

## SUPPLEMENTARY INFORMATION

# The effect of alloying with scandium in Al-containing High-Entropy Alloys

Sephira Riva <sup>1</sup>, Shahin Mehraban <sup>1</sup>, Nicholas P. Lavery <sup>1</sup>, Stefan Schwarzmüller <sup>2</sup>, Oliver Oeckler <sup>2</sup>, Stephen G. R. Brown <sup>1</sup>, and Kirill V. Yusenko <sup>1,3,\*</sup>

<sup>1</sup> College of Engineering, Swansea University, Swansea SA1 8EN, Wales, UK

<sup>2</sup> Leipzig University, Faculty of Chemistry and Mineralogy; Institute for Mineralogy, Crystallography and Materials Science; Scharnhorststr. 20, 04275 Leipzig, Germany

<sup>3</sup> Institute of Solid State Chemistry, Pervomaiskaia str. 91, 620990 Ekaterinburg, Russia

**Table S1.** Rationale of the alloys presented in this work, with the corresponding characterization. The acronyms RT, HT and LT refer to synchrotron experiments performed at room temperature, high-temperature and low-temperature respectively. The notation Thermoelectric properties includes the measurement of Seebeck coefficient, electrical conductivity and thermal diffusivity.

Alloy	Form	Performed analysis
Al <sub>2</sub> CoCrFeNi	As cast pellet	SEM-EDX, Density, Vickers hardness, DSC, Disc punch test
	Annealed pellet (850 °C, 12h)	SEM-EDX, RT PXRD
	Powder from as-cast pellet	RT PXRD, HT PXRD, LT PXRD
Al <sub>2</sub> CoCrFeNi + 0.3wt.% Sc	As-cast pellet	SEM-EDX, RT PXRD, Thermoelectric properties
Al <sub>2</sub> CoCrFeNi + 0.5wt.% Sc	As-cast pellet	SEM-EDX, RT PXRD, Disc punch test
Al <sub>2</sub> CoCrFeNi + 2wt.% Sc	As-cast pellet	SEM-EDX, RT PXRD, Disc punch test
Al <sub>2</sub> CoCrFeNi + 3wt.% Sc	As-cast pellet	SEM-EDX, Density, RT PXRD, Vickers hardness, DSC
	Annealed pellet (900 °C, 12h)	SEM-EDX, RT PXRD
	Powder from as-cast pellet	RT PXRD, HT PXRD, LT PXRD
Al <sub>2</sub> CoCrFeNi + 5wt.% Sc	As-cast pellet	SEM-EDX, RT PXRD, Thermoelectric properties
Al <sub>0.5</sub> CoCrCuFeNi	As-cast pellet	SEM-EDX, Vickers hardness, DSC
	Annealed pellet (850 °C, 12h)	SEM-EDX
	Powder from as-cast pellet	RT PXRD, HT PXRD
Al <sub>0.5</sub> CoCrCuFeNi + 0.5wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness
Al <sub>0.5</sub> CoCrCuFeNi + 2wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness
Al <sub>0.5</sub> CoCrCuFeNi + 3wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness, DSC
	Annealed pellet (930 °C, 6h)	SEM-EDX
	Powder from as-cast pellet	RT PXRD, HT PXRD
AlCoCrCu <sub>0.5</sub> FeNi	As-cast pellet	SEM-EDX, Vickers hardness, DSC, Disc punch test
	Annealed pellet (850 °C, 12h)	SEM-EDX
	Powder from as-cast pellet	RT PXRD
AlCoCrCu <sub>0.5</sub> FeNi + 0.5wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness
AlCoCrCu <sub>0.5</sub> FeNi + 2wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness

AlCoCrCu <sub>0.5</sub> FeNi + 3wt.% Sc	As-cast pellet	SEM-EDX, Vickers hardness, DSC, Disc punch test
	Annealed pellet (930 °C, 6h)	SEM-EDX
	Powder from as-cast pellet	RT PXRD

### Atomic composition and element distribution according to EDX maps.

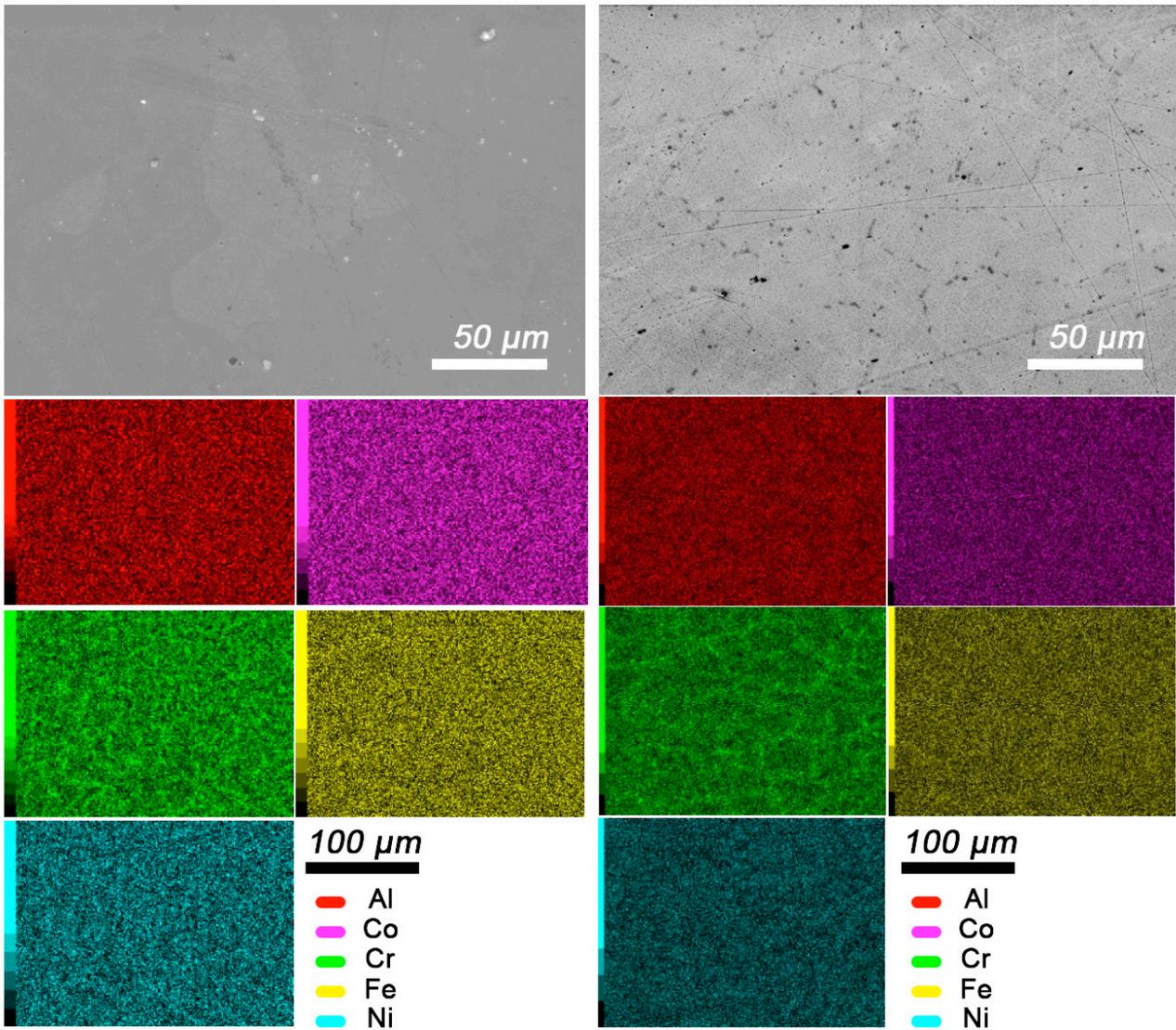
**Table S2.** Atomic composition of the synthesized samples according to EDX map (x500, x2000).

	Al <sub>2</sub> CoCrFeNi at.%		Al <sub>2</sub> CoCrFeNi + 3wt.% Sc		Al <sub>0.5</sub> CoCrCuFeNi at.%		Al <sub>0.5</sub> CoCrCuFeNi + 3wt.% Sc		AlCoCrCu <sub>0.5</sub> FeNi at.%		AlCoCrCu <sub>0.5</sub> FeNi + 3wt.% Sc	
	As melted (±0.04)	Anneal. (±0.04)	Grain at. % (±0.05)	Inter- grain at. % (±0.03)	As melted (±0.03)	Anneal. (±0.04)	Grain at. % (±0.04)	Inter- grain at. % (±0.04)	As melted (±0.03)	Anneal. (±0.04)	Grain at. % (±0.05)	Inter- grain at. % (±0.04)
Al	44.4(3)	39.5(1)	29.2(6)	18.4(2)	13.2(2)	6.6(3)	7.2(6)	2.8(5)	22.8(2)	27.5(7)	10.7(1)	8.8(3)
Co	14.7(2)	15.7(7)	19.6(4)	16.2(8)	17.9(4)	19.8(3)	20.4(0)	3.2(3)	17.2(5)	16.8(0)	21.3(3)	10.6(0)
Cr	13.6(2)	13.8(2)	14.1(8)	11.1(1)	16.6(6)	18.0(6)	17.3(2)	1.6(5)	17.6(0)	16.0(6)	29.9(3)	6.3(2)
Cu	-	-	-	-	16.9(4)	11.1(9)	16.2(7)	75.7(4)	8.6(7)	6.9(7)	6.0(1)	51.8(6)
Fe	14.3(4)	15.1(4)	16.5(1)	17.7(1)	18.5(1)	20.1(4)	20.2(3)	2.4(8)	17.8(4)	16.8(9)	23.2(5)	8.6(1)
Ni	12.8(9)	15.7(7)	19.9(9)	19.4(5)	17.5(2)	17.6(8)	18.2(6)	10.6(5)	15.8(1)	15.7(1)	14.6(3)	13.0(4)
Sc	-	-	0.4(2)	17.0(2)	-	-	0.2(2)	3.4(1)	-	-	0.1(4)	0.7(5)

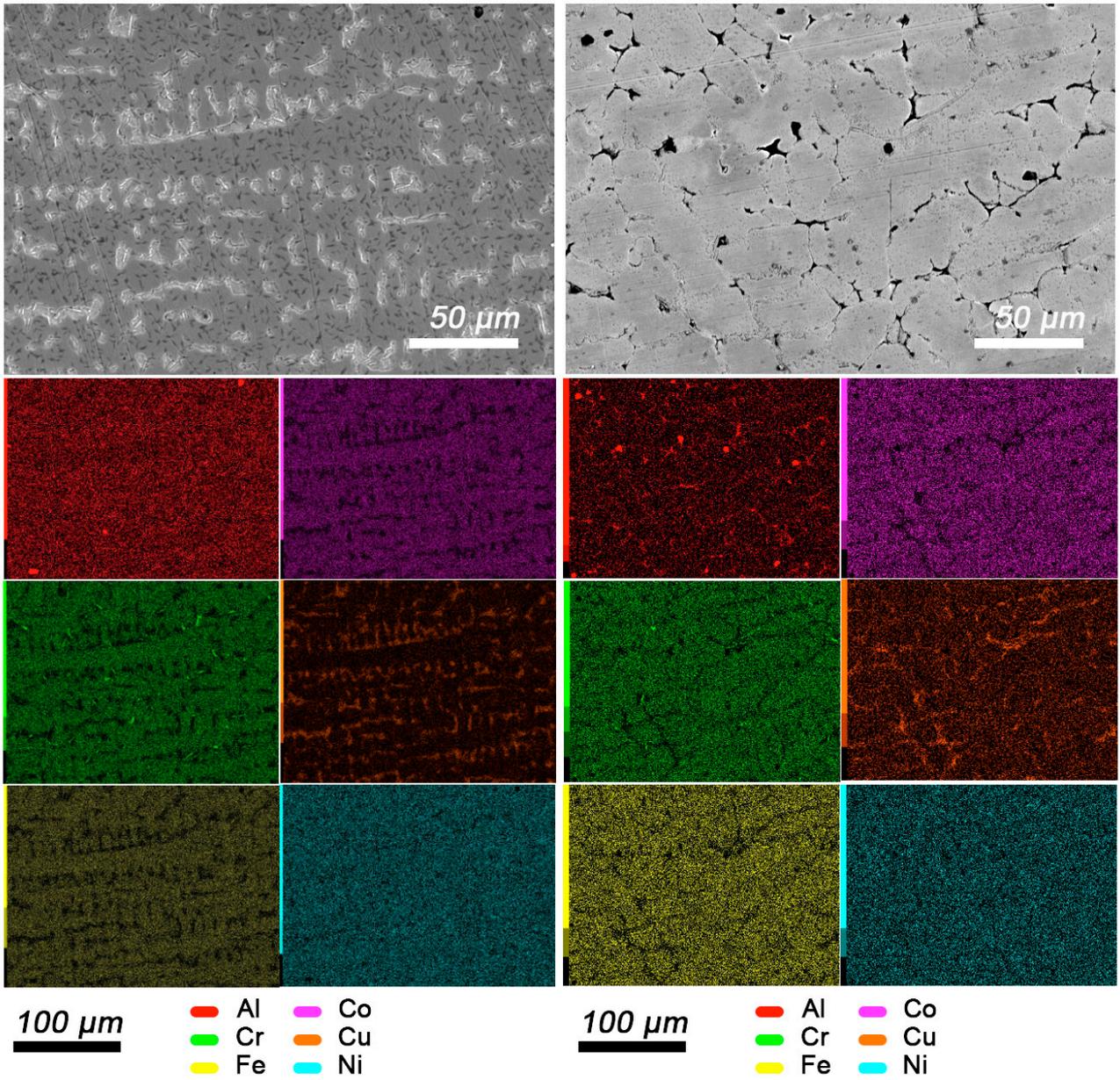
Element distribution of the as-cast and annealed alloys according to EDX maps

a.  $\text{Al}_2\text{CoCrFeNi}$  as cast

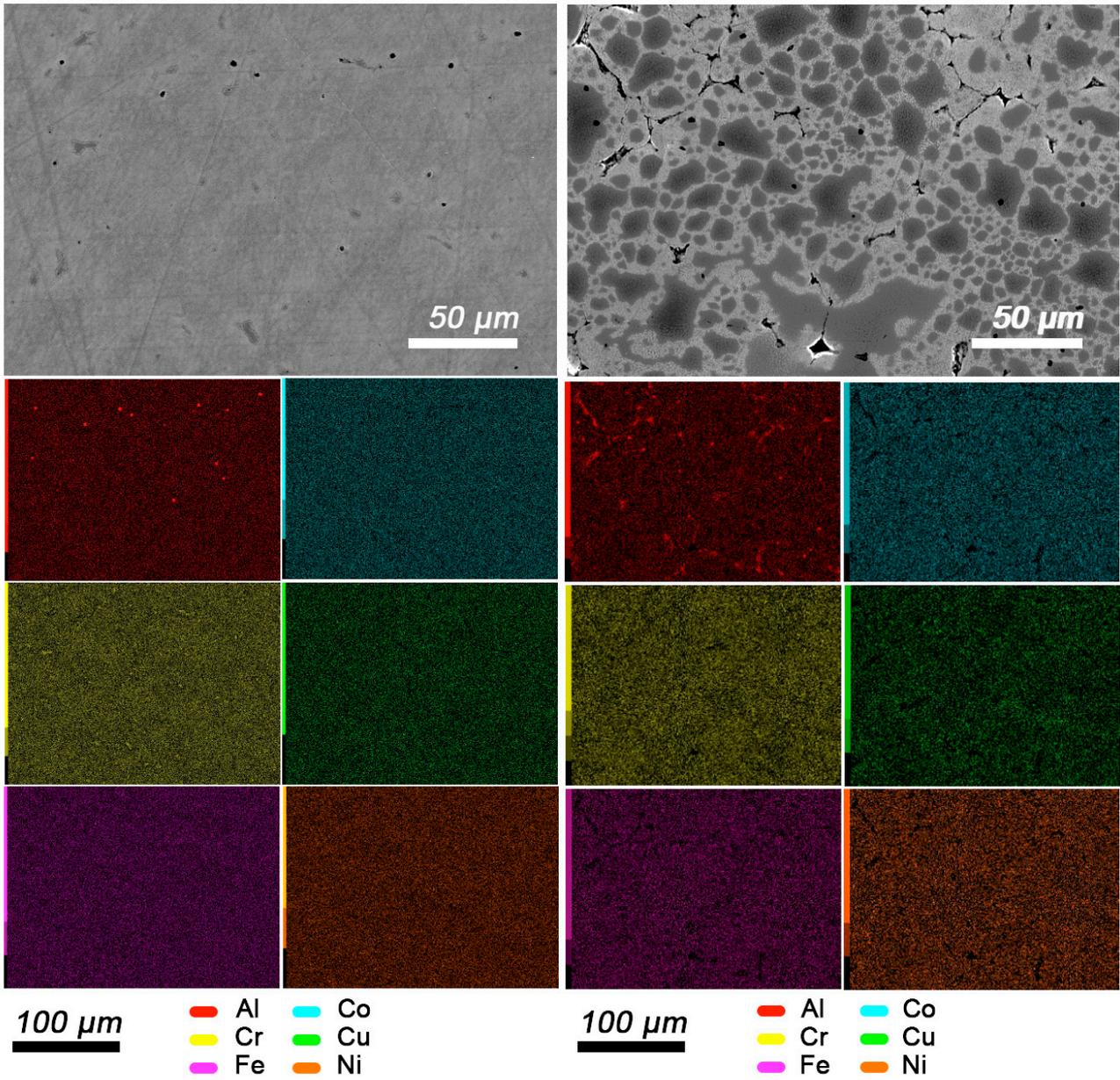
b.  $\text{Al}_2\text{CoCrFeNi}$  annealed



**Figure S1.** BSE images and element distribution of as cast and annealed  $\text{Al}_2\text{CoCrFeNi}$  samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Fe, Ni.

a. Al<sub>0.5</sub>CoCrCuFeNi as castb. Al<sub>0.5</sub>CoCrCuFeNi annealed

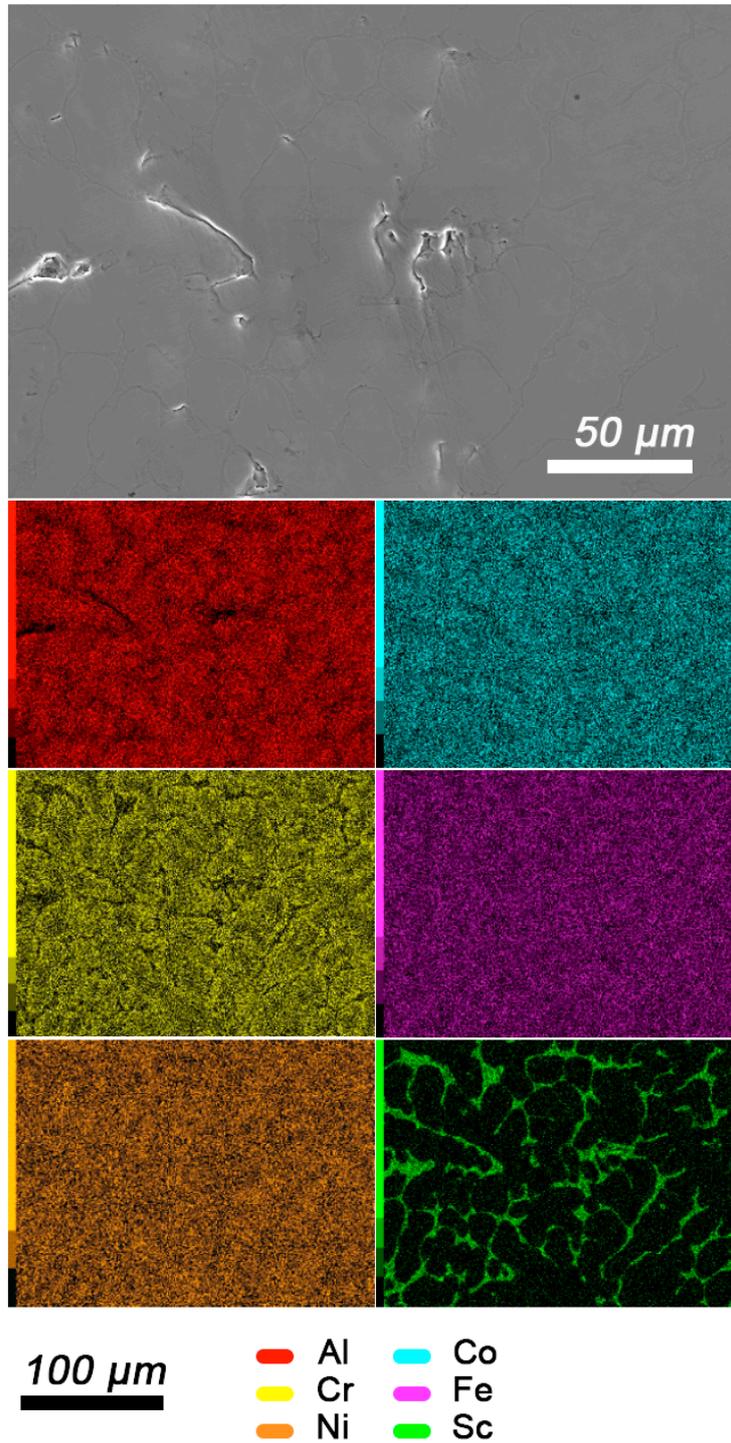
**Figure S2.** BSE images and element distribution of as cast and annealed Al<sub>0.5</sub>CoCrCuFeNi samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni.

a. AlCoCrCu<sub>0.5</sub>FeNi as castb. AlCoCrCu<sub>0.5</sub>FeNi annealed

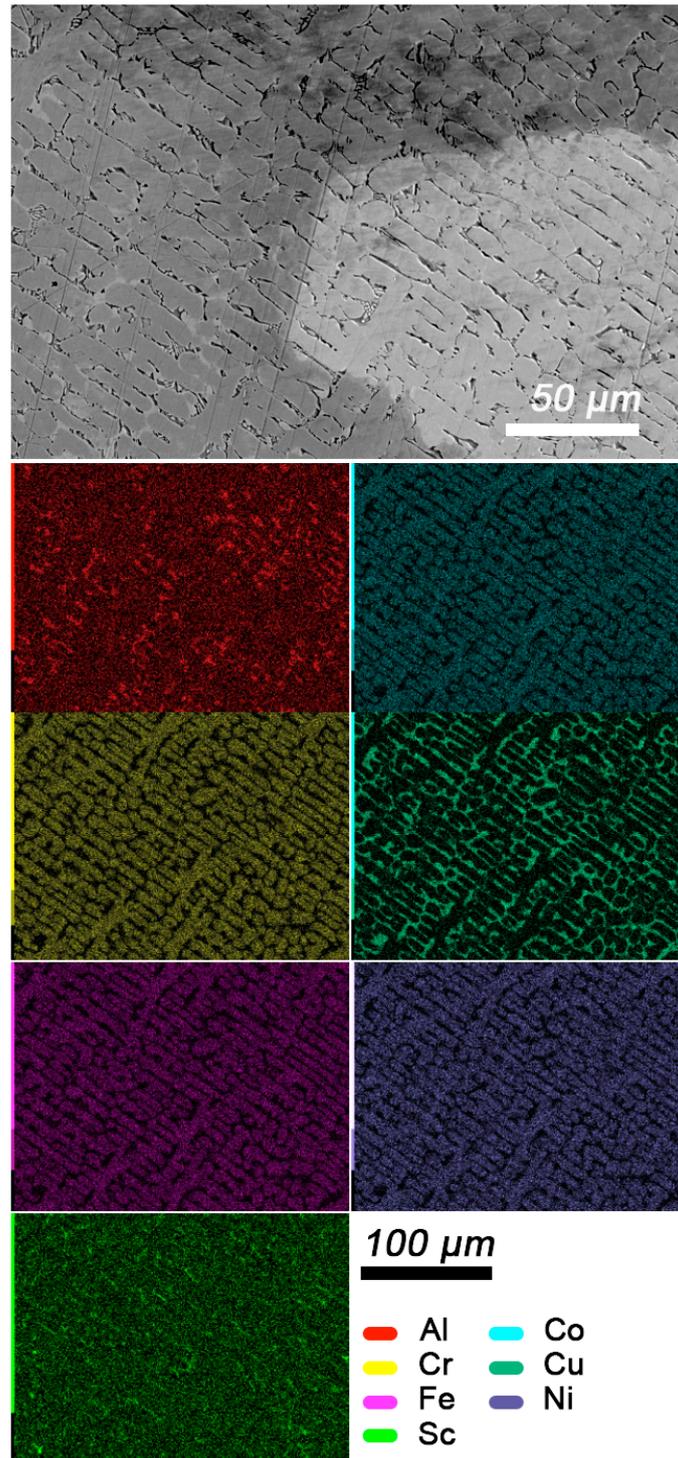
**Figure S3.** BSE images and element distribution of as cast and annealed AlCoCrCu<sub>0.5</sub>FeNi samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni.

Element distribution of the as-cast Sc-containing alloys according to EDX maps

$\text{Al}_2\text{CoCrFeNi} + 3 \text{ wt.}\% \text{ Sc}$  (as cast)

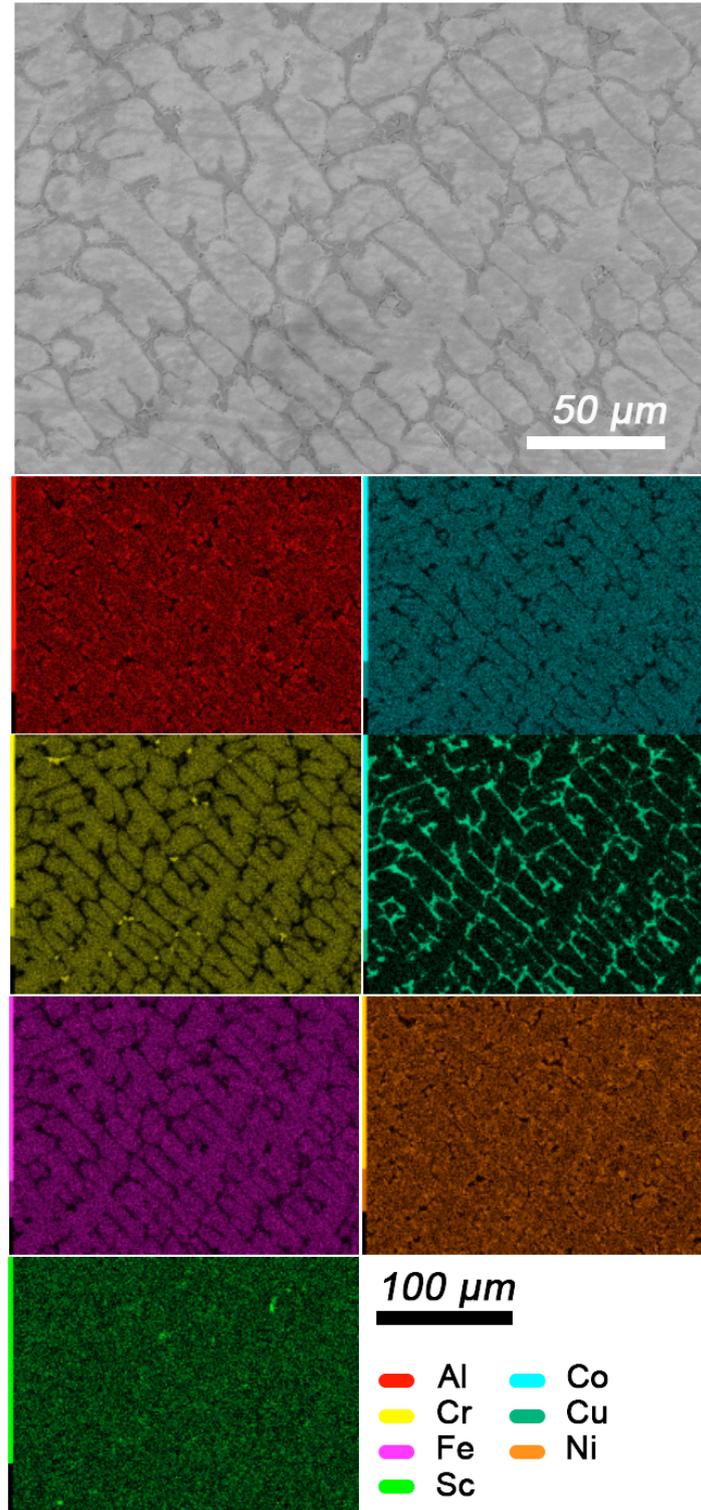


**Figure S4.** BSE image and element distribution of as cast  $\text{Al}_2\text{CoCrFeNi} + 3\text{wt.}\%\text{Sc}$  samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Fe, Ni and Sc.

$\text{Al}_{0.5}\text{CoCrCuFeNi} + 3 \text{ wt. \% Sc}$  (as cast)

**Figure S5.** BSE image and element distribution of as cast  $\text{Al}_{0.5}\text{CoCrCuFeNi} + 3\text{wt.\%Sc}$  samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni and Sc.

AlCoCrCu<sub>0.5</sub>FeNi + 3 wt.% Sc (as cast)



**Figure S6.** BSE image and element distribution of as cast AlCoCrCu<sub>0.5</sub>FeNi +3wt.%Sc samples according to EDX. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni and Sc.

### Mechanical properties: disk-punch test

Applied force was plotted against disk's displacement. To normalize the disks for the standard 0.5 mm thickness, the following equation(s) were used:

**Ultimate tensile strength for brittle materials [MPa = Nmm<sup>-2</sup>] [1]**

$$Cl = A - (D + 2t) = 8 - (4 + 2t)$$

$$UTS = \frac{F_m}{t(0.14D - 0.82Cl + 2.17u_m + 0.6)}$$

Where  $F_m$  is the maximum load during PT,  $t$  is the disk thickness in mm,  $D$  is the punch diameter (4 mm),  $Cl$  is the die clearance in mm and  $u_m$  is the displacement at failure. In the first equation,  $A$  is the diameter of the lower die (8 mm).

**Punch test results obtained after normalizing thickness to 0.5mm: [2]**

The inflexion point is a constant in the following equations.

For  $P_{test} < P_{inflexion}$

$$P_{0.5} = 0.5^2 \left( \frac{P_{test}}{t^2} \right)$$

For  $P_{test} > P_{inflexion}$

$$P_{0.5} = 0.5 \left( \frac{P_{test}}{t} \right) + 0.5 P_{inflexion} \left( \frac{0.5 - t}{t^2} \right)$$

Ultimate tensile strength [MPa = Nmm<sup>-2</sup>]

$$UTS = \frac{0.4964 F_m}{u_m h_o} - 94.146$$

Yield stress

$$YS = \frac{0.4454 F_e}{h_o^2} + 86.866$$

Where  $F_m$  is the maximum load during PT,  $u_m$  is the displacement related to the maximum load  $F_m$ ,  $h_o$  is the normalized thickness (0.5mm) and  $F_e$  is the load illustrating the conversion between linearity and yield zone (intersection between zone 1 and 2). [3]

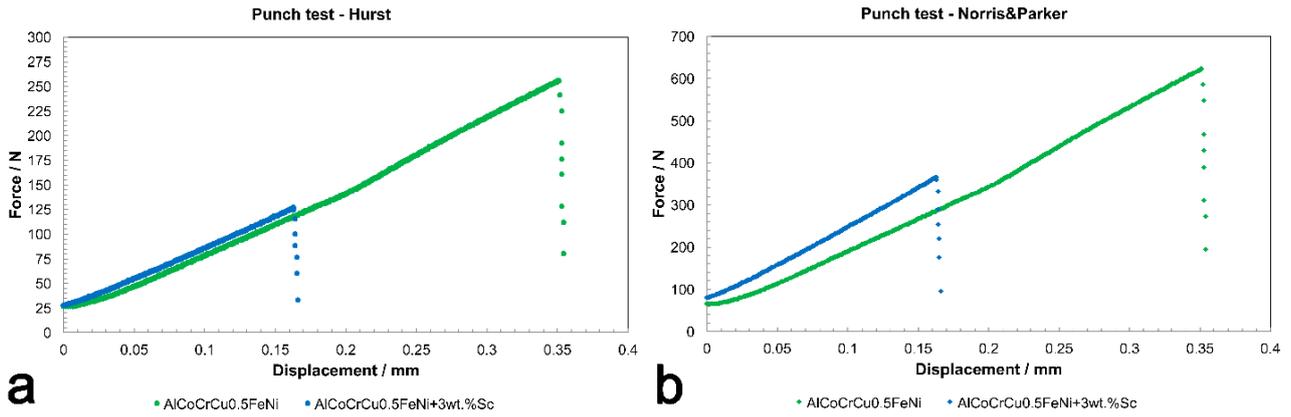
Fracture stress for brittle materials

$$\sigma_f = 130 \frac{F_m}{t^2} - 320$$

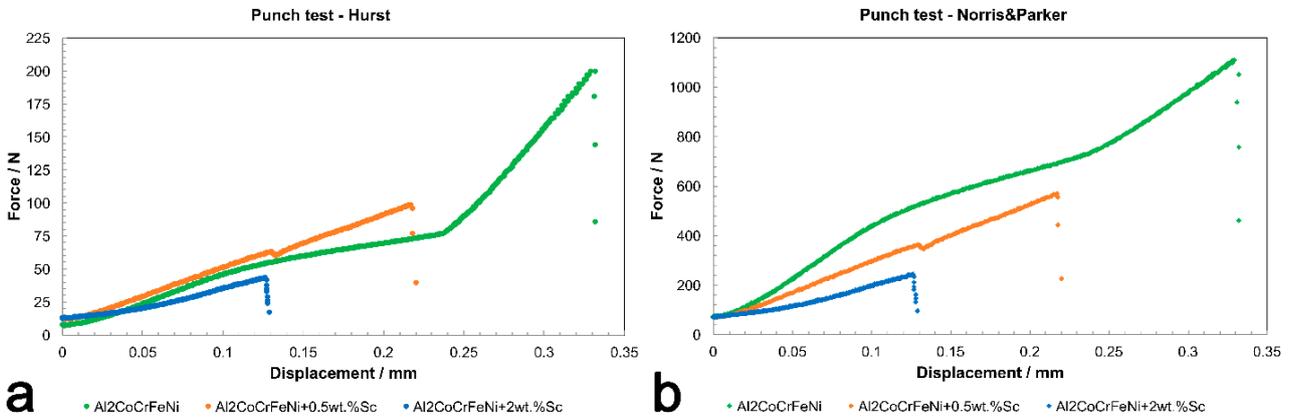
Fracture toughness for brittle materials

$$K_{IC} = 0.07(\sigma_f)^{2/3}$$

The units of KIC are MPa,  $F_m$  is in N and  $t$  is the initial thickness in mm. [4]

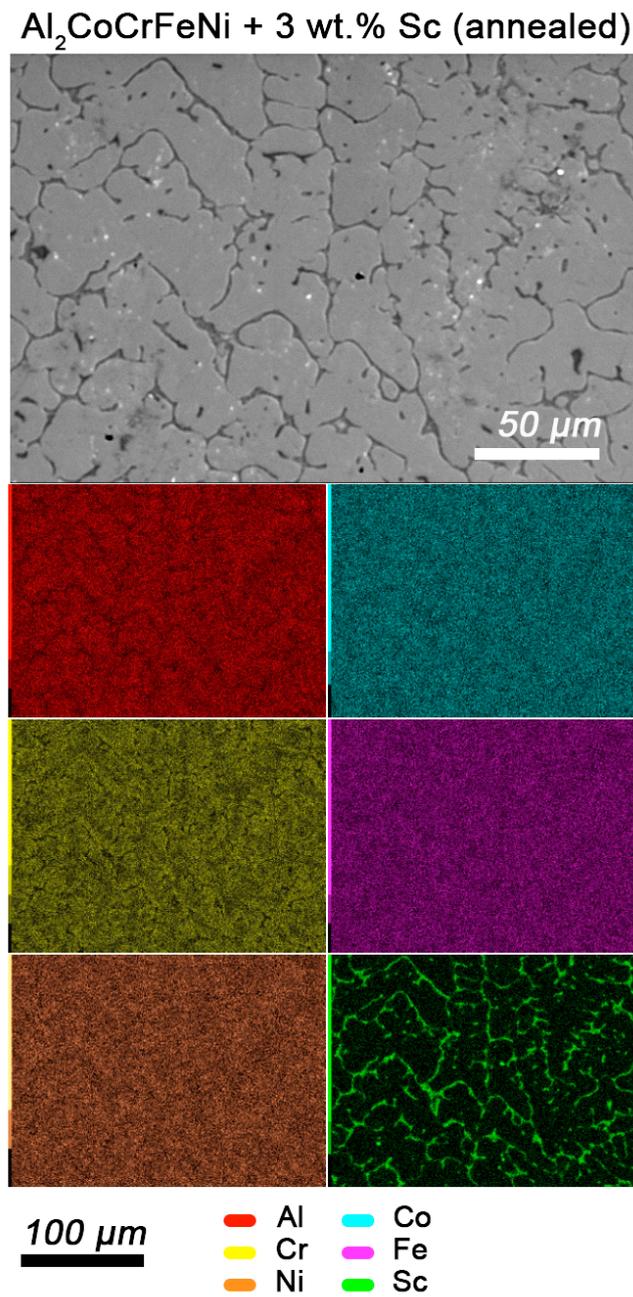


**Figure S7.** Disk punch test for the AlCoCrCu<sub>0.5</sub>FeNi HEA with 0 and 3wt.% Sc, data elaborated according to the equations reported by Norris and Parker (*right*) and Hurst (*left*) [1], [3].



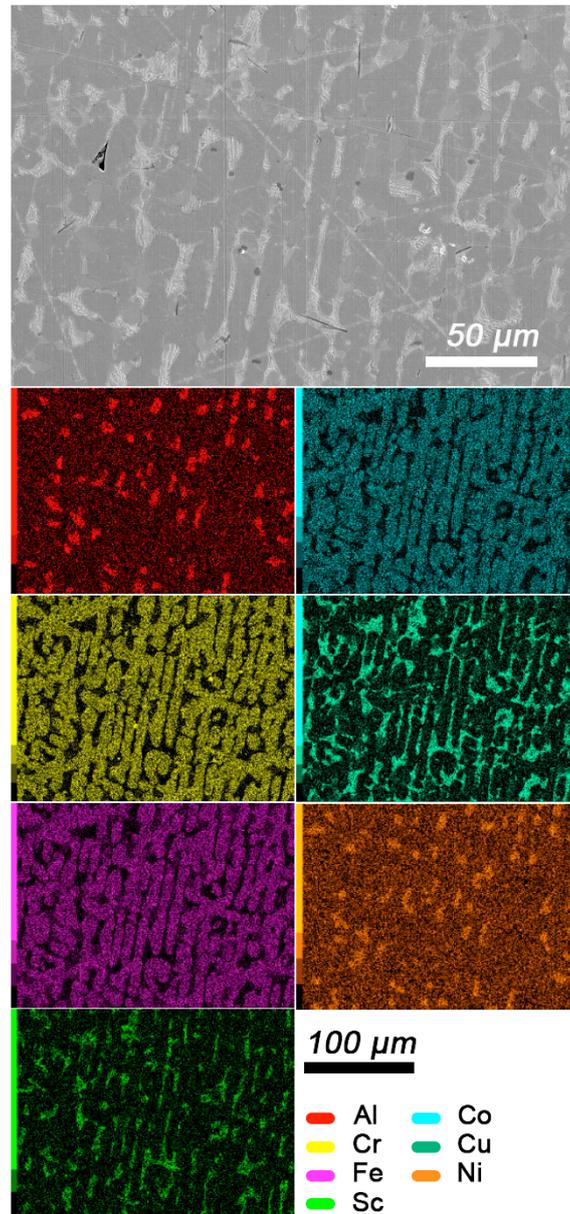
**Figure S8.** Disk punch test for the Al<sub>2</sub>CoCrFeNi alloy with 0, 0.5 and 2wt.% Sc, data elaborated according to the equations reported by Hurst (*left*) and Norris and Parker (*right*) [1], [3].

## Element distribution of the annealed alloys according to EDX maps



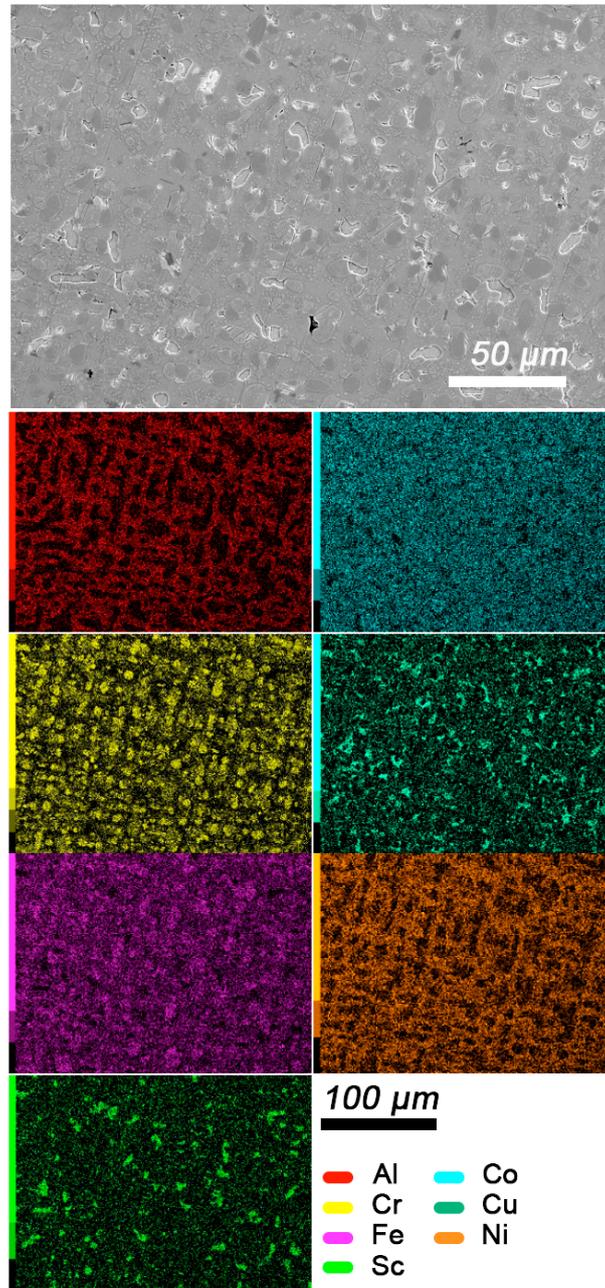
**Figure S9.** BSE image and element distribution of  $\text{Al}_2\text{CoCrFeNi} + 3 \text{ wt.}\% \text{ Sc}$  samples after annealing at  $900^\circ\text{C}$ , 12h. Data from EDX maps. From top to bottom and left to right, elements are: Al, Co, Cr, Fe, Ni and Sc.

$\text{Al}_{0.5}\text{CoCrCuFeNi} + 3 \text{ wt.}\% \text{ Sc}$  (annealed)



**Figure S10.** BSE image and element distribution in  $\text{Al}_{0.5}\text{CoCrCuFeNi} + 3\text{wt.}\%\text{Sc}$  samples after annealing at 930°C, 6h, respectively. Data from EDX maps. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni and Sc.

AlCoCrCu<sub>0.5</sub>FeNi + 3 wt.% Sc (annealed)

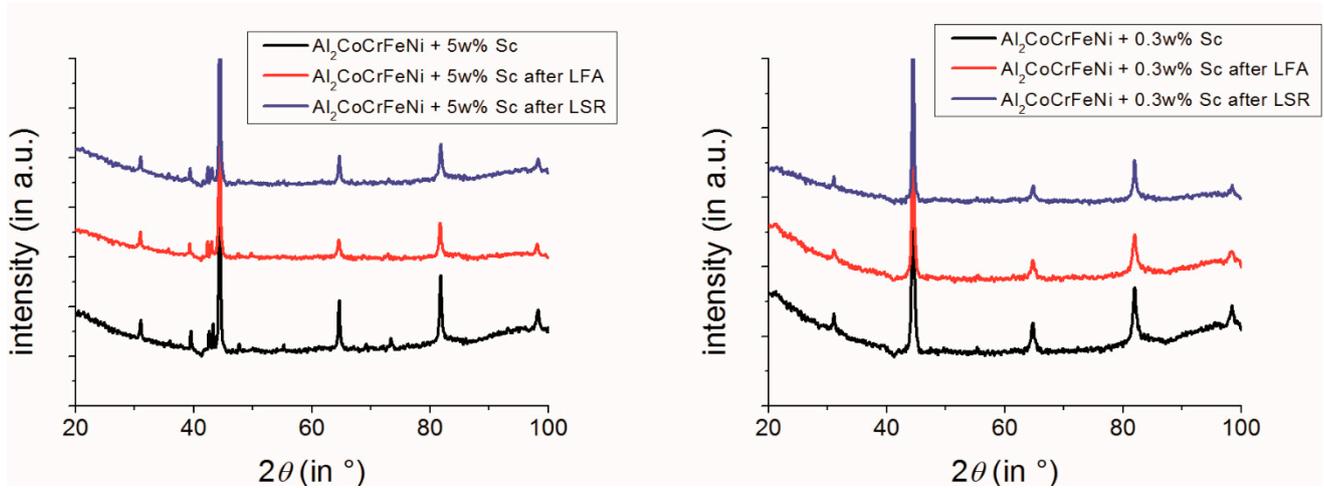


**Figure S11.** BSE image and element distribution of AlCoCrCu<sub>0.5</sub>FeNi +3wt.%Sc samples after annealing at 930°C, 6h, respectively. Data from EDX maps. From top to bottom and left to right, elements are: Al, Co, Cr, Cu, Fe, Ni and Sc.

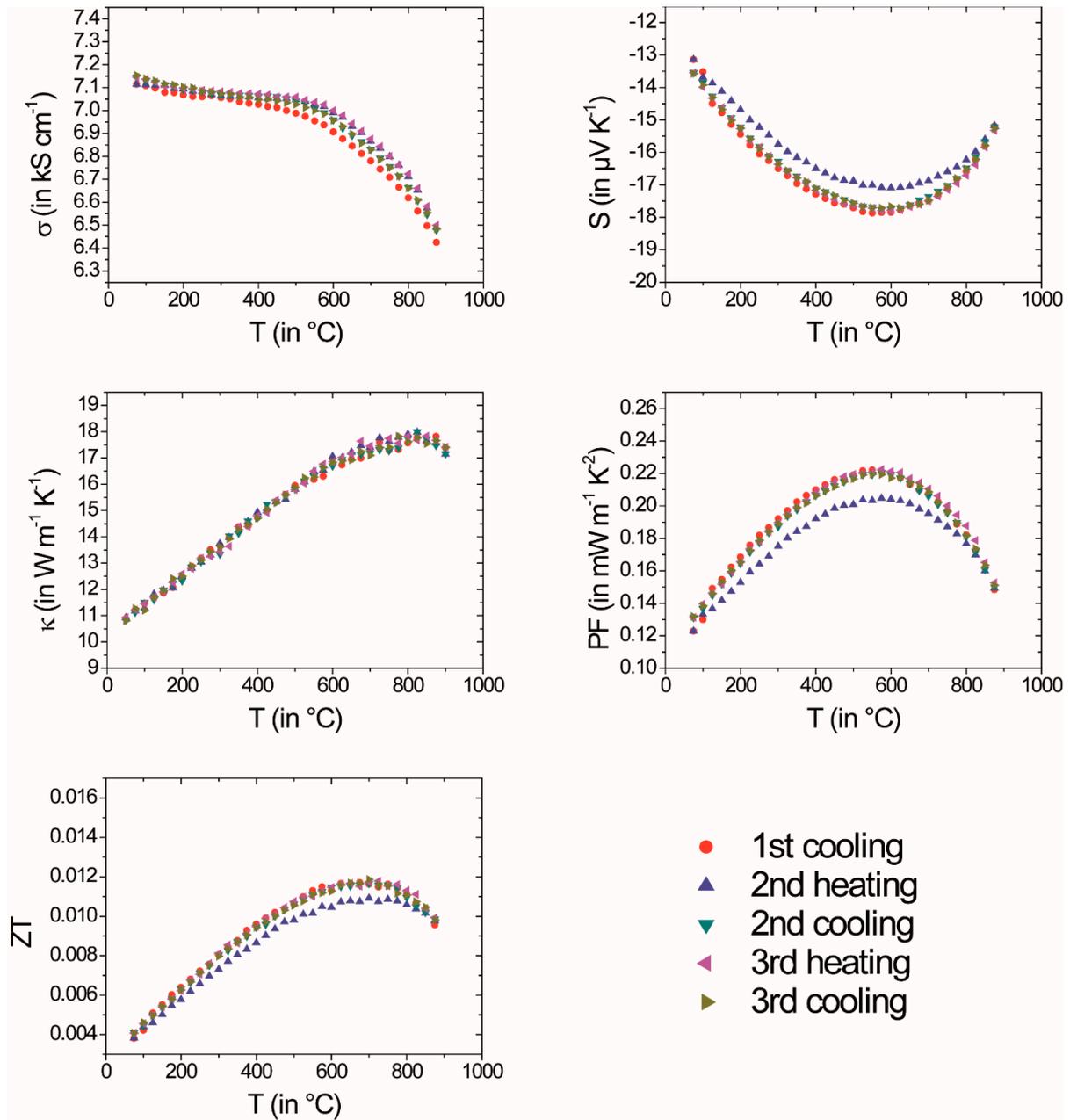
## Electrical and thermal transport measurements

**Table S3.** Density and Dulong-Petit heat capacity used for the calculation of thermal conductivity.

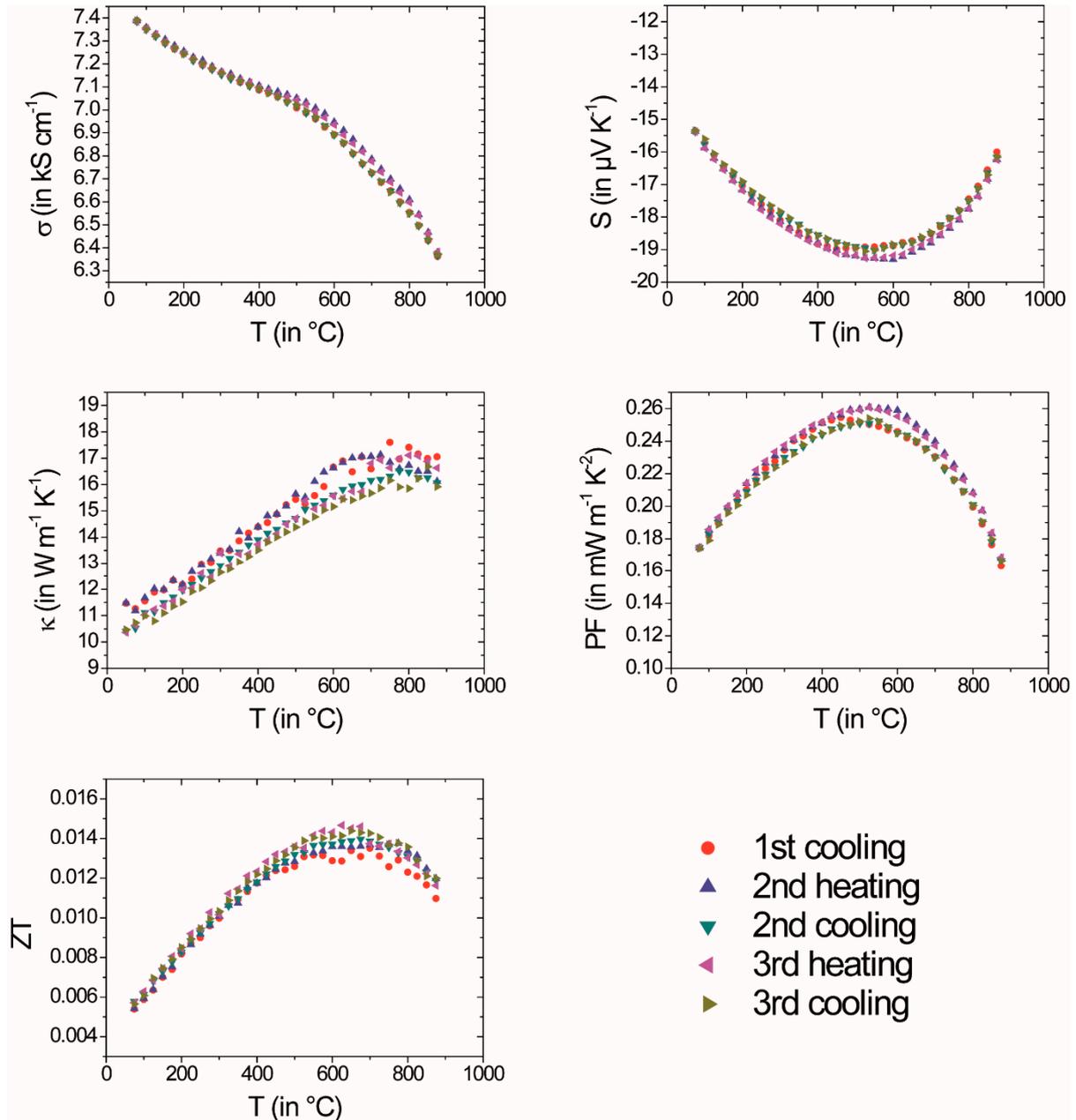
Composition	Density (in $\text{g cm}^{-3}$ )	$C_p$ (Dulong-Petit, in $\text{J g}^{-1} \text{K}^{-1}$ )
$\text{Al}_2\text{CoCrFeNi} + 5 \text{ w\% Sc}$	5.99	0.53651
$\text{Al}_2\text{CoCrFeNi} + 0.3 \text{ w\% Sc}$	6.35	0.53565



**Figure S12.** PXRD data of  $\text{Al}_2\text{CoCrFeNi} + 5 \text{ w\% Sc}$  (left) and  $\text{Al}_2\text{CoCrFeNi} + 0.3 \text{ w\% Sc}$  (right) before thermoelectric measurements (black) and after LFA (red) and LSR (blue), respectively.



**Figure S13.** Thermoelectric properties of  $\text{Al}_2\text{CrCoFeNi} + 5 \text{ w\% Sc}$  for three consecutive cycles (without first heating) up to  $875 \text{ }^\circ\text{C}$ : electrical conductivity  $\sigma$  (top, left), Seebeck coefficient  $S$  (top, right), thermal conductivity  $\kappa$  (middle, left), power factor  $\text{PF}$  (middle, right) and thermoelectric figure of merit  $\text{ZT}$  (bottom, left).



**Figure S14.** Thermoelectric properties of Al<sub>2</sub>CrCoFeNi + 0.3 w% Sc for three consecutive cycles (without first heating) up to 875 °C: electrical conductivity  $\sigma$  (top, left), Seebeck coefficient S (top, right), thermal conductivity  $\kappa$  (middle, left), power factor PF (middle, right) and thermoelectric figure of merit ZT (bottom, left).

## References

1. Norris, S.D., Parker, J.D., Deformation processes during disc bend loading, *Mat. Sci. Technol.* **1996**, *12*, 163-170.
2. Lacalle, R., Alvarez, J.A., Gutiérrez-Solana, F., Analysis of key factors for the interpretation of small punch test results, *Fatigue Fract. of Eng. Mat Struct.* **2008**, *31*, 841-849.
3. Hurst, R., The european code of practice for small punch testing: where do we go from here?, *Metall. J.* **2010**, *63*, 5-11.
4. Džugan, J., Konopik, P., Evaluation of fracture toughness properties for low carbon steel in the brittle state by small punch test technique, *Metall. J.* **2010**, *63*, 119-122.