 0.04397 =0.04680 0.00482 0.01239 0.01191 C15 1 -0.28761 0.12828 0.34960 11.00000 0.04376 0.05221 = 0.04616 0.00501 0.01313 0.01377 AFIX 43 H15 2 -0.33189 0.12517 0.26759 11.00000 -1.20000 AFIX 0 C21 1 0.90269 0.35127 0.10086 11.00000 0.05147 0.04538 = 0.03587 - 0.00006 0.00625 0.00803AFIX 43 H21 2 0.98247 0.41040 0.16282 11.00000 -1.20000 AFIX 0 C12 1 -0.16206 0.12897 0.59179 11.00000 0.07265 0.07116 = 0.04001 0.00346 0.02346 0.02361 AFIX 43 H12 2 -0.12095 0.12682 0.67333 11.00000 -1.20000

AFIX 0 C19 1 0.82241 0.22493 -0.08681 11.00000 0.05053 0.05627 = 0.04823 - 0.00880 0.02124 0.00968AFIX 43 H19 2 0.84716 0.19842 -0.15291 11.00000 -1.20000 AFIX 0 C11 1 -0.06461 0.12784 0.51938 11.00000 0.05270 0.06139 = 0.03865 0.00041 0.01337 0.02169 AFIX 43 H11 2 0.04264 0.12651 0.55231 11.00000 -1.20000 AFIX 0 C4 1 0.22613 0.31234 0.44614 11.00000 0.03678 0.06339 = 0.04295 -0.01709 0.01104 0.00797 $C14 \quad 1 \quad -0.38289 \quad 0.13246 \quad 0.42355 \quad 11.00000 \quad 0.04919 \quad 0.07764 =$ 0.07051 0.01040 0.02504 0.02592 AFIX 43 H14 2 -0.48985 0.13476 0.39158 11.00000 -1.20000 AFIX 0 $C7 \quad 1 \quad 0.38028 \quad 0.50445 \quad 0.63536 \quad 11.00000 \quad 0.06037 \quad 0.12292 =$ 0.09155 -0.07040 0.01549 0.00185 AFIX 43 H7 2 0.43290 0.56910 0.69886 11.00000 -1.20000 AFIX 0 C9 1 0.16233 0.40864 0.45611 11.00000 0.05965 0.05914 = 0.06400 - 0.01718 0.01526 0.01395AFIX 43 H9 2 0.06610 0.40881 0.39914 11.00000 -1.20000 AFIX 0 C23 1 1.14903 0.32988 -0.10714 11.00000 0.05250 0.08042 = 0.08300 0.00093 0.03139 0.01305 AFIX 137 H23A 2 1.12849 0.23988 -0.11804 11.00000 -1.50000 H23B 2 1.26410 0.37522 -0.09776 11.00000 -1.50000 H23C 2 1.08127 0.35360 -0.17555 11.00000 -1.50000 AFIX 0 C13 1 -0.31943 0.13322 0.54484 11.00000 0.07096 0.08269 = 0.06612 0.00793 0.04227 0.02843 AFIX 43 H13 2 -0.38326 0.13662 0.59478 11.00000 -1.20000 AFIX 0 C24 1 1.24198 0.44671 0.09504 11.00000 0.04708 0.06166 = 0.06690 0.00930 0.00395 0.00483

AFIX 137 H24A 2 1.21987 0.52442 0.10560 11.00000 -1.50000 H24B 2 1.34510 0.46525 0.07664 11.00000 -1.50000 H24C 2 1.24925 0.40699 0.16715 11.00000 -1.50000 AFIX 0 C8 1 0.24118 0.50521 0.55081 11.00000 0.07780 0.06850 = $0.09326 - 0.03264 \quad 0.03254 \quad 0.00996$ AFIX 43 H8 2 0.19867 0.57058 0.55637 11.00000 -1.20000 AFIX 0 C6 1 0.44222 0.40916 0.62694 11.00000 0.06213 0.17406 = 0.08734 - 0.07994 - 0.01848 0.04084AFIX 43 H6 2 0.53654 0.40824 0.68561 11.00000 -1.20000 AFIX 0 C5 1 0.36685 0.31337 0.53218 11.00000 0.05765 0.13011 = 0.07237 -0.05112 -0.01061 0.04415 AFIX 43 H5 2 0.41176 0.24941 0.52679 11.00000 -1.20000 H1 2 0.15930 0.04591 0.02181 11.00000 0.06325 HKLF 4

_refine_special_details

Refinement of F^2^ against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2^,Conventional R-factors R are based on F, with F set to zero forNegative F^2^. The threshold expression of $F^2^2 > 2sigma(F^2^2)$ is used only forCalculating R-factors(gt) etc. and is Not relevant to theChoice of reflections for refinement. R-factors based on F^2^ are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

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refine ls extinction method SHELXL refine ls extinction coef 0.014(3)refine ls extinction expression $Fc^*=kFc[1+0.001xFc^2^1/3^/sin(2)]^{-1/4'}$ _refine_ls_number reflns 5004 refine ls number parameters 275 refine ls number restraints 0 refine ls R factor all 0.0836 refine ls R factor gt 0.0538 refine ls wR factor ref 0.1422 refine ls wR factor gt 0.1218 refine ls goodness of fit ref 1.035 refine ls restrained S all 1.035 _refine_ls_shift/su_max 0.000 refine ls shift/su mean 0.000 loop atom site label atom_site_type_symbol atom site fract x atom site fract y atom site fract z _atom_site_U_iso_or_equiv atom site adp type _atom_site_occupancy atom site symetry multiplicity atom site calc flag atom site refinement flags atom site disorder assembly _atom_site_disorder group N1N 0.23539(17) 0.20313(14) 0.27176(12) 0.0429(4) Uani 1 1 d ... N2N -0.00808(18) 0.04621(14) 0.14092(12) 0.0436(4) Uani 1 1 d ... N3N -0.09474(17) 0.05074(14) 0.21620(12) 0.0432(4) Uani 1 1 d ... N5N 0.39670(18) 0.17391(14) 0.10685(13) 0.0441(4) Uani 1 1 d ... N4N 0.23205(18) 0.10501(15) 0.09231(13) 0.0465(4) Uani 1 1 d ... C16C 0.4474(2) 0.15251(17) 0.01887(16) 0.0448(4) Uani 1 1 d ... H16H 0.3716 0.0958 -0.0464 0.054 Uiso 1 1Calc R ... C2C 0.1450(2) 0.21106(17) 0.34257(15) 0.0404(4) Uani 1 1 d ... C3C -0.0221(2) 0.13015(16) 0.31745(14) 0.0384(4) Uani 1 1 d ... C17C 0.6170(2) 0.21217(17) 0.01568(15) 0.0424(4) Uani 1 1 d ... C10C -0.1259(2) 0.12870(16) 0.39699(15) 0.0401(4) Uani 1 1 d ... C18C 0.6626(2) 0.17612(18) -0.08029(17) 0.0498(5) Uani 1 1 d ...

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the fullCovariance matrix. TheCell esds are taken

into account individually in the estimation of esds in distances, angles and torsion angles;Correlations between esds inCell parameters are only used when they are defined byCrystal symmetry. An approximate (isotropic) treatment ofCell esds is used for estimating esds involving l.s. planes. ;

loop_

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C12C11H11 119.9 . . ? C10C11H11 119.9 . . ? C5C4C9 118.71(18) . . ? C5C4C2 120.87(18) . . ? C9C4C2 120.41(18) . . ? C13C14C15 120.0(2)..? C13C14H14 120.0 . . ? C15C14H14 120.0 . . ? C6C7C8 119.8(2) . . ? C6C7H7 120.1 . . ? C8C7H7 120.1 . . ? C4C9C8 120.3(2) . . ? C4C9H9 119.9 . . ? C8C9H9 119.9 . . ? N6C23H23A 109.5 . . ? N6C23H23B 109.5 . . ? H23AC23H23B 109.5 ...? N6C23H23C 109.5 . . ? H23AC23H23C 109.5..? H23BC23H23C 109.5 ...? C12C13C14 119.96(19) . . ? C12C13H13 120.0 . . ? C14C13H13 120.0 . . ? N6C24H24A 109.5 . . ? N6C24H24B 109.5 ...? H24AC24H24B 109.5 . . ? N6C24H24C 109.5 . . ? H24AC24H24C 109.5 . . ? H24BC24H24C 109.5 . . ? C7C8C9 120.1(2) . . ? C7C8H8 119.9 . . ? C9C8H8 119.9 . . ? C7C6C5 120.8(3) . . ? С7С6Н6 119.6..? С5С6Н6 119.6..? C4C5C6 120.2(2) . . ? C4C5H5 119.9 . . ? C6C5H5 119.9 . . ?

loop_

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Molecule 4Cif

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chemical name common
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CrysAlisPro, Agilent Technologies,

Version 1.171.36.20 (release 27-06-2012CrysAlis171 .NET)

(compiled Jul 11 2012,15:38:31)

Empirical absorptionCorrection using sphericalHarmonics,

implemented in SCALE3 ABSPACK scaling algorithm.

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_iucr_refine_instructions details TITL 14097 in P2(1)/c CELL 0.71073 5.9756 21.5731 14.9805 90.000 93.447 90.000 ZERR 4.0000 0.0018 0.0056 0.0040 0.000 0.022 0.000 LATT 1 SYMM -X, 0.5+Y, 0.5-Z SFACCHN O UNIT 92 76 20 4 MERG 2 FMAP 2 GRID PLAN 20 **TEMP 23** SIZE 0.05 0.08 0.48 BOND \$H HTAB CONF

L.S. 20

ACTA 52

WGHT 0.02180 0.00000 0.00000 0.00000 0.00000 0.33330

FVAR 1.69020

- O1 4 1.60874 0.41310 0.94281 11.00000 0.07147 0.08726 = 0.08046 0.00578 -0.02662 -0.00019
- N1 3 0.40402 0.35009 0.58890 11.00000 0.04992 0.04967 = 0.05303 0.00216 -0.00043 -0.00648
- N2 3 0.30440 0.43955 0.50047 11.00000 0.05052 0.04896 = $0.06466 \ 0.00143 \ -0.00525 \ -0.00137$
- N3 3 0.12818 0.40936 0.46126 11.00000 0.04805 0.05515 = 0.05971 0.00165 -0.00407 0.00092
- N4 3 0.62325 0.44122 0.58888 11.00000 0.05869 0.05261 = 0.06208 0.00461 -0.01612 -0.00987

AFIX 43

 $H4 \quad 2 \quad 0.64324 \quad 0.47722 \quad 0.56601 \quad 11.00000 \quad -1.20000$

AFIX 0

- N5 3 0.77881 0.41939 0.65359 11.00000 0.05624 0.05530 = 0.05242 -0.00253 -0.00885 0.00159
- C1 1 0.43856 0.40747 0.56000 11.00000 0.04820 0.05064 = 0.04908 0.00425 0.00275 0.00286
- C2 1 0.22268 0.32186 0.55276 11.00000 0.04271 0.04990 = 0.04181 0.00298 0.00426 0.00114
- C3 1 0.08431 0.35113 0.48454 11.00000 0.04319 0.04251 = 0.04982 0.00051 0.00565 0.00340
- C4 1 0.17969 0.25920 0.58764 11.00000 0.04459 0.04857 = 0.04099 0.00430 -0.00508 -0.00432
- C5 1 0.33970 0.21325 0.58139 11.00000 0.04747 0.05908 = 0.05816 0.00481 -0.00035 -0.00207

AFIX 43

```
H5 2 0.47327 0.22209 0.55521 11.00000 -1.20000
```

AFIX 0

C6 1 0.30303 0.15481 0.61346 11.00000 0.06740 0.05151 = 0.07096 0.00513 -0.00564 0.00425

AFIX 43

H6 2 0.40982 0.12399 0.60725 11.00000 -1.20000

AFIX 0

C7 1 0.10916 0.14150 0.65477 11.00000 0.08041 0.05691 = 0.06422 0.01512 -0.00507 -0.01296

AFIX 43

H7 2 0.08485 0.10188 0.67668 11.00000 -1.20000

AFIX 0

C8 1 -0.04866 0.18733 0.66341 11.00000 0.06669 0.07522 = 0.06261 0.01322 0.00984 -0.01721 AFIX 43 H8 2 -0.17815 0.17881 0.69264 11.00000 -1.20000 AFIX 0 C9 1 -0.01625 0.24557 0.62917 11.00000 0.05326 0.06124 = 0.06158 0.00459 0.00509 -0.00351 AFIX 43 H9 2 -0.12560 0.27588 0.63380 11.00000 -1.20000 AFIX 0 C10 1 -0.10908 0.32283 0.43189 11.00000 0.04671 0.05251 = 0.04420 0.00027 0.00045 0.00023 C11 1 -0.12049 0.26099 0.40957 11.00000 0.05002 0.06235 = 0.05891 0.00293 -0.00613 -0.00107 AFIX 43 H11 2 -0.00533 0.23465 0.43001 11.00000 -1.20000 AFIX 0 C12 1 -0.29937 0.23697 0.35738 11.00000 0.06126 0.06120 = 0.07264 - 0.00545 - 0.00166 - 0.00994AFIX 43 H12 2 -0.30288 0.19512 0.34249 11.00000 -1.20000 AFIX 0 C13 1 -0.47277 0.27576 0.32758 11.00000 0.05370 0.08541 = 0.05614 0.00288 -0.00703 -0.01153 AFIX 43 H13 2 -0.59508 0.25983 0.29373 11.00000 -1.20000 AFIX 0 C14 1 -0.46381 0.33783 0.34811 11.00000 0.05198 0.07977 = 0.05177 0.00622 -0.00326 0.00377 AFIX 43 H14 2 -0.57878 0.36412 0.32732 11.00000 -1.20000 AFIX 0 C15 1 -0.28347 0.36109 0.39974 11.00000 0.05158 0.06109 = 0.04589 0.00039 0.00136 0.00749 AFIX 43 H15 2 -0.27852 0.40316 0.41328 11.00000 -1.20000 AFIX 0 C16 1 0.93780 0.45812 0.67206 11.00000 0.05638 0.05521 =0.05547 - 0.00234 - 0.00732 - 0.00541AFIX 43 H16 2 0.94002 0.49535 0.64084 11.00000 -1.20000 AFIX 0

C17 1 1.11498 0.44529 0.74065 11.00000 0.05349 0.04754 = 0.04661 -0.00213 -0.00032 -0.00167 C18 1 1.12508 0.39093 0.79028 11.00000 0.05679 0.05639 = 0.06396 -0.00294 -0.00697 -0.00507 AFIX 43 H18 2 1.01849 0.36013 0.77846 11.00000 -1.20000 AFIX 0 C19 1 1.29145 0.38206 0.85696 11.00000 0.06806 0.05696 = 0.06783 0.00846 -0.00691 -0.00011 AFIX 43 H19 2 1.29513 0.34567 0.89031 11.00000 -1.20000 AFIX 0 C20 1 1.45299 0.42720 0.87435 11.00000 0.05667 0.06206 = 0.05572 -0.00543 -0.01090 0.00618 C21 1 1.44882 0.48071 0.82603 11.00000 0.06194 0.05952 = 0.06587 - 0.00923 - 0.01070 - 0.00939AFIX 43 H21 2 1.55791 0.51094 0.83713 11.00000 -1.20000 AFIX 0 C22 1 1.27842 0.48933 0.75977 11.00000 0.06931 0.04814 = 0.06232 0.00361 - 0.00772 - 0.00766AFIX 43 H22 2 1.27448 0.52606 0.72722 11.00000 -1.20000 AFIX 0 C23 1 1.78566 0.45639 0.96182 11.00000 0.06311 0.10751 = 0.08569 - 0.02149 - 0.01883 - 0.00220**AFIX 137** H23A 2 1.87234 0.46079 0.91027 11.00000 -1.50000 H23B 2 1.88034 0.44169 1.01138 11.00000 -1.50000 H23C 2 1.72336 0.49584 0.97659 11.00000 -1.50000 HKLF 4

_refine_special_details

;

Refinement of F^2^ against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2^,Conventional R-factors R are based on F, with F set to zero forNegative F^2^. The threshold expression of $F^2^2 > 2sigma(F^2^2)$ is used only forCalculating R-factors(gt) etc. and is Not relevant to theChoice of reflections for refinement. R-factors based on F^2^ are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

```
refine ls structure factor coef Fsqd
                             full
refine ls matrix type
refine ls weighting scheme
                                Calc
refine ls weighting details
'calc w=1/[s^2(Fo^2)+(0.0576P)<sup>2</sup>+0.0000P] where P=(Fo<sup>2</sup>+2Fc<sup>2</sup>)/3'
atom sites solution primary
                                direct
atom sites solution secondary
                                 difmap
atom sites solution hydrogens
                                 geom
refine ls hydrogen treatment
                                mixed
refine ls extinction method
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                              ?
refine ls extinction coef
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refine ls goodness of fit ref 0.955
refine ls restrained S all
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refine ls shift/su max
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refine ls shift/su mean
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atom site fract z
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_atom_site_adp_type
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_atom_site_calc_flag
_atom_site_refinement_flags
atom site disorder assembly
 atom site disorder group
N1N 0.24100(16) 0.9759(3) 0.02249(10) 0.0594(6) Uani 1 1 d . . .
N3N 0.14906(16) 1.2823(4) 0.07838(11) 0.0631(6) Uani 1 1 d ...
C2C 0.28801(18) 1.1305(4) 0.06162(11) 0.0519(7) Uani 1 1 d ...
N2N 0.10195(16) 1.1322(4) 0.03740(11) 0.0656(6) Uani 1 1 d ...
```

C3C 0.24111(18) 1.2833(4) 0.09301(12) 0.0524(7) Uani 1 1 d . . . N5N 0.13020(17) 0.6597(4) -0.05376(11) 0.0660(6) Uani 1 1 d . . . C1C 0.1496(2) 0.9805(5) 0.01395(13) 0.0592(7) Uani 1 1 d . . . C4C 0.38883(19) 1.1287(4) 0.06992(11) 0.0527(7) Uani 1 1 d . . . N4N 0.09520(19) 0.8212(4) -0.02047(12) 0.0741(7) Uani 1 1 d . . . C15C 0.2389(2) 1.6421(4) 0.14746(13) 0.0616(7) Uani 1 1 d ... H15H 0.1844 1.6726 0.1166 0.074 Uiso 1 1Calc R ... C10C 0.28417(18) 1.4457(4) 0.14384(12) 0.0505(6) Uani 1 1 d ... C9C 0.4370(2) 1.3147(4) 0.06129(13) 0.0619(7) Uani 1 1 d . . . H9H 0.4059 1.4465 0.0512 0.074 Uiso 1 1Calc R ... C16C 0.0711(2) 0.5232(4) -0.08416(13) 0.0645(8) Uani 1 1 d ... H16H 0.0104 0.5364 -0.0812 0.077 Uiso 1 1Calc R ... C11C 0.36520(19) 1.4045(5) 0.19072(12) 0.0624(8) Uani 1 1 d ... H11H 0.3964 1.2737 0.1896 0.075 Uiso 1 1Calc R ... C17C 0.0950(2) 0.3477(4) -0.12331(13) 0.0605(7) Uani 1 1 d ... C22C 0.0277(2) 0.1973(5) -0.15222(14) 0.0733(9) Uani 1 1 d . . . H22H -0.0308 0.2092 -0.1448 0.088 Uiso 1 1Calc R ... C7C 0.5771(2) 1.1122(6) 0.08330(14) 0.0748(9) Uani 1 1 d . . . H7H 0.6403 1.1065 0.0874 0.090 Uiso 1 1Calc R . . C14C 0.2736(2) 1.7923(5) 0.19612(15) 0.0711(9) Uani 1 1 d ... H14H 0.2425 1.9226 0.1980 0.085 Uiso 1 1Calc R ... C12C 0.3999(2) 1.5565(6) 0.23906(13) 0.0764(9) Uani 1 1 d . . . H12H 0.4546 1.5282 0.2699 0.092 Uiso 1 1Calc R . . O1 O 0.25154(16) 0.4654(4) -0.10809(15) 0.1261(10) Uani 1 1 d ... H1H 0.2336 0.5543 -0.0848 0.151 Uiso 1 1Calc R ... C5C 0.4365(2) 0.9344(5) 0.08544(13) 0.0644(8) Uani 1 1 d . . . H5H 0.4049 0.8076 0.0909 0.077 Uiso 1 1Calc R . . C8C 0.5308(2) 1.3060(6) 0.06764(14) 0.0721(9) Uani 1 1 d . . . H8H 0.5627 1.4313 0.0613 0.086 Uiso 1 1Calc R ... C13C 0.3538(3) 1.7491(6) 0.24151(15) 0.0804(10) Uani 1 1 d ... H13H 0.3772 1.8506 0.2742 0.096 Uiso 1 1Calc R . . C18C 0.1816(2) 0.3283(6) -0.13547(17) 0.0848(10) Uani 1 1 d . . . C6C 0.5308(2) 0.9282(5) 0.09282(14) 0.0731(8) Uani 1 1 d . . . H6H 0.5627 0.7981 0.1043 0.088 Uiso 1 1Calc R ... C21C 0.0456(3) 0.0312(5) -0.19158(17) 0.0931(11) Uani 1 1 d . . . H21H 0.0001 -0.0690 -0.2102 0.112 Uiso 1 1Calc R ... C19C 0.1992(3) 0.1626(7) -0.1761(2) 0.1140(13) Uani 1 1 d ... H19H 0.2568 0.1512 -0.1850 0.137 Uiso 1 1Calc R ... C20C 0.1315(3) 0.0167(7) -0.20273(19) 0.1083(13) Uani 1 1 d . . . H20H 0.1442 -0.0952 -0.2291 0.130 Uiso 1 1Calc R ... H10H 0.019(3) 0.810(5) -0.0309(15) 0.107(11) Uiso 1 1 d . . .

loop_

atom site aniso label _atom_site_aniso_U_11 _atom_site_aniso_U_22 _atom_site_aniso_U_33 atom site aniso U 23 _atom_site_aniso_U_13 atom site aniso U 12 N1 0.0526(16) 0.0672(14) 0.0538(13) -0.0064(11) 0.0040(11) -0.0122(13) N3 0.0500(16) 0.0739(15) 0.0629(14) -0.0089(12) 0.0088(12) -0.0101(13) C2 0.0500(18) 0.0617(16) 0.0418(13) 0.0004(13) 0.0069(13) -0.0089(14) N2 0.0454(15) 0.0769(16) 0.0698(15) -0.0158(14) 0.0047(12) -0.0136(13) $C3\ 0.0393(17)\ 0.0662(17)\ 0.0489(15)\ -0.0003(13)\ 0.0054(12)\ -0.0095(14)$ N5 0.0576(16) 0.0661(14) 0.0672(15) -0.0087(13) 0.0016(13) -0.0039(13) $C1\ 0.0496(19)\ 0.0700(19)\ 0.0517(15)\ -0.0033(14)\ 0.0003(14)\ -0.0093(17)$ C4 0.0485(18) 0.0649(17) 0.0447(14) -0.0089(13) 0.0110(12) -0.0094(15) N4 0.0562(18) 0.0772(16) 0.0805(17) -0.0267(14) 0.0001(14) -0.0171(15) $C15\ 0.0598(19)\ 0.0673(18)\ 0.0581(17)\ -0.0003(15)\ 0.0147(15)\ -0.0107(16)$ $C10\ 0.0487(17)\ 0.0616(16)\ 0.0431(14)\ -0.0012(13)\ 0.0147(13)\ -0.0106(15)$ C9 0.059(2) 0.0693(18) 0.0593(16) -0.0039(14) 0.0190(15) -0.0092(16) $C16\ 0.0554(19)\ 0.0680(18)\ 0.0627(17)\ -0.0115(15)\ 0.0000(15)\ -0.0068(16)$ $C11\ 0.0519(18)\ 0.087(2)\ 0.0456(15)\ -0.0058(15)\ 0.0072(13)\ -0.0060(16)$ $C17\ 0.0529(19)\ 0.0639(17)\ 0.0611(17)\ -0.0006(15)\ 0.0069(14)\ 0.0039(15)$ C22 0.070(2) 0.0732(19) 0.0729(19) -0.0166(17) 0.0089(17) -0.0055(18) $C7\ 0.055(2)\ 0.106(3)\ 0.0648(19)\ -0.0170(19)\ 0.0160(16)\ -0.005(2)$ $C14\ 0.082(3)\ 0.0650(19)\ 0.071(2)\ -0.0086(17)\ 0.029(2)\ -0.0128(18)$ $C12\ 0.066(2)\ 0.105(2)\ 0.0530(18)\ -0.0089(18)\ 0.0038(15)\ -0.017(2)$ O1 0.0523(16) 0.144(2) 0.179(3) -0.044(2) 0.0222(16) -0.0111(16) C5 0.059(2) 0.0665(19) 0.0653(18) -0.0097(15) 0.0098(15) -0.0061(16) C8 0.061(2) 0.090(2) 0.070(2) -0.0072(17) 0.0259(16) -0.0183(19) $C13\ 0.098(3)\ 0.088(2)\ 0.0569(19)\ -0.0215(18)\ 0.022(2)\ -0.030(2)$ $C18\ 0.054(2)\ 0.096(2)\ 0.097(2)\ -0.010(2)\ 0.0039(19)\ 0.007(2)$ $C6\ 0.060(2)\ 0.083(2)\ 0.074(2)\ -0.0125(17)\ 0.0105(16)\ 0.0058(18)$ $C21\ 0.098(3)\ 0.081(2)\ 0.096(3)\ -0.027(2)\ 0.015(2)\ 0.004(2)$ $C19\ 0.080(3)\ 0.130(3)\ 0.133(3)\ -0.028(3)\ 0.028(3)\ 0.027(3)$ $C20\ 0.103(4)\ 0.111(3)\ 0.107(3)\ -0.029(2)\ 0.018(3)\ 0.031(3)$

_geom_special_details

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the fullCovariance matrix. TheCell esds are taken into account individually in the estimation of esds in distances, angles

and torsion angles;Correlations between esds inCell parameters are only used when they are defined byCrystal symmetry. An approximate (isotropic) treatment ofCell esds is used for estimating esds involving l.s. planes.

loop_

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C12C13 1.374(4) . ? C12H12 0.9300 . ? O1C18 1.357(4) . ? O1H1 0.8200 . ? C5C6 1.384(4).? C5H5 0.9300 . ? C8H8 0.9300 . ? C13H13 0.9300 . ? C18C19 1.392(5).? C6H6 0.9300 . ? C21C20 1.365(5) . ? C21H21 0.9300 . ? C19C20 1.366(5).? C19H19 0.9300 . ? C20H20 0.9300 . ? loop_ _geom_angle_atom_site_label_1 _geom_angle_atom_site_label_2 _geom_angle_atom_site_label_3 _geom_angle geom angle site symmetry 1 _geom_angle_site_symmetry_3 _geom_angle_publ_flag C1N1C2 115.9(2) . . ? N2N3C3 120.3(2) . . ? N1C2C3 120.3(2) . . ? N1C2C4 116.0(2) . . ? C3C2C4 123.7(2) . . ? C1N2N3 118.0(2)...? N3C3C2 119.1(2) . . ? N3C3C10 114.3(2) . . ? C2C3C10 126.5(2) . . ? C16N5N4 114.9(2) . . ? N1C1N2 125.9(3) . . ? N1C1N4 121.2(3) . . ? N2C1N4 112.9(3) . . ? C9C4C5 118.9(3) . . ? C9C4C2 121.9(3) . . ?

C14C13 1.367(4) . ? C14H14 0.9300 . ?

C5C4C2 119.2(2) . . ?

C1N4N5 121.9(3) . . ? C1N4H10 127.2(16) . . ? N5N4H10 110.5(16) . . ? C14C15C10 121.0(3) . . ? C14C15H15 119.5 . . ? C10C15H15 119.5 . . ? C11C10C15 118.1(2) . . ? C11C10C3 122.8(2) . . ? C15C10C3 119.0(2) . . ? C8C9C4 120.4(3) . . ? C8C9H9 119.8 . . ? C4C9H9 119.8 . . ? N5C16C17 122.4(3) . . ? N5C16H16 118.8 . . ? C17C16H16 118.8 . . ? C12C11C10 120.5(3) . . ? C12C11H11 119.7..? C10C11H11 119.7 . . ? C18C17C22 118.3(3) . . ? C18C17C16 122.6(3) . . ? C22C17C16 119.1(3) . . ? C21C22C17 121.7(3) . . ? C21C22H22 119.2 . . ? C17C22H22 119.2 . . ? C6C7C8 120.3(3) . . ? C6C7H7 119.8 . . ? C8C7H7 119.8 . . ? C13C14C15 119.9(3) . . ? C13C14H14 120.0 . . ? C15C14H14 120.0 . . ? C13C12C11 120.1(3) . . ? C13C12H12 119.9 . . ? C11C12H12 119.9 . . ? C18 O1H1 109.5 . . ? C6C5C4 120.2(3) . . ? C6C5H5 119.9 . . ? C4C5H5 119.9 . . ? C7C8C9 120.0(3) . . ? C7C8H8 120.0 . . ? C9C8H8 120.0 . . ? C14C13C12 120.3(3) . . ? C14C13H13 119.9 . . ?

C12C13H13 119.9 . . ? O1C18C17 121.9(3) . . ? O1C18C19 118.0(3) . . ? C17C18C19 120.0(3) . . ? C7C6C5 120.2(3) . . ? С7С6Н6 119.9..? С5С6Н6 119.9..? C20C21C22 118.7(4) . . ? C20C21H21 120.7 . . ? C22C21H21 120.7 . . ? C20C19C18 119.8(4) . . ? C20C19H19 120.1 . . ? C18C19H19 120.1 . . ? C21C20C19 121.6(4) . . ? C21C20H20 119.2 . . ? C19C20H20 119.2 . . ?

loop_

_geom_torsion_atom_site label 1 geom torsion atom site label 2 geom torsion atom site label 3 _geom_torsion_atom_site_label 4 _geom_torsion geom torsion site symmetry 1 _geom_torsion_site_symmetry_2 geom torsion site symmetry 3 geom torsion site symmetry 4 geom torsion publ flag C1N1C2C3 1.9(3) ? C1N1C2C4 - 178.7(2) ? C3N3N2C1 2.5(3) . . . ? N2N3C3C2 3.5(3) ? N2N3C3C10 -174.5(2)? N1C2C3N3 -5.8(3)? C4C2C3N3 174.8(2)? N1C2C3C10 171.9(2) ? $C4C2C3C10 - 7.4(4) \dots ?$ C2N1C1N2 4.5(4) . . . ? C2N1C1N4 -174.6(2) ? N3N2C1N1 -6.9(4)? N3N2C1N4 172.3(2)? N1C2C4C9 129.3(2)?

 $C3C2C4C9 - 51.3(3) \dots ?$ N1C2C4C5 - 49.3(3) ? C3C2C4C5 130.1(3)? N1C1N4N5 -6.6(4)? N2C1N4N5 174.1(2)? C16N5N4C1 -179.4(2)? C14C15C10C11 0.2(4) ? C14C15C10C3 176.3(2)? N3C3C10C11 143.3(2) ? C2C3C10C11 - 34.6(4) ? N3C3C10C15 -32.6(3)? C2C3C10C15 149.5(2) ? C5C4C9C8 0.4(4) ? $C2C4C9C8 - 178.2(2) \dots ?$ N4N5C16C17 178.0(2)? $C15C10C11C12 - 0.7(4) \dots ?$ C3C10C11C12 -176.6(2) ? N5C16C17C18 -6.3(4) ? N5C16C17C22 176.5(3)? C18C17C22C21 0.6(4) ? C16C17C22C21 178.0(3) . . . ? C10C15C14C13 0.2(4) ? C10C11C12C13 0.7(4) ? C9C4C5C6 0.7(4) . . . ? C2C4C5C6 179.3(2)? C6C7C8C9 -0.2(4) ? $C4C9C8C7 - 0.7(4) \dots ?$ C15C14C13C12 -0.2(4)? C11C12C13C14 -0.2(4) ? C22C17C18 O1 -178.6(3) ? C16C17C18 O1 4.1(5)? C22C17C18C19 0.5(5) ? C16C17C18C19 - 176.8(3) ? C8C7C6C5 1.3(4) ? $C4C5C6C7 - 1.6(4) \dots ?$ $C17C22C21C20 - 0.7(5) \dots ?$ O1C18C19C20 177.7(4) ? C17C18C19C20 -1.4(6) ? C22C21C20C19 -0.2(6) ? C18C19C20C21 1.2(6) ?

_diffrn_reflns_theta_full 26.00 _diffrn_measured_fraction_theta_full 0.999 _refine_diff_density_max 0.129 _refine_diff_density_min -0.161 _refine_diff_density_rms 0.035